electronics

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CHECKING AUTOPILOT OF JET DRONE MISSILE

DOTS

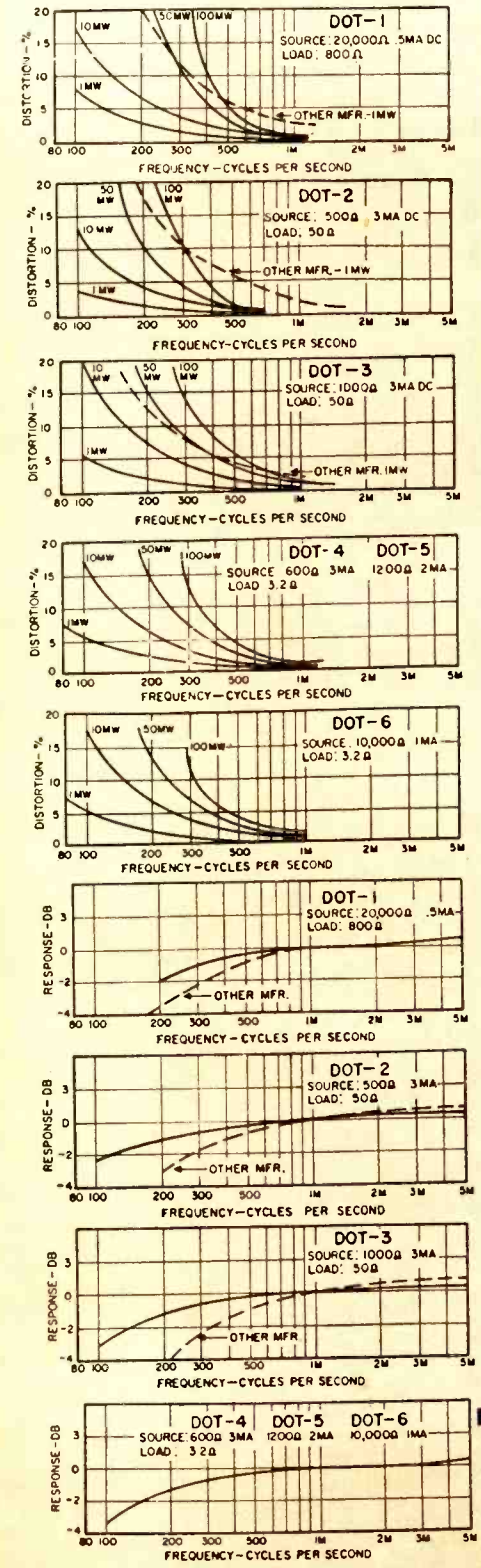
Deci-Ouncer Transformers

REVOLUTIONARY TRANSISTOR TRANSFORMERS

of unequalled power handling capacity and reliability

TYPICAL DOT PERFORMANCE CURVES

Power curves based on setting output power at 1 KC, then maintaining same input level over frequency range.



Conventional miniaturized transistor transformers have inherently poor electrical characteristics, perform with insufficient reliability and are woefully inadequate for many applications. The radical design of the new UTC DOT transistor transformers** provides unprecedented power handling capacity and reliability, coupled with extremely small size. Twenty-two stock types cover virtually every transistor application. Special types can be made to order.

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DOT-1 has 850 ohm pri. resistance, 125 ohm sec.; other mfr. approx. 1200 and 200.

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DOT units are hermetic sealed compared to other mfr. open structures.

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Other variations available.

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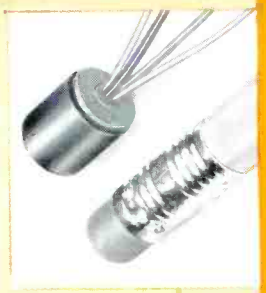

DOT CASE

Diameter . . . . . 5/16"
Length . . . . . 13/32"
Weight . . . . . 1/10 oz.

Type No.	Application	Level Mw.	Pri. Imp.	D.C. Ma.‡ in Pri.	Pri. Res.	Sec. Imp.
DOT-1	Interstage	50	20,000 30,000	.5 .5	850	800 1200
DOT-2	Output	100	500 600	3 3	60	50 60
DOT-3	Output	100	1000 1200	3 3	115	50 60
DOT-4	Output	100	600	3	60	3.2
DOT-5	Output	100	1200	2	115	3.2
DOT-6	Output	100	10,000	1	1000	3.2
DOT-7	Input	25	200,000	0	8500 630	1000
DOT-8	Reactor 3.5 Hys. @ 2 Ma. DC					
DOT-9	Output or driver	100	10,000 12,500	1 1	930	500 CT 600 CT
DOT-10	Driver	100	10,000 12,500	1 1	930	1200 CT 1500 CT
DOT-11	Driver	100	10,000 12,500	1 1	930	2000 CT 2500 CT
DOT-12	Single or PP output	500	150 CT 200 CT	10 10	11	12 16
DOT-13	Single or PP output	500	300 CT 400 CT	7 7	20	12 16
DOT-14	Single or PP output	500	600 CT 800 CT	5 5	43	12 16
DOT-15	Single or PP output	500	800 CT 1070 CT	4 4	51	12 16
DOT-16	Single or PP output	500	1000 CT 1330 CT	3.5 3.5	71	12 16
DOT-17	Single or PP output	500	1500 CT 2000 CT	3 3	108	12 16
DOT-18	Single or PP output	500	7500 CT 10,000 CT	1 1	505	12 16
DOT-19	Output to line	500	300 CT	7	19	600
DOT-20	Output or matching to line	500	500 CT	5.5	31	600
DOT-21	Output to line	500	900 CT	4	53	600
DOT-22	Output to line	500	1500 CT	3	86	600

‡DCMA shown is for single ended useage (under 5% distortion—100MW—1KC) . . . for push pull, DCMA can be any balanced value taken by .5W transistors (under 5% distortion—500MW—1KC)

*DOT units have been designed for transistor applications only . . . not for vacuum tube service **Pats. Pending

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electronics

MARCH 1 • 1957

A McGRAW-HILL PUBLICATION

CHECKING AUTOPILOT OF JET DRONE MISSILE—Technicians work on autopilot tray assembly of Ryan Firebee turbojet pilotless plane. Drone is capable of serving as 600-mph ground-controlled target for guided missiles or as missile itself (see p 182). Photo by David A. Gossett.....COVER

FEATURES

CONTINUED ON NEXT PAGE

contents

continued

SHOP

▶**DATA HANDLING** . . . Statistics on some segments of the industry are indeed difficult to obtain, for various commercial reasons. Most companies are cooperative, and we are truly thankful.

To obtain some material for this month's *Industry Report*, assistant editor Arnold long-distanced a dozen companies. Most supplied figures immediately on the phone.

One made bingo in its cooperation, however. It telegraphed the reply, six pages of business statistics!

▶**GRACIOUS** . . . Occasionally an author is in a position where he cannot accept a check we have sent him in payment for a manuscript.

Recently we noted that one author, R. R. Unterberger of California Research Corp., LaHabra, California, endorsed his check over to Whittier College, to further its liberal arts educational program.

▶**BRAIN FOOD** . . . Readers in certain parts of the world have problems peculiar to the climate; many of us in temperate zones do not fully appreciate them.

The following suggestion has been received from Frank Watlington, chief electronics engineer at a geophysical field station of Columbia University.

"Of interest to your readers may be the following. We have had a great deal of trouble in Bermuda due to the fact that cockroaches find the backs of your magazines

electronics

MARCH 1, 1957 Vol. 30, No. 3

Member ABC and ABP

TALK

excellent feeding material, and sooner or later they consume it to a point where the cover falls off.

"We have been able to discourage them by spraying the backs with a clear acrylic protective coating."

► **WAS OUR SECRET** . . . Letters from a company making high-fidelity equipment have a pair of musical notes typed right at the beginning of each paragraph. The effect is quite pleasing and serves to remind the recipients of the company's products.

For many months ELECTRONICS has used an intentionally ambiguous device for a similar purpose. It's the integration sign that starts the word SUMMARY up near the top of each feature article. We would have preferred to use a summation sign but shuddered at the appearance of ΣUMMARY. So did the print shop.

Even the integration sign we use is not on a typesetting machine; it is made as a cut which, in the mechanics of the printing business, meets the type only in one of the final operations. For many months the printer's proofreader sent galleys to us questioning UMMARY.

► **DATA STORAGE** . . . Perennial problem for readers (and editors) is that of keeping copies of ELECTRONICS and other periodicals out of normal traffic patterns around the house. A centralized storage system that also provides ready access for quick-look purposes has been built by feature editor Markus for his cellar. Shelf space totals 96 feet.

ELECTRONICS stacks nicely in shelving spaced for maximum utilization of space

Even this isn't enough for orderly storage of the technical material that accumulates for reference. As a result, the one-of-each items get piled on the top shelves and those at the lower rear. Only the guy who put them there can find what he wants, provided no one else tries to housekeep the mess.

Construction hints: No. 2 pine, with one coat rubbed-effect varnish. Shelves run full 16-ft length. Risers are 12 inches, lightly nailed between shelves since weight of magazines holds them in position. Back is quarter-inch plywood.

Assembled upright in middle of room, back sheets were nailed on, then entire unit slid into position against wall and top trim added. Height, 7 feet. A dehumidifier was found essential.

Published three times a month, with an additional issue in June, by McGraw-Hill Publishing Company, Inc., James H. McGraw (1860-1948), Founder. **Executive, Editorial and Advertising Offices: McGraw-Hill Building, 330 W. 42 St., New York 36, N. Y.** Longacre 4-3000. Publication Office, 99-129 North Broadway, Albany 1, N. Y. Donald C. McGraw, President; Joseph A. Gerardi, Executive Vice President and Treasurer; John J. Cooke, Secretary; Nelson Bond, Executive Vice President. Publications Division; Ralph B. Smith, Vice President and Editorial Director; Joseph H. Allen, Vice President and Director of Advertising Sales; A. R. Venezian, Vice President and Circulation Coordinator.

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BRANCH OFFICES: 520 North Michigan Avenue, Chicago 11, Ill.; 68 Post Street, San Francisco 4; McGraw-Hill House, London E. C. 4; National Press Bldg., Washington, D. C. 4; Architects Bldg. 17th & Sansom Sts., Philadelphia 3; 1510 Hanna Bldg. Cleveland 15; 856 Penobscot Bldg., Detroit 26; 3615 Olive St., St. Louis 8; 350 Park Square Bldg., Boston 16; 1321 Rhodes Hagerty Bldg., Atlanta 3, Ga.; 1125 West Sixth St., Los Angeles 17; 919 Oliver Building, Pittsburgh 23. ELECTRONICS is indexed regularly in The Engineering Index.

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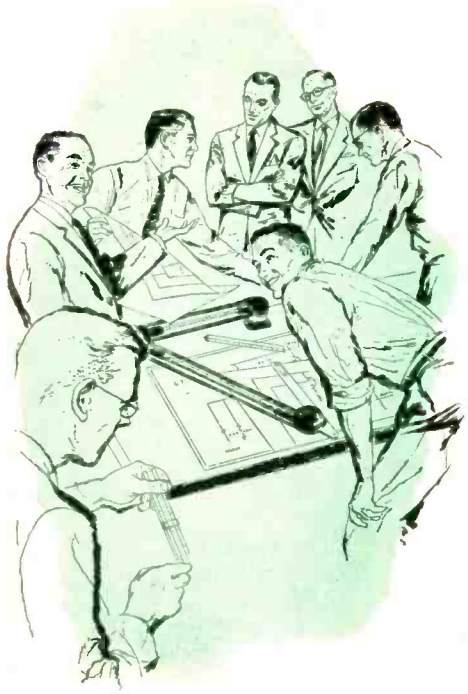

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Distortion	3% max.
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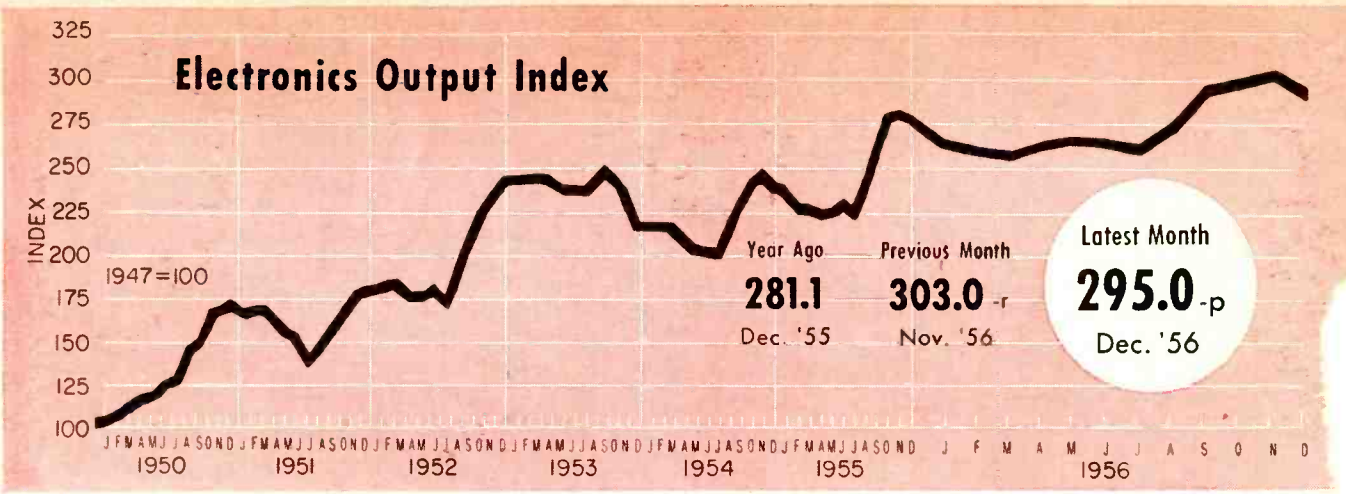


FIGURES OF THE MONTH

RECEIVER PRODUCTION

(Source: RETMA)	Latest Month	Previous Month	Year Ago
	Dec. '56	Nov. '56	Dec. '55
Television sets, total	626,984	679,993	604,626
With UHF	104,205	116,183	89,606
Color sets	nr	nr	nr
Radio sets, total	1,715,209	1,381,831	1,786,330
With F-M	513	2,326	40,305
Auto sets	840,359	609,139	864,261

RECEIVER SALES

(Source: RETMA)	Dec. '56	Nov. '56	Dec. '55
Television sets, units	957,193	560,391	933,467
Radio sets (except auto)	1,651,950	689,409	1,388,801

RECEIVING TUBE SALES

(Source: RETMA)	Dec. '56	Nov. '56	Dec. '55
Receiv. tubes, total units	34,340,000	39,489,000	38,049,000
Receiv. tubes, value	$29,111,000	$31,476,000	$30,673,000
Picture tubes, total units	795,476	957,765	881,465
Picture tubes, value	$13,423,157	$16,014,839	$17,533,105

INDUSTRIAL TUBE SALES

(Source: NEMA)	Quarterly Figures: Latest Quarter	Previous Quarter	Year Ago
	3rd '56	2nd '56	3rd '55
Vacuum	$8,895,012	$7,680,250	$9,027,845
Gas or vapor	$2,936,765	$2,983,488	$3,438,835
Magnetrons and velocity modulation tubes	$14,948,477	$16,254,025	$10,998,967
Gaps and T/R boxes	$1,196,369	$1,238,469	$1,421,138

MILITARY PROCUREMENT

(Source: Defense Dept.)	3rd '56	2nd '56	3rd '55
Army	$23,107,000	$44,882,000	$19,477,000
Navy	$22,273,000	$34,132,000	$20,054,000
Air Force	$84,952,000	$128,781,000	$128,023,000
Total—Electronics	$130,332,000	$207,795,000	$167,554,000

BROADCAST STATIONS

(Source: FCC)	Latest Month: Jan. '57	Previous Month: Dec. '56	Year Ago: Jan. '56
TV stations on air	513	511	484
TV stations CPs—not on air	120	120	105
TV stations—new requests	62	59	26
A-M stations on air	3,014	3,008	2,834
A-M stations CPs—not on air	123	117	120
A-M stations—new requests	288	291	242
F-M stations on air	527	530	538
F-M stations CPs—not on air	24	24	16
F-M stations—new requests	8	5	3

COMMUNICATION AUTHORIZATIONS

(Source: FCC)	Dec. '56	Nov. '56	Dec. '55
Aeronautical	54,231	53,192	44,836
Marine	60,390	60,153	53,950
Police, fire, etc.	22,066	21,829	19,885
Industrial	33,046	32,788	27,269
Land transportation	9,346	9,287	8,481
Amateur	156,203	154,839	142,819
Citizens radio	22,463	22,036	14,426
Disaster	330	330	321
Experimental	764	775	674
Common carrier	2,585	2,559	2,093

EMPLOYMENT AND PAYROLLS

(Source: Bur. Labor Statistics)	Nov. '56	Oct. '56	Nov. '55
Prod. workers, comm. equip.	423,900-p	418,400-r	409,400
Av. wkly. earnings, comm.	$78.74-p	$78.12	$75.53
Av. wkly. earnings, radio	$74.96-p	$75.70-p	$71.81
Av. wkly. hours, comm.	40.8 -p	40.9	41.5
Av. wkly. hours, radio	40.3 -p	40.7 -r	40.8

SEMICONDUCTOR SALES ESTIMATES

	Oct. '56	Sept. '56	Aug. '56*
Transistors, Units	1,290,000	1,155,000	1,315,000

STOCK PRICE AVERAGES

(Source: Standard and Poor's)	Jan. '57	Dec. '56	Jan. '56
Radio-tv & electronics	336.3	345.2	435.6
Radio broadcasters	439.9	454.1	500.5

p—provisional r—revised nr—not reported
*1955 not available

FIGURES OF THE YEAR

TOTALS FOR THE YEAR	1956	1955	Percent Change
Television set production	7,357,029	7,756,521	— 5.2
Radio set production	13,981,800	14,894,695	— 6.1
Television set sales	6,804,756	7,421,084	— 8.3
Radio set sales (except auto)	8,332,077	6,921,384	+20.4
Receiving tube sales	464,186,000	479,802,000	— 3.3
Cathode-ray tube sales	10,987,021	10,874,234	+ 1.0

INDUSTRY REPORT

Computers Multiply In Canadian Market

Doubled sales in three years indicate bright future for all computer types

PROCESS industries as well as aircraft, electrical-electronic and chemical are responsible for the growth of the computer industry in Canada. The pulp and paper industry, primarily a Canadian market, offers several possible applications for analog computers in the fields of pH control in sulphite mills, pipe line pulsation studies as well as heat-balance studies between groundwood and paper mills.

► **Digital**—It is estimated that the next five years will see about 50 large digital computers installed in Canada. Outlook for the small and medium sized units is more optimistic with an estimated 150 units installed during the same period.

► **Analog**—Potential sales of analog units are difficult to estimate owing to the number of unexplored applications that exist, however it appears that the next three years should see sales of general-purpose units climb from $700,000 to $1.5 million.

► **Latest**—Most recent example of the expanding computer business is the opening of a computing center at Bells Corners, Ontario, by Computing Devices of Canada Ltd. The center contains a specially built Reac computer having a total of 96 amplifiers.

ENGINEERS of BTL hold experimental solid-state oscillator showing how . . .

New Amplifier Gains Are Forecast

Solid-state oscillator development leads to low-noise amplifier employing electron spin

SUCCESSFUL operation of a new solid-state microwave oscillator putting out 20 microwatts at 9,000 mc has been announced by Bell Labs where a crystal containing a small amount of paramagnetic salt was employed.

Ordinary electronic oscillators depend upon the motion of charged particles at high temperatures. Since the new device operates with electron spin in a paramagnetic crystal, it should have, according to theory, very low inherent noise.

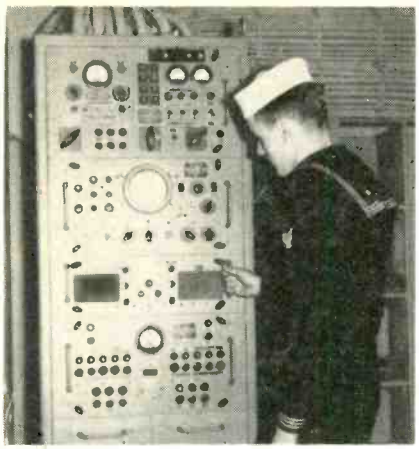
► **Equipment**—Operating in a magnetic field, the solid-state oscillator comprises a waveguide cavity immersed in liquid helium. Energy at 17,500 kc is fed into the cavity and radiation at 9,000 mc is taken out by means of a strip waveguide.

Concurrent with the Bell Labs' announcement was one from Massachusetts Institute of Technology in which a new amplifying device called the Versitron was postulated. Uses of the amplifier to be operated at low temperature include differentiating between sources with slightly unequal temperatures and located some distance away.

More Picket Ships Join Radar Net

ELECTRONIC gear on the recently commissioned radar picket ship *USS Outpost*, YAGR-10, is valued at more than $3 million, including installation costs.

The *Outpost* is the tenth converted Liberty ship to join the sea-going portions of the horseshoe-shaped radar warning net



Height-finding radar aboard USS Outpost

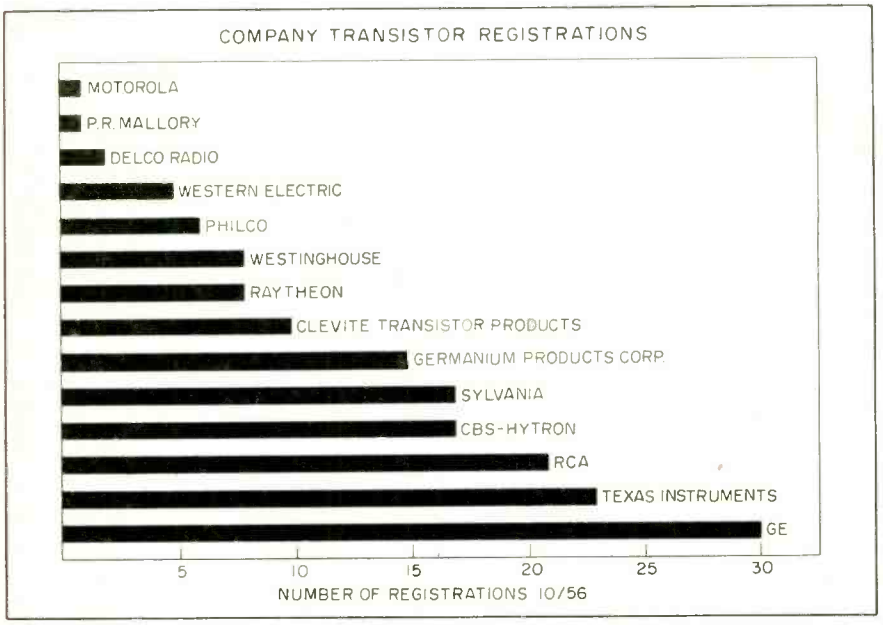
that extends roughly from Santa Barbara, Calif. through Alaska and northern Canada, down to Savannah, Ga.

▶**Firms** — The ship's electronics officer estimates that electronic equipment on board was supplied by from 50 to 100 companies. Radar equipment includes: GE's AN/SPS-8A: Raytheon's surface search, AN/SPS-5; RCA's air search, AN/SPS-17; and Westinghouse air-search radar.

Bendix, Federal Telephone and Radio and others supplied communications equipment.

▶**DER** — Beyond the ten YAGR ships now commissioned, the Continental Air Defense Command's sea surveillance includes converted destroyers known as DER's. Ships will patrol offshore and in midocean. Plans call for several hundred new radar sites which will include the chain of radar sea platforms extending 125 miles off the East Coast from Norfolk to Newfoundland.

Transistor Registrations Double



Number of types registered reached 164 in 1956, up 89 over the 1955 grand total

SUMMARY of all transistors registered through October 1, 1956 with the Joint Electron Tube Engineering Council indicates that as many of the devices were registered in the first nine months of 1956 as in all previous years combined. The number of registrations now totals over 164. Five companies, GE, Texas Instrument, RCA, Sylvania and CBS-Hytron account for well over half of the registrations. Nine other companies had units registered.

▶**Production**—Registration of a transistor type with JETEC does not mean that the type is in actual production. But, according to RETMA, it is a good indication that production is underway or will be shortly.

▶**Types**—Over 90 of the registrations were for *pnp* transistors and 55 were *npn* types. The remainder were point-contact types. Although specific applications were not disclosed for many of the units, of those that were given hearing-aid applications were numerous along with switching and power output applications.

▶**Production Progress**—The upward trend in registrations is expected to continue. Sylvania estimates that its production and sales of all transistor types in 1956 were about ten times the company's 1955 totals. The firm expects its transistor output this year to be about four times the 1956 total.

▶**Volume**—The industry's production of transistors in 1957 will total 30 million units, according to another company. It estimates that potential uses which cannot now be foreseen will require from one-third to one-half of the industry's total transistor volume beginning in 1960.

The firm estimates that annual transistor production will reach over 290 million units by 1966.

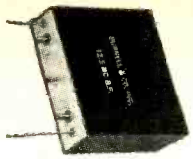
Multiplex F-M Gathers Momentum

Subcarrier programs may replace wire lines to subscribers of background music

ESTIMATED as a market with billings in excess of $200 million, background music is beginning seriously to consider getting its programs from studio to customer by radio rather than wire.

Two methods are available—one is temporary and the other more expensive. Until July, the Federal Communications Commission will permit operators of f-m broadcast stations to transmit programs in which announcements are accompanied by an ultrasonic, inaudible, beep. Unheard in the average receiver, the beep tone actuates controls in special subscribers' re-

(Continued on page 10)



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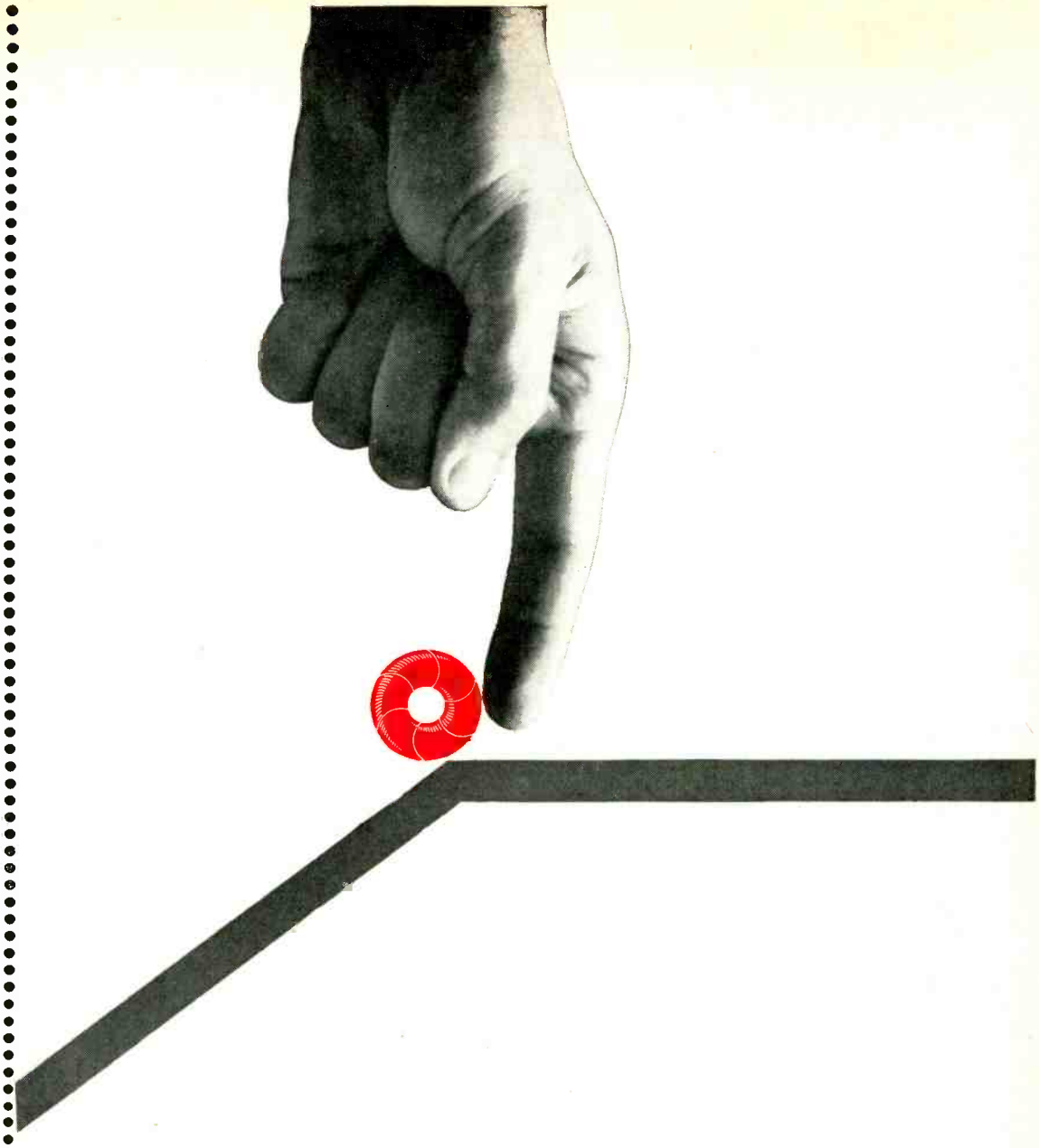

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ceivers to step up volume (to make announcements more penetrating) or to cut out the commercial announcement entirely.

▶ **Multichannel Plan**—Broadcasters may obtain a subsidiary communications authorization that permits use of one or more subcarriers—each carrying a separate program—that can be picked up by appropriate receivers. While the main channel transmits classical music for hi-fi enthusiasts, the other channels can carry paid commercial programs or furnish special background music to special subscribers.

Out of some 520 f-m stations on the air, only 77 are licensed for the special services. According to one industry authority, about 60 percent are simplex (beep tone) and the rest multiplex. However, the percentages seem to be shifting in the other direction. Probably about half of those licensed are actually multiplexing now.

▶ **Dollar Value**—Independent market research claims an equipment potential (transmitter modulators and subcarrier receivers) of $5 million over the next five years. This splits into $1 million for transmitting equipment and $4 million for receivers.

Less than half a dozen electronics manufacturers are known to be building equipment. Installations to date have been generally hand-adjusted.

Business Briefs

▶ **Higher sales** than a year ago are expected for the second quarter of 1957 by almost 66 percent of some 1,500 business men surveyed by Dun & Bradstreet. Profit margins were expected by many to be lower

▶ **Electronics** constituted at least 40 percent of Bendix Aviation's output in terms of finished products utilizing electronic circuits or controls. The firm's net sales in 1956 totaled $581.4 million compared to $567.2 million for 1955

▶ **Merger** of Beckman Instruments and Statham Labs is in the works. It will involve a stock exchange of up to 400,000 shares of Beckman for all of the Statham interests. The firm, with annual sales of $5 million, produces precision pressure transducers, accelerometers and other devices

▶ **New orders** totaling $80.9 million were booked by Lear in 1956, the largest volume in the firm's history. Backlog reached $64.7 million compared to $53.4 million in 1955. Much of the gain is attributed to expanded sales of automatic flight control and flight reference systems

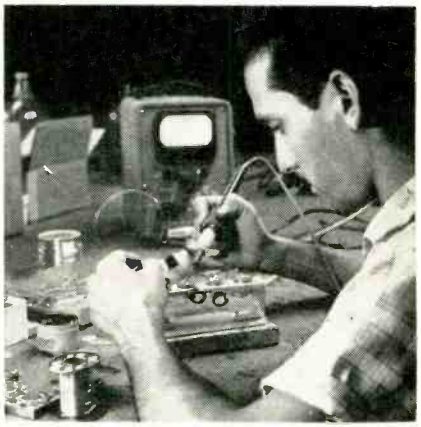
▶ **World-wide** sales exceeded $100 million in 1956 for Addressograph-Multigraph Corp., a 15-percent increase over 1955. No defense contract work was done in 1956 by either the corporation or any of its subsidiaries

Magnistors Catch On And Output Expands

Expect up to a five-fold increase in output as facilities in Puerto Rico are opened

THE magnistor, a type of saturable reactor developed by Potter Instrument about two years ago, is gaining ground fast. Today at least 10,000 of the units are in use representing a gross dollar volume of about $200,000.

Potter recently opened a new 12,500 sq ft branch plant in Lugville, Puerto Rico to manufacture the devices. By the end of 1957 30,000 to 50,000 of the components are expected to be in use.



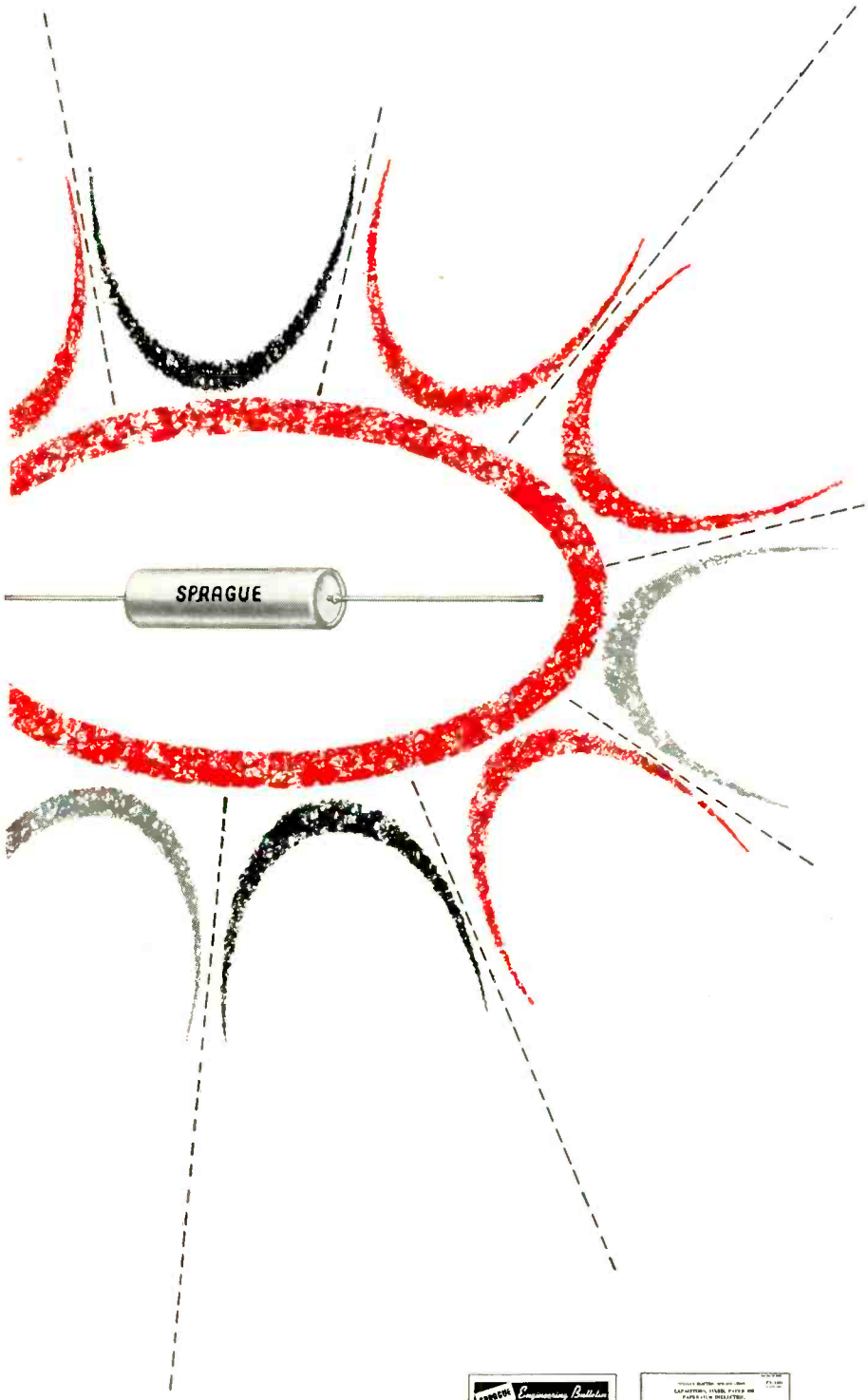
Magnistor production setup

▶ **Production**—The company set up its new magnistor plant in Puerto Rico because most coil winding machines are not delicate enough to handle the fine wire used in magnistors without breaking it. Puerto Ricans, known for their needle work and manual dexterity, do the job better and cheaper than machines. The favorable tax laws along with other economic factors also were behind the move.

The company had planned to

(Continued on page 12)

Hyrel® Q the most reliable capacitors available anywhere!

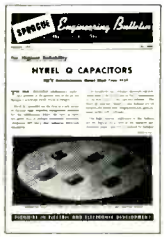


The name "Hyrel" heralds a complete new line of Sprague Capacitors conforming to the most rigorous set of capacitor specifications ever written. Techniques, materials, and processes combine to make it the most reliable paper capacitor possible within the present state of the art. After two years of exhaustive pilot runs, these high reliability units are in high volume production *now*.

In missiles, jets, warning networks, computers, controls . . . *wherever reliability is important* . . . Hyrel Q capacitors find scores of applications. A glance at Sprague Specification PV-100 tells you why. It's far above and beyond commercial or present MIL military levels . . . and it calls for outstanding performance under high *g* shock, vibration, humidity, immersion, as well as under accelerated life test. Complete facilities for making every test called for have been installed in a special plant area in which Hyrel Q capacitors are manufactured by specially selected personnel.

The first Hyrel Q capacitors—Type 195P—are subminiature metal-clad paper units hermetically sealed with *compression*-type glass-to-metal solder-seal terminals. Available in both conventional tubular and screw-neck mounting styles, all are Vitamin Q impregnated and designed for operation from −55°C to +125°C. Voltage ratings of 200, 300, 400, and 600 VDC are standard.

Complete technical information is provided in Engineering Bulletin 2900 and Specification PV-100. Both are available on letterhead request to the Technical Literature Section, Sprague Electric Company, 35 Marshall St., North Adams, Mass.



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hire 50 workers to reach its initial production goals. Workers were hired one at a time and trained in making the components. The firm found that by the time it had hired some 16 people, its production rate had been reached. Thus output per worker was three times higher than expected.

▶ **Markets**—Chief reason for the rise in magnistor sales and production is increasing applications in computers and in aircraft. One large manufacturer has built a computer that uses magnistors instead of tubes. Potter is manufacturing its flying typewriter utilizing the devices. Because prices of the units range between $18 and $25 the market is still limited. But the future outlook is bright and a drop in prices is foreseen as production grows.

▶ **Growth**—Electronics industry in Puerto Rico has grown from a few plants in 1950 to 44 at the start of 1957. Shipments to the U. S. have increased from under $1 million six years ago to a record $20 million in 1955-56. Under the islands complete freedom from Federal corporate taxes, electronics and electrical product manufacturers there earned a profit on sales of 33 percent net compared to a U. S. average of 5 percent.

Snark Finds Its Way With Gyros

Business-end of Air Force's Snark intercontinental missile which uses an inertial guidance system. In the 5,000-mile-range category, the missile has overall length of 69 feet

NINE HUNDRED pages of typing are eliminated at GE by 2,400 feet of magnetic tape as . . .

Magnetic Recording Adds Volume

Business increased about 20 percent in 1956. More foreign companies enter field

ALTHOUGH final official business statistics for the magnetic recording industry are not yet available, estimates from leading manufacturers in the field indicate that the industry scored a 20-percent gain in volume during 1956.

▶ **Volume**—An estimated 430,000 tape recorders were sold in 1956, a 20-percent increase over the 360,000 sold in 1955. This was nearly 200,000 more than the 235,000 reported sold in 1954 by Magnetic Recording Industry Association. The Census Bureau estimates that there were 274,000 tape recorders shipped in 1954 with a total value of $25.7 million or an average value per unit of about $94.

There are about 1.6 million tape recorders in use today, according to one leading manufacturer. The following breakdown shows the major markets: About 800,000 recorders are in use in the home, 160,000 in schools, 80,000 in churches and some 560,000 in business, studios, stations, agencies and industry in general. Of the 1.6 million units in use, about 1.4 million are home-type machines and the remainder are professional units.

▶ **Tape**—Minnesota Mining and Manufacturing Co., which began making magnetic tape in 1947, estimates that total tape production for the industry in 1956 reached a value of $10 million. This is nearly a $2-million increase over 1955 volume of $8.1 million and nearly $3 million more than 1954 value of $7.1 million. It also represents the largest yearly increase in tape production since the product has been on the market. For 1957, 3M expects tape production to increase 17 percent to a value of $11.7 million.

The 3M figures on tape production are considered to be conservative. Census Bureau pegs the value of tape shipped in 1954 at $8.3 million, about $1.2 million higher than 3M estimates for '54.

▶ **Manufacturers** — Armour Research Foundation's licensing operations during 1956 indicate the changes that have taken place

(Continued on page 14)

Component Specification: ARNOLD

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  Types C, E and O
- ✔ TOROIDAL CORES
  Nylon and Aluminum cased
- ✔ BOBBIN CORES

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ENGINEERING DATA

For data on the various types of Arnold Tape Cores, write for these Bulletins:

TC-107—*Silectron Cores, Types C, E and O*
TC-101A—*Toroidal Cores, nylon and aluminum cased*
TC-108—*Bobbin Cores*

ADDRESS DEPT. E-73

How to be *sure* of tape core performance and uniformity? Just specify and use *Arnold* Cores in your transformer, magnetic amplifier, reactor and computer assemblies, etc.

Here's why!

To begin with, Arnold is a fully integrated company, controlling every manufacturing step from the raw material to the finished core. Then, modern testing equipment permits 100% inspection of cores before shipment. Finally, you're matching your requirements against the most experienced and complete line of tape cores in the industry. Arnold produces Types C, E and O Silectron cores, nylon and aluminum cased toroidal cores, and bobbin cores to meet whatever your designs may require in tape thickness, material, core size or weight. Wide selections of cores are carried in stock as standard items for quick delivery: both for engineering prototypes to reduce the need for special designs, and for production-quantity shipments to meet your immediate requirements.

Let us help you solve your tape core problems. Check Arnold, too, for your needs in Mo-Permalloy or iron powder cores, and for cast or sintered permanent magnets made from Alnico or other materials.

WSW6447

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Repath Pacific Division Plant: 641 East 61st Street, Los Angeles, Calif.

District Sales Offices:
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among manufacturers in the tape recording field. Five new magnetic recording licenses were added during the year, according to Armour, bringing the total of participating companies to 66. There are 49 U. S. magnetic recording manufacturers and 17 foreign manufacturers. The new licensees are Telectro Industry, of Long Island City, N. Y. and EMI, Ltd., Collaro, Ltd., Simon Equipment, Ltd., and Tape Recorders, Ltd., all in Great Britain. Two U. S. licensees dropped out of the field in 1956.

During 1956, 11 new magnetic recording patents were issued in the U. S. and 17 in foreign countries. Five new applications for patents were filed domestically and four overseas, according to Armour.

New Batteries Bid For Electronics Market

Transistorized equipment along with new developments boost the market potential

THREE new batteries have been introduced in the past few months. National Carbon has a new 1.5-volt platinum-cobalt battery in the Hamilton electric wrist watch now on the market. Elgin National Watch and Walter Kidde Nuclear Labs developed a battery that uses the decay energy of a beta-emitting radioisotope as its source of energy. GE has a one-inch long battery in pilot production that is said to be 60 times stronger than the ordinary flashlight battery and to have a projected life of more than 20 years.

► **Applications**—The National Carbon battery is expected to have important applications in the hearing aid field. The Kidde-Elgin battery, although not yet commercially available, is expected to be used in transistorized portable radios and in civil defense warning receivers for the home. Use of the units for missile, rocket and deep space work is foreseen. The GE device is seen as a power source in remote fire and radiation warning devices, deep well survey equipment, and in transistorized instruments.

► **Market**—Importance of the electronics field as a market for battery makers shows in Department of Commerce figures. Hearing aids took over 40 million batteries in 1954 worth nearly $10 million.

Battery shipments for portable radios totaled 12.4 million units in 1954 worth $12.3 million. Farm radio battery shipments totaled 1.9 million units worth $7.4 million. In the military field, dry-cell primary battery shipments were valued at $32.8 million.

(Continued on page 16)

Atomic-powered battery, developed by Elgin Watch and Kidde Labs, can deliver usable current for five years

Military Electronics

► **Army** has set up a special agency to push development and production of electronic combat surveillance systems for use by battlefield commanders. The new unit is called Army Combat Surveillance Agency (ACSA) and will be headed by Brig. Gen. Francis F. Uhrhane, former Army Signal Corps r & d chief. Now being tested is a system using helicopter-borne tv gear

► **Six-million** dollar electronics plant is planned by Hughes Aircraft in California to produce components of ground radar systems for the Army, Navy and civil airways

► **Guided** missile instrumentation subcontract worth $19.5 million has been awarded by Martin to Associated Missile Products of Pomona, Calif., subsidiary of AMF. The firm has leased 46,000 sq ft of space to handle the work

► **Plant** representing a $50-million government investment has been operated in Kansas City for the past eight years by Bendix Aviation, the firm recently revealed. The operation is devoted exclusively to the atomic weapons program of the AEC under contract. The plant has a work force of 4,300 employees and occupies 1 million sq ft of floor space. It manufactures and assembles a wide variety of complex electronic, electromechanical and mechanical devices

► **Contract** totaling $9.9 million has been awarded Collins Radio by Air Force for uhf ground communication equipment. Included in the order are over 1,500 units each of transmitters, receivers and modulator-power supplies, which make up the AN/GRC-27 radio set

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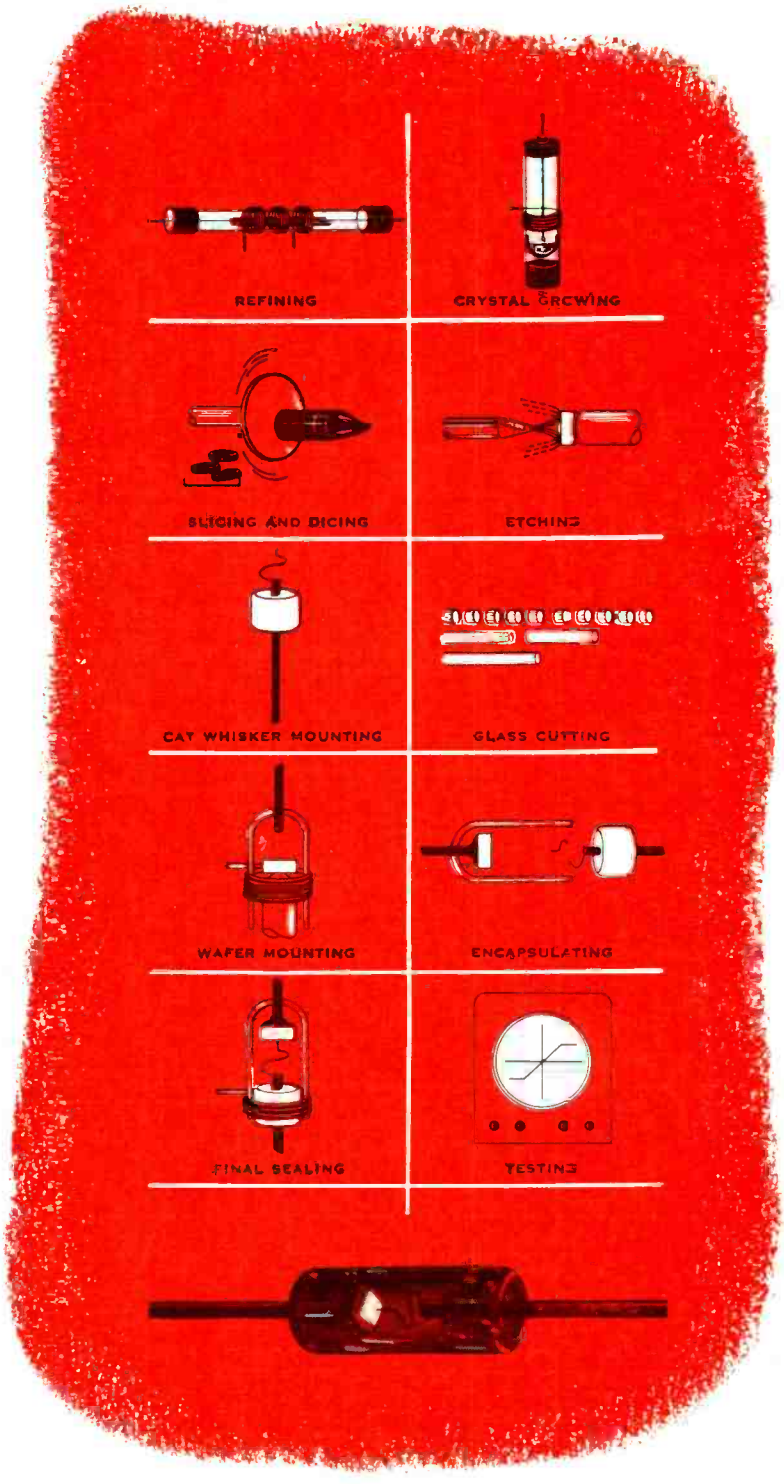
Send for technical information about all Kahle Semiconductor Manufacturing Machines . . . please mention your applications or requirements.



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Industry's Biggest Convention Readies 1957 Program

More than 50,000 visitors are expected at the IRE show March 18-21 in Manhattan

COMPREHENSIVE program of fifty-five technical sessions at which over 150 technical papers will be delivered will be featured at the annual IRE show and convention to be held at the Waldorf-Astoria Hotel and at New York's new Coliseum.

All four floors of the Coliseum will be occupied by some 840 exhibitors of electronics products and by-products. Last year there were 714 exhibits.

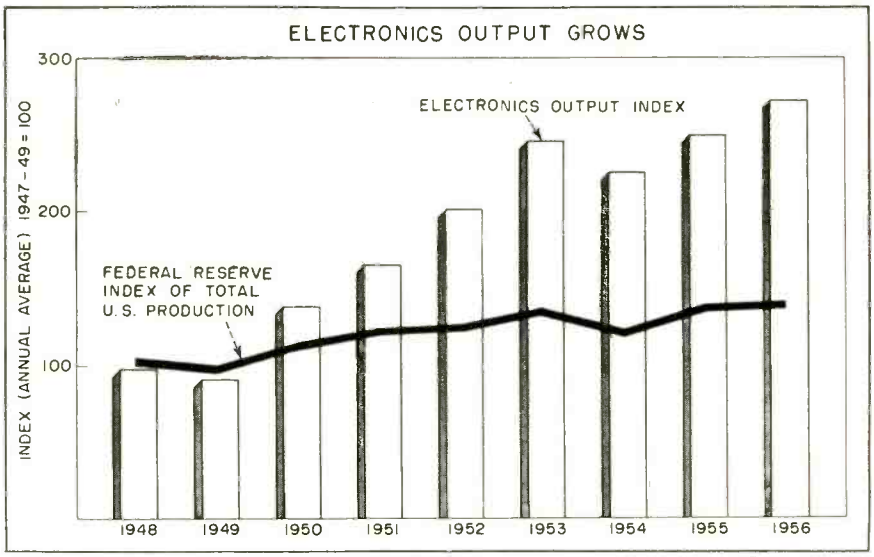
▶ **Sessions**—Of the 55 technical sessions scheduled for this year's convention, 33 will be held at the Waldorf and 22 at the Coliseum. Two highlight sessions will cover the future use of air space and microminiaturization, both to be held March 19 in the evening. A list of scheduled technical papers and sessions begins on page 461 of this issue of ELECTRONICS.

▶ **Show** — Exhibits at the Radio Engineering Show have been grouped to save some time and wear on visitors. Computer and communications exhibits will be together on the first floor; component parts on the second, instruments, microwave and components on the third and production tools, materials and services on the fourth floor.

▶ **Time**—Even with the convenient exhibit arrangement and new exhibit building this year, it will still be quite an endurance feat to cover the show. Spending just two minutes at each exhibitors display will consume nearly 30 hours or about three days of the show leaving one day for attending technical sessions.

The annual meeting of the IRE will be held on the opening morning of the convention. Registration for the convention and show may be made at either the Waldorf or the Coliseum.

Electronics Output Paces Industry



Growth has almost tripled since 1949 while total U.S. industrial output has risen 50 percent

THE electronics industry has been one of the fastest growing major industries in the U.S. Basis for this is evident when the ELECTRONICS output index is compared to the Federal Reserve Board Industrial Production Index for U.S. industry as a whole. The industry has nearly tripled its business ac-

(Continued on page 20)

It is the essence of G-R's design and manufacturing philosophy that every General Radio instrument shall be built to operate as reliably years later as it did upon first purchase by the customer.

This policy has built the reputation for quality and long life which has come to be synonymous with the G-R trademark and now makes possible a *two-year warranty* to purchasers of G-R products. This warranty applies to all newly purchased General Radio products shipped after March 1, 1957.

General Radio Company

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- Increased clearance between elements
- Controlled operation time
- Tighter limits for important characteristics
- Greater uniformity
- Lower microphonics
- Better resistance to shock and fatigue
- Pulse emission specification (where applicable)

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Raytheon RELIABILITY + Subminiature Tubes are made and assembled under glass in air conditioned, lint-free and dust-proof quality controlled areas. Every detail of construction is subject to the most advanced mechanical techniques including semi-automatic jigs and fixtures so that operator skill is no longer the critical factor. That's why these Raytheon Subminiature Tubes provide *Reliability Plus* performance.

RAYTHEON RELIABLE SUBMINIATURE TUBES For Guided Missile, Military and All Other Critical Applications
TYPICAL CHARACTERISTICS

TYPE	DESCRIPTION	Vibration Output* (maximum) mVac	Vibration Output** peak to peak mV	Heater Volts	Heater mA	Plate Volts	Plate mA	Cathode Bias Resistor ohms	Screen Volts	Screen mA	Amplification Factor	Mutual Conductance μmhos
CK5702WB	Video Amplifier, Pentode	50	240	6.3	200	120	7.5	200	120	2.6	—	5000
CK5703WB	High Frequency Triode	10	50	6.3	200	120	9.4	220	—	—	25.5	5000
CK5704†	High Frequency Diode	—	25	6.3	150	Max. inverse peak = 460 volts; max. I_o = 10 mA						
CK5744WB	High Mu Triode	15	75	6.3	200	250	4.2	500	—	—	70	4000
CK5783WB	Voltage Reference	50	—	Operating voltage approximately 85 volts between 1.5 and 3.5 mA								
CK5784WB	RF Mixer Pentode	75	300	6.3	200	120	5.5	230	120	4.1	—	3200
CK5787WB	Voltage Regulator	50	—	Operating voltage approximately 98 volts between 5 and 25 mA								
CK6247WA	Low Microphonic	2.5	25	6.3	200	250	4.2	500	—	—	60	2650
CK6533WA	Low Microphonic Triode	1.0	—	6.3	200	120	0.9	1500	—	—	54	1750

Each type is electrically and mechanically interchangeable with earlier versions of the same basic type. Developed under Navy sponsorship.

Bulb temperature ratings to 265°C.

†Type number for improved CK5704 not assigned.

*15g, 40 cps, fixed frequency
**15g, 30 to 1000 cps sweep

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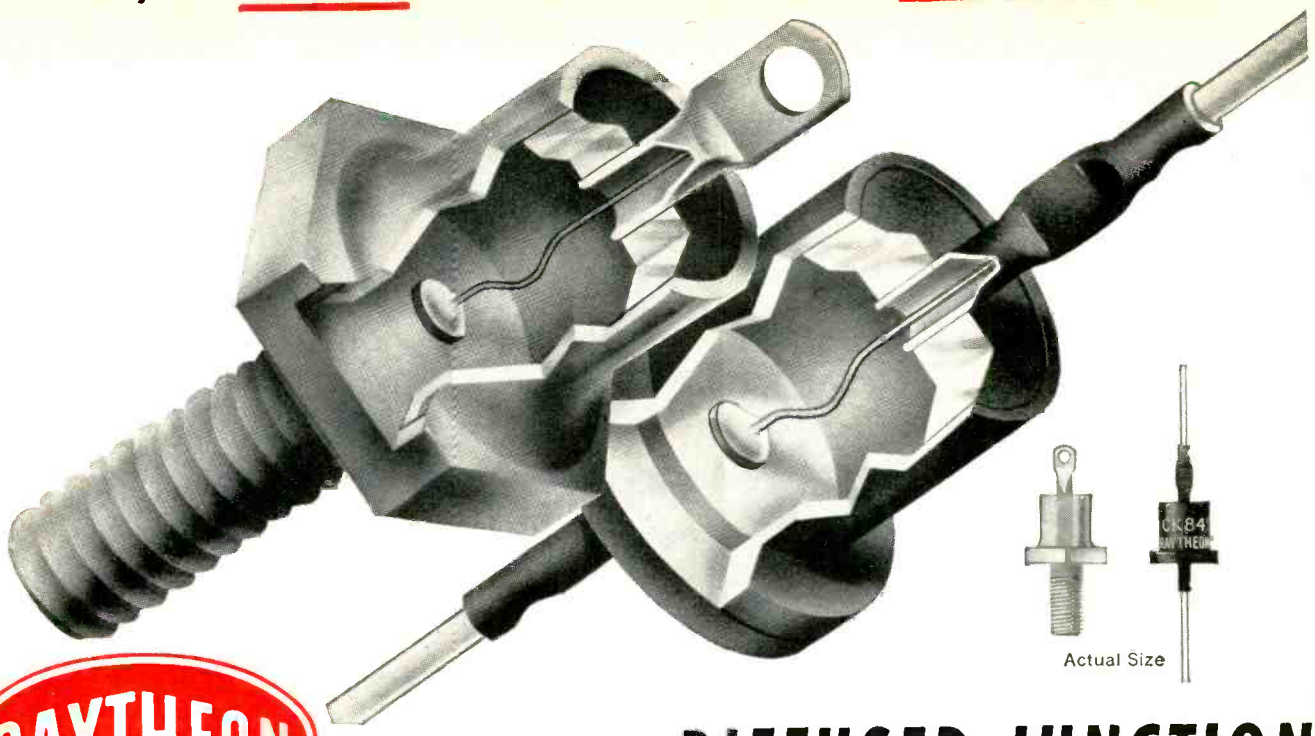

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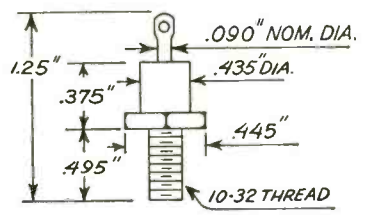
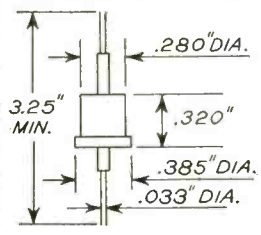
AVERAGE CHARACTERISTICS				Case Dimensions***
Type	Peak Inverse Volts*	Forward Current** Amps. 150°C Case Temp.	Reverse Current (max.) at PIV mAdc at 25°C	
CK846	100	1.0	0.002	
CK847	200	1.0	0.002	
CK848	300	1.0	0.002	
CK849	400	1.0	0.002	
CK850	500	1.0	0.002	
CK851	600	1.0	0.002	



Type	Peak Inverse Volts*	Forward Current** Amps. 150°C Ambient	100°C Ambient	Reverse Current (max.) at PIV mAdc at 25°C
CK840 (1N537)	100	0.25	0.5	0.002
CK841 (1N538)	200	0.25	0.5	0.002
CK842 (1N539)	300	0.25	0.5	0.002
CK843 (1N540)	400	0.25	0.5	0.002
CK844	500	0.25	0.5	0.002
CK845	600	0.25	0.5	0.002



*PIV ratings apply from −65°C to +150°C
**Average rectified current into inductive or resistive load
***All dimensions maximum except where noted

Operating Temperature—minus 65°C to plus 165°C

Storage Temperature — up to 175°C

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Flat Junctions for Uniformity and Control of Characteristics

Uniform characteristics and uniformly high quality are assured by the Raytheon Solid State Diffusion Process which permits flat junctions and provides exact control of junction penetration.

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tivity over that in the 1947-49 period while total U.S. industry increased its output 50 percent.

▶ **Rank**—A look at the FRB indexes of individual industries shows there are only a handful that have even doubled in activity since the 1947-49 base period and only one that exceeds electronics industry growth. They are specifically: electrical machinery, which includes electronics, 212; aluminum, 269; aluminum mill shapes, 220; heavy trucks, 201; aircraft and parts, 578; concrete and plaster products, 206; millwork and plywood, 200; synthetic rubber, 241; and canned and frozen foods, 247. Only aircraft outranks the electronics industry in rate of growth among the major industries covered by FRB indexes.

CHASSIS will be installed in portable tv sets at RCA's plant as . . .

Small Sets Do Big Business

Manufacturers say portable tv sets are still gaining and may hit 3 million in 1957

ALTHOUGH television set manufacturers do not like the low profit margins that come with portable tv sales they are impressed by the high unit volume record the sets have made and seem likely to surpass in 1957.

RETMA says that the portable tv set has been an outstanding success with about 1.5 million produced in 1956. It estimates that 3 million may be produced in 1957.

Here 's how individual manufacturers look at the portable tv business:

▶ **Admiral**—Estimates that tv output of the entire industry might reach a record 9 million units in 1957 with nearly half in 10, 14 and 17-inch portable models.

▶ **Motorola**—Plans to emphasize portables more so in 1957 than it did in 1956. It expects that portables will account for 2.5 million of a 6.8 mililon total tv volume in 1957.

▶ **Philco**—Says that units will have increasing popularity in 1957 following the trend toward second sets in the home. It expects the big volume of sales will be in lower priced receivers on which there is a small margin of profit.

▶ **Sylvania**—Sees the portable tv picture as similar to a period that the radio industry passed through 20 years ago when the public stopped buying consoles and began buying table models that were less expensive and carried a shorter margin of profit. The company sees more than 6.9 million sets sold to the public in 1957 with portables accounting for up to 40 percent of the total. In 1955 portable sales accounted for less than 4 percent of all tv sales. In 1956 it jumped to 20 percent and in the final quarter had risen to 51 percent of distributor sales to dealers. The trend in portables is expected to get a boost during 1957 through the new 110-degree picture tube sets, according to the company.

Experimental Radio Service Expands

Activity in the field reaches new high with yearly applications exceeding 1,500

GROWING amount of research and development work being carried on by the electronics industry is partially reflected in the increased activity of the experimental radio service.

Today there are over 750 experimental stations licensed. Annual number of applications handled has climbed from less than 1,000 in fiscal 1952 to over 1,500 in fiscal 1956. This is the best measure of activity since a separate license is required for each experimental project and the license is cancelled when the project is completed.

▶ **Kinds**—The experimental radio service provides for four classes of stations: research, developmental, export and contract. Research stations are used for basic research in radio such as investigations of propagation, exploration of the various ionized layers in the ionosphere, studies of tropospheric effects and research in new circuitry and modulation techniques.

Developmental stations cover development of new radio services, new techniques and procedures in existing services. Export stations are used to test equipment for overseas markets and contract stations are those used for contract work for the government, much of which is classified.

▶ **Techniques** — Most present experimental stations are operated in behalf of contract work

(Continued on page 22)

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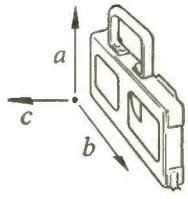
Starfighters' Fire-control Radars Use Barry's NEW Integral* Mounting Systems

In the most advanced airplane of its type ever developed — Lockheed's F-104A Starfighter — Barry's new Integral* Mounting Systems are solving the toughest combination of shock, vibration, and sustained-acceleration problems ever posed by jet aircraft. Literally a "missile with a man in it", the F-104A demands that equipment mounts give superior performance, in less space, and at lighter weight than ever before.

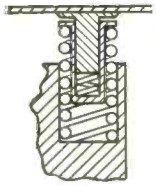
Here's how Barry's Integral* Mounting Systems are meeting this demand in the production models of the Starfighter.

In a space only 12¾ x 5⅜ x 1-13/32" on each side of a 150-pound load . . . a pair of units weighing less than three pounds each . . . provides adequate vibration isolation at 4g sustained acceleration in all radial directions . . . passes all shock-test requirements of this supersonic fighter . . . performs reliably through wide temperature and altitude ranges . . . and provides positive, quick-release attachment to the airframe to satisfy Lockheed's requirements for "plug-in" electronics-system components.

Here's the way this system works.



Helical springs designed to function in their axial direction only are grouped about the load attachment points so as to provide controlled resistance to movement along the *a* and *b* axes. For the *c* axis, resistance is provided by the slightly tapered side flanges of the mounting frame working against the displacement of all the load-carrying springs.



Damping adjustments (see diagram), completely independent of the stiffness of the load-carrying springs, provide design flexibility for obtaining desired natural frequency, transmissibility at resonance, and degree of vibration and shock isolation.

Write for THO-5 containing a full exposition of this All-Angl Integral* Mounting System.

BARRY CONTROLS INCORPORATED

BARRY B MOUNT

SALES REPRESENTATIVES IN ALL PRINCIPAL CITIES

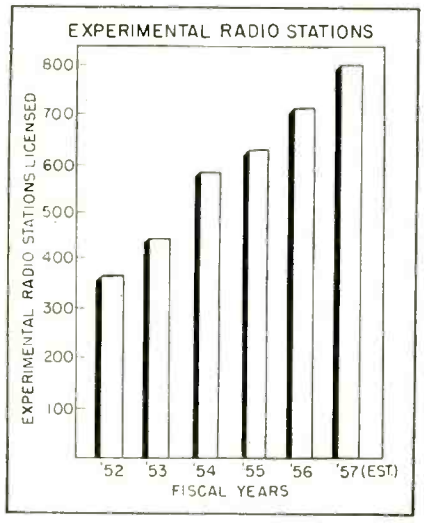
707 PLEASANT STREET, WATERTOWN 72, MASSACHUSETTS

Integral means . . .

Designed specifically for the environment performance requirements.

Built specifically for the equipment.

You can save time, space, and trouble by bringing your shock and vibration problems to us. Call your Barry sales representative.



for Federal agencies, chiefly the Department of Defense. Stations operated by manufacturers and developmental labs are engaged primarily in development of new radio and electronic techniques.

Narrow band, split-channel communication is receiving increased attention, according to FCC. New aids to navigation are being developed, including high-definition radar sets as well as lightweight radar equipments. Broad-band multiple-channel microwave experimentation as well as ionospheric scatter tests are receiving greater attention from both civilian and military research development groups.

Among the organizations presently most active in the experimental radio field are RCA, GE, Bell Labs and Harvard University.

Some organizations have over 100 experimental station authorizations, according to FCC frequency assignments.

► **Problems**—Practically all usable frequency bands in the spectrum have been allocated to the regular radio services, according to FCC, and it is necessary to borrow frequencies from these services for experimentation. The difficulties of doing this have compelled the Commission to restudy its allocation policy and the frequency assignment procedures for the experimental radio services.

FCC Actions

► **Amended** motor carrier rules to permit 45-mc communications during local pickup and delivery by vehicles engaged in interurban transport

► **Clarified** requirements for filing data on allocations above 890 mc. Only those not intending to present oral testimony are bound by Feb. 4 deadline

► **Postponed** for six months the requirements concerning radiation interference above 260 mc for uhf-tv receivers on request of RETMA

► **Received** petition to amend rules looking towards allocation of new channels to reduce separations between frequencies in the 152-162 mc band

► **Scheduled** hearing on continued use of 6-mc for ship-shore public telephone on the Mississippi River system

► **Studied** request for changes in regulations concerning remote control of objects by radio—including the 27 and 460-mc regions

Computer Centers Increase Fast

Number of centers has tripled since 1954. Many foreign centers are scheduled

PLANS by Electronic Associates to establish an analog computer center in Brussels, Belgium by next July emphasizes the rapid growth of computer centers at home and abroad.

Today there are about 10 commercial computer centers abroad and about 50 in the U.S. In 1954 there were about 20 centers worldwide. In the past month, plans for 14 new centers were announced.

► **Why**—The centers have proved valuable to U.S. and European industry and to computer manufacturers themselves. Electronic Associates says that there is still a growing need in industry for a facility such as it will establish in Brussels. One purpose of the centers is to educate business and industry on the capability of computers to economically solve many of their problems with a substantial saving of time and money.

► **Growth**—Increasing importance of computer centers to computer manufacturers is also indicated by the expanding operations of IBM. The company recently set up The Service Bureau Corp., a subsidiary, which operates the firm's 15 computer centers in the U.S. The IBM World Trade Corp. another subsidiary, has computer centers operating in Paris, Stuttgart, London and Toronto. A center in Caracas, Venezuela opened in February.

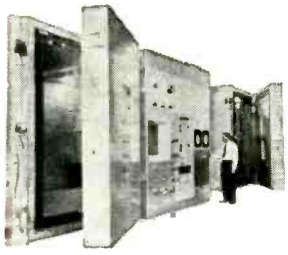
In the next two years, IBM data processing centers are scheduled to begin operation in eleven other cities outside the U.S.

(Continued on page 24)

ENVIRONMENTAL TEST CHAMBERS

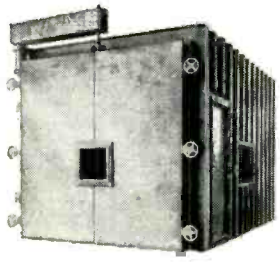
AIRECO, INC. are designers and builders of standard and custom-built environmental testing equipment for maintaining thermo, sub-zero and stratosphere conditions. Each is individually designed for its specific purposes and will produce and maintain temperatures from —150F to +750F, altitudes from sea level to 150,000 feet and humidity from 10 to 95%. Known the world over, you can rely on AIRECO, INC. service guaranteed test chambers.

CUSTOM BUILT FOR GE



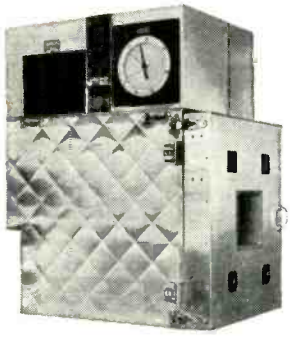
This custom built environmental test chamber was one of seven built for the General Electric Company, French Road Plant, Utica, New York. AIRECO, INC. in conjunction with the development engineers of G. E. decided on design temperatures of —100F to +250F; humidity from 20 to 95% and altitudes varying from sea level to 150,000 feet. This design assured long usage in the face of ever changing MIL spcifications. Pull down is from ambient to —100F in 1½ hours with 1500 lbs. mass load and 5 kw heat dissipation. The chambers were to hold —100F at 100,000 feet with a 5 kw heat dissipation load at all times; reach 250F from room ambient with the same mass load in 1 hour; maintain the desired humidity range from 33F to 250F; perform any one of these requirements for a period of 320 consecutive hours. Want more information?

TESTS TAIL GUN TURRETS



This environmental chamber is one of the largest of it's kind in the country and was designed and constructed for the General Electric Company for the testing of complete jet bomber tail gun turrets under all conditions of temperature, humidity and altitude. The size of this chamber is 15′ x 15′ x 25′. The exterior pressure shell was designed to withstand 15 psi for simulated altitude conditions to 150,000 ft. The equipment door is opened, closed and locked by means of a high pressure hydraulic system. Chambers of this type are constructed on job because of their immense size and weight. The temperature range is —100F to +250F; with a cooling capacity from ambient to —65F in 1 hr.; humidity range, 20 to 95% relative, altitude to 150,000 ft.

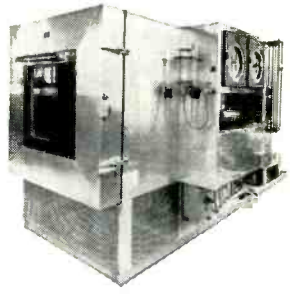
FOR TESTING GAS TURBINE STARTERS



Custom front opening cabinet completely portable for the testing of gas turbine starters under varying temperature conditions for the Bendix Aviation Corp. This cabinet has all its refrigeration equipment mounted on top to allow the working area to be as close to the floor as possible. The temperature range is —85F to +200F, with a cooling capacity from ambient to —85F. in 3 hours.

For normol operation the door is removed and a stationary bulkhead is used in it's place for the mounting of the jet starter. The cabinet is then moved into position and clamped to the bulkhead. The equipment is then cooled or heated and the box is moved away for the starter to be fired.

IDEAL FOR ELECTRONIC COMPONENTS



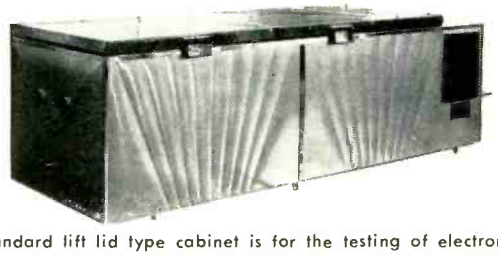
Standard front opening environmental chamber for testing electronic components and equipment under all conditions of temperature, humidity and altitude. This cabinet was originally manufactured for the General Electric Company. The working space is 27 cubic feet. All stainless steel interior. The temperature range is —100F to +300F; humidity range from 20 to 95% relative; altitude to to 150,000 ft; with a cooling capacity from ambient to —100F in 3 hours.

This cabinet has wide applications throughout the electronic industry for either military, commercial or laboratory uses. Perhaps, you are interested in a larger or smaller capacity in this design, if so, please communicate directly with Aireco Inc at the address below.

COMPLETE OUTDOOR ALL WEATHER TESTING

This lift lid type cabinet was specially designed and constructed for the U. S. Navy for the testing of rockets at —100F. It has a 75 cubic foot capacity and was completely constructed on both the inside and outside of stainless steel for operation in an outdoor location continuously exposed to the various elements. The refrigeration system was designed for year round operation under all weather conditions without the use of water. The temperature range is from —100F to +200F with a cooling capacity from ambient to —100F in 4 hours with full load.

FOR ELECTRONIC COMPONENTS AND EQUIPMENT



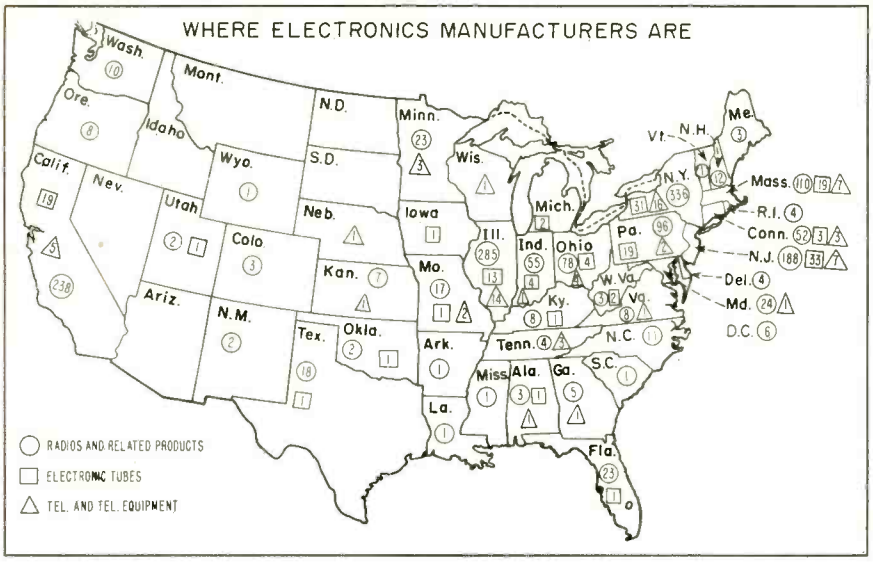
This standard lift lid type cabinet is for the testing of electronic components under all temperature conditions from —100 to +200F. Working space of 50 cubic feet with stainless steel interior. Cover is operated hydraulically. The temperature range is —100F to +225F, with a cooling capacity of ambient to —100F in 3 hours.

All types of testing equipment for lease. Contact us for particulars.

AIRECO INCORPORATED

ENGINEERED ENVIRONMENTAL EQUIPMENT FOR RESEARCH AND TESTING

2323 SECOND AVENUE, CARMAN
SCHENECTADY 3, NEW YORK



Electronics Sinks New Roots

Six states continue to hold the bulk of the industry but new areas grow

ADVANCE report by the U. S. Census bureau gives the latest authoritative picture of where electronics manufacturers are located in the U. S. It shows that six states, long-term centers for electronics, maintain their positions as of 1954, latest Census figures.

► **Big Six**—As indicated on the map, New York, California, Illinois, New Jersey, Massachusetts and Pennsylvania lead in the number of manufacturers of radios and related products. They also lead in number of tube manufacturers and telephone and telegraph firms.

Importance of these six key states in the industry is indicated by the number of workers employed. Together, they employ some 207,000, about 70 percent of the 293,998 employees in radios and related products.

In electronic tube manufacturing, the six states account for about 53,000 of the tube industry's 71,000 employees or 74 percent. Of telephone and telegraph firms, about 57,000 employees out of 65,000 total, or 87 percent, are in these states.

► **Change**—Growth of the electronics industry, even since 1954, is changing its direction somewhat. For some states the change has been drastic.

In Arizona, the map shows not one company classified by Census in the electronics field in 1954. Today there are ten major electronics firms in the state and a score of smaller subcontractors. Much of the growth has been due to the establishment of Ft. Huachuca Army Electronics Proving Ground.

Special weapons research centers in New Mexico are fostering the development of a small but growing electronics industry. The map shows that there were only 2 firms there classified as electronic. Today there are over a dozen.

Financial Roundup

DOZEN manufacturers in the electronics field that reported in the past month on net profits showed mixed results for the fiscal periods indicated. Here are the results for the 12 companies covered:

Company	1956 Net Profit	1955
ACF Industries 6m	$3,758,407	$3,874,775
American Elect. 9m	242,425	177,377
Bendix Aviation 12m	24,278,263	25,888,599
Cook Electric 6m.	370,032	*50,840
Daystrom 9m	1,838,000	1,295,000
Emerson Radio 12m	84,852	2,468,063
General Instrument 9m	337,146	241,994
National Research 12m	130,000	*337,000
ORRadio Industries 9m	85,986	64,293
Topp Industries 9m	90,000	
Packard-Bell 3m..	259,950	
Varian 3m	226,000	80,000

* (loss)

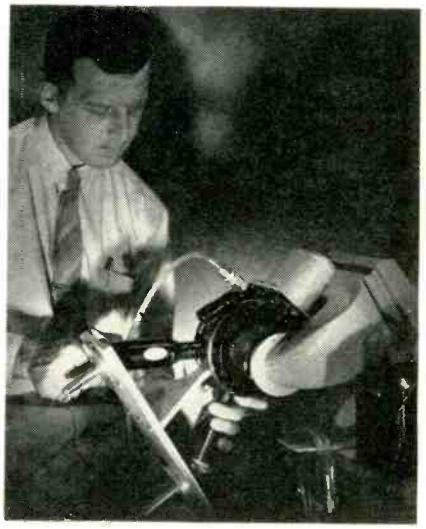
Magnetron Research Improves Cohos

New amplifier increases efficiency, aids in avoiding radar interference

A HIGH-POWERED broadband microwave amplifier has resulted from research by Raytheon on magnetrons. Called the amplitron, the new tube provides 800-kw peak power output and has a pass band of about 10 percent. It is said to have efficiencies of 50 to 70 percent.

► **Need**—Coherent moving-target indicating systems (cohos) require that there be no change in phase from one radar pulse to the next. The output of a continuously operating oscillator such as a klystron can drive the amplitron, which in turn radiates a pulse. The phase of the echo is remembered and compared with the phase of future echoes. If there is a difference, the target from which the echo is received is moving.

► **Interference**—The amplitron is also helpful in avoiding radar interference. Because it will amplify a broad band of frequencies without mechanical or electrical adjustments, the frequency of an oscillator operating into the amplitron can be changed quickly to a frequency where less interference is encountered.



Testing new microwave amplifier tube

(Continued on page 26)

NOW...A MORE COMPACT 28 VOLT, 100 AMPERE

tubeless magnetic amplifier regulated DC POWER SUPPLY

by PERKIN!

24 to 32 Volts Adjustable Range...
IMMEDIATE DELIVERY!

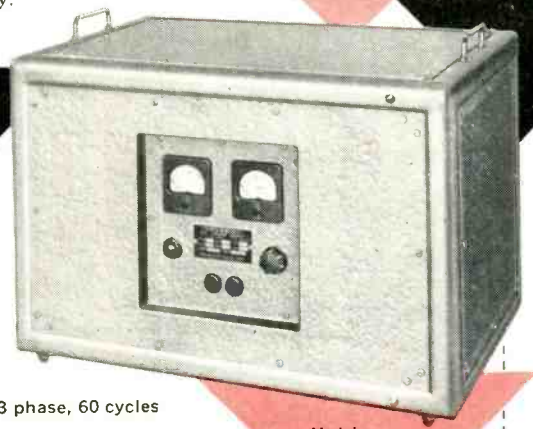
This power supply represents the latest design thinking of the nation's top specialists in the field. Hundreds of these units are now in operation, replacing generators and batteries in electronic laboratories, industrial plants, and military ground radar systems, etc., where utmost reliability and performance are essential. Over 15,000 Perkin power supply units are in operation in industry today.

No tubes, moving parts or vibrating contacts.

Regulation ±½%

IMMEDIATE DELIVERY!

DIMENSIONS: 26½" L x 17" D x 17" H.



Model MR2432-100XA

Additional Specifications:

Ripple: 1% RMS

AC Input: 208, 230 or 460V ±10%, 3 phase, 60 cycles

Weight: 230 lbs.

MODEL NO. MR917-100XA — also available: specifications same as above except output of 9 — 17 volts DC.

When you require a power supply, SPECIFY PERKIN, for a wider range of standard models and immediate delivery from stock.

Wire factory collect for prices. For a prompt reply on your application, write factory on your letterhead or contact local representatives listed below.

OTHER PERKIN STANDARD DC POWER SUPPLIES

28 Volt Models

Model	Volts	Amps	Reg.	AC Input (60 cps)	Ripple rms
28-5VFM	0-32 V	5	15-20% (24-32V range)	115 V 1 phase	2%
28-10WX	24-32 V	10	±½%	100-125 V 1 phase	1%
MR532-15A	2-36V	15	±½%	105-125V 1 phase	1%
28-15VFM	0-32 V	15	15-20% (24-32V range)	115 V 1 phase	5%
M60V	0-32V	25	±1%	115V 1 phase	1%
MR1040-30A	5-40V	30	±1%	100-130V 1 phase	1%
28-30WXM	24-32V	30	±½%	100-125V 1 phase	1%
28-50WX	24-32 V ±10%	50	±½%	230 V* 3 phase	1%
MR2432-100XA	24-32V	100	±½%	208/230V* 3 phase	1%
MR2432-200	24-32 V	200	±½%	208/230V* 3 phase	1%
MR2432-300	24-32 V	300	±½%	208/230V* 3 phase	1%
MR2432-500	24-32 V	500	±½%	208/230V* 3 phase	1%

*±10%. Also available in 460 V ±10% AC input. Will be supplied with 230 V input unless otherwise specified.

6, 12, 115 Volt Models

	Model	Volts	Amps	Reg.	AC Input (60 cps)	Ripple rms
6 Volt	6-5WX	6 ±10%	5	±1%	95-130 V 1 phase	1%
	6-15WX	6 ±10%	15	±1%	95-130 V 1 phase	1%
	6-40WX	6 ±10%	40	±1%	95-130 V 1 phase	1%
12 Volt	12-15WX	12 ±10%	15	±1%	95-130 V 1 phase	1%
115 Volt	115-5WX	115 ±10%	5	±½%	95-130 V 1 phase	1%
	MR15125-5	15-125	5	±1%†	95-130 V 1 phase	1%††
	G125-25**	115-125	25	±1½-4%	230/460 V 3 phase	5%

**Germanium Rectifier Unit ††Increases to 4% @ 15V.
†Increases to 2% @ 15V.

PERKIN

PERKIN ENGINEERING CORPORATION

345 KANSAS STREET, EL SEGUNDO, CALIFORNIA • OREGON 8-7215

Leader in Tubeless Magnetic Amplifier Regulation

New York Area: Sales and Warehousing: 1060 Broad St., Newark 2, N.J., MArket 3-1454

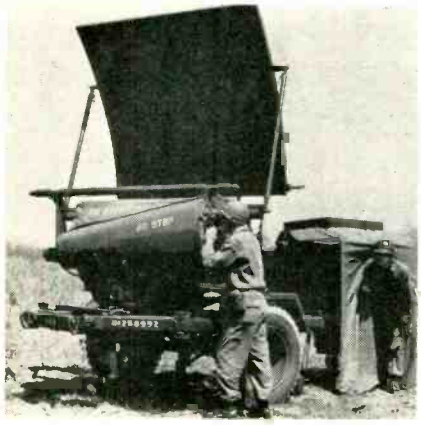
SALES OFFICES: Chicago: PA 5-6824 • Philadelphia: BR 5-2600 • Boston: MI 8-0756 • Albuquerque: 5-9632 Atlanta: EL 3020 • Charlotte: ED 2-7356 • Dallas: FO 8-8306 • Denver: MA 3-0343 • Kansas City, Mo.: VA 1-5330 • Miami: MO 5-1563 • Minneapolis: MI 4-7884 • Seattle: MO 4895 • St. Louis: PA 5-7701 Winston-Salem: 4-9750 • Canada: Agincourt, Ontario: AX 3-7011.

Radar-Computer Finds Mortars

Enables counter-fire within seconds. Set up from trailers in from 10 to 15 minutes

ARMY Signal Corps and GE have added an improved electronic computer to a modified version of the mobile radar equipment used in the Korean fighting for locating enemy mortars. Enemy position can be pinpointed in seconds.

GE will begin an accelerated manufacturing program to produce the first production models early this year. Completion of the order is expected by March, 1958.



Radar picks up enemy mortar shell in flight, computer determines location of mortar. New equipment is more compact and accurate than gear used in Korea

▶ **How** — Trajectory of enemy's mortar shell passing through the radar beam is registered by blips on the operator's indicator screen. Cross hairs lined up on the blips provide a direct map coordinate reading of the source of fire. Relayed to an artillery battery, this information triggers immediate counterattack.

Transportable on two small trailers, the equipment, known as AN/MPQ-4, can be set up in 10 to 15 minutes. It can be controlled in the trailer or from a remote position.

Impact point of the Army's own mortar shells can be read from the equipment for correcting fire direction.

INSPECTOR checks monochrome picture tubes at RCA plant as . . .

Envelope Sales Keep Growing

High volume of tube sales in 1956 meant more business for bulb companies

MORE tv picture tubes were sold by tube makers in 1956 than in any previous year. Cumulative picture tube sales for 1956 totaled 10.9 million units valued at $196.2 million compared to 10.8 million units valued at $209 million in 1955.

The number of receiving tubes produced by the industry last year was exceeded only by record sales in 1955. Receiving tube sales totaled 464.1 million units valued at $374.1 million in 1956, compared to 479.8 million units valued at $358.1 million in 1955.

▶ **Sales**—General Electric has estimated that about 14 million tv picture tubes will be sold in 1957. Of these, 6.8 million will be for replacement. It also estimates that receiving tube volume will reach $400 million in 1957.

At an average tv bulb price of about $8, next year's sales in picture tubes could mean a dollar volume of $112 million for envelope makers. However, glass companies may never sell that much because tube rebuilders will take a sizable share of the market.

One glass maker estimates that the rebuilt tube business now runs at an annual volume of some 5 million units, half of the business accounted for by legitimate tube manufacturers and the other half by fringe operators that may not label the tubes as rebuilts.

▶ **Color**—One of the new developments that may boost glass envelope sales substantially in 1957 is RCA's recent adoption of an all-glass envelope for its color tv picture tube. It has used a metal envelope manufactured by I-T-E Circuit Breaker in Philadelphia.

RCA plans to produce the new tube about midyear. The envelope and a new technique of glass sealing were developed by glass manufacturers working with the company. Price of the new tube will be comparable to the present metal envelope type. The problem of sealing the faceplate and funnel in the all-glass tube was solved through use of a glass flux that initially melts at relatively low temperature but thereafter almost assumes the qualities of the original glass bulb.

▶ **Deflection**—Envelope makers are moving into the 110-degree deflection tube field fast. An increasing

(Continued on page 28)

DO YOU KNOW

. . . transistors can be 20-30 db less noisy than low noise vacuum tubes?

These two companies use the new "hushed transistor" circuit in their most sensitive instruments.

SENSITIVE
AC & DC
VOLTMETERS
LOW NOISE
LOW DRIFT
10 UV
FULL SCALE

Type MV - 45A
TRANSISTOR
VOLTMETER
Range:
2 uV to 1 kV
2 cps to 150 KC

"Hushed Transistors" (having zero or reversed collector junction voltage) exhibit noise voltages, referred to their shorted input terminals, which are at least 20 db lower than the noise voltages of the finest low-noise vacuum tubes, available today. In a direct coupled circuit they also have less drift. Our new transistor voltmeters for AC and DC have lowest ranges of *10 uV* and highest ranges of 1 kV *full scale*.

SENSITIVE
AC & DC
AMPLIFIERS
SINGLE &
PUSH - PULL

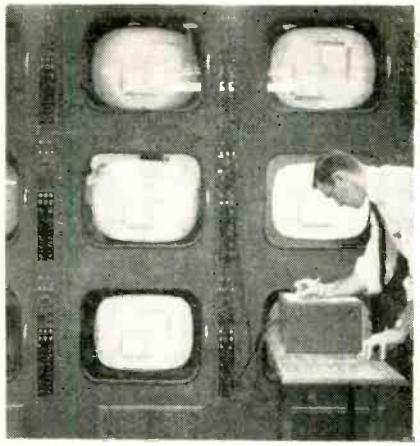
Type VS - 64A
LOW NOISE
AC-AMPLIFIER
Gain: 8 0 db
$E_{Nsh} = 0.45$ uV
(B = 60 kc)
Range: 2 cps-180
kc.

The discovery of the principle of "Hushed Transistor" operation by Dr. W. K. Volkers and Mr. Norman E. Pedersen, which was first disclosed at the National Electronic Conference in Chicago, a year ago, has led to the development of pre-amplifiers for AC and DC which have less than *500 muV RMS noise voltage*, referred to the shorted input terminals. These amplifiers have been in production during the past 12 months and have given an excellent account of themselves.

Visit Booths 3204-3206 IRE Show, N. Y. Coliseum.

MILLIVAC INSTRUMENT CORP.
BOX 997, SCHENECTADY, N. Y.

VOLKERS & SCHAFFER MFG. CORP.
Box 996, Schenectady, N. Y.



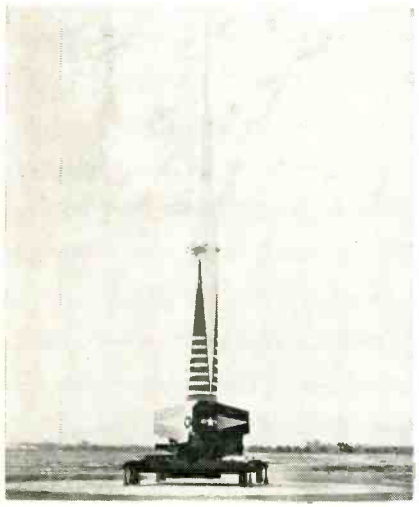
Envelopes undergo life test at Corning Glass

number of tv set makers have the wide angle receivers on the market. The bulbs are 3 inches shorter than 90-degree bulbs and weigh about five pounds less.

Corning Glass has two types of 110-degree 21-inch bulbs. One is ready for production and the other is being sampled to manufacturers. The company uses a process for flame-proofing the bulbs which substantially reduces thermal shock breakage during evacuation and other tube manufacturing operations.

Cathode-ray tubes for radar are also undergoing a change. The tubes are now being made with optical quality faceplates so that glass imperfections cannot hide small blips.

Stand-in For Atlas



High as o four-story building Lockheed's three-stoge X-17 missile helps solve problems that will orise when ICBM's reenter earth's atmosphere

Meetings Ahead

Feb. 27-28: Symposium On Nuclear Radiation Effects On Semi-conductor Devices and Materials, Advisory Group On Electron Tubes, Western Union Auditorium, New York, N. Y.

March 11-15: 1957 Nuclear Congress, EJC, Convention Hall, Phila., Pa.

March 18-21: IRE National Convention, Waldorf-Astoria Hotel, New York Coliseum, New York, N. Y.

March 18-21: Military Automation Show, Cancelled.

Apr. 8-11: British Radio And Electronic Component Show, Grosvernor House and Park Lake House, London, England.

Apr. 9-10: Annual Industrial Electronics Educational Conf., IRE, Armour Research, Ill. Institute of Technology, Chicago, Ill.

Apr. 11-13: Southwest IRE Regional Conference & Electronics Show, Shamrock Hilton Hotel, Houston, Texas.

Apr. 14-16: National Symposium On Telemetering, IRE, Sheraton Hotel, Phila., Pa.

Apr. 23-25: International Symposium On the Role of Solid State Phenomena In Electric Circuits, IRE, Eng. Soc. Bldg., New York, N. Y.

Apr. 24-26: Seventh IRE Region Technical Conference & Trade Show, San Diego, Calif.

Apr. 26-27: Eleventh Annual Spring Technical Conference On TV, IRE, Engineering Society Bldg., Cincinnati, Ohio.

Apr. 29-May 1: Third National Flight Test Instrumentation Symposium, ISA, Statler Hotel, Los Angeles.

May 1-3: 1957 Electronic Components Symposium, Morrison Hotel, Chicago, Ill.

May 9-10: 1957 PGMTT Meeting, Western Union Auditorium, New York, N. Y.

May 13-15: National Aero & Navigational Electronics Conference, IRE, Dayton, Ohio.

May 14-16: Industrial Nuclear Technology Conference, ARF, Ill. Tech, Nucleonics Magazine, Museum of Science and Industry, Chicago, Ill.

May 20-23: 1957 Electronic Parts Distributors Show, Conrad Hilton Hotel, Chicago, Ill.

May 22-25: URSI Spring Meeting, Hotel Willard, Washington, D. C.

May 27-29: 1957 National Telemetering Conference, AIEE, ISA, IAS, Hotel Cortez, El Paso, Texas.

June 6-7: First National Symposium On Production Techniques, IRE, Willard Hotel, Washington, D. C.

Aug. 20-23: 1957 WESCON, IRE, WCEMA, Cow Palace, San Francisco, Calif.

Industry Shorts

► **Thirty-three** newly developed large-screen projection tv units have been acquired by Upjohn Co., pharmaceutical manufacturers, from GPL.

► **New** magnetic alloy, developed at Bell Labs called Supermendur, has high permeability and lower hysteresis losses at higher flux densities than any material heretofore available, according to Bell.

► **North** American Philips Co. has acquired about 2,000 U.S. patents and 1,200 patent applications formerly held by the Hartford National Bank and Trust Co., as trustee. They cover inventions made in the research labs of Philips in Holland and other countries.

► **Output** of electronic equipment in the capital goods field, by British firms in 1956, is expected to be greater than that in the radio and tv side of the industry, according to Britain's Radio Communication and Electronic Engineering Association.

► **Plant** for making electronic modules was opened in Puerto Rico by Modular Systems.

NEW . . . All Electronic High-Level Broad-Band Sweeping Oscillator with MARKERS WHERE YOU WANT THEM!

KAY

Vari-Sweep MODEL RADAR

A Vari-Sweep *With Markers* for Rapid, Accurate Alignment of Radar IF's

SWEEP

- **High Output—1.0 V rms Into 70 Ohms**
- **Wide Range—10-145 mc, All at Fundamental**
- **Constant Output—Fast-Acting A.G.C.**

MARKERS

- **Variable—Birdie Pip Direct Reading Frequency Dial 5-170 mc**
- **Crystal—11 Precise Markers, Individually Switched—to Customers' Specifications**

SPECIFICATIONS

Range: Fundamental frequency—10-145 mc, continuously variable in 6 overlapping bands accurately calibrated on a direct reading dial.

RF Output: 1.0 V rms into 70 ohms. Flat within ± 0.5 db over widest sweep and tuning range.

Sweep Width: Continuously variable to 60% of center frequency below 50 mc, 30 mc sweep width above 50 mc.

Sweep Rate: Variable around 60 cps. Also line lock at 60 cps.

Markers: Variable, Birdie Pip type continuously variable from 5 to 170 mc in 6 overlapping bands. Calibrated to ± 1.0% on separate direct reading dial. 11 individually switched, crystal-controlled, pulse-type marks over the band width, providing separate and simultaneous operation.

Attenuators: Switched 20, 10, and 3db plus continuously variable 6 db.

Marker Amplitude: Continuously variable zero to 10 V positive.

Power Supply: Electronically regulated 105 to 125 V AC. 50-60 cycles.

Price: $950.00 F.O.B. Plant

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ELECTRIC COMPANY

Dept. E-3, 14 Maple Avenue, Pine Brook, N. J. • CAldwell 6-4000

Announcing the Raytheon

—a new type of broadband, high power.....

QK520
AMPLITRON
TYPICAL OPERATION (PULSED)

ANODE VOLTAGE	40 kV
ANODE CURRENT	35 amps
PEAK POWER OUTPUT	800 kw
AVERAGE POWER OUTPUT	1200 watts
EFFICIENCY	55%
OPERATING BAND (± 1 db)	1225–1350 Mc
PEAK POWER INPUT	80 kw
PHASE STABILITY WITH ANODE CURRENT	1°/amp

The Amplitron is a new type of tube developed by Raytheon, capable of power amplification at microwave frequencies. Amplification is obtained over a broad range of frequencies with no mechanical or electrical adjustments required. This device is a derivative of the magnetron and retains many of its advantages—such as high operating efficiency, construction simplicity, small size, light weight, low operating voltage. Where efficiency counts in high-power systems, the broadband Amplitron has applications of major significance.

The Amplitron uses crossed electric and magnetic fields, a reentrant beam produced by a magnetron-type cathode, and a non-reentrant broadband circuit matched at either end to external circuits.

AMPLITRON*

cross-field microwave amplifier

.....*high efficiency*

This amplifier has bandwidths of 10% with efficiencies of 50-70% over the entire band. Variations in anode current or voltage have little effect upon the total phase shift. This results in very low phase pushing and excellent reproduction of the input spectrum despite slow pulse rise time and ripple. Because the device has low insertion loss, duplexing may be accomplished at the input rather than the output of the final rf amplifier.

The Amplitron is another example of Raytheon's unequalled leadership in microwave tubes. A limited quantity of preliminary literature will be available shortly; to be sure of a copy, write now.

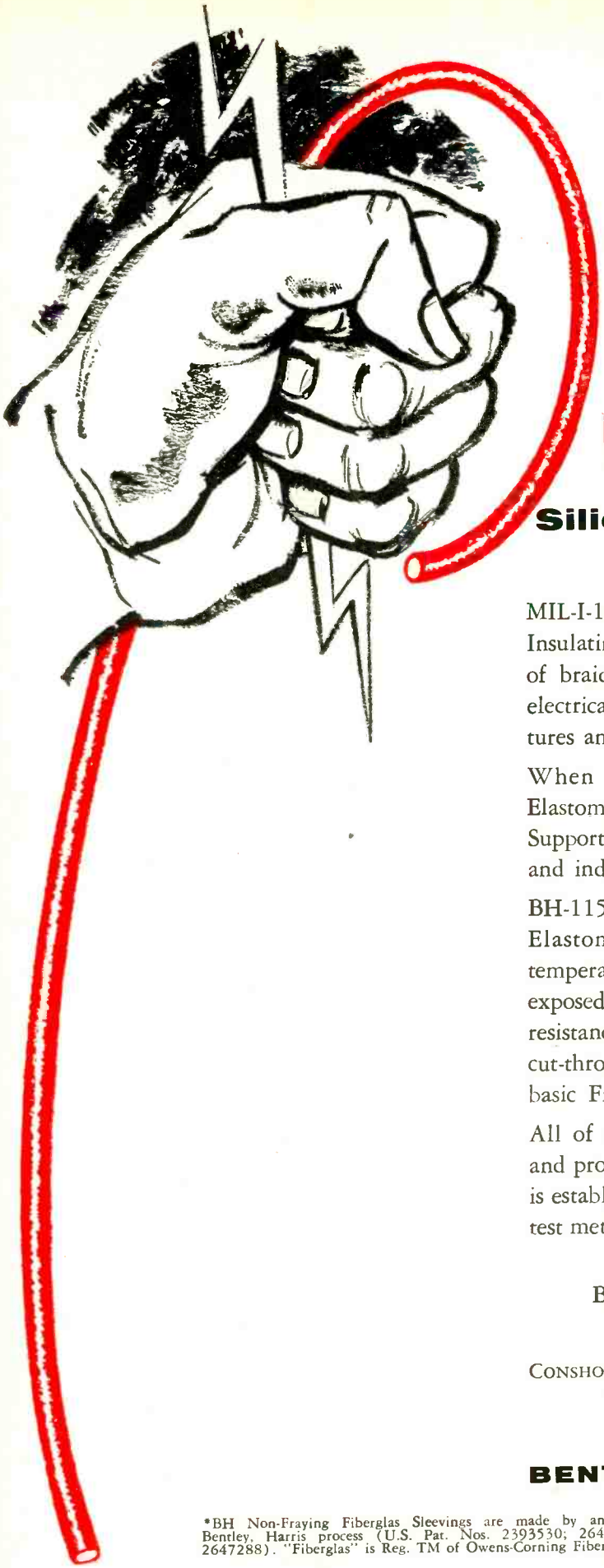
See it at the I.R.E.—Raytheon Booths 2611-14

RAYTHEON

Excellence in Electronics

RAYTHEON MANUFACTURING COMPANY
Microwave and Power Tube Operations, Section PT-02
Waltham 54, Massachusetts

*Raytheon Trademark



For all the stringent requirements of MIL-I-18057

BH "1151"

Silicone Rubber Sleeving

MIL-I-18057 is a functional type test — for Class H Insulating Sleeving. It sets the standard for performance of braided Fiberglas Silicone Elastomeric sleeving in electrical insulating systems subjected to high temperatures and mechanical stress.

When you specify BH-1151 Fiberglas Silicone Elastomeric Sleeving, it meets these high standards. Supported by long record of service in both military and industrial applications.

BH-1151 combines the superior qualities of Silicone Elastomer — extreme low temperature and high temperature flexibility, resistance to degradation when exposed to high temperature, chemical inertness, and resistance to crazing — with the support, resistance to cut-through and dimensional stability offered by the basic Fiberglas braid.

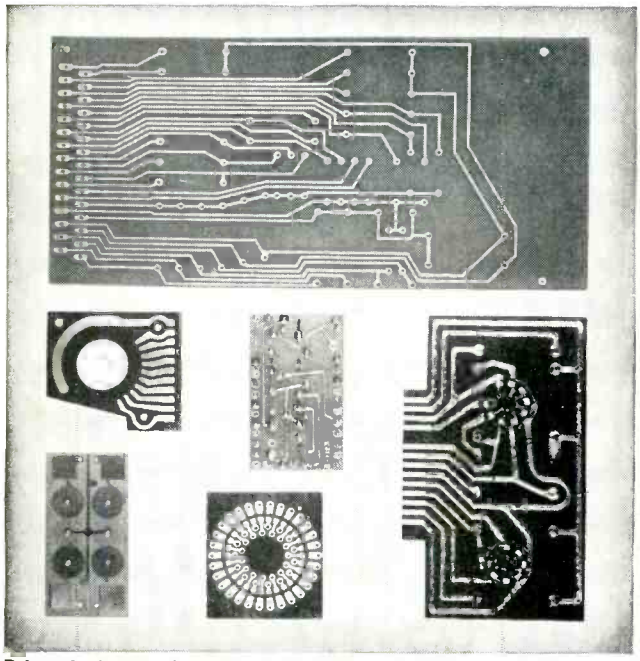
All of these properties are required by MIL-I-18057 and proof of BH-1151's ability to meet these standards is established by data obtained in each of the prescribed test methods. These data sheets are available on request.

BENTLEY, HARRIS MANUFACTURING CO.
303 Barclay Street
CONSHOHOCKEN, PA. TELEPHONE: TAYLOR 8-0634

BENTLEY, HARRIS Fiberglas* **SLEEVINGS**

*BH Non-Fraying Fiberglas Sleevings are made by an exclusive Bentley, Harris process (U.S. Pat. Nos. 2393530; 2647296 and 2647288). "Fiberglas" is Reg. TM of Owens-Corning Fiberglas Corp.

For the most dependable printed circuits, you need the high bond strength, workability, heat-resistance of C-D-F DILECTO® METAL-CLAD LAMINATES



Printed circuits based on C-D-F materials are being used with great success in military electronic equipment, commercial television and radio sets, telephone switchboards—even sub-miniature radiosonde equipment and hearing aids.
Photos courtesy of Photocircuits, Inc., Glen Cove, N. Y.

HIGH BOND STRENGTH—C-D-F's special adhesive for metal-clad Dilecto bonds the copper foil to the plastic without affecting the laminate's superior electrical properties. Heat-resistance, dissipation factor, dielectric constant, dielectric strength, and insulation resistance of the Dilecto base remain unaffected. The closely-bonded foil can be etched cleanly and dipped in hot solder to 450°F. for ten seconds with a guarantee of no blistering or separating. Metal-Clad Dilecto can be punched or machined either before or after etching.

EXCELLENT WORKABILITY—On all four Dilecto metal-clad grades, you can solder, punch, saw, and assemble components either by hand or automatically. Thanks to the inherently superior workability of the plastics laminate over that of ceramic-type materials, Dilecto can be dropped, jammed into tight chassis, and otherwise treated roughly on the assembly line and in service.

HIGH HEAT-RESISTANCE—Metal-Clad Dilecto Laminates are made of phenolic, epoxy, or Teflon* resin for various conditions of service and assembly, and have either cellulosic paper or woven glass-fabric base. All are ideally suited to printed-circuit applications in which heat-dissipation is a major problem. Continuous exposure to high ambient operating temperatures in enclosed electronic equipment has no significant effects on Dilecto's electrical and physical properties.

UNLOAD YOUR HEADACHE HERE! C-D-F, a big, reliable source of supply, can help you get the most for your printed-circuit money by reducing rejects, lowering fabrication costs, assuring dependable quality every time. Send us your print or problem, and we'll gladly supply appropriate test samples free. See our catalog in the Product Design File (Sweet's) or send for the new 20-page Dilecto catalog. Let your nearby C-D-F sales engineer (listed in Sweet's) help you right from the design stage!

TYPICAL PROPERTY VALUES

	Copper-Clad PHENOLIC (Grade XXXP-26)	Copper-Clad PHENOLIC (Grade XXXP-28)	Copper-Clad EPOXY (Grade GB-181E)	Copper-Clad TEFLON* (Grade GB-112T)
BOND STRENGTH—0.0014" foil (Lbs. reqd. to separate 1" width of foil from laminate)	7 to 11	5 to 9	8 to 12	4 to 8
MAXIMUM CONTINUOUS OPERATING TEMP. (Deg. C.)	120	120	150	200
DIELECTRIC STRENGTH (Maximum voltage per mil.)	800	800	650	700
INSULATION RESISTANCE (Megohms) 96 hrs. at 35° C. & 90% RH	50,000	25,000	20,000	Over 10^6 megohms
DIELECTRIC CONSTANT 10^6 Cycles	4.20	4.20	4.54	2.85
DISSIPATION FACTOR 10^6 Cycles	0.026	0.052	0.018	0.0006
ARC-RESISTANCE (Seconds)	10	5	120	180
TENSILE STRENGTH (psi.)	16,000 x 13,000	12,000 x 10,000	48,000 x 44,000	23,000 x 21,000
FLEXURAL STRENGTH (psi.)	21,000 x 18,000	18,000 x 16,000	65,000 x 55,000	13,000 x 11,000
IZOD IMPACT STRENGTH edgewise (ft. lbs. per inch of notch)	0.40 x 0.35	0.40 x 0.35	13.5 x 11.5	6.0 x 5.0
COMPRESSIVE STRENGTH flatwise (psi.)	28,000	22,000	62,000	20,000
BASE MATERIAL OF LAMINATE	Cotton rag paper	Cotton rag paper	Medium-weave, medium-weight glass cloth	Fine-weave, medium-weight glass cloth
COLOR OF UNCLAD LAMINATE	Natural greenish	Natural Brown	Natural	Natural

All these standard grades are available with 0.0014", 0.0028", 0.0042", or thicker electrolytic or rolled copper foil on one or both surfaces. Other metal foils and other resin-and-base combinations can be supplied on special order.

*duPont Trademark

CDF

CONTINENTAL DIAMOND FIBRE

CONTINENTAL-DIAMOND FIBRE DIVISION OF THE BUDD COMPANY, INC.

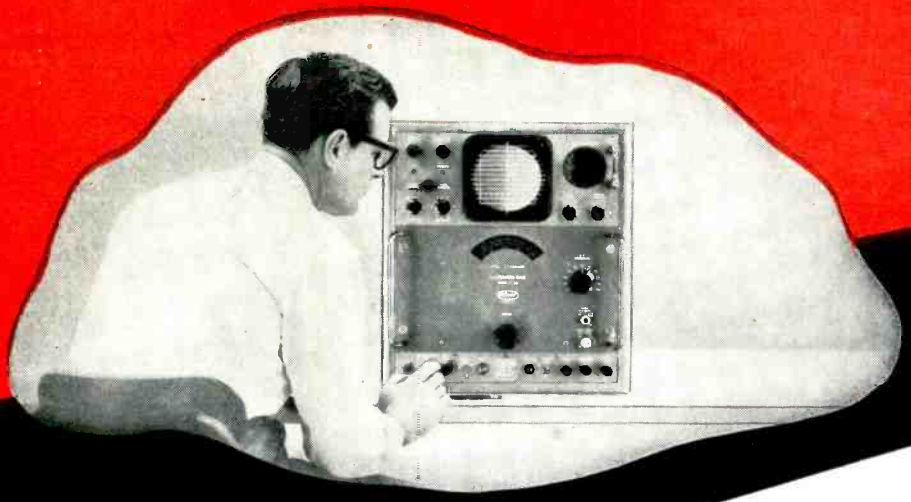
NEWARK 16, DELAWARE

Direct Reading Spectrum Analyzer

for

- Visual frequency calibration — high resolution
- Leakage and interference measurements
- Standing wave measurements
- Pulse modulation analysis
- Sensitive receiver

The BASIC SCOPE for VISUAL MICROWAVE



SPECIFICATIONS

Model No.	Equipment
Model Du.....	Spectrum Display and Power Unit
Model STU-1...	RF Tuning Unit 10-1,000 mc.
Model STU-2A.	RF Tuning Unit 910-4, 560 mc.
Model STU-3A.	RF Tuning Unit 4,370-22,000 mc.
Model STU-4...	RF Tuning Unit 21,000-33,000 mc.
Model STU-5...	RF Tuning Unit 33,000-44,000 mc.

Frequency Range: 10 mc to 44,000 mc.
Frequency Accuracy: ±1%
Resolution: 25 kc.
Frequency Dispersion: Electronically controlled, continually adjustable from 400 kc to 25 mc per one screen diameter (horizontal expansion to 20 kc per inch)

Input Impedance: 50 ohms—nominal
Overall Gain: 120 db
Input Power: 400 Watts
Sensitivity: (minimum discernible signal)
STU-1: 10-400 mcs—89 dbm
400-1,000 mcs—84 dbm
STU-2A: 910-2,200 mcs—87 dbm
1,980-4,560 mcs—77 dbm
STU-3A: 4,370-10,920 mcs—75 dbm
8,980-22,000 mcs—60 dbm
STU-4: 21,000-33,000 mcs—55 dbm
STU-5: 33,000-44,000 mcs—45 dbm
Attenuation:
RF internal 100 db continuously variable (STU-1, STU-2A, STU-3A)
IF 60 db continuously variable

Frequency differences as small as 40 kc measurable by means of variable frequency marker with adjustable amplitude.
Portable and completely self-contained.

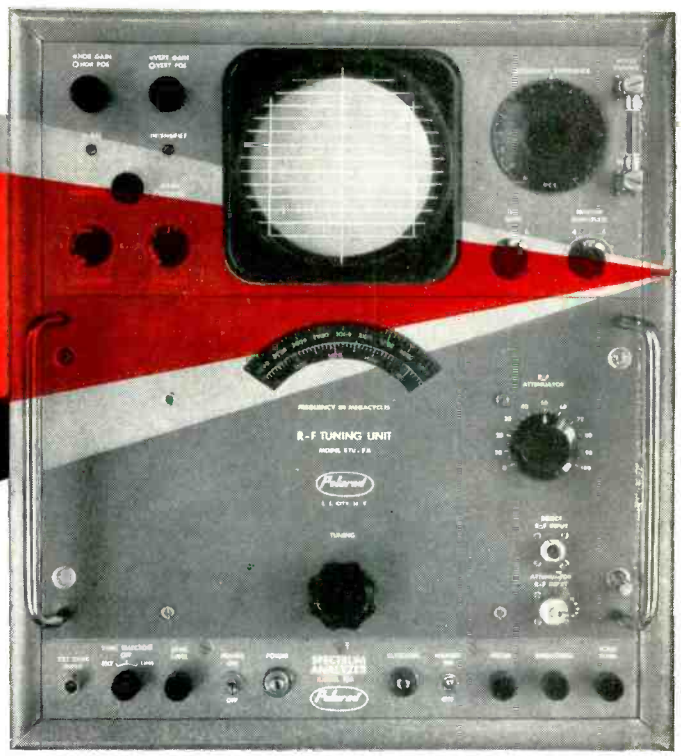
Broadband 10-44,000 mc

ANALYSIS

Now, the Polarad Model TSA Spectrum Analyzer provides the same visual advantages for microwave testing as the standard oscilloscope accomplishes for low frequency signals. This is a "must" instrument for microwave work! It displays with high sensitivity on a bright easily defined CRT, pulse modulation components, frequency differences, attenuation and band width characteristics, leakage detection, radiation and interference signals, and VSWR information.

This is visual instrumentation—it provides immediate and complete information because of the high resolution obtainable.

Frequencies are read directly on the linear dial with 1% accuracy as the set is tuned. Maximum reliability and long life are assured through use of non-contacting oscillator plungers. A variable frequency marker with both frequency and amplitude adjustable is provided.



Write today—directly to Polarad, or your nearest Polarad representative—to find out how the Model TSA Spectrum Analyzer can speed your research and solve your microwave measurement and testing problems.

Write for your copy of the Polarad "Handbook of Spectrum Analyzer Techniques". 50c per copy. Includes discussion of Spectrum Analyzer operation, applications and formulae for analysis techniques.

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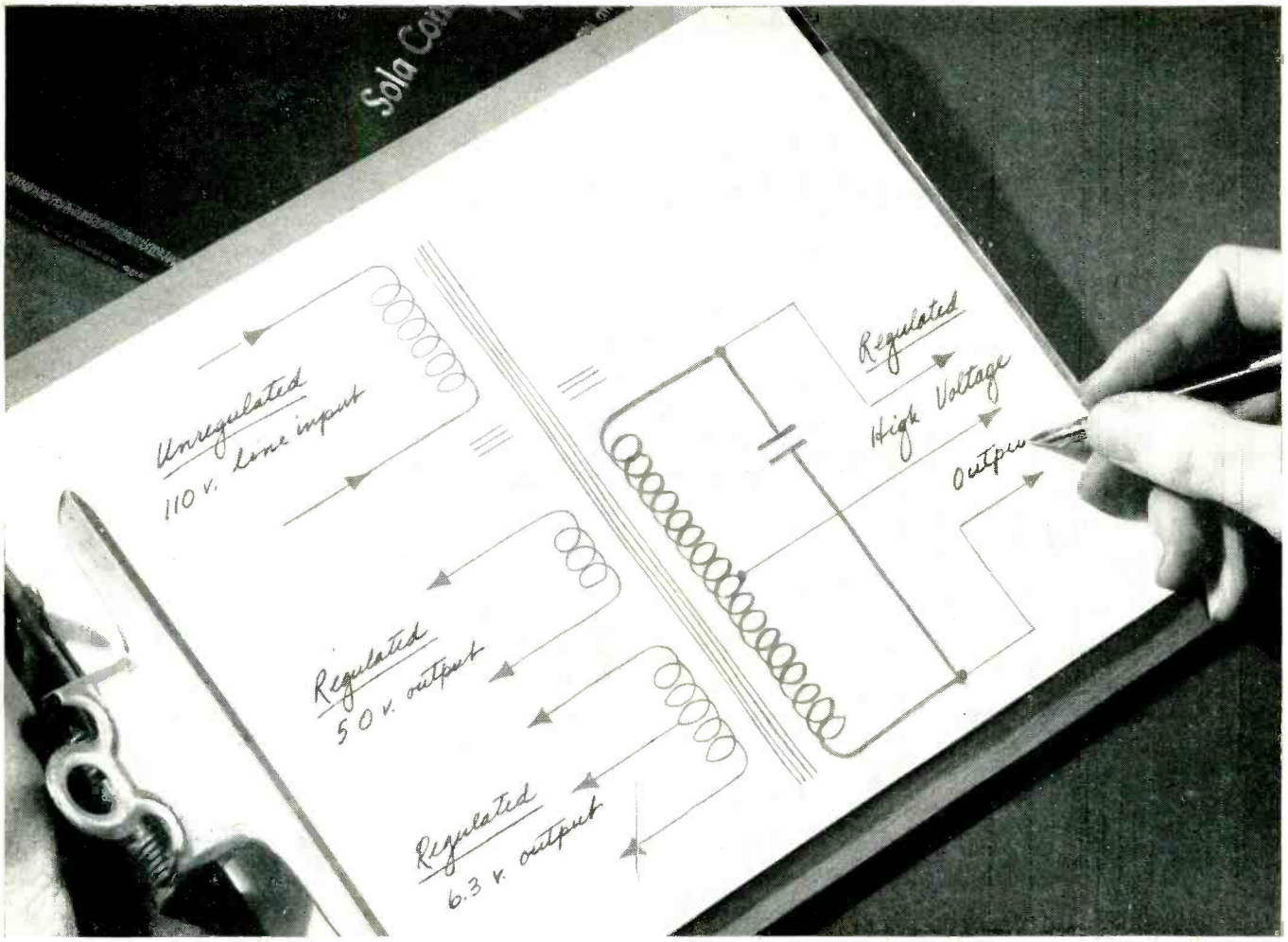

SCHEMATIC DIAGRAM OF SOLA CIRCUIT modified to supply regulated plate and filament voltages. Regulation on one stepped-up output and two stepped-down outputs is within ±3% for input variations of ±13%. Other units available regulate as close as ±1% for input variations of ±15%.

YOU GET VOLTAGE REGULATION AND MORE FROM A SOLA:

Closely Regulated Voltage Plus Transformer Step-Up or Step-Down with Sola Constant Voltage Transformers

Today's complex electrical and electronic equipment, with its narrow limits for adequate performance, makes a fixed level of input voltage virtually essential. There are many fine voltage regulators available for this duty alone. However, the Sola Constant Voltage Transformer delivers one-to-one, stepped-up, or stepped-down voltages closely regulated. One Sola unit may replace both voltage-regulating circuit or component, *and* conventional power transformer.

The Sola Constant Voltage Transformer is a static-magnetic voltage regulator. It offers many important advantages over other stabilizers which depend solely upon saturation of core materials for their regulating action; or electronic types employing tubes.

To meet the exact requirements of many load devices or service conditions, Sola voltage regulators are available in stock models, or custom designs in production quantities. Your Sola representative will be happy to provide you with information on their feasibility for your particular application.

SOLA *Constant Voltage* **TRANSFORMERS**

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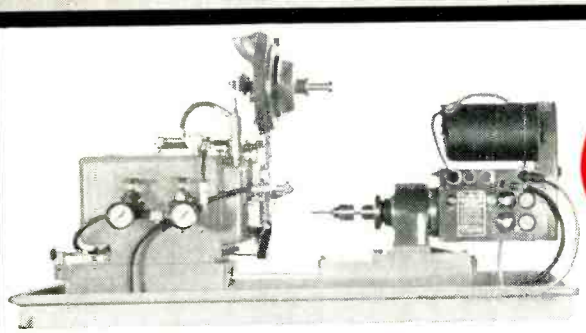
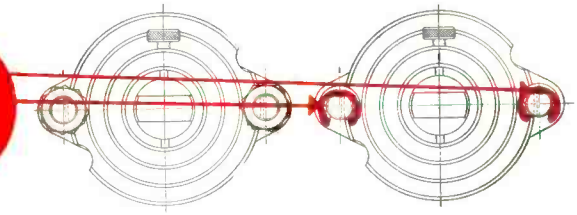
Waldes Truarc Retaining Rings Eliminate Machining and Parts—Cut Assembly Time on Drill and Tapper



Beco Model 410 Drill and Tapper

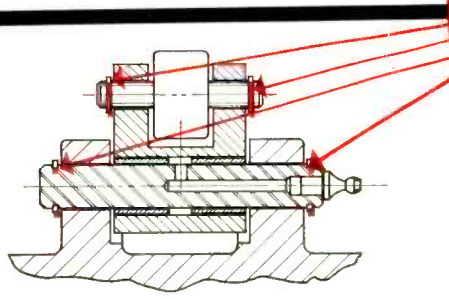
The Batchelder Engineering Co., Inc., Springfield, Vermont uses 4 different sizes of 2 different type Waldes Truarc rings in their new BECO Model 410 Automatic Drill and Tapper. Truarc rings speed assembly, reduce machining, improve design.



ALTERNATE DESIGN TRUARC DESIGN

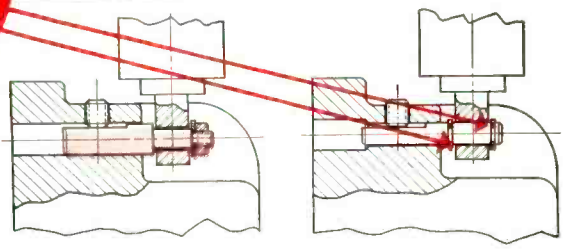
Clamp Cylinder Rod Stop Assembly

Truarc "E" Rings (Series 5133) replace stop nuts in the Clamp Cylinder assembly. They eliminate need for threading 2 rods ...the danger of cross-threading nuts...and costly rejects. Truarc Rings cut assembly time and cost.



Bell Crank Pivot Assembly

Truarc Rings (Series 5100) in Bell Crank Pivot assembly permit grease hole not possible with cotter pin fastener. Use of nuts would have increased machining and assembly costs considerably.



ALTERNATE DESIGN TRUARC DESIGN

Hopper Cylinder Anchor Pin Assembly

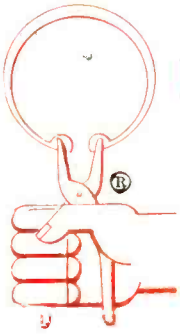
2 Truarc Rings (Series 5100) secure and position end of vertical air cylinder. Rings eliminate extra cost of machining 3-diameter pin, threading and undercutting...plus nut and washer. Assembly is quick and sure.

Whatever you make, there's a Waldes Truarc Retaining Ring designed to improve your product...to save you material, machining and labor costs. They're quick and easy to assemble and disassemble, and they do a better job of holding parts together. Truarc rings are precision engineered and precision made, quality controlled from raw material to finished ring.

36 functionally different types...as many as 97 different sizes within a type...5 metal specifications and 14 different finishes. Truarc rings are available from 90 stocking points throughout the U. S. A. and Canada.

More than 30 engineering-minded factory representatives and 700 field men are available to you on call. Send us your blueprints today...let our Truarc engineers help you solve design, assembly and production problems...without obligation.

For precision internal grooving and undercutting...Waldes Truarc Grooving Tool!



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TRUARC®

RETAINING RINGS

WALDES KOHINOOR, INC.
47-16 AUSTEL PLACE, L. I. C. 1, N. Y.

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Please send the new supplement No. 1 which brings Truarc Catalog RR 9-52 up to date.
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EO39

WALDES TRUARC Retaining Rings, Grooving Tools, Pliers, Applicators and Dispensers are protected by one or more of the following U. S. Patents: 2,382,948; 2,411,426; 2,411,761; 2,416,852; 2,420,921; 2,428,341; 2,439,785; 2,441,846; 2,455,165; 2,483,379; 2,483,380; 2,483,383; 2,487,802; 2,487,803; 2,491,306; 2,491,310; 2,509,081; 2,544,631; 2,546,616; 2,547,263; 2,558,704; 2,574,034; 2,577,319; 2,595,787, and other U. S. Patents pending. Equal patent protection established in foreign countries.

Want more information? Use post card on last page.

ELECTRONIC SLIDE RULE ILLUSTRATES SUPERIORITY OF BORG MICROPOTS

LOADING ERROR SOLVED BY BORG

Loading error, an important consideration in many potentiometer applications, has been solved by Borg.

LOADING ERROR DEFINED

Loading error is caused by current flow through the contact arm to a finite value of resistance (RL) connected to the output terminals of the pot. Ratio of total resistance of the pot to the load resistance determines the linearity error caused by the load. (Fig. 2).

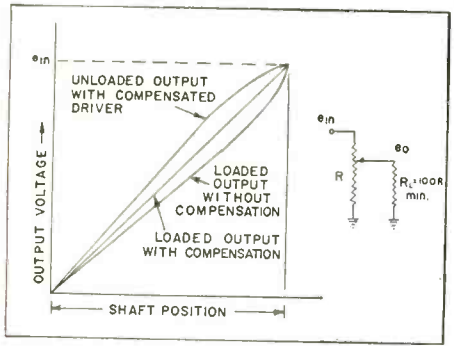


Fig. 2—Series resistance adjustment to minimize loading error.

PARTIAL REMEDIES

Fig. 2 shows a restriction of the usable portion of the pot to the relatively flat portion of the curve. This requires trimming resistors and at best makes use of less than ⅔ of the total rotation.

Another method is to tap the resistance wire at the point of maximum load error and make straight line approximations by use of a padding resistor (RP), Fig. 3. Load error is not entirely eliminated and the cost of the tap, selection and installation of the trimmer, is substantial.

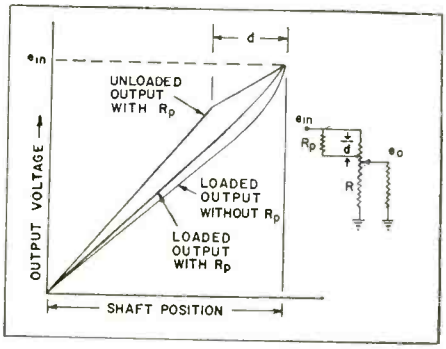


Fig. 3—Preloading to minimize loading error.

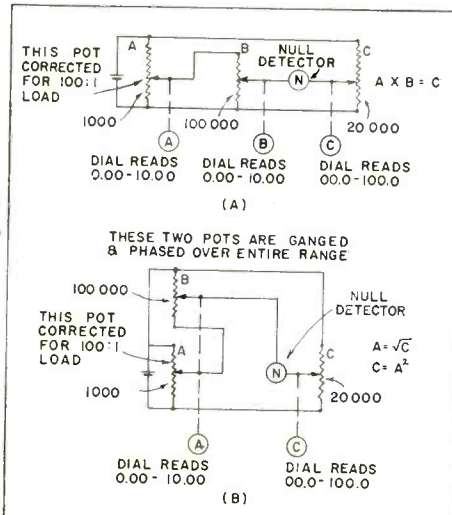


Fig. 1—Electronic slide rule for multiplication (A) and for squares and square roots (B).

THE ELECTRONIC SLIDE RULE

Electronic slide rule. (Fig. 1) was designed to illustrate this correction method in an actual application. It is not possible without two features found only in Borg's 900 Series, accurate load correction over the entire range of 0 to 100%, in pot A, and absolute linearity on all pots. The ganged assembly of pots A and B shown in (B) phased over entire range, illustrates another valuable feature of the Borg 900 Series Micropot Potentiometer.

THE BORG METHOD

The Borg method of eliminating load error is made possible by the design of the Borg 900 Series Micropot. Loading error correction is built into the potentiometer by means of an integral nonlinear actuator contact drive. It is computed to introduce motion equal in magnitude and opposite in sign to the error of a given load ratio. (Fig. 4).

This method provides accurate load correction over the entire range of 0 to 100% without trimming or tapping. Dual correction can be made when the application requires positive and negative values from a center tap.

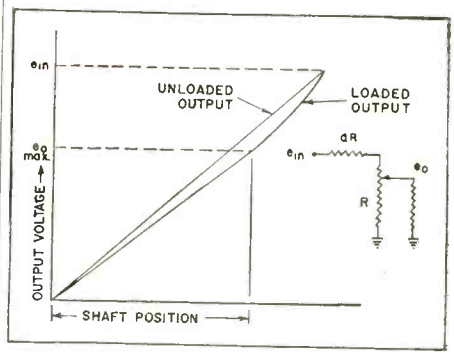


Fig. 4—Compensated drive to offset loading error, 100:1 ratio.

BORG 900 SERIES MICROPOTS ACHIEVE OPTIMUM PERFORMANCE

Borg has designed the 900 Series to achieve optimum electrical and mechanical performance and to meet the most severe environmental conditions while presenting to the equipment designer a highly flexible unit to fill a vast range of applications.

Write for complete engineering data
Catalog BED-A56

BORG EQUIPMENT DIVISION
THE GEORGE W. BORG CORPORATION
JANESVILLE, WISCONSIN

ELECTRONIC — MECHANICAL BORG EQUIPMENT *Built by Borg*

Square *RE-USABLE* Metal *Pad-Kaging* Containers

ELIMINATE majority of handling and storage problems

REDUCE shipping weights and cubic footage

These RE-USABLE Metal Pad-Kaging Containers were developed by PETERS-DALTON for the U. S. Armed Forces. They have been approved and are in use for shipping and storing innumerable items.

P-D Containers eliminate the storing of many cumbersome and highly inflammable materials—they also eliminate the excess labor usually required in packaging such items as delicate radar instruments. Older methods caused finished packages to be heavy and bulky. They were susceptible to breakage and penetration to moisture and fungus. They were wasteful because of their excessive use of man-hours and materials, culminated by the eventual scrapping of the expensive packaging. Also, when reshipping was required, old fashioned containers after having once been opened, were seldom satisfactory for adequate repackaging of the materials — endangering them to damage while in transit. These inadequacies and limitations have been virtually eliminated through P-D RE-USABLE Metal Shipping Containers.

★ ★ ★

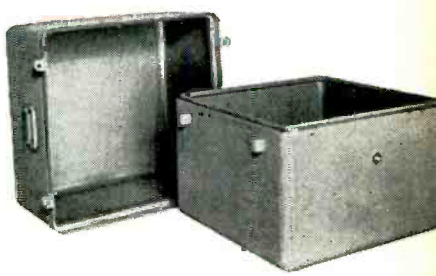
Features include: Lightness: Completed packs weigh far less than older style types. Compactness: The P-D RE-USABLE Metal Containers frequently save more than 50% of cubic footage. Economy: Material and man-hour outlays for packaging are reduced 25%.

Special Features: Containers are equipped with air fill valves to eliminate dangers of fungus or moisture and dial type humidity indicators. Drop handles furnished for containers weighing less than 200 lbs.—heavier containers have been designed for fork truck lifting. Extremely simple to close, only ordinary bolts (4 on the smallest container to 14 on the largest) are required; the simplest of hand tools perform the closing or opening operations. Optional: Pressure relief valves to equalize inside to outside pressures.

★ ★ ★

These RE-USABLE Metal Containers were manufactured by PETERS-DALTON for items ranging from aircraft engines, electronic parts, to large A-N containers in all types and sizes for shipping purposes. Complete engineering and manufacturing facilities are at your disposal for design, testing and fabricating. We'll be glad to tell you more—just write, wire or phone.

Materials formerly used in packaging one light military electronic item.



Only two parts to handle.

P-D Re-Usable Container ready to be closed and sealed. Note the simplicity of design.

STEEL SHIPPING CONTAINER DIVISION

PD Peters-Dalton INC.

A SUBSIDIARY OF DETROIT HARVESTER CO.

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- Industrial Washing Equipment
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Split Seconds

ELAPSED TIME . . . AS CLOSE AS 0.001 OF A SECOND

PRACTICALLY ALL Representative Manufacturing, Processing and Research Plants *USE* STANDARD PRECISION TIMERS

At one of the world's largest automotive manufacturers — timing test action in automatic transmission research.

At Eastman Kodak Co. — timing photo cell controlled exposures in automatic photo printing machine.

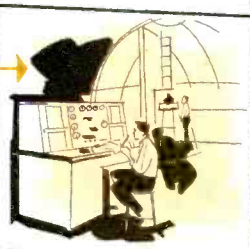
At Yucca Pass, Nevada Proving Grounds — helping maintain split-second control of atomic bomb tests.

It is our frank belief that literally hundreds of concerns have not yet scratched the surface of usefulness to which Standard Precision Timers can be put to work in their plants.

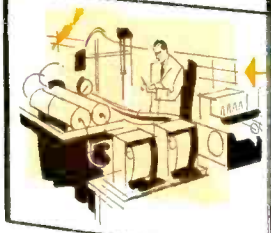
At General Electric Co. — Trumbull Division — measuring operating time of circuit breakers.

In Bell Telephone offices throughout the U. S. — timing elements required to complete telephone connections.

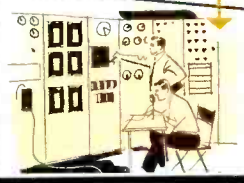
For Glenn L. Martin Co.'s Gunnery Trainer — in 12-channel Playback System designed by Cook Research Laboratories.



At American Brass Co. — indicating metallurgical analysis in Direct Reading Spectroscope developed by Baird Associates.



At Bendix — Westinghouse Research Dept. laboratories — measuring brake application and release time to 1/100th of a second.



Model	Scale Divisions	Totalizes	Accuracy
S-100	1/5 sec.	6000 sec.	±.1 sec.
S-60	1/5 sec.	60 min.	±.1 sec.
SM-60	1/100 min.	60 min.	±.002 min.
S-10	1/10 sec.	1000 sec.	±.02 sec.
S-6	1/1000 min.	10 min.	±.0002 min.
S-1	1/100 sec.	60 sec.	±.01 sec.
MST	1/1000 sec.	.360 sec.	±.001 sec.
MST-500	1/1000 sec.	30 sec.	±.002 sec.

World's most accurate and rugged time measuring instrument. Built in many different and advanced designs to meet practically every need of precision time measurement. Requires minimum maintenance.

Synchronous motor drive. Electric clutch controlled by manual switch, automatic switch or output of electronic tubes. Manual or electric zero reset.

SEND TODAY for Bulletin #198 describing entire line with partial list of thousands of customers, and summary of some of the most frequent (and some of the most unusual) ways they use STANDARD ELECTRIC TIMERS.

We suggest you check your requirements for Standard Timers and other products today. Your order or inquiry will receive prompt attention.

The STANDARD ELECTRIC TIME Co.
97 Logan St., Springfield 2, Mass.

Please send Bulletin 198 describing your line of instruments for measuring elapsed time as close as 0.001 seconds.

Name.....Title.....

Firm.....

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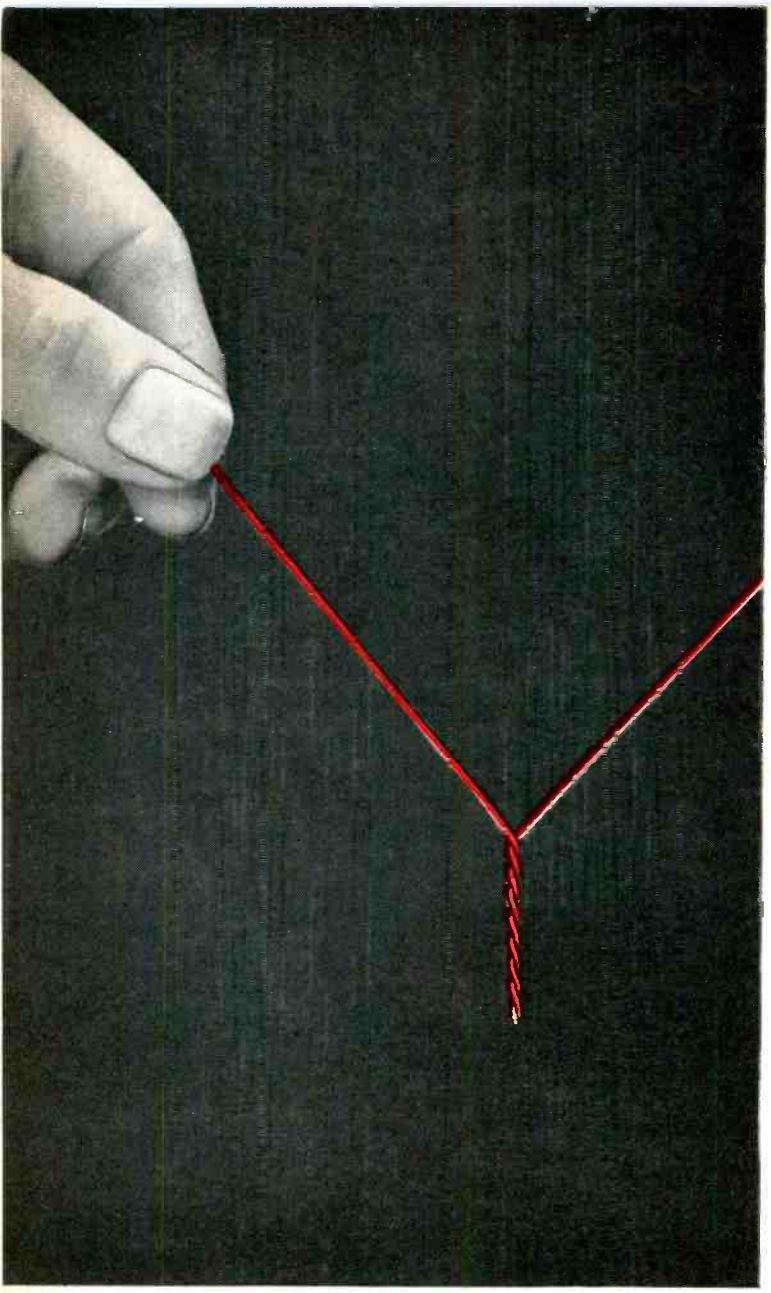
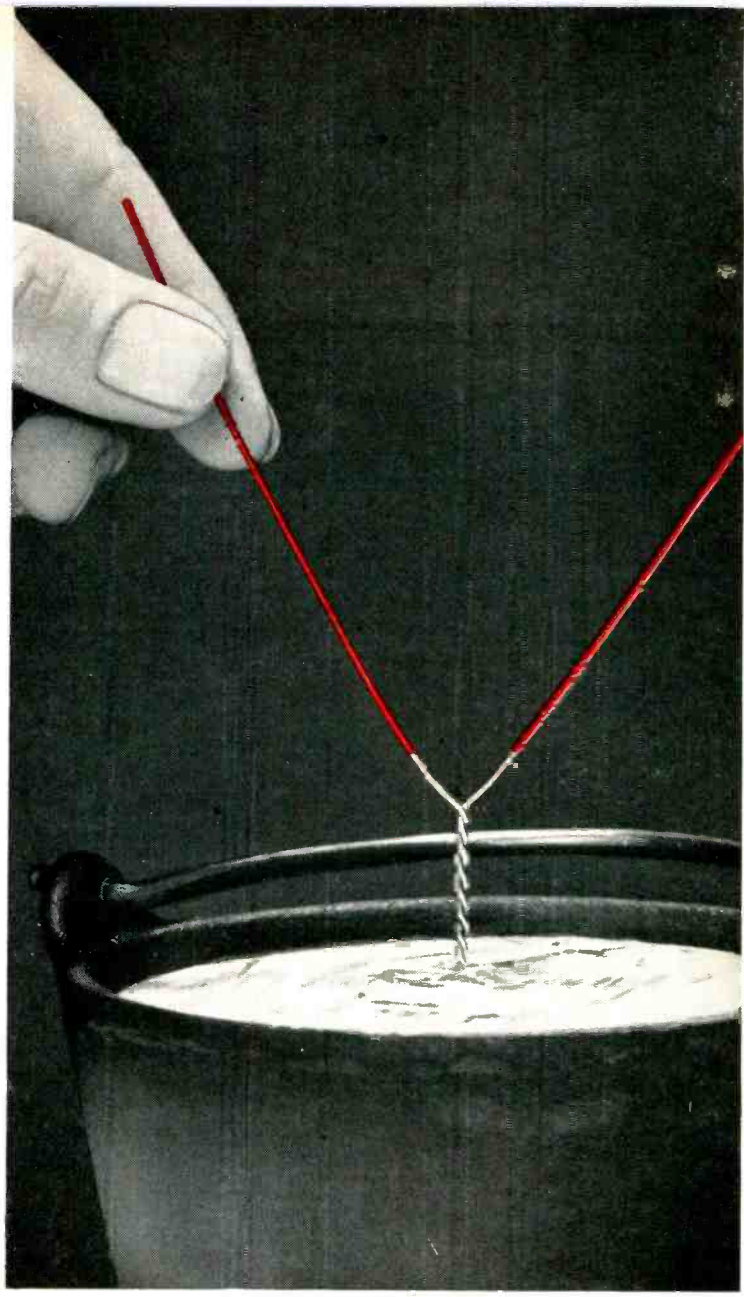


TWIST WIRES . . .



DIP IN SOLDER . . .

Anaconda announces Analac an improved

New Analac* film-insulated, solderable magnet wire can be used similarly to Formvar or Plain Enamel—except that it is solderable without stripping!

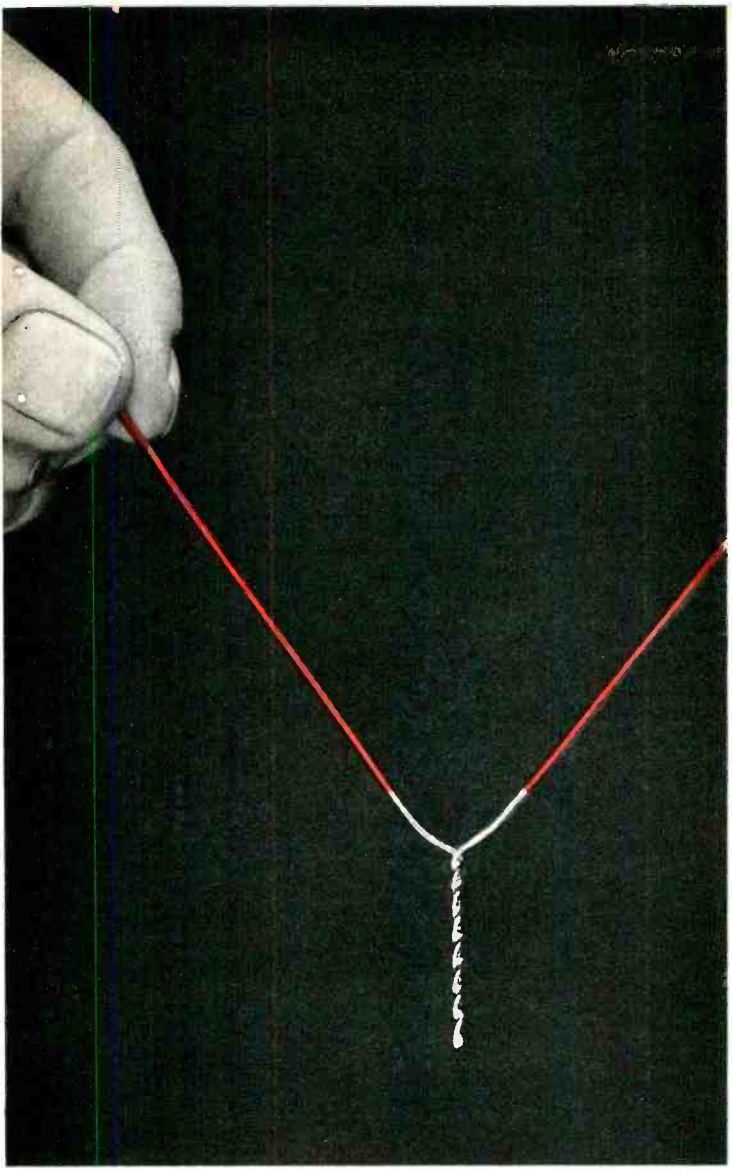
Soldering by dipping, iron or gun produces a perfect joint—in just one second in finer sizes—without prior removal of the insulation. Analac reduces labor, saves time and money wherever many soldered connections are made, or where small diameter wire makes other means of insulation removal hazardous to the insulation or wire.

Not only this, Analac has the excellent abrasion resistance and other good mechanical properties of the enamel wire you're now using. It handles readily, performs well in high-speed winding.

Analac is colored a bright red with stable dye used many years for identical applications—making it highly visible even in finest sizes. This helps operators feel more secure, results in higher quality work. Distinctive color simplifies its identification, too, from nonsolderable wires.

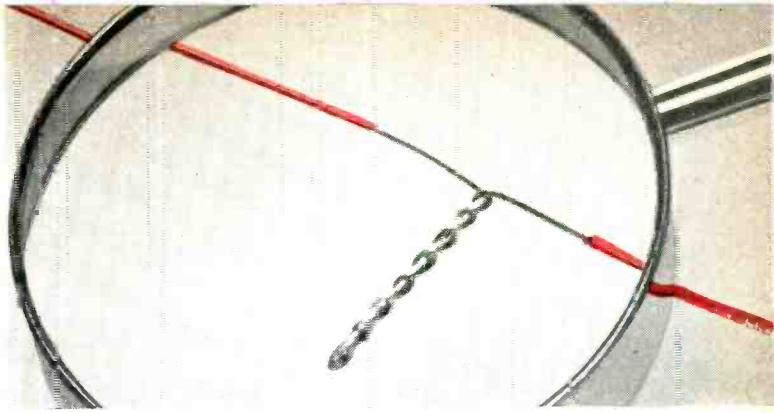
Analac is available in an exceptionally large range of sizes. The Man from Anaconda will be glad to give you more information and help with a production run in your plant. See "Anaconda" in your phone book—in most principal cities—or write: Anaconda Wire & Cable Company, Magnet Wire Headquarters, Muskegon, Michigan.

*Reg. U. S. Pat. Off. 57398

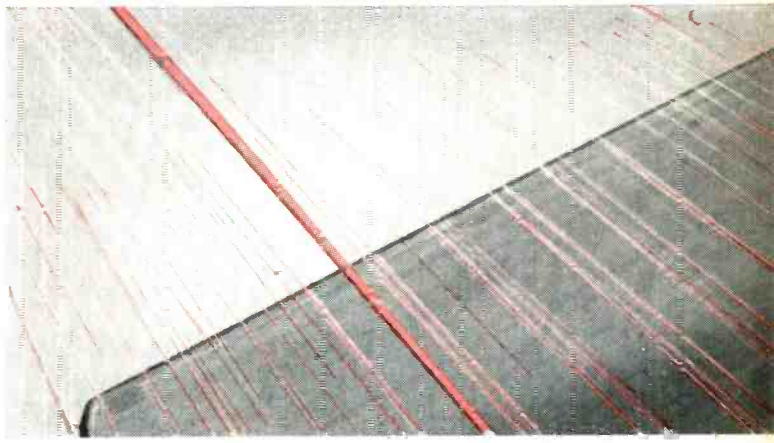


JOINT IS COMPLETED WITHOUT STRIPPING WIRE with Analac wire dipped in a 50-50 tin-lead solder at 360°C (680°F). The insulation is removed at the temperature of molten solder.

solderable magnet wire



1. STRONG JOINTS—as strong as the same joints made in bare copper wire—are produced. Here in laboratory test, joint holds under high stress.



2. EXCELLENT ABRASION RESISTANCE of Analac is shown in this test. It has the same high windability normally associated with Formvar, Plain Enamel.

3. MOLDED-PLASTIC CASES — designed and developed by Anaconda—protect spools of Analac from damage during shipping. Result: no breaks due to bent spools.

See the Man from

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Analac

magnet wire

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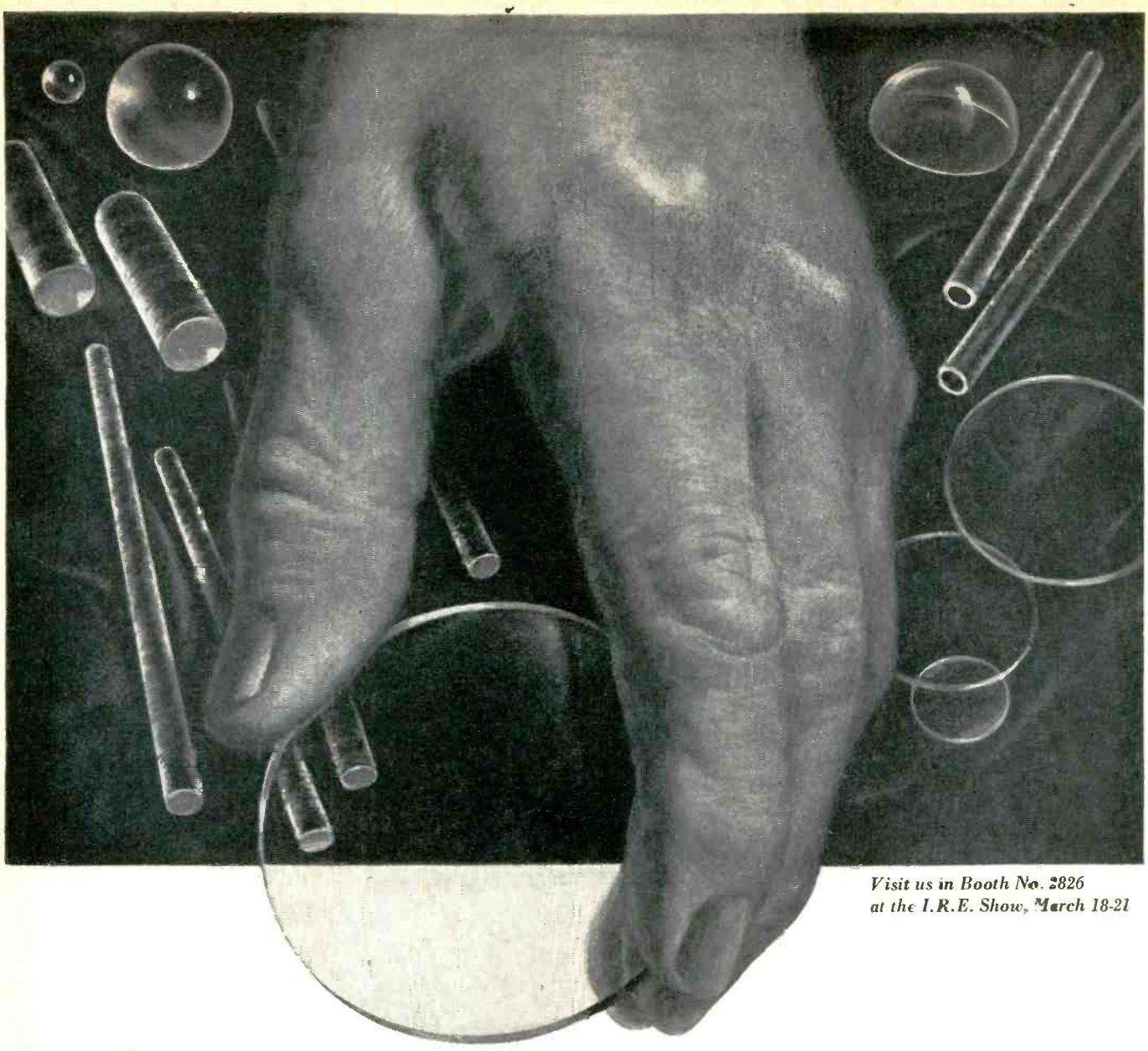

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LINDE sapphire is transparent, non-porous, and has excellent ultra-violet and infra-red transmission characteristics. Infra-red transmission is 92% at 3 microns, 50% at 6 microns (1 mm thickness). Typical uses are as windows, spacers, and supports in electronic tubes; for light pipes; and for ultra-violet and infra-red devices. High- and low-temperature seals can be made to metals as well as to glass and ceramics. Inquiries regarding mechanical, optical, thermal, and electrical properties of LINDE sapphire are invited. Write Crystal Products, Dept. BD-3.

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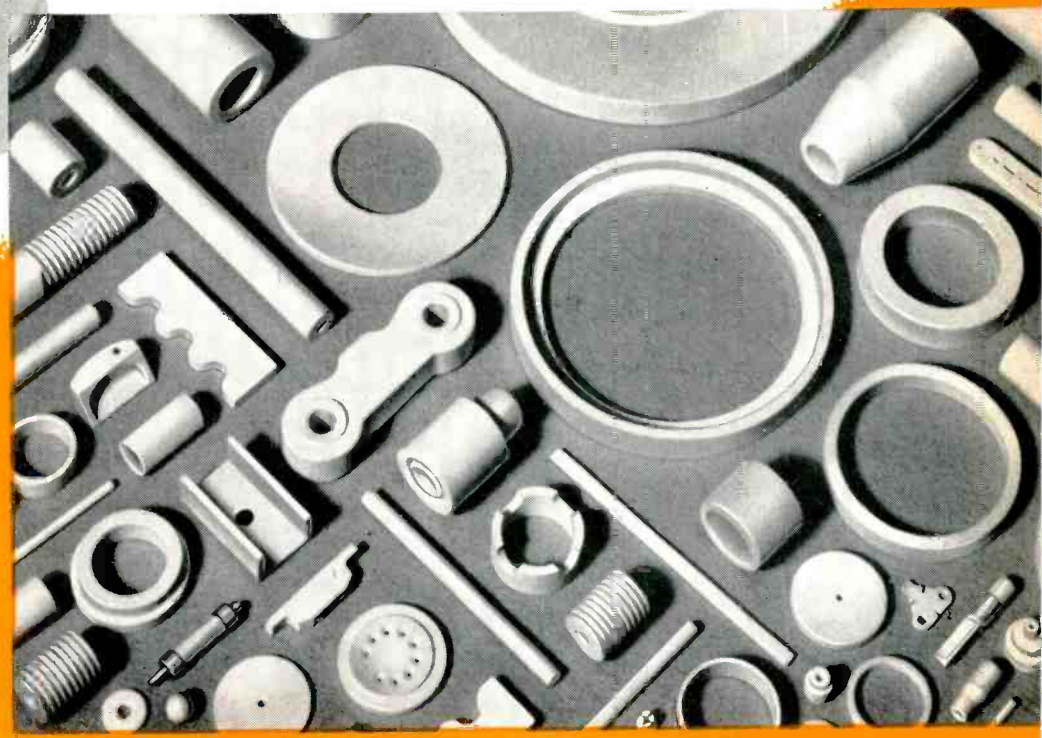
3 More experience. AlSiMag Aluminas are produced by skilled personnel, thoroughly familiar with the most modern methods . . . and highly specialized techniques perfected in over 55 years' experience in the manufacture of quality technical ceramics.

4 Dependable metal-ceramic combinations. Standard or custom designs available in volume. Wide choice of metals combined with strong, rugged Alumina ceramics. Permanent bonding. Close dimensional tolerances. High or low temperature types . . . for hard or soft solder.



For complete information on AlSiMag Aluminas, for your application, send blueprint or sketch with details of your operating procedure.

Ask for a free copy of Bulletin No. 562—AlSiMag Alumina Ceramics.

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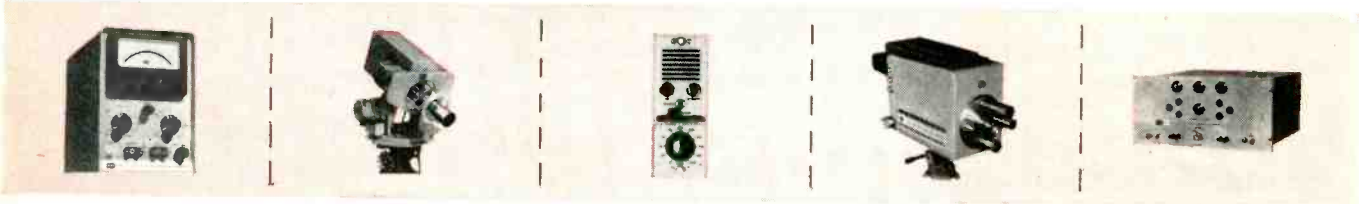

UNIVERSAL DC MICROVOLTMETERS

INDUSTRIAL TELEVISION EQUIPMENT

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BROADCAST TELEVISION EQUIPMENT

ABSOLUTE DC POWER SUPPLIES AND METER CALIBRATORS

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Want more information? Use post card on last page.

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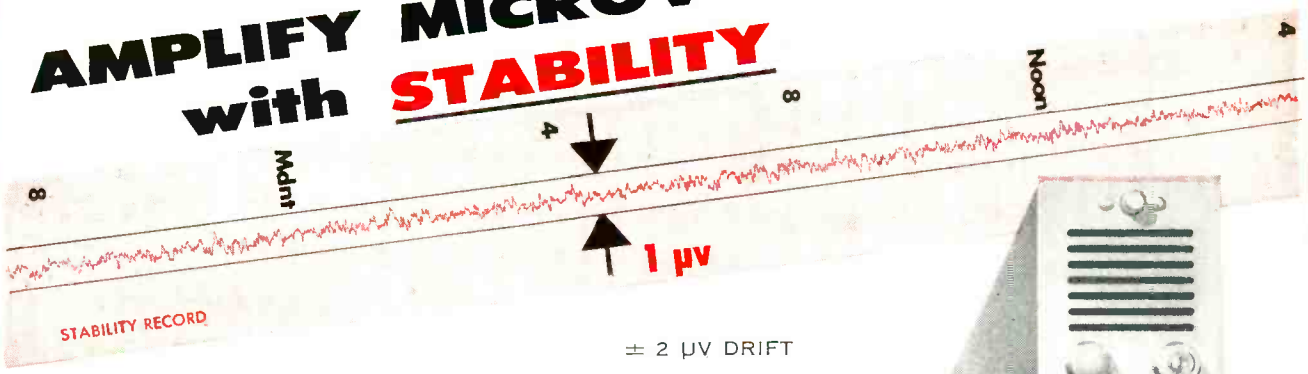
[KAY LAB]

FOR DRIFT-FREE DC INSTRUMENTATION

AMPLIFY MICROVOLTS with STABILITY



± 2 μV DRIFT

INTEGRAL POWER SUPPLY

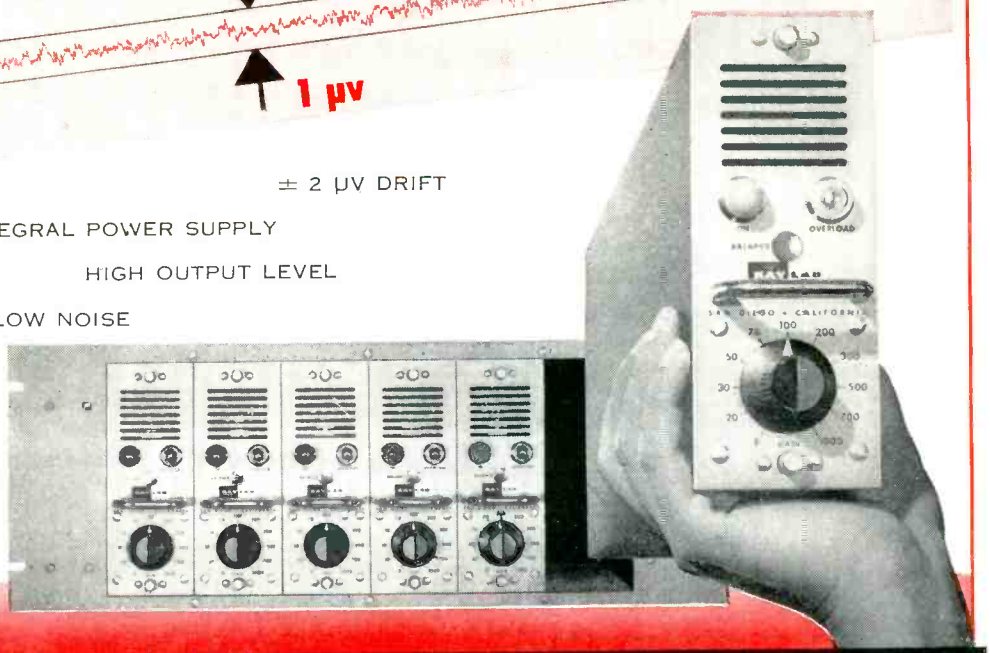
HIGH OUTPUT LEVEL

EXTREMELY LOW NOISE

BROAD BANDWIDTH

10 ACCURATE GAIN RANGES

HIGH INPUT IMPEDANCE



The **KINTEL** Model 111 amplifier provides maximum stability and the lowest drift of any commercially available broadband d-c amplifier. It is the end result of years of research in the field of chopper stabilized broadband d-c amplifiers. Thousands of **KINTEL** amplifiers are in daily use.
The Model 111 incorporates **KINTEL's** proven chopper amplifier circuitry and provides ten extremely precise, feedback controlled gain ranges. Several feedback loops assure high accuracy, stability and uniform frequency response. The completely new and unique circuit provides rapid recovery from severe overloading and unsurpassed dynamic performance—unaffected by load or gain changes.
The Model 111 is available in a single-unit cabinet or in a six-unit rack-mountable module. The amplifiers are extremely compact; the six-unit module occupies only a 19-inch rack width.
APPLICATIONS: The Model 111 is ideal for permanent low level d-c instrumentation, telemetering, or as a strain gage amplifier, transducer amplifier, scope preamplifier, recorder driver amplifier, or general purpose laboratory amplifier.

SPECIFICATIONS

Gain	0, 20, 30, 50, 70, 100, 200, 300, 500, 700, 1000
Gain Accuracy	± 1% DC to 2 KC
Input Impedance	100,000 Ω
Output Capability at DC	0 to ± 35 V where R_L > 1000 Ω 0 to ± 40 MA where R_L is 10 to 400 Ω
Output Impedance	Less than 1 Ω in series with 25 μh
Equivalent Input Drift	± 2 μv with regulated line
Equivalent Input Noise	0 to 3 cps, less than 5 μv peak to peak 0 to 750 cps, less than 5 μv RMS 0 to 50 kc, less than 12 μv RMS
Chopper Intermodulation	Less than 0.1%
Linearity	Better than 0.1% to 2 KC
Frequency Response	± 3% (0.3 db) DC to 10 KC, less than 3 db down at 40 KC

Power Requirements:	
Amplifier	117 V — 60 cycles — 70 VA
Cabinet	117 V — 60 cycles — 15 VA
6 Unit Rack Adaptor	117 V — 60 cycles — 45 VA
Dimensions: Amplifier Unit	2⅞" wide, 7⅝" high, 14⅝" deep
Rack Adaptor for 6 Units	19" wide, 8¾" high, 18¼" deep
Net Weight — Amplifier	11 pounds
PRICE: Amplifier Unit	$550.00
19-inch Rack Adaptor for 6 amplifier (with fans and connectors)	200.00
Cabinet for single amplifier (with fan and connector) is available.	

...the Standard in chopper-stabilized instruments

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MORE THAN 50 TRANSISTORS

CUSTOMER CONFIDENCE 10th ANNIVERSARY SEMICONDUCTOR PROGRESS

		PNP	NEW PNP	NPN	NEW NPN
GERMANIUM — ENTERTAINMENT	AUDIO PNP	2N186			
		2N186A			
		2N187			
		2N187A	2N319		
		2N188			
		2N188A	2N320		
		2N190	2N322		
		2N191	2N323		
		2N192	2N324		
		2N241			
		2N241A	2N321		
		2N265			
		*For new PNP			
		†For new PNP			
	IF NPN			2N168A	2N164A
				2N169	2N165
				2N169A	
				2N292	2N313
				2N293	2N314
	TETRODE NPN				3N31 (formerly ZJ-7-3)
GERMANIUM — INDUSTRIAL COMPUTER MILITARY	AUDIO PNP	2N43			
		2N43A			
		4JD1A17			
		2N44			
		2N45			
	COMPUTER PNP	2N123	2N123		
	COMPUTER NPN			2N78	
				2N167	
	SYMMETRICAL SWITCHING PNP (Formerly called Bilateral ZJ-20)	4JD1B3			
		4JD1B4			
	TETRODE NPN				3N29
					3N30
					3N31
	HIGH FREQ. AMPLIFIER NPN			2N78	
SILICON — INDUSTRIAL COMPUTER MILITARY	COMPUTER (TRADIC) NPN DCTL (Formerly ZJ-12)				4JD4A3
	HIGH FREQ. AMPLIFIER NPN (Formerly ZJ-12)				4JD4A2
					4JD4A4
					4JD4A5
	UNIJUNCTION (Formerly ZJ-14 Double Base Diode)				4JD5A1

FOLD OUT OPPOSITE PAGE FOR G-E RECTIFIER INFORMATION

The specification and rating data presented on the five preceding pages have been condensed to cover but a few basic design requirements. Detailed information concerning General Electric's full line of transistors and rectifiers may be obtained by contacting your nearest G-E Semiconductor Products district representative or by writing to:

GENERAL ELECTRIC COMPANY
Semiconductor Products Department
Electronics Park, Syracuse, New York

When writing for information, please specify by publication numbers the material desired.

TRANSISTORS

TYPES	PUBLICATION NUMBERS
ENTERTAINMENT	
2N186 thru 2N192 (PNP)	ECG-144
2N241A (PNP)	ECG-170
2N265 (PNP)	ECG-171
2N319 (PNP)	ECG-206
2N320 (PNP)	ECG-207
2N321 (PNP)	ECG-208
2N322 (PNP)	ECG-209
2N323 (PNP)	ECG-210
2N324 (PNP)	ECG-211
2N168A (NPN)	ECG-190
2N169A (NPN)	ECG-191
2N292 and 2N293 (NPN)	ECG-192
2N164A (NPN)	ECG-196
ENTERTAINMENT	
2N165 (NPN)	ECG-197
2N313 and 2N314 (NPN)	ECG-198
INDUSTRIAL/COMPUTER/MILITARY	
2N43 (PNP)	ECG-20B
2N43A (PNP)	ECG-76
4JD1A17 (PNP)	ECG-117
2N44 (PNP)	ECG-21B
2N45 (PNP)	ECG-22B
2N123 (PNP)	ECG-100
2N167 (NPN)	ECG-119
2N78 (NPN)	ECG-78A
Symmetrical Switching Transistor (PNP)	ECG-204

RECTIFIERS

Germanium Diffused Junction	ECG-59
Germanium Stacks	ECG-53B
Germanium High Temperature and Magnetic Amplifier	ECG-131
Germanium Medium Current	ECG-152
Silicon Low Current	ECG-134A
Silicon High Current	ECG-166A

TRANSISTOR MANUAL HAS THE FULL STORY

What they are—How they work—Where they are used

- **Principle of Semiconductors** . . . how electrons move through the transistor, and how the movement is directed.
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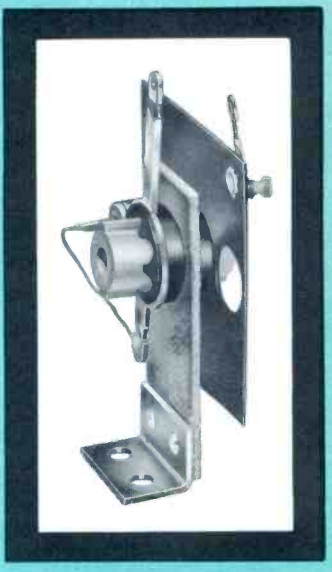
GERMANIUM JUNCTION RECTIFIERS

1N90 SERIES

The G-E types 1N91, 1N92 and 1N93 rectifiers employ the alloy principle for creating P-N junctions, a process developed by General Electric. High reliability is maintained by an all-welded, hermetically-sealed construction. The 1N93 is the commercial version of the G-E U. S. Navy approved USN-1N93 rectifier.

1N150 SERIES

The G-E 1N90 series rectifiers are single-cell units. The ratings of these units can be increased up to 5 times by the addition of a single copper fin. Single-fin rectifiers are represented by the General Electric types 1N151, 1N152 and 1N153. A two-fin rectifier—type 1N158—provides for increased voltage and current ratings with higher heat dissipation.



ABSOLUTE MAXIMUM RATINGS *(for 60 cycle, 55° C., resistive load)*

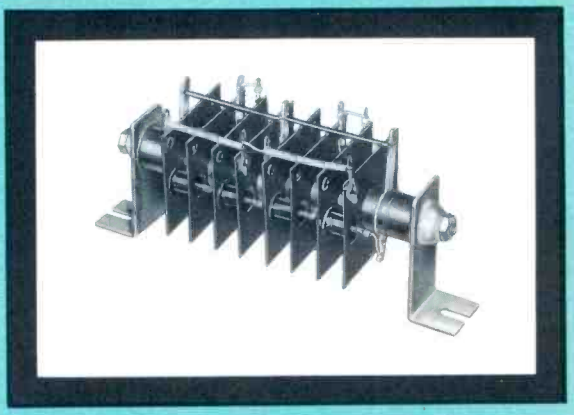
	1N91	1N92	1N93	1N151	1N152	1N153	1N158	
Peak Inverse Voltage	100	200	300	100	200	300	380	volts
D-C Output Current	150	100	75	500	500	500	500	ma
Full Load Voltage Drop	0.5	0.5	0.5	0.7	0.7	0.7	1.4	peak volt
Continuous Reverse Working Voltage	30	65	100	30	65	100	185	volts

GERMANIUM RECTIFIER STACKS

4JA211 SERIES

The G-E 4JA211 finned rectifiers may be arranged in stacks of up to twelve fins to produce over 160 different circuit combinations. Arranged in series or parallel, stacked rectifiers may be operated as half wave, full wave, bridge circuits, and many other types of single or polyphase circuits. A typical rectifier stack rating is listed below.

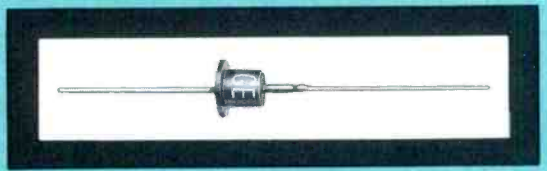
Note: Standard General Electric rectifier stacks are constructed with a new "ruggedized" mounting bracket which assures a vibration-free installation.



TYPICAL RATING

1φ Bridge — 3 amps, 188 V @ 55° C. — Free Convection Ambient

GERMANIUM HIGH TEMPERATURE RECTIFIERS



1N315, USAF-1N315, AND 1N368

The G-E Type 1N315 rectifier is specifically designed for high operating temperatures—up to 85° C.—and for low reverse current. This unit is ideal for use in magnetic amplifiers and other circuits where low leakage current is important. The 1N315 is Air Force approved and is supplied to the government per a military specification.

For magnetic amplifier applications, the G-E 1N368 junction rectifier is particularly adaptable. Featuring a very low reverse current at a high d-c reverse voltage, this rectifier is ideal for blocking applications.

SPECIFICATIONS *(Resistive or Inductive Load)*

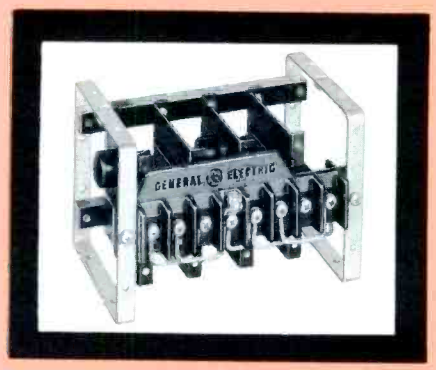
	1N315 and USAF-1N315			1N368	
	55° C	71° C	85° C	55° C	
Max. Allowable Peak Inverse Voltage	300	200	100	200	volts
Max. Allowable D-C Output Current	75	100	100	100	ma
Max. Full Load Forward Voltage Drop	.48	.46	.44	.48	peak volts
Continuous Reverse Working Voltage	150	100	50	150	volts (d-c)
Min. Forward/Reverse Current Ratio (1N315)	700	300	200		
Max. Leakage Current @ −150 V D-C (1N368)				300	μa

GERMANIUM MEDIUM CURRENT RECTIFIERS

4JA3011 SERIES

The General Electric 4JA3011 Medium Current Rectifier is available in cell PIV ratings of 100, 200 and 300 volts. Its extremely low power dissipation and forward voltage drop provide excellent efficiency and regulation, while its low leakage current meets exacting magnetic amplifier specifications.

G-E medium power rectifiers are available in stacks of up to 12 fins. Stacked in series or parallel, these rectifiers provide ratings in thousands of watts, depending upon the design of the circuit, and operate to over 100° C.



TYPICAL RATING

1φ Bridge 24 amps, 125 V @ 55° C. Free Convection Ambient

SILICON LOW CURRENT RECTIFIERS

1N536, 1N537, 1N538, 1N539 AND 1N540.

These silicon alloy junction low current rectifiers provide maximum forward conductance at high operating temperatures. A prime feature of the devices is the ability to carry high current loads without the use of any external heat sink. Also, units will solder directly into circuit for machine assembly.

	1N536	1N537	1N538	1N539	1N540	
Maximum Allowable Peak Inverse Voltage	50	100	200	300	400	volts
Maximum Allowable RMS Voltage	35	70	140	210	280	volts
Maximum Allowable D-C Output Current (at 150° C, ambient)	250	250	250	250	250	ma
Maximum Allowable D-C Output Current (at 50° C, ambient)	750	750	750	750	750	ma

SILICON LOW CURRENT RECTIFIER STACKS

4JA411 SERIES

A combination of high temperature operation (up to 150° C.) and increased power ratings (up to 18 amps) provides General Electric low current silicon rectifier stacks with sufficient circuit versatility to solve just about any rectifier design problem you may encounter. These silicon low current stacks offer the same Mil-approved bracket construction as our "ruggedized" germanium low current rectifiers (illustrated on opposite page.)

TYPICAL RATING

1φ Bridge 9 amps, 250 V @ 30° C. Free Convection Ambient

SILICON HIGH CURRENT RECTIFIER

4JA60 SERIES

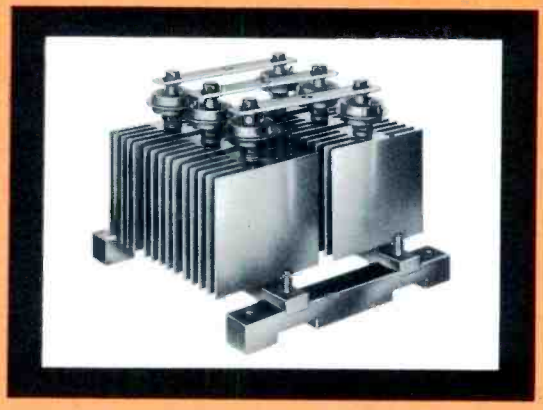
The 4JA60 is a large area junction silicon rectifier designed for power supply applications requiring d-c outputs as high as 85 amperes per rectifying element at rms input voltage up to 210 volts. A combination of extremely low forward voltage drop, minimum thermal impendance (1° D./watt—junction to stud), and a tapered pipe thread heat sink connection contributes to high allowable current ratings with very little external cooling required.

Versatility is increased by the availability of a negative polarity (stud is anode) unit, which facilitates construction of bridge circuits and permits the use of either a positive or negative heat sink in half-wave and center-tap applications.

RATINGS AND SPECIFICATIONS
(Resistive or Inductive Load, 60 cps)

	4JA60C	4JA60B	4JA60A	4JA60F
Maximum Allowable Peak Inverse Voltage	300	200	100	50
Maximum Allowable Rms Voltage	210	140	70	35

Maximum Allowable Forward Current . . . Depends on study temperature. See curves reverse side.
Maximum Allowable One Cycle Surge Current . . . 900 amperes.
Reverse Current . . . 50 ma @ max. PIV, 200° C junction temperature.
Operating Temperature . . . −65° C to +200° C (Limited by junction temperature of 200° C).
Storage Temperature . . . −65° C to +200° C.
All General Electric silicon rectifiers will meet rigid military mechanical specifications.



SILICON HIGH CURRENT RECTIFIER STACKS

4JA6011 SERIES By stacking the General Electric Type 4JA60 rectifiers, a device is created which will provide you with just about the best power-, inch-, pound-per-dollar values you'll find anywhere. These 4JA6011 series high current silicon rectifier stacks are small, lightweight, and powerful enough to give you an output of 76.5 kilowatts—without forced air cooling—from a volume of less than 1/3 of a cubic foot.

TYPICAL RATING

3φ Bridge 270 amps, 283 V @ 35° C. Free Convection Ambient

NEW POWER * UNIFORMITY PACKAGE DESIGN * *

Silicon high frequency transistors for DCTL switching applications and linear amplifiers up to 5 mc. Silicon unijunction transistors for bistable and monostable applications—can replace two transistors in many circuits. Symmetrical switching transistors—200 mw dissipation, controlled forward and inverse current gain—will efficiently switch large currents at high speeds.

More than 50 G-E transistor types to cover just about every application requirement. Nearly all G-E transistors are presented on this page—a line of devices that offers you the very latest in internal design and packaging techniques. Increased power, higher frequency and tightly controlled parameters for maximum circuit utility, make your selection of General Electric transistors a wise choice.

New G-E transistor cases eliminate tubulation and flange, for greater compactivity. The new NPN package lead arrangement provides for printed circuit plug-in use.

MAXIMUM RATINGS

TYPICAL VALUES

Maximum Collector Dissipation @ 25° C (mw) P_C	Breakdown Voltage Collector To Emitter (volts) BV_{CE}	Collector Current (ma) I_C	Maximum Junction Temp. (° C) T_j	D-C Current Gain h_{FE}	Alpha Cutoff Freq. (mc) $F_{\alpha b}$	Power Gain (db) G_e	Class B Power Output (mw) P_o	Collector Capacity ($\mu\mu$f) C_{ob}	Collector To Base Current I_{CO} @ V_{CB}	
75	—25	—200	85	24	.8	28	300	35	16	25
180	—25	—200	85	24	.8	28	750	35	16	25
75	—25	—200	85	36	1	30	300	35	16	25
180*	—25*	—200	85	36	1*	30	750	35	16	25
75	—25	—200	85	54	1.2	32	300	25	16	25
180*	—25*	—200	85	54	1.2*	32	750	35	16	25
75	—25†	—50	85	36	1*	39		35	16	25
75	—25†	—50	85	54	1.2*	41		35	16	25
75	—25†	—50	85	75	1.5*	43		35	16	25
100	—25	—200	85	73	1.3	35	300	35	16	25
180*	—25*	—200	85	73	1.3*	35	750	35	16	25
75	—25	—50	85	110	1.3	43		35	16	25
*200	*20				*3_{mc}					
	†—16									
							Freq. of G_e			
65	15	20	85	40	8	30	455 kc	2.4	5	15
55	15	20	75	72	4	26	455 kc	2.4	5	15
55	25	20	75	72	5	26	455 kc	2.4	5	15
65	15	20	85	25	5	26	455 kc	2.4	5	15
65	15	20	85	25	8	30	455 kc	2.4	5	15
50	$7V_{CB}$	20	85		15		15 mc	3.1	25	7
150	—20	—50	100	50	1		1 kc	40	15	45
150	—20	—50	100	50	1		1 kc	40	15	45
150	—20	—50	85	40	1		1 kc	40	16	45
150	—20	—50	100	22	1		1 kc	40	15	45
150	—20	—50	100	12	1		1 kc	40	15	45
100	—15	—125	85	50	8			15		
65	15	20	85	40	8		500 kc	2.4	5	15
65	30	75	85	36	8			4	1.5	15
200	—30	1A	85	15-15	.8			45	20	30
200	—30	1A	85	20-20	.8			45	20	30
50	$7V_{CB}$	20	85		40	10 G_b	30 mc	4.2	25	7
50	$7V_{CB}$	20	85		80	10 G_b	120 mc	5	25	7
50	$7V_{CB}$	20	85		20	10 G_b	15 mc	3.1	25	7
65	15	20	85	40	8	30	500 kc	2.4	5	15
150	10	20	150		25			14	.15	5
150	15	20	150	14	25	15	5 mc	14	.15	5
150	15	20	150	15	25	33	1 kc	14	.15	5
150	15	20	150	40	25	36	1 kc	14	.15	5
P_{BB}	V_{BB}	I_E	T_J			$\frac{V_{B2}}{V_p}$			I_{EO}	
250	45	50	150			2			50	45

FOLD OUT PAGE FOR G-E RECTIFIERS

COMPUTERS AND PROCESS CONTROL discussed by *Eric Weiss*

The application of digital computers to the direct control of processes brings up these two questions: (1) Can the control functions be properly formulated? (2) Can computers be made reliable enough?

Speed is no problem. Today's memory developments offer practically instantaneous access. A 50 kc or 100 kc serial computer is fast enough to satisfy most control operations. When this is not fast enough, the overall speed can easily be increased one or two orders of magnitude through the use of a parallel machine.

There is another way of speeding up a computer. Rather than build a general purpose machine which can compute any problem we like to code into it, special purpose computers can be designed and built for special jobs. The same proven elements would be utilized, but would be arranged in different arrays in order to come up faster and more directly with the desired solution. The resulting machine would most likely do the job faster without actually increasing the repetition rate.

The problem of reliability is not so easily disposed of. In the past, digital computers were primarily used as mathematical tools to compute lengthy mathematical problems or to process repetitive data. If a computer made an error once every billion operations (which at the rate of 100 kc would be every three hours), it was not too serious. The error was caught and the problem, at the worst, computed again.

The moment we start thinking about a computer in direct control applications, the problem becomes more critical. If the computer controls some sort of manufacturing or chemical process, a single error at the wrong time in the wrong spot can be catastrophic. Under such circumstances, an error probability of 1 in a billion cannot be tolerated. An almost errorless operation is required.

Most digital computers presently in production have a large number of hot vacuum tubes. These are the least reliable elements in a computer. Their filaments burn out; envelopes leak; or various fragile elements short.

During the last decade, a series of solid state elements has been developed which make it feasible to build a computer without vacuum tubes or moving elements. The diode, the transistor, the magnetic amplifier, the magnetic core and several other elements in this class can be expected, unless abused, to live and operate without mistakes practically indefinitely. Furthermore, they are considerably smaller, lighter, and less power consuming.

Consider a flip-flop, for example. Utilizing vacuum tubes, a flip-flop consists of at least a double triode, several crystal diodes, resistors, capacitors, plus the necessary hardware to mount the same. Such an assembly normally occupied the same space as a king-size package of cigarettes, and the required accessory equipment, such as power supply or air conditioning, occupied a similar space. In contrast, a transistor flip-flop could be packaged in a volume of the size of a peanut shell with the corresponding power supply even less. The power consumption is so minute that the unit can be potted and it is quite likely in the near future a whole computer could be potted.

Eric Weiss, nationally-recognized authority on computer philosophy and design, discusses the use of digital computers in process control.

The major obstacle to the use of computers in control applications is the lack of understanding of the processes which are to be controlled. A scientist can play with a general purpose computer in a control system. He can code it by trial and error. Once the formulae have been determined, a special purpose computer that would be smaller, faster, and more efficient, can be built to control the process.

By applying the latest proven techniques, our well-qualified staff at Daystrom Systems is prepared to take single responsibility of assembling and installing a system to meet your needs. We are currently compiling a file of new applications and papers on various parts of systems, both industrial and military. If you are interested in receiving the file and periodic additions, please write us.

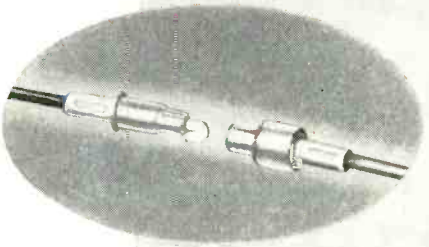
HUBBELL *Interlock* PLUGS

TRADE MARK

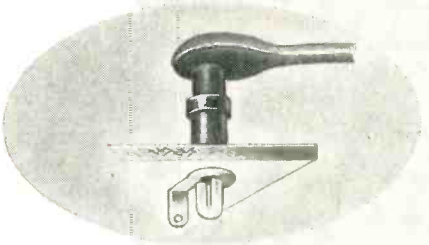
Stay Locked IN ACTION!

Won't Disconnect Accidentally . . .
Yet Disconnect Quickly When Intended

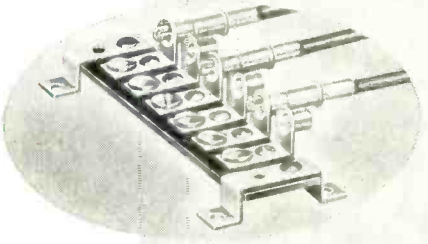
Today's engineers ask more of the connectors they use than simply that they make contact. Computers and modern, automatic machinery require *constant, positive* connections . . . aircraft wiring must be vibration proof and unaffected by temperature changes . . . printed circuits need sub-miniature connectors that will remain fixed. Hubbell *Interlock* Connectors are designed with all these features — and more! Whether they're used for connecting wire to wire, wires to panels, or wires to terminal strips, the combination of *Interlock* plugs and eyelets or plugs and jacks provides *automatic locking, quick disconnect* wiring that assures constant low contact resistance. Contact is maintained by a coil spring that adjusts for temperature and pressure changes and is part of the disconnect mechanism that permits fast rearrangement of circuitry and ease of maintenance.



Wire to Wire



Wire to Panel



Wire to Terminal Strip

TYPE "A" PLUGS, JACKS AND EYELETS Nylon Insulated and Non-Insulated. Current Capacity: 10 amps. Wire Sizes: #14 to #18

TYPE "B" PLUGS AND JACKS Nylon Insulated and Non-Insulated. Current Capacity: 5 amps. Wire Sizes: #18 to #22

TYPE "A" ANGLE PLUGS AND DOUBLE ENDED JUMPER CORDS Current Capacity: 10 amps.

TYPE "C" SUB-MINIATURE PLUGS AND EYELETS Current Capacity: 1 amp. Wire Sizes: #20 to #22 or smaller

TYPE "S" PLUGS AND JACKS Nylon Insulated. Current Capacity: 15 amps. Wire Sizes: #14 to #18

TYPES "A" AND "B" LAMINATED TERMINAL STRIPS AND TYPE "B" FLEXIBLE TERMINAL STRIPS

IT PAYS TO HAVE HUBBELL GOOD CONNECTIONS

HARVEY HUBBELL, Inc.

Interlock Electronic Connector Dept.,

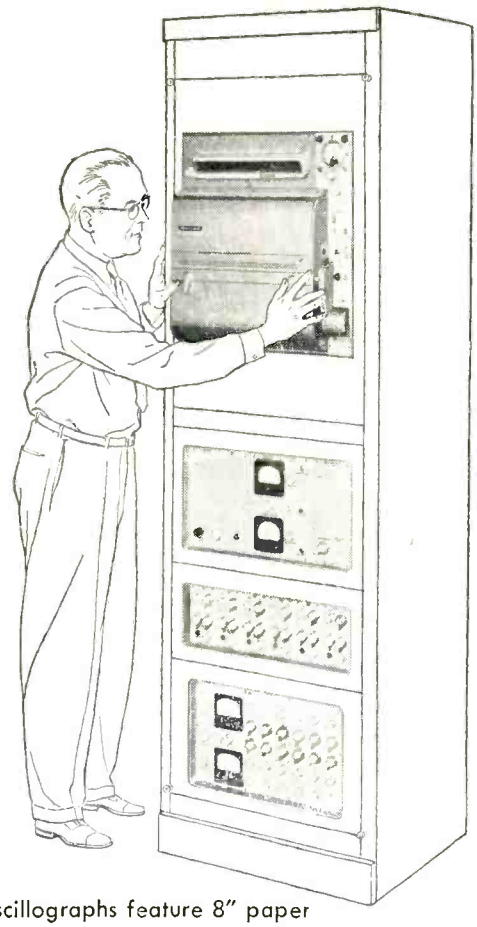
Bridgeport 2, Conn.

SELF-LOCKING HUBBELL CONNECTORS

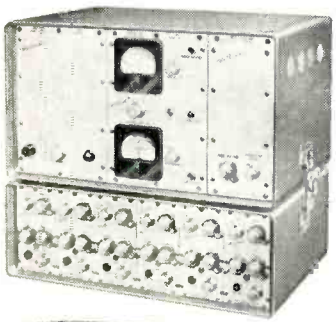
The HEILAND Dynamic Recording System gives you more...

- *VERSATILITY*
- *PERFORMANCE*
- *EASE OF OPERATION*

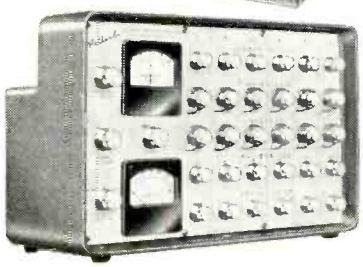
FOR TABLE, MOBILE, OR RELAY RACK MOUNT



Oscillograph● The Series 700C oscillographs feature 8" paper width with 1–36 channels, or 12" paper width with 1–60 channels. Available for 23 v.d.c. or 115 v.a.c. operation, the 700C Series has paper speeds adjustable from .030 to 144"/sec., and writing speeds in excess of 20,000"/sec. Separate supply and take-up drums are light-weight—and light tight for easy daylight loading.
For details and specifications, write for Bulletin 701-NK



Amplifier● The Heiland 119 Amplifier System offers up to 6 channels, in any combination, of either linear-integrate amplifiers or carrier amplifiers. Carrier amplifier channels provide linear frequency response from 0 to 1000 CPS, for resisitive, linear differential transformer, or variable reluctance type transducer inputs. Linear-integrate amplifier channels provide linear frequency response from 5 to 3000 CPS for self-generating transducers. Provides high-amplitude recording up to 8" peak to peak deflection.
For details and specifications, write for Bulletin 101-NK



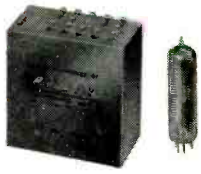
Bridge Balance● The Heiland 82-6 Bridge Balance and Strain Indicator Unit provides a simple and accurate means of balancing, calibrating and measuring static and dynamic phenomena from resistive-type transducers where you don't need amplification. When used as a strain-indicating device without an oscillograph, an input of 25 microamperes produces full scale on the indicating meter.
For details and specifications, write for Bulletin 101-NK

For versatility, performance, and ease of operation, choose the Heiland dynamic recording system

MINNEAPOLIS **Honeywell**

HEILAND INSTRUMENTS

5200 EAST EVANS AVENUE • DENVER 22, COLORADO



MEET THE

MIGHTY MIDGET

OF AIRCRAFT FIRE POWER

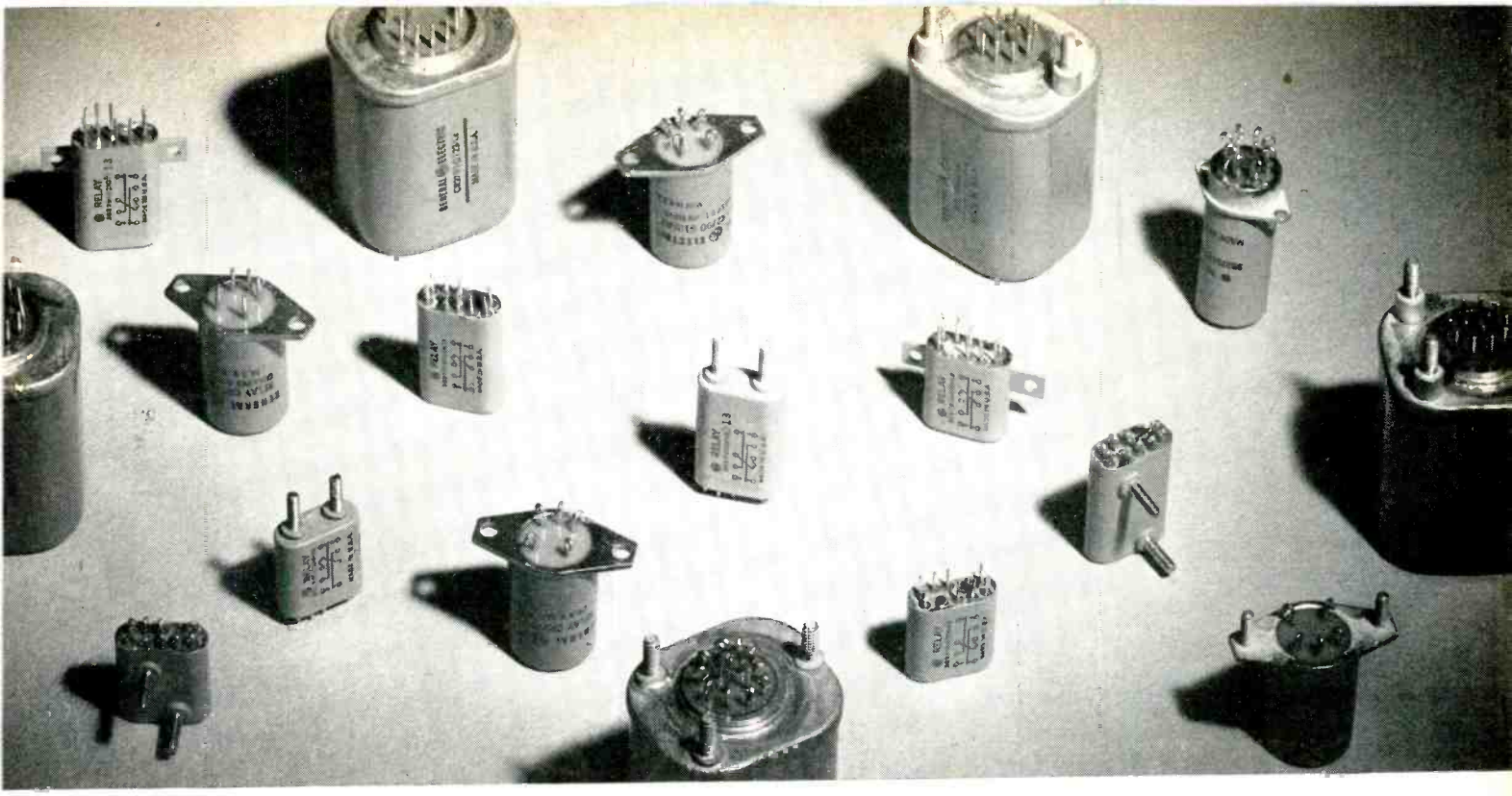
This new TRANSISTORIZED CONTROL AMPLIFIER weighs only 11 ounces...but it is a vital control element in the voltage regulation of an entire aircraft fire control system. Developed as part of an integrated power supply, the "MIGHTY MIDGET" operates from −55° to +125° C...reduces ripple to less than 50mv peak-to-peak...is adaptable to voltages of ±50 to ±1000...controls voltage regulation to ±1%. Here is another example of Packard Bell's skill in developing lighter, more efficient airborne equipment... another result of more than 30 years of electronic leadership.

See it at the New York IRE SHOW... booths 3705–3707.

PACKARD BELL ELECTRONICS

TECHNICAL PRODUCTS DIVISION

Los Angeles 64, California



NOW . . . ONLY 3-WEEK SHIPMENT* on General Electric's full-line of sealed relays

Improved production techniques now make it possible for General Electric to offer its complete line of standard-listed hermetically sealed relays—including the amazing micro-miniature—*on only 3-week shipment from order date!*

And, what's more—General Electric is equipped to provide you rapid service on samples and prototypes.

FOR ALL ELECTRONIC SYSTEMS

G-E miniature, sub-miniature, and micro-miniature relays combine small size with unusual reliability under severe temperature, shock, and vibration conditions—making them ideal for all radio, radar, fire control, navigational equipment, and industrial electronics jobs.

Though initially designed for military applications, more and more G-E sealed relays are being used for industrial jobs. Their extreme reliability and small size now are utilized by industrial designers. Resistance welding and other industrial electronic circuitry is being simplified and miniaturized with G-E sealed relays.

WIDE RANGE OF COIL RATINGS, HEADER TYPES, AND MOUNTINGS

Whatever your small sealed relay needs —you'll find the answer with one of the many forms of these three models:

Miniature: Standard, current-sensitive, and voltage-sensitive models; in 2-, 3-, or 4-pole double-throw and 6-pole normally open forms. Rated 5 amps at 28 volts d-c at 85C. 3-amp make-before-break forms and 125C forms available.

Sub-miniature: 2 amps; .651 in. in diameter, 1.6 in. long; weighs one ounce. Unaffected by vibrations of 10 to 55 cps at .12 in. maximum excursion or 55 to 500 cps at 15Gs acceleration. Withstands shock tests in excess of 40Gs. Operates in ambients of 125C.

Micro-miniature: Weighs only 0.5 oz., measures .36 in. by .80 in. by .88 in. Rated 2 amp resistive at 28 v d-c or 115 v a-c. Also available in current-sensitive models. Standard relays withstand ambients of 125C and 20Gs acceleration at 50 to 500 cps. *Contact your G-E Apparatus Sales Office, or mail coupon. Specialty Control Dept., Waynesboro, Va.*

**Average shipment time for all standard listed relays. Actual time: MICRO-MINIATURE (up to 100 units—2 weeks, 100 to 1000 units—4 weeks); SUB-MINIATURE (up to 100 units—3 weeks, 100 to 1000 units—5 weeks); MINIATURE (up to 100 units—1-2 weeks, 100 to 1000 units—3 weeks).*

MAIL TODAY FOR G-E RELAY DATA

General Electric Co., Sect. A 792-6, Schenectady 5, N. Y.

- ☐ Miniature—Bulletin GEA-6213
- ☐ 2PDT Sub-miniature—Bulletin 6412
- ☐ Micro-miniature—Bulletin 6346
- ☐ HAVE G-E SALES ENGINEER CALL

NAME .....

COMPANY .....

ADDRESS .....

CITY ..... STATE .....

GENERAL ELECTRIC

Each pound of reduced weight is worth something to you. The new Bendix Pygmies reduce connector weight drastically. These miniature aluminum connectors are for compact electronic equipment and aircraft use. Contacts are size 20 heavily gold-plated, featuring machined closed entry sockets. Choice of quick disconnect coupling between a modified double stub thread or 3 point bayonet lock. Provisions for grommet sealing, potting, cable sealing, conduit applications.

Bendix "Pygmy" Connectors weigh less, take up less space than Standard AN Connectors. Think of the advantages!

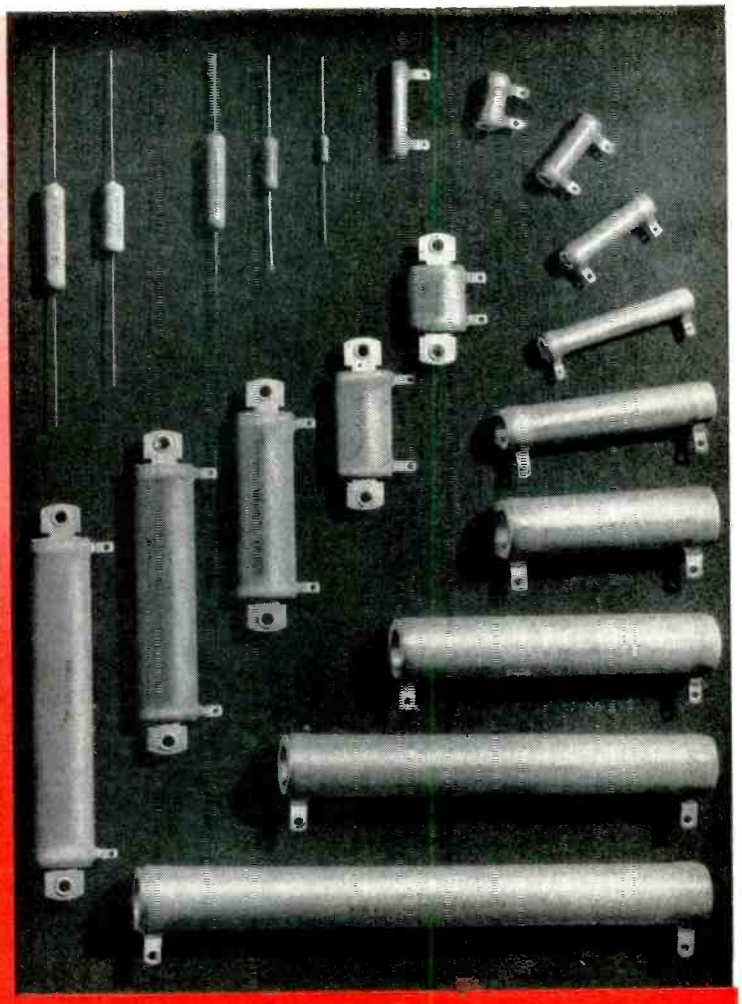
Available in a wide variety of shell styles and insert arrangements. Shell sizes range from $\frac{3}{8}$" I.D. to $1\frac{3}{8}$" I.D. and incorporate from 1 to 55 contacts. Write Dept. PC for descriptive literature on this dramatic improvement in Aviation Electronics.

Avnet

AVNET EASTERN SALES, 36 N. MOORE ST., NEW YORK 13, N. Y. BEEKMAN 3-5780 (AVNET ELECTRONIC SUPPLY CO., INC.)
AVNET WESTERN SALES, 8966 NATIONAL BLVD., LOS ANGELES 34, CAL. TEXAS 0-7950, VERMONT 7-1461 (AVNET CORPORATION)

Now!

Vitrohm MIL-R-26C Resistors *in all styles!*



Famous Ward Leonard Vitrohm® vitreous-enameled resistors are now available in every style to meet all requirements of Military Specification MIL-R-26C including the severe bogeys on moisture resistance, thermal shock, insulation resistance and many other properties.

What's more, this line offers you *all* characteristics—G, V, and the exacting Y—and *all* specification sizes and resistance values—even the highest values using the finest wire (0.00175" dia.) permitted by the spec.

Tab-terminal, axial-lead and stack-mounting types are available in styles and characteristics shown in table.

For complete data on these MIL-R-26C resistors, write us for Bulletin 12. (And incidentally, for Vitrohm resistors to *highest commercial and industrial standards*, get W/L Catalog 15.) Ward Leonard Electric Co., 31 South Street, Mount Vernon, N.Y. In Canada: Ward Leonard of Canada Ltd., Toronto.

ENGINEERING DATA

TYPE	STYLE	AVAILABLE IN CHARACTERISTICS	RESISTANCE RANGE
Stack Mtg.—Tab	RW20 thru 24	G	All values in Spec.
Tab terminal	RW29 thru 47	V, Y* and G	All values in Spec.
Axial lead	RW55 thru 59	V and G	All values in Spec.†

*Characteristic Y applies to styles RW30, 33, 37 and 47 only. Characteristic Y is similar to V but requires high insulation resistance at end of moisture-resistance tests.

†Maximum values for single-layer-wound resistors with 0.00175" diameter wire.

LIVE BETTER...*Electrically*

7.7

WARD LEONARD ELECTRIC COMPANY
MOUNT VERNON, NEW YORK

RESISTORS · RHEOSTATS · HEATS · CONTACTS · DIMMERS

Result-Engineered Controls Since 1892

What's YOUR Electronic

Solderability?...

Temperature?...

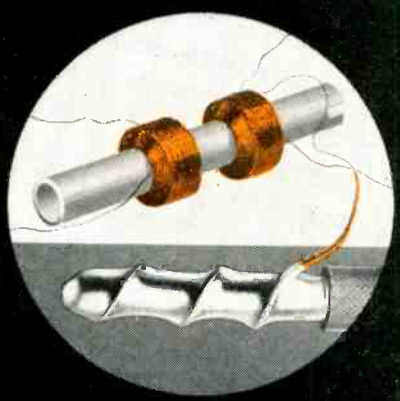
Unusual Shapes?...

Space?...

Here are five proven solutions to

THERMALEZE

A Class "B" 130 C epoxide-polyester film wire for higher temperature windings.



SODEREZE

A polyurethane-coated wire—solders at low temperature—without stripping!

ENAMEL

Modern black enamel with uniform O.D., high tensile for layer-wound coils.

First for Lasting Quality—from Mine to Market!

Visit Our Booth, No. 4516-4518, at the I.R.E. Show, March 18-21

Coil Problem?...

Phelps Dodge can supply the right answer to your particular magnet wire problem from its complete, up-to-date line. The products shown here have varied electronic applications. These magnet wires are the result of Phelps Dodge research and development of new materials, combined with practical experience in application engineering.

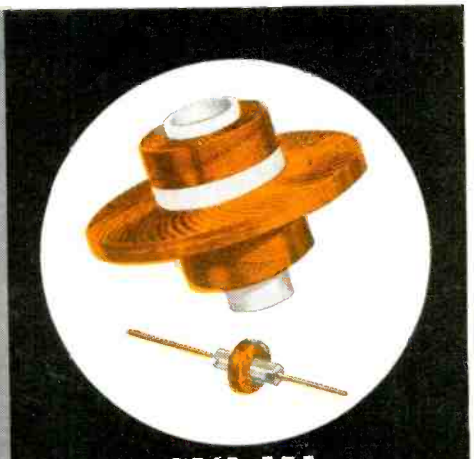
The complete line of Phelps Dodge magnet wire includes:

Enamel • Formvar • Sodereze® • Bondeze® • Thermaleze® • Grip-eze® • Sylkyd
Daglas® • Daglas® Silicone • Paper • Cotton • Multiple Combinations

lower-cost electronic coils

BONDEZE

Self-bonding wire for turn-to-turn bonding in unusual shaped coils, bobbinless coils, yoke coils, etc.



GRIP-EZE

Controlled friction solderable film wire for winding universal lattice-wound coils, fly-back coils, choke coils, etc.

Wire packaged in Phelps Dodge special "Pakeze" containers if required.

Any time magnet wire is your problem, consult Phelps Dodge for the quickest, easiest answer!

PHELPS DODGE COPPER PRODUCTS CORPORATION

INCA MANUFACTURING DIVISION

FORT WAYNE, INDIANA

Want more information? Use post card on last page.

NOW: available on a

For engineering evaluation of thermistor and varistor characteristics, you can now obtain any of 37 individual test kits, each containing six pieces. The minimum quantity per order is three kits. Shipment will be made postpaid to any destination in the United States and Canada.

Globar® THERMISTORS

To evaluate thermistor circuit applications for:

1. Temperature compensation.
2. Time delay.
3. Temperature sensing and control.

Test Kit No.	Type	Body Size		R at 25° C ± 20%	Nom. Temp. Coeff. "B" Constant	Max. Watt Loading at 40° C	Price
		Length	Dia.				
T-1	997F	19/64"	7/64"	40 ohms	1500	0.25	$3.95
T-2	997F	19/64"	7/64"	220 ohms	1750	0.25	3.95
T-3	997F	19/64"	7/64"	10000 ohms	1950	0.25	3.95
T-4	763F	5/8"	7/32"	5 ohms	1200	0.5	3.70
T-5	763F	5/8"	7/32"	10 ohms	1400	0.5	3.70
T-6	763F	5/8"	7/32"	15 ohms	1500	0.5	3.70
T-7	763F	5/8"	7/32"	20 ohms	1500	0.5	3.70
T-8	763F	5/8"	7/32"	120 ohms	1700	0.5	3.70
T-9	763F	5/8"	7/32"	1000 ohms	1800	0.5	3.70
T-10	763F	5/8"	7/32"	10000 ohms	2100	0.5	3.70
T-11	763F	5/8"	7/32"	120000 ohms	2150	0.5	3.70
T-12	763F	5/8"	7/32"	330000 ohms	2150	0.5	3.70
T-13	416H	1/16"	5/16"	1200 ohms	3800	0.5	3.95
T-14	479H	1/8"	1/2"	1000 ohms	3800	1.5	3.95
T-15	373H Metallized Faces Only	1/8"	3/4" o.d. 1/4" i.d.	10 ohms	2700	3.5	4.55
T-16	373H Metallized Faces Only	1/8"	3/4" o.d. 1/4" i.d.	40 ohms	2700	3.5	4.55
T-17	343H	1/8"	3/4" o.d. 1/4" i.d.	5.5 ohms	2700	3.5	4.85
T-18	343H	1/8"	3/4" o.d. 1/4" i.d.	20 ohms	2700	3.5	4.85
T-19	549H	3/4"	7/64"	5000 ohms	3200	0.75	3.95
T-20	588H	1"	7/64"	11000 ohms	3200	1.	4.25
T-21	763H	5/8"	7/32"	500000 ohms	4600	0.5	3.95

Globar® THERMISTORS

For evaluation of surge current suppression in series filament and pilot light circuits in radio and television receivers.

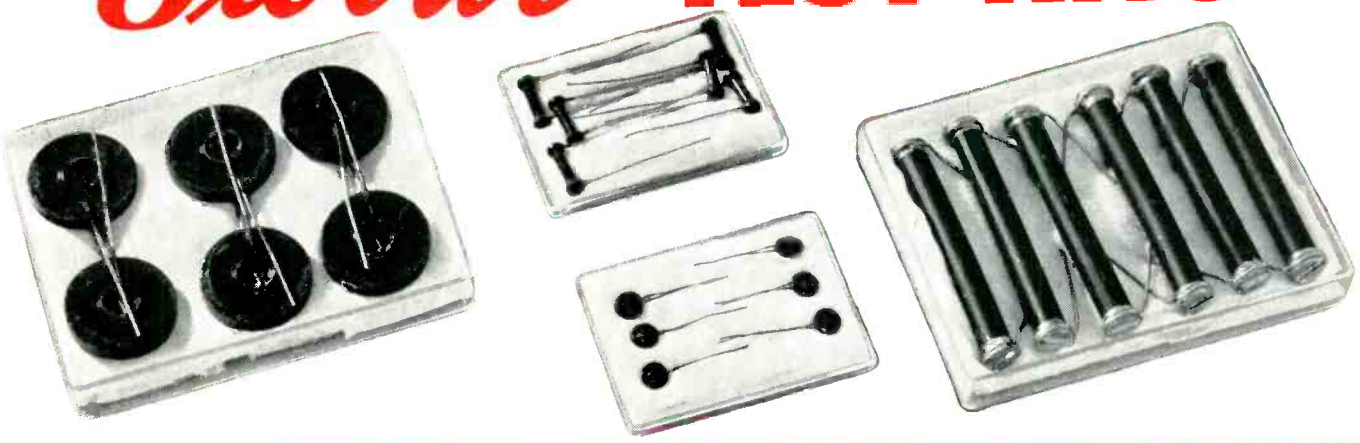
Test Kit No.	Type	Body Size		R at 25° C ± 30%	Nominal R at 45° C and Rated Current	Price
		Length	Dia.			
T-22	763F	5/8"	7/32"	145 ohms	40 ohms at 150 m.a.	$3.70
T-23	759F	3/4"	1/4"	500 ohms	85 ohms at 135 m.a.	3.95
T-24	441F	1 1/8"	3/8"	880 ohms	100 ohms at 150 m.a.	4.25
T-25	341F	3/4"	5/8"	375 ohms	40 ohms at 300 m.a.	4.55
T-26	525F	1 7/8"	1/2"	250 ohms	20 ohms at 600 m.a.	4.55
T-27	327F	3 1/8"	1/2"	460 ohms	35 ohms at 600 m.a.	4.85
T-28	421F	3 3/16"	1" x 1/8" Wafer Type	125 ohms	43 ohms at 600 m.a.	5.15
T-14	479H	1/8"	1/2"	1000 ohms	50 ohms at 150 m.a.	3.95
T-17	343H	1/8"	3/4" o.d. 1/4" i.d.	5.5 ohms	.31 ohms at 3.0 amps.	4.85

Want more information? Use post card on last page.

selective basis . . .

THERMISTOR AND VARISTOR

Globar® TEST KITS



Globar® VARISTORS Type BNR

To evaluate varistor circuit applications for:

1. Reduction of surge voltage peaks.
2. Reduction of relay contact arcing.
3. Voltage stabilization.
4. Generation of harmonics.

Test Kit No.	Type	Body Size		R ± 20% at D.C. Calibration Voltage	Max. Watt Loading at 40° C	Price
		Length	Dia.			
V-1	432BNR	1/16"	1/2"	1000 ohms at 10.5V	0.25	$3.70
V-2	432BNR	1/16"	1/2"	25000 ohms at 10V	0.25	3.70
V-3	432BNR	1/16"	1/2"	100000 ohms at 10V	0.25	3.70
V-4	432BNR	1/16"	1/2"	1 megohm at 10V	0.25	3.70
V-5	479BNR	1/8"	1/2"	100000 ohms at 100V	0.3	3.75
V-6	328BNR	1/16"	3/4"	10000 ohms at 40V	0.5	3.85
V-7	463BNR	1/8"	1"	24000 ohms at 40V	1.	3.95
V-8	524BNR	3/16"	1 1/4"	24000 ohms at 100V	1.5	4.25
V-9	430BNR	1/4"	1 1/2"	17500 ohms at 175V	2.7	4.55

ORDER YOUR KITS NOW! Use this handy coupon

Globar®

Over 30 years' experience in the field of ceramic special resistance devices.

THE CARBORUNDUM COMPANY, GLOBAR DIVISION, Dept. E-87-72,
Niagara Falls, New York

Please ship the following test kits (Min. quantity per order—3 kits).

THERMISTORS:
TEST KIT
Numbers _____

VARISTORS:
TEST KIT
Numbers _____

NAME _____ TITLE _____

COMPANY _____

ADDRESS _____

CITY _____ ZONE _____ STATE _____

☐ Check enclosed ☐ Please invoice us

87-72

Want more information? Use post card on last page.

Sylvania is your source!

If you manufacture transistors or diodes of any type, you will find that Sylvania can supply the kind of germanium you need.

The following Sylvania germanium products are available: spectrographically pure dioxide; polycrystalline as-reduced ingots; polycrystalline purified ingots; and vertically grown, undoped single crystals. All Sylvania germanium is n-type, and, in the purified ingot or single crystal form, has a minimum resistivity of 40 ohm cm.

Manufacturers of diodes and transistors report important benefits gained through using Sylvania germanium. They report they can use the same doping schedule from shipment to shipment. They report higher yield in the growth of doped single crystals. And for those who grow doped crystals horizontally, Sylvania germanium ingots are purified in five standard boats to fit single crystal boats in popular use.

Whether you prefer germanium in the form of dioxide, as-reduced ingots, purified ingots, or undoped single crystals, Sylvania can fulfill your requirements. Send for a technical bulletin on all forms of Sylvania germanium. Write to:

SYLVANIA ELECTRIC PRODUCTS INC.
Tungsten and Chemical Division
Towanda, Penn.

TUNGSTEN • MOLYBDENUM • CHEMICALS • PHOSPHORS • SEMICONDUCTORS

SYLVANIA

LIGHTING • RADIO • ELECTRONICS • TELEVISION • ATOMIC ENERGY

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DYNASERT

Resistor inserting speed tripled...

Product quality improved...

Costs cut at HARMAN-KARDON

Dynasert individually operated machines mechanize insertion of resistors at Harman-Kardon, Incorporated, Westbury, Long Island, New York. Costs were reduced, quality increased and inserting time cut by two-thirds over hand methods.

Improved product quality, increased speed and greater flexibility were the most important reasons why Harman-Kardon decided to use Dynasert individually operated bench machines.

With printed circuit boards ranging from 2″ square to 6″ x 14″ with comparatively short runs, easy changeover is essential. Also, errors resulting from inserting wrong component or wrong location are practically eliminated. They use these machines to feed a variety of components with axial leads. Machines cut, form, insert and clinch leads. Each operator now turns out three times her former output. In addition fewer components are wasted.

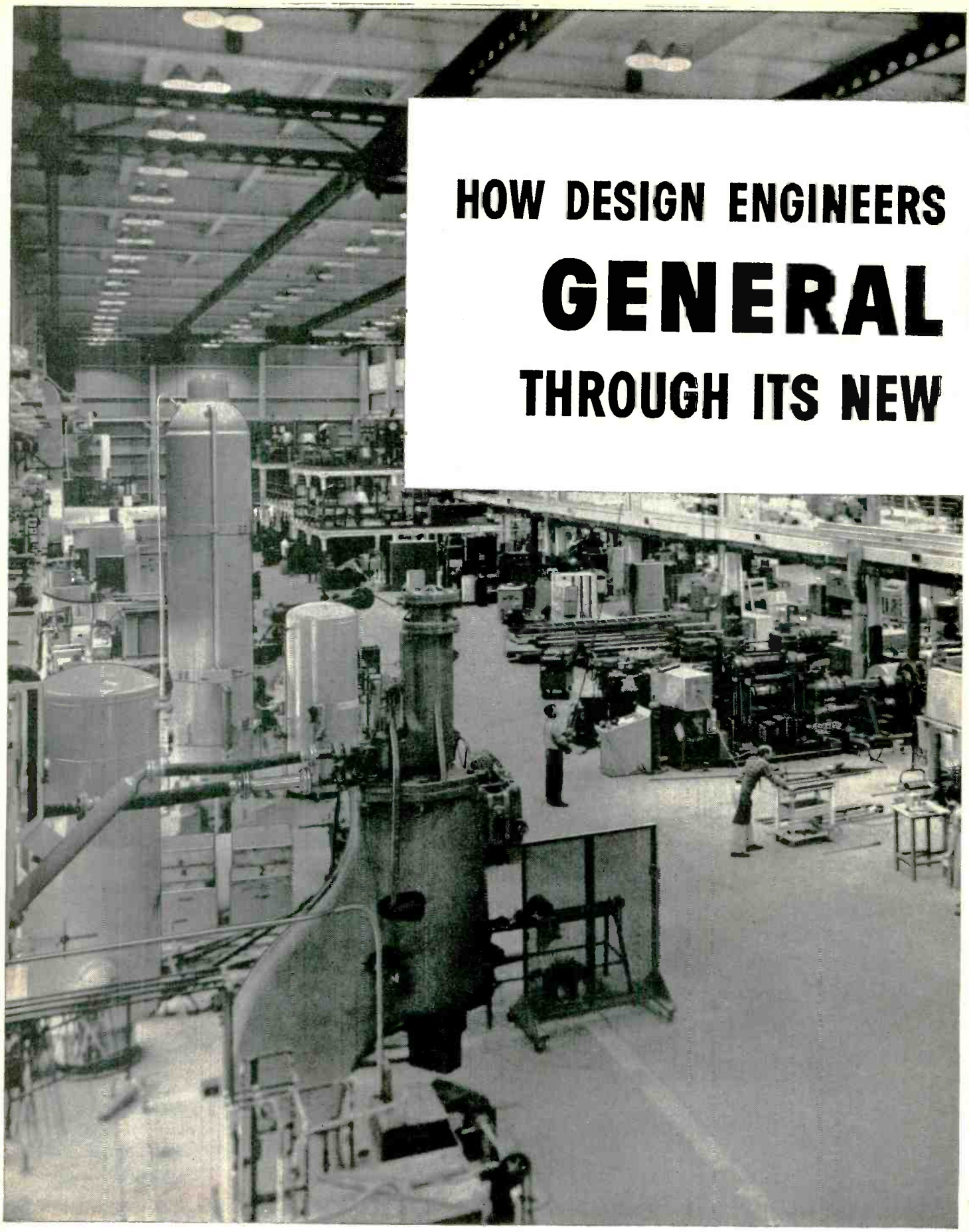
If you would like to cut your component inserting time on printed circuits and improve the quality at the same time, call or write us now.

Industrial Sales Division

United
SHOE MACHINERY CORP.
140 FEDERAL STREET, BOSTON, MASS.
Liberty 2-9100

Production Equipment for Electronics

BOOTH 1419 IRE



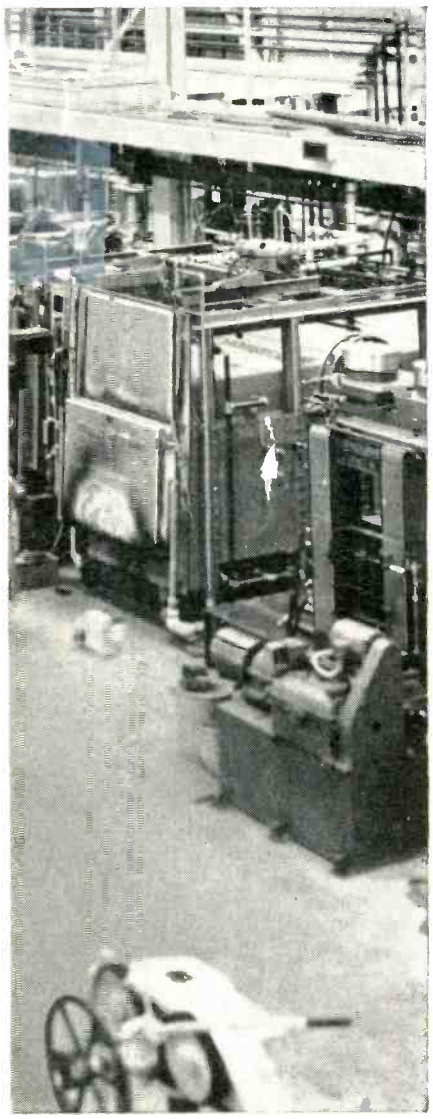
HOW DESIGN ENGINEERS GENERAL THROUGH ITS NEW

Laboratory with factory-size equipment — that's the new $5,000,000 G-E metals and ceramics laboratory in Schenectady. From here will come many of the products manufactured by the Metallurgical Products Department of General Electric Company, 11137 E. 8 Mile Road, Detroit 32, Michigan.

BENEFIT FROM THE RESOURCES OF

ELECTRIC

METALLURGICAL PRODUCTS DEPARTMENT



Solutions to your most pressing problems — plus developments ahead of industry trends — are now being worked out in our laboratories

Because designers needed a metal harder and more wear-resistant than steel, General Electric brought out Carboloy® cemented carbides. Because designers needed a more powerful magnetic material, General Electric developed improved types of Alnico permanent magnets. Because designers needed better high-temperature metals, General Electric created new vacuum-melted alloys.

These, and many other vital products for design engineers, are the result of General Electric's tremendous resources of technological know-how and skilled manpower in the field of metallurgy. They are created in G-E laboratories . . . and produced for industry by the new Metallurgical Products Department.

This Department is the successor to the Carboloy Department, which was originally organized to manufacture carbides. It now produces such widely divergent metallurgical products as hevimet, thermistors, and Thyrite® varistors . . . in addition to chrome and tungsten carbides, and permanent magnets.

The very range of its products indicates how the resources of General Electric are being put to work solving the design engineer's most pressing problems through modern metallurgy.

Perhaps more important, G-E resources like the new Research Laboratory in Schenectady, and the manufacturing facilities of the Metallurgical Products Department, are now combining their talents to produce *ahead* of the trends and needs of industry.

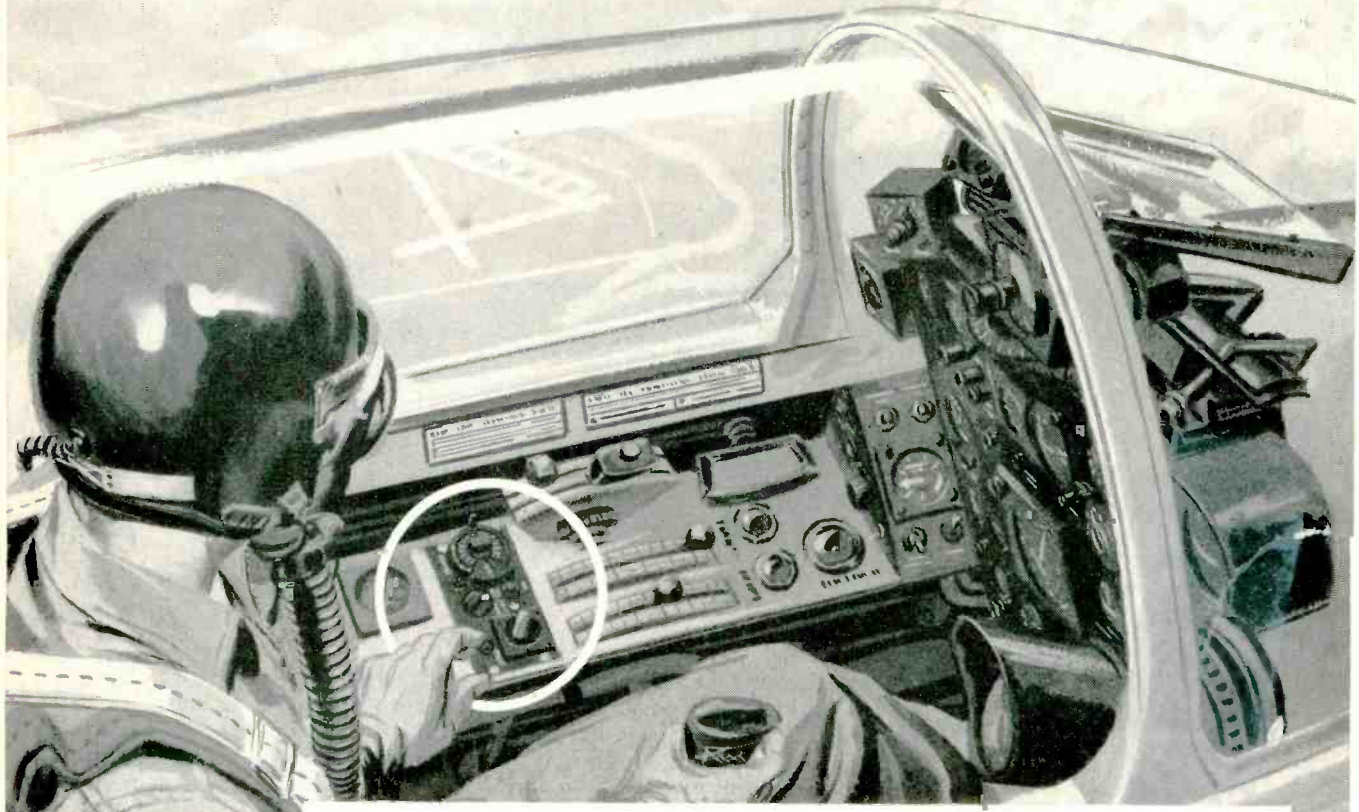
In the Metalworking Industry, for example, this combination of G-E resources has already made one such contribution: Carboloy Cemented Oxide — a new kind of cutting tool material with so great a potential for super high-speed machining, that new machine tools must be designed to take advantage of all it offers.

Developments like these are essential to industrial progress . . . and they are typical of the parade of products design engineers can expect from the G-E Metallurgical Products Department.

Progress Is Our Most Important Product

GENERAL ELECTRIC

You can't shrink the pilot
...so *Admiral* shrinks the controls



New transceiver control box reduced to one-fifth former size

The cockpit of a modern fighter plane is packed as tight as a filling in a hollow tooth. As more and more electronic equipment is added to the plane's complement, each new device must fight for space on and behind the instrument panel or console. Now Admiral, maker of the famed AN/ARC27 transceiver, has designed a control box that "moves over" to make room for other needed equipment.

Heart of the new control is an ingenious "mechanical memory" drum that selects any one of 20 preset frequencies with a single knob. Another knob controls three coaxial switches designed by Admiral so the pilot can manually select any of the transceiver's 1750 frequencies. This single compact unit will be universally employed to replace any one of 15 currently used control box combinations. It occupies as little as one-fifth the space and also reduces weight up to 80%.

Here is another instance where Admiral initiated and perfected an important advance in the science of military electronics. Inquiries are invited regarding Admiral's capabilities and production capacity for electronic or electro-mechanical equipment.

Admiral®
CORPORATION
Government Laboratories Division, Chicago 47

RESEARCH • DEVELOPMENT • PRODUCTION
IN THE FIELDS OF:
COMMUNICATIONS UHF AND VHF • MILITARY TELEVISION • RADAR
RADAR BEACONS AND IFF • RADIAC • TELEMETERING
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TEST EQUIPMENT • ELECTRONIC COUNTERMEASURES

ENGINEERS: The wide scope of work in progress at Admiral creates challenging opportunities in the field of your choice. Write Director of Engineering and Research, Admiral Corporation, Chicago 47, Illinois.

See What's New...

with BECKMAN / BERKELEY TEST INSTRUMENTS • BOOTHS 3416-18

NEW APPLICATIONS

★ **FERRISTORS* AND HOW TO USE THEM**

Data File #110 gives detailed examples of 14 magnetic circuits, plus complete technical data on FERRISTORS* and how to use them.

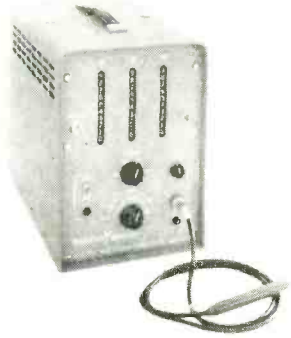
★ **FREQUENCY MEASUREMENTS AND HOW TO MAKE THEM**

Data File #111 covers Berkeley EPUT* meter techniques for low and medium frequencies; Berkeley EPUT* and heterodyne techniques for RF, VHF and UHF; preset counter and time interval meter techniques for rapid low frequency measurements; measurement of rpm, flow, pressure, temperature and strain; setting up a standard of frequency, and nuclear counting techniques.

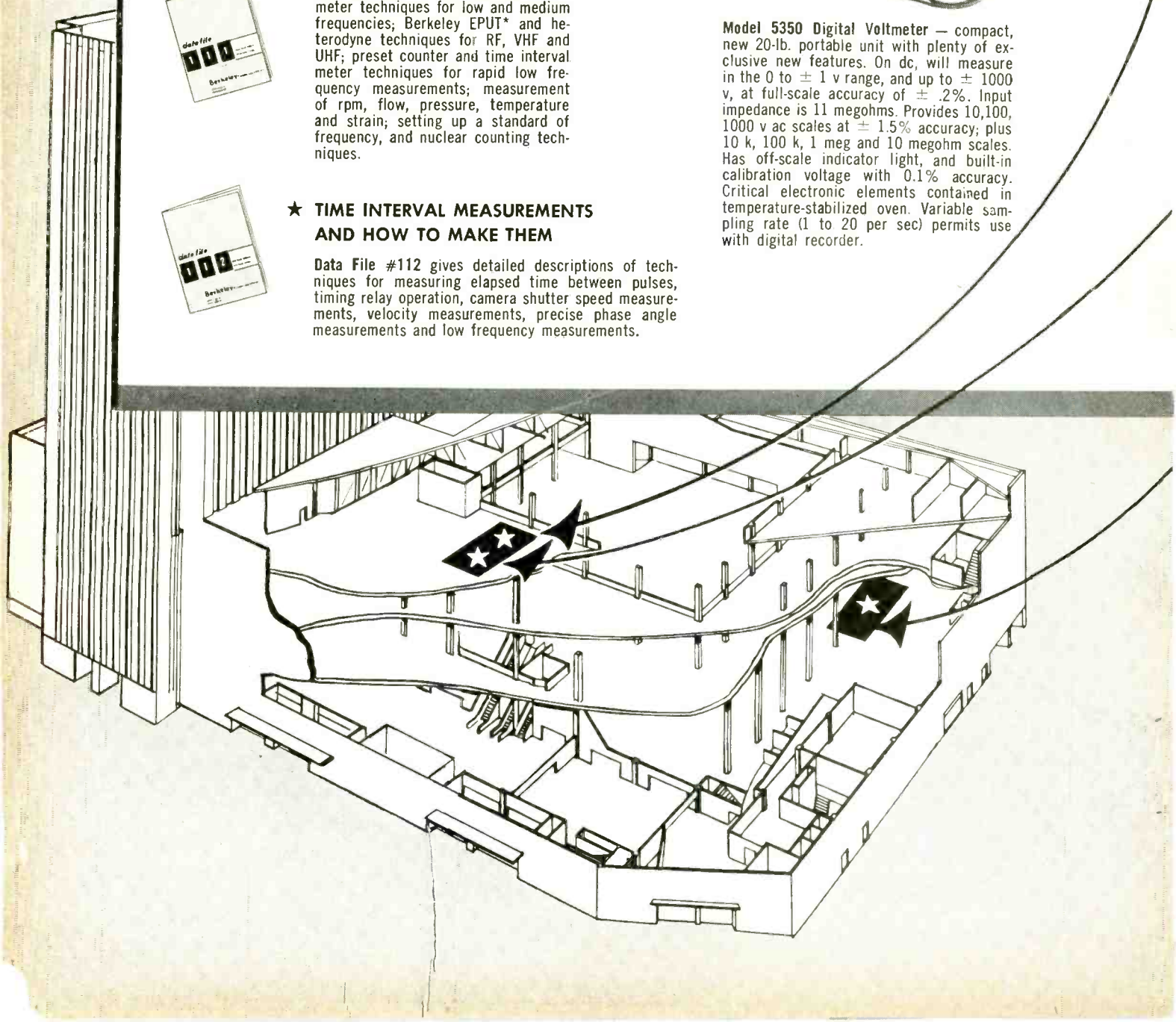
★ **TIME INTERVAL MEASUREMENTS AND HOW TO MAKE THEM**

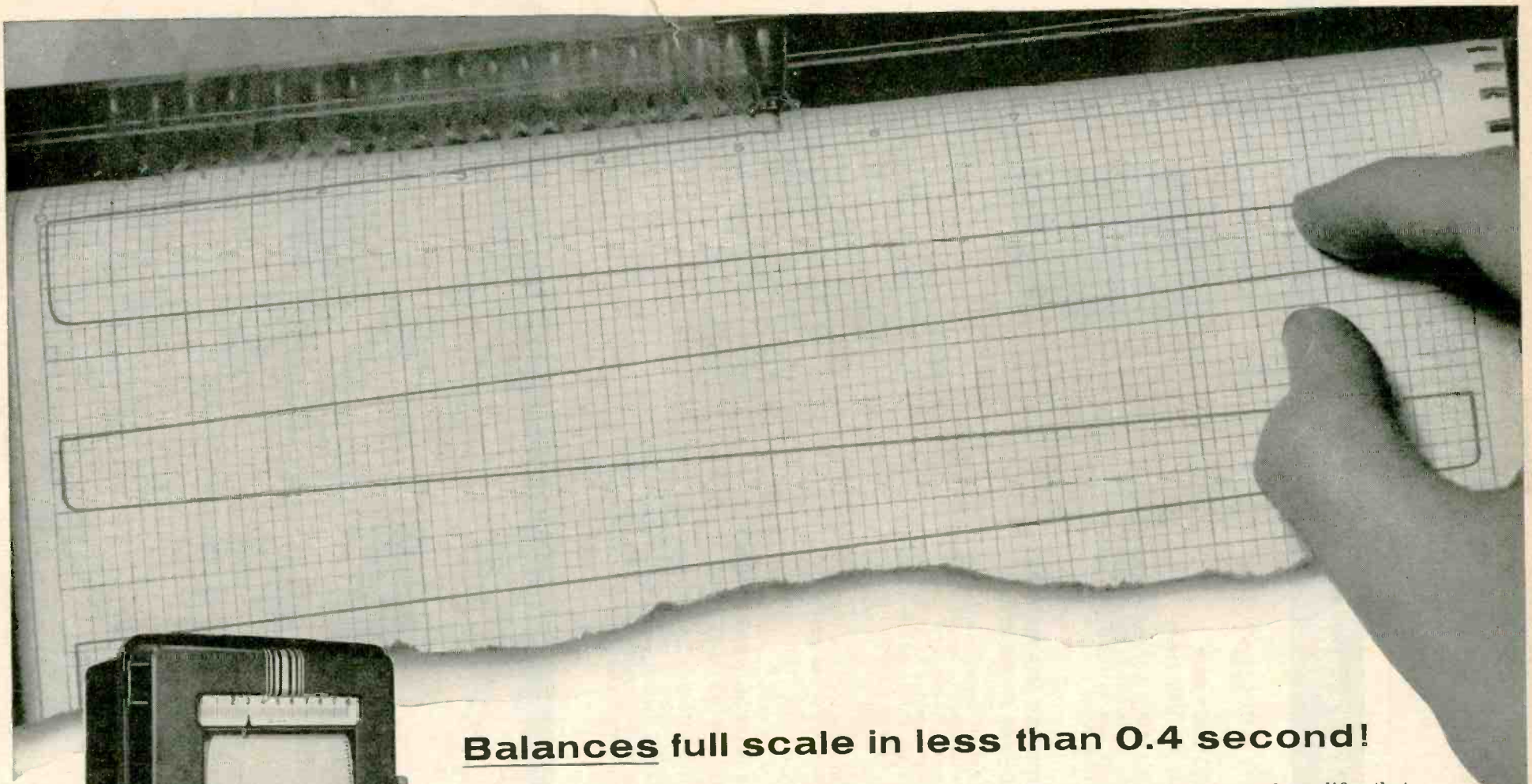
Data File #112 gives detailed descriptions of techniques for measuring elapsed time between pulses, timing relay operation, camera shutter speed measurements, velocity measurements, precise phase angle measurements and low frequency measurements.

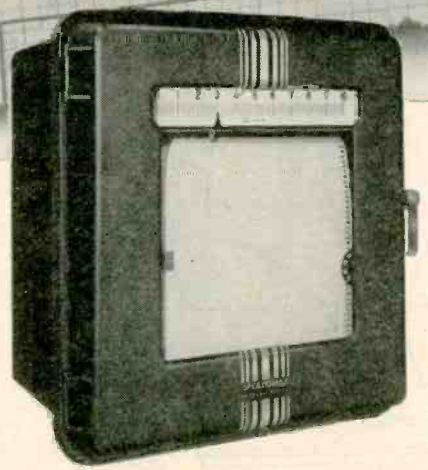
NEW PRODUCTS ON DISPLAY



Model 5350 Digital Voltmeter — compact, new 20-lb. portable unit with plenty of exclusive new features. On dc, will measure in the 0 to ± 1 v range, and up to ± 1000 v, at full-scale accuracy of ± .2%. Input impedance is 11 megohms. Provides 10,100, 1000 v ac scales at ± 1.5% accuracy; plus 10 k, 100 k, 1 meg and 10 megohm scales. Has off-scale indicator light, and built-in calibration voltage with 0.1% accuracy. Critical electronic elements contained in temperature-stabilized oven. Variable sampling rate (1 to 20 per sec) permits use with digital recorder.







Balances full scale in less than 0.4 second!

Even though loaded with an alarm contact, a transmitting slidewire and a digital encoder, this high speed Speedomax G Recorder will balance in 0.4 second or less. The recording pen sweeps across the 9⅞" chart to reach final balance—without overshoot (chart speed is 1" per second).

If you're engaged in rocket or jet engine testing, neutron density measurements in atomic pile startups, in data handling applications, etc., this fast new Speedomax G Recorder will enable you to measure and record extremely fast changes in the d-c millivolt signal under test.

This fast balancing speed with instrument loading is a result of a newly engineered amplifier that delivers power to a new high-speed balancing motor. The minimum electrical range is 0 to 2 mv with a maximum external circuit resistance of 2000 ohms.

For more information on this fast, powerful Speedomax instrument, write to your nearest L&N Sales Office or to Leeds & Northrup Company, 4979 Stenton Ave., Phila. 44, Pa.

LEEDS Instruments NORTHRUP Automatic Controls • Furnaces

Jrl. Ad E-ND46(6)

with BECKMAN/SHASTA INSTRUMENTS • BOOTH 3414

NEW APPLICATIONS

★ WWV RECEIVERS AND HOW TO USE THEM

Shasta **Data File #10** describes the functions of NBS radio broadcasts from WWV and WWVH, explains in detail how these broadcasts can be utilized for the precise calibration of standard radio frequencies, audio frequencies, time intervals, and musical pitch.

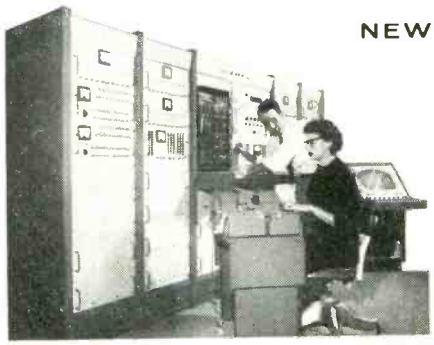
NEW PRODUCTS ON DISPLAY

Model 905 WWV Receiver — covers all six WWV and WWVH frequencies with separate crystals for each; has built-in audio filters for 440, 600, 1000 cps discrimination, and 300 ohm antenna input matcher. Bands and audio discriminators selectable by panel switch — no plug-ins. Rock mounted; modular construction with blower cooling.

Model 100 Transformation Ratio Meter— an rms-reading expanded scale voltmeter with precision voltage divider and input switching for rapid testing of synchros to ± 0.2% accuracy. Nominal input voltages are 57.3, 78, 90, 105 and 115; input frequency, 50 to 1,000 cps, impedance 10,000 ohm/v.

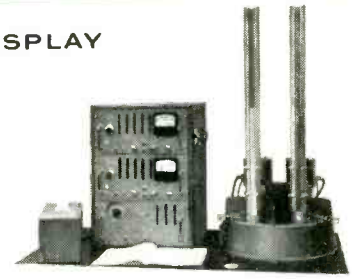
with BECKMAN/BERKELEY COMPUTERS & SYSTEMS • BOOTH 1728

NEW PRODUCTS ON DISPLAY



New EASE* 1100 Series Computers with DO/IT (Digital Output — Input Translator system) — a wholly-new concept in analog computation. Provides digital input-output by means of punched tape or electric typewriter, automatic static or dynamic problem checking, complete pushbutton monitoring, fully shielded color-coded patchboard, and many other advanced-design features.

New Analog-Digital Tachometry Systems measure rotational speed, indicate in both analog and digital form. System displayed is similar to those used by Ford Motor Co., and Allison division of General Motors. Analog uses 2-meter indication; first (full scale) has accuracy of 1%; second expanded-scale meter (covers 5% of full scale) has 0.25% accuracy. Digital data is displayed on remote in-line readout with acuracy of ± 1 count, 1 part in 10,000.



New Automatic Radioassay Equipment — complete systems for automatic sample counting and data recording. Two detector sample changer takes up to 250 samples; data may be recorded by digital printer or fed to card punch for automatic data processing.

Model 5699 Digital Flow Indicator — gives direct-reading digital indication of transducer output frequency or percentage ratio of speed and volume, etc. Features higher sensitivity (ranges from 5 mv @ 5 cps to 1 v @ 100 kc), improved pulse resolution (10 μsec paired input pulses, 100 μsec on totalizing), dual range preset time (0-1 sec in 0.1 millisec increments or 1 to 10 sec in 1 millisec increments), time base stability of 1 part in 10^5 per day, 5 digit presentation, and versatility to drive digital recorders, remote indicators, data converters, etc.

DON'T MISS THESE TWO BECKMAN/BERKELEY EXHIBITS if you attend the IRE show. If you can't attend, please write us for application data and technical bulletins on the new techniques and new products that interest you. For prompt action, please address Dept. G-3 _____.

Beckman® / **Berkeley** *Division*
Richmond 3, California
a division of Beckman Instruments, Inc.

*Trademark

From Electro Instruments comes a revolutionary new concept in digital instrumentation.

transistorized, plug-in modules for precision measurements of dc, ac, ohms and ratios

NOW GET MAXIMUM FLEXIBILITY FOR CUSTOM APPLICATIONS WITH STANDARD, OFF-THE-SHELF MODULES

Check these new specifications and features — the result of thousands of applications and field experience of more than 1,000 digital instruments

Fully transistorized circuits in the new modules provide

1. Increased reliability.
2. Reduced power consumption.
3. Low heat dissipation.
4. Miniaturized packages.
5. Elimination of radio noise and line transients.

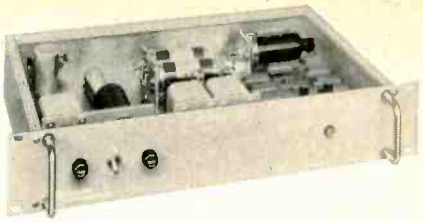
New specifications and features

1. Wider dynamic range covering all voltages from 100 microvolts to 1,000 volts, resistance range from 10 milliohms to 10 megohms — in single instruments!
2. Input power frequencies from 50 to 400 cycles!
3. New balance logic speeds down ranging!
4. Automatic ac ranging from 30 to 10,000 cycles!
5. Controlled stepping switch drive increases switch life by a factor of three!

Complete flexibility

1. Universal 3½" x 19" x 12" chassis with mounting hardware for any rack.
2. No modifications required for operating printers, IBM Punches, etc., or for combining with auxiliary E-I input modules or instruments.
3. All contacts readily accessible at rear panel on connectors.
4. With auxiliary plug-in modules, digitized data is provided in printed form, punched cards or tape with no modification to basic measuring instruments.

BASIC MODULES



Universal Power Module, Models DXA-000 or DXB-000

Supplies *all* power and reference voltages for other E-I modules. Power and reference supplies and stepper drive amplifier are transistorized. Powers one or more modules.

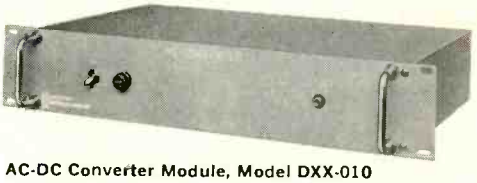
Calibration: Automatic
Reference Stability: 0.01% from 40° to 125° F.
Input Power: 115 volts, 50 to 400 cycles.
Write for Bulletin 175-1

DC Switch Module
Model DVX-400: 4 digits; **Model DVX-500:** 5 digits

Contains Digital Potentiometer. Provides visual in-line read-out of digits, polarity, decimal point. All contacts accessible at rear panel connector. Front and rear panel input connectors. Power supplied by Universal Power Module.
Write for Bulletin 175-2

DC Pre-Amp Module, Model DXX-020

Input: 1 range scale, gain of 10.
Output: 0.0001 to .9999 volts. **Linearity:** 0.01%.
Gain Multiplication Accuracy: 0.01%.
Input Power: 115 volt, 50 to 400 cycles.
Drift: 10 microvolts per hour.
Write for Bulletin 175-5



AC-DC Converter Module, Model DXX-010

A fully transistorized AC-DC converter.

Accuracy: 0.1% of reading, or 2 mv.
Frequency Response: 30 to 10,000 cycles.
Range: .0001 to 999.9 volts.
Zin, AC: 1 meg. on the 1 volt scale, 10 megs. on other scales; 20 mmf.
Ranging: Automatic. **Reading time:** 3 seconds, average.
Write for Bulletin 175-4

Resistance Switch Module
Model DOX-400: 4 digits; **Model DOX-500:** 5 digits

Contains balance circuit, bridge ratio arms. Provides visual in-line read-out of digits, range. All contacts accessible at rear panel connector. Power supplied by Universal Power Module.
Write for Bulletin 175-3

Using E-I's new, transistorized, modular design, any precision instrument for measuring DC, AC-DC, Ohms, DC and AC ratios can be constructed from basic units!

DC Digital Voltmeters

specifications	**Model DVA-400** (Combines Universal Power Supply, Model DXA-000, and Model DVX-400 Modules.)	**Model DVA-500** (Combines Universal Power Supply, Model DXA-000, and Model DVX-500 Modules.)
Display:	4 digits, plus or minus, decimal point.	5 digits, plus or minus, decimal point.
Accuracy:	±1 digit.	±0.01%, plus or minus 1 digit.
Range:	.0001 to 999.9.	0.0001 to 999.99.
Automatic Features:	Ranging, polarity.	Ranging, polarity.

(Adding the E-I Pre-Amp Module, Model DXX-020, increases sensitivity to 10 microvolts.)

DC RATIOMETER – Same modules as Voltmeter except uses external reference. Ratio range: 0.0000 to 1.0999.

AC-DC Digital Voltmeters

specifications	Model DVA-410	Model DVA-510
DC Specifications:	Same as Model DVA-400.	Same as Model DVA-500.
AC Specifications:	Same as Model DXX-010.	Same as Model DXX-010.

(AC RATIOMETER combines Model DVA-400, with two Model DDX-040 or Model DXX-050 Modules. Ratio range is 0.0000 to 1.0999.)

Digital Ohmmeter

specifications	Model DOA-400 (Combines Model DXA-000 and DOX-400 Modules.)	Model DOA-500 (Combines Model DXA-000 and DOX-500 Modules.)
Display:	4 digits.	5 digits.
Range:	Automatic, 0.01 ohms to 10 megohms.	Automatic, 0.01 ohms to 10 megohms.
Accuracy:	0.01 to 0.1%.	0.01 to 0.1%.

OPERATING MACHINE READ-OUTS

Pictured here is a typical Automation System constructed with standard E-I modules. This system automatically scans and measures 400 channels of AC and DC voltages with punched tape read-out. E-I Model 200 X-Y Recorder provides plotted data. With auxiliary plug-in input and output modules, complete custom data handling systems may be set up. Write for Bulletin 175-6.

NEW HAND-CARRY MODEL

The Mark IV is the ideal companion to the new E-I rack-mounted modular equipment. Compact, weighs only 25 lbs.; 0.05% accuracy. Write for Bulletin 170.

SEE THIS EQUIPMENT AT THE IRE SHOW, BOOTH #3614.

ELECTRO INSTRUMENTS

INC. 3794 Rosecrans, San Diego, California

NEW LITERATURE AVAILABLE—Write for new short form Bulletin 175 containing information about the new Electro Instruments modular design.

Subject: DYNAMIC AND STATIC LOAD RATINGS

DYNAMIC LOAD RATINGS

Load ratings of MICRO bearings are based on standards established by the Anti-Friction Bearing Manufacturers Association and are the result of extensive tests.

The "life" of an individual bearing is defined as the number of revolutions which the bearing makes before the first evidence of fatigue develops. Fatigue, in turn, is a function of bearing load and although other factors, such as contamination and high temperature, affect the life of a bearing, it is assumed that clean bearings running at normal temperatures are being considered.

It is not possible to predict the life of any individual bearing. The problem, therefore, is best approached by a consideration of empirically derived dispersion curves which provide a means of determining bearing life on a probability basis. That is, they permit the average life of a given group of bearings to be accurately specified.

For purposes of standardization, the "rating life" of a group of apparently identical ball bearings is defined as the number of revolutions that 90% of the group will complete or exceed before the first evidence of fatigue develops. This figure is approximately one-fifth of the average life.

If two groups of similar bearings are run under different loads F_1 and F_2 within the normal operating range of loading and rpm, their lives L_1 and L_2 are inversely proportional to the cubes of the loads, i.e.,

$$\frac{L_1}{L_2} = \left(\frac{F_2}{F_1}\right)^3$$

The BASIC LOAD RATING C is that radial load which a group of apparently identical bearings can endure for a rating life of one million revolutions, with stationary load and rotating inner ring. Within normal operating ranges the rating life for any load *is a constant number of revolutions*, so the following relationship, a restatement of the inverse cube proportion, may be used to compute rating life when basic load rating and applied radial load are known:

$$L = \left(\frac{C}{P}\right)^3$$

where, L = rating life in millions of revolutions
C = basic load rating in pounds
P = applied radial load in pounds

The nomograph illustrated permits the quick evaluation of any one of the three quantities when the other two are known. For example, if the C rating of a given bearing is 95 pounds, and the bearing is loaded radially with 12 pounds, P, a straightedge crossing these two values in their respective columns shows that the bearing could be expected to have a life, L, of 450 million revolutions.

DEFINITION OF EQUIVALENT LOAD

Bearings whose loads are primarily radial are usually also subjected to axial forces. When the axial component of the load is greater than a negligible value, this combined radial and thrust load may be expressed in terms of a simple radial load in order that the basic load rating C may be calculated. This simple radial load is known as the "equivalent load", which is that constant stationary radial load which, if applied to a rotating inner ring, would give the same life as that which the bearing will attain under the *actual* conditions of load and rotation.

FORMULA FOR EQUIVALENT LOAD

For conventional bearing types other than those with filling notches, the equivalent radial load is given by the maximum of the two values:

a) $P_r = VF_r$ — X is a radial factor
b) $P_r = XVF_r + YF_a$ — Y is a thrust factor
where, V is a rotation factor — F_r is the radial load
F_a is the thrust load

The factor e represents the ratio of $\frac{F_a}{VF_r}$ for which the two equations are equal. If the ratio of loads is such that $\frac{F_a}{VF_r} \leqq e$ then formula (a) is used: if $\frac{F_a}{VF_r} > e$ then formula (b) is used.

For inner ring rotation V = 1.0 in all cases; for outer ring rotation V = 1.2 in all cases except for self-aligning bearings, where V = 1.0. In most calculations involving MICRO bearings, the following values are sufficiently accurate: X = 0.30, Y = 1.04, and e = 0.67. In the case of self-aligning bearings, however, X = 0.40 and Y = 7.6.

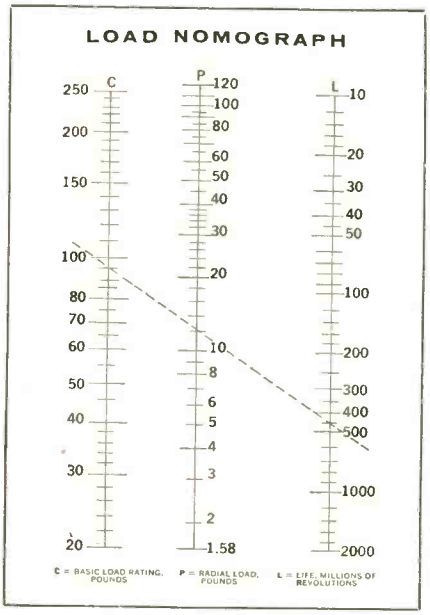
In practice, the angular contact type of bearing should not be subjected to a predominantly radial load unless opposed by another bearing.

When a bearing is loaded and at rest the dynamic life formula $\left[L_x = \left(\frac{C}{P}\right)^3\right]$ cannot be used because when $L_x = 0$ then $P = \infty$. Obviously there is a limit to the Static load which the bearing can carry, this limit being determined by permanent deformations which develop in the load carrying surfaces. Such deformations appear even under very light loads and increase gradually with increasing load, with no sharply defined limit beyond which they begin. The static load limit is dependent on the permissible magnitude of deformation, consistent with requirements of quietness and freedom from vibration. Experience indicates that a permanent deformation in the raceway of less than 0.0001 times the diameter of the rolling elements ordinarily has no objectionable influence on the functioning of the bearing.

In order to obtain an expression for the load carrying capacity at rest, and a numerical value that can be used as a reference, the pure radial load which corresponds to this negligible magnitude of permanent deformation has been selected as the basic static load rating and given the designation C_o.

If the load is much higher than C_o when the bearing is not rotating, minute depressions are formed in the raceways, causing the bearing to be noisy and to vibrate when operating at high speed, even though the bearing friction is not noticeably increased or the bearing otherwise injured. Depending on the requirements in this respect, the static load may occasionally be allowed to exceed the C_o value.

If a load considerably higher than C_o acts only while the bearing rotates, the permanent deformations that occur will be evenly distributed in the raceways and cause no serious impairment until the deformations become relatively large. However, under such a heavy load, the fatigue life will be comparatively short in terms of the number of revolutions. Static load rating values for all MICRO bearings are presented in our catalog-data book.



Plain | Flanged Plain | Plain and Shielded | Flanged and Shielded

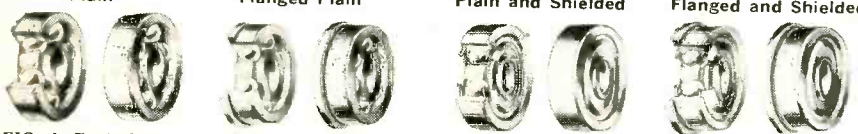
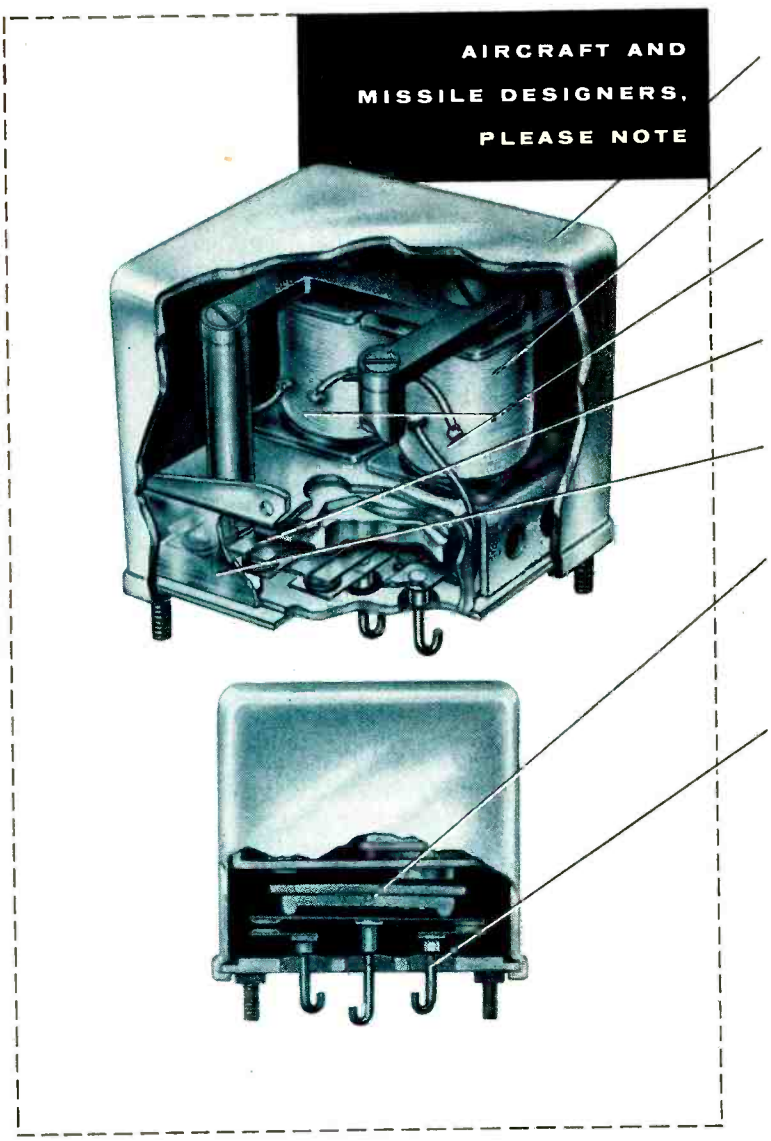


FIG. 1. *Typical cut-away views of instrument-type retainer ball bearings. Complete tabular data on "C" factors and static load ratings are contained in the MICRO Bearings Catalog.*

Get unprecedented performance—

See for yourself why the new LEACH BALANCED-ARMATURE RELAYS outperform all other types in resistance to shock, acceleration and vibration



ONE-PIECE DIE CAST ALUMINUM HOUSING for maximum strength and vibration resistance with minimum weight.

MAGNET COIL wound with Teflon insulated magnet wire on one-piece Kel F bobbin assures reliability at elevated ambients.

DUAL COIL construction is the most efficient magnetic circuit for minimum height and maximum resistance to vibration and shock.

BIFURCATED CONTACTS assure high reliability in contact making circuits. Overtravel and high contact pressures produced by the pivoted armature result in immunity to shock and vibration.

ARC BARRIER of Kel F molded construction provides long arc path for use on 3 phase ac circuits, prevents phase-to-phase flashover.

BALANCED-ARMATURE DESIGN. In a *Balanced-Armature* construction, shock and vibration forces cannot cause the relay armature to move. This eliminates faulty operation of contacts due to vibration and shock forces.

HEADER AND CONTACT ASSEMBLY features simplified construction which eliminates internal wiring, lowers lead resistance, provides maximum resistance to vibration. Contacts and working parts are readily accessible throughout assembly, so that Leach is able to measure contact gap, contact pressure and overtravel, prior to sealing, on 100 per cent of production. Customers are assured of maximum performance from every production relay. Patent Pending.

MEETS ALL REQUIREMENTS OF THE MOST EXACTING OPERATING ENVIRONMENTS

The Leach Balanced-Armature Relays meet or exceed requirements of MIL-R-5757, MIL-R-6106, MIL-E-5272. Typical ratings include: vibration, 20 G's to 500 cps (higher ratings available); shock and acceleration, more than 50 G's; temperature, −50° to +125°C; life, 50,000 continuous operations minimum at rated load; coils, any resistance to 10,000 ohms – also available for 115 vac, 400 cps operation.

Write today for your copy of the Leach Balanced-Armature Relay Catalog.

LEACH CORPORATION | **LEACH RELAY DIVISION**

5915 AVALON BOULEVARD, LOS ANGELES 3, CALIFORNIA

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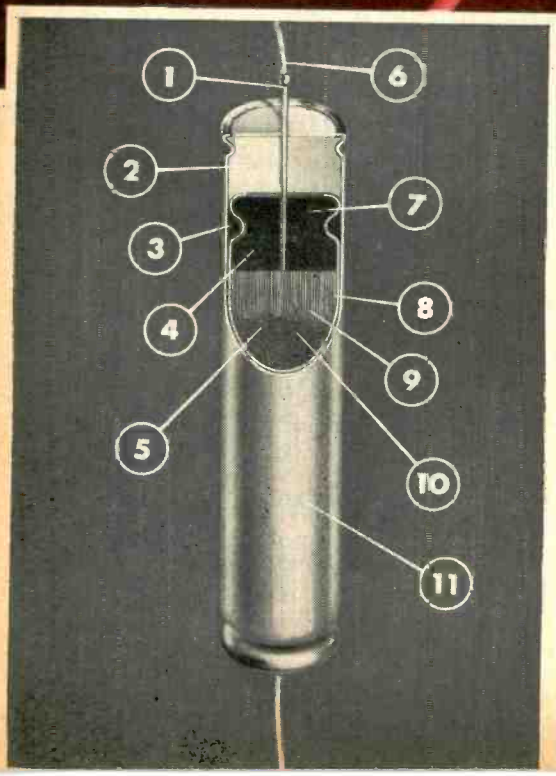
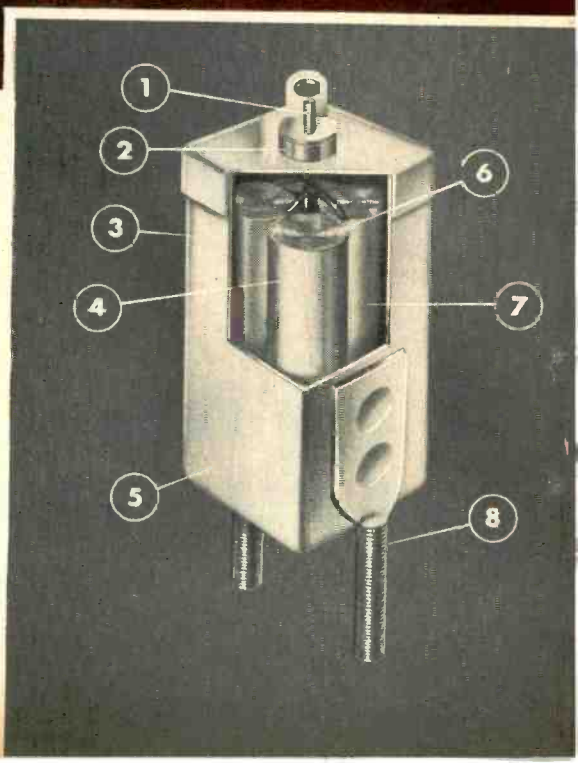
CAPACITORS



HIGH TEMPERATURE TANTALYTIC CAPACITOR — TUBULAR — features: 1 —Tantalum lead, 2 — Teflon* bushing, 3 — Mylar* insulating sleeving, 4 — Insulation, 5 — Paper and tantalum foil roll, 6 — Solderable nickel lead, 7 — Rubber bushing, 8 — Double metal case construction, 9 — Non-acid electrolyte, 10 — Plain and etched foil, 11 — Polar or non-polar construction.

HIGH TEMPERATURE TANTALYTIC CAPACITOR — RECTANGULAR — features: 1 — Tantalum stud, 2 — Silicone bushing, 3 — Polar or non-polar construction, 4 — Paper and tantalum foil rolls, 5 — Silver-plated metal case, 6 — Plain and etched foil, 7 — Non-acid electrolyte, 8 — Mounting stud (optional).

*DuPont Co. Trade Mark



General Electric Tantalytic* capacitors

operate at +125 C ambient

for 1000 hours at full rated voltage

To help you solve difficult space problems in design functions demanding high reliability miniaturized equipment capable of operating in ambient temperatures ranging from —55C to +125C at full rated voltage, General Electric offers a variety of shapes and sizes of high temperature Tantalytic capacitors.

The Tantalytic capacitor is built for at least 1000 hours operation at +125C with no more than 20% loss in capacity. Below +125C, capacitor life is extended in proportion to the reduction in ambient temperature.

Whatever your capacitor requirements might be, there is a General Electric subminiature capacitor for most applications. Take, for example, the metal-clad tubular capacitor — mineral oil impregnated, built to MIL-C-25A — often applied to "work horse" applications in military electronic circuits. Or, capacitor pulse forming networks, adhering to strict capacitance tolerance and temperature range, are engineered for missiles and radar equipment.

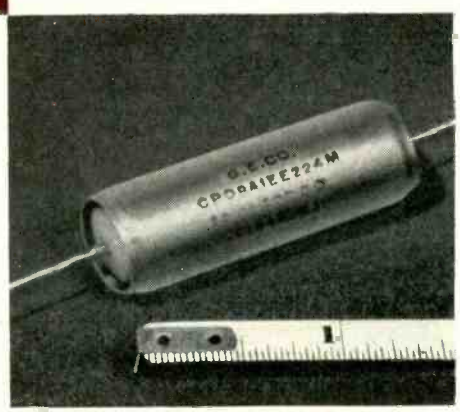
New permafil capacitors, built to meet the characteristic "K" requirements of MIL-C-25A, are now available in rectangular case styles. These solid dielectric capacitors can withstand the violent shock and vibration found in today's missile and airborne electronic systems.

For assistance with capacitor applications contact your General Electric Apparatus Sales Engineer or write to the General Electric Company, Section 442-40, Schenectady 5, New York.

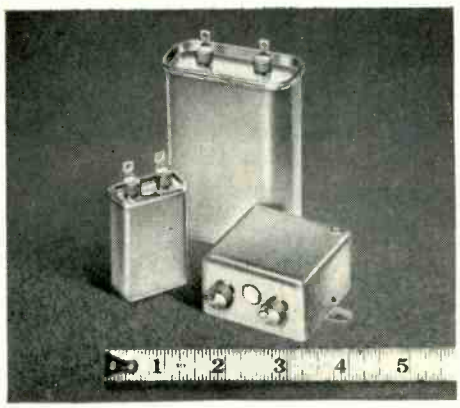
*Registered Trade Mark of General Electric Co.

Progress Is Our Most Important Product

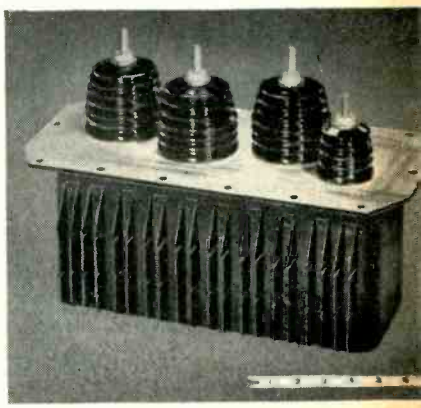
GENERAL ELECTRIC



METAL-CLAD TUBULAR CAPACITORS— +85C, mineral oil impregnated. Built to MIL-C-25A. Ratings: .001 to 1.0 uf, 100-600 v. d-c. Tol: ± 5%, ± 10%, or ± 20%. Write for GEC-1390.



PERMAFIL RECTANGULAR solid dielectric in case styles CP50, CP60, and CP70 series. Built to electrical requirements of characteristic "K", MIL-C-25A. Ratings: .01 uf to 10 uf; 100 v. d-c to 1500 v. d-c, Temp. range: —55C to +125C.



CAPACITOR PULSE FORMING NETWORKS — for missiles and radar equipment. Capacitance tolerance: + 7% (at +25C). Temp. range: —55C to +125C. Write for GEA-4996.

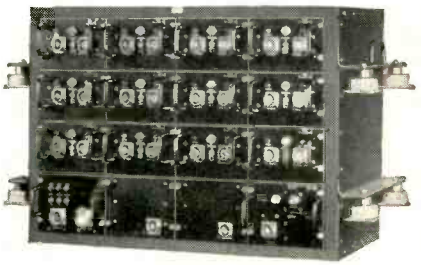
VERSATILITY

TDI MINIATURE TELEMETRIC RECEIVING SYSTEMS

Miniature and mobile, here's a telemetric receiving system designed for a host of military and civilian applications . . . airborne, ground or marine!

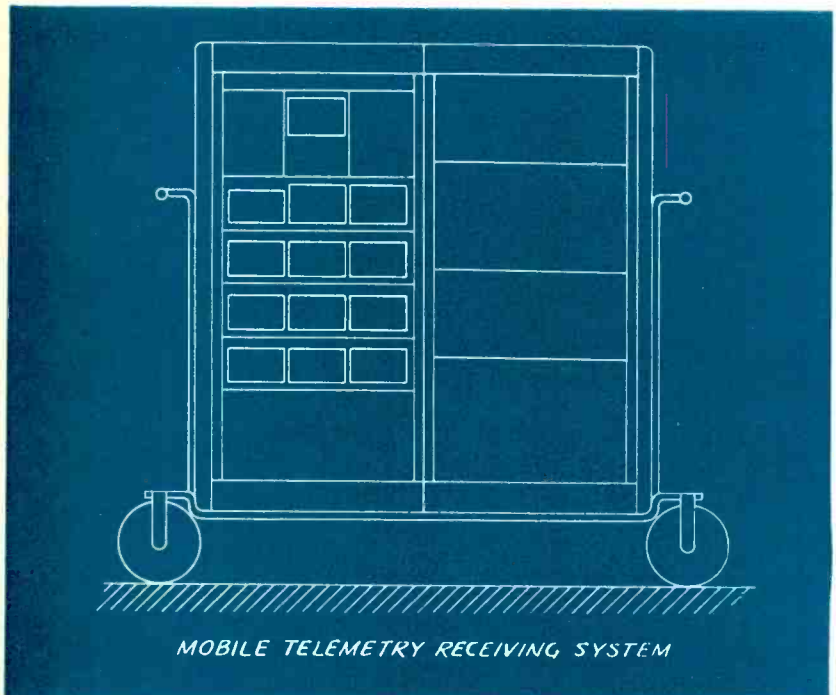
For missile checkout, flight tracking experimental aircraft and missiles, the TDI systems are highly effective, even under the most severe field service conditions. They operate ideally with tape recording, oscillographic, photographic and similar types of recording equipment . . . and this rugged equipment can be installed in jeeps, autos and trailers.

Design-wise, these systems achieve substantial reductions in weight, size and power consumption—yet a high degree of accuracy, exceptional stability and simplicity of operation are maintained.



TDI 12-Channel Receiver. Modular construction permits wide flexibility of arrangement and actual form factor of receiving equipment. Packages or combinations in any number from one to eighteen units can be arranged in various mounting styles.

TDI Type 2701A 4-Channel Receiver. Use as flexibly as 12-channel unit—split up in combinations to suit your particular receiving requirements. Ideal for flight line checkout.



MOBILE TELEMETRY RECEIVING SYSTEM

← Telemetering on wheels! New portable test cart enables users to perform wide variety of telemetering functions in previously inaccessible locations, with greater efficiency and accuracy than ever before.

Technical bulletins on miniature receiving systems and other TDI products available on request.

TDI's newest office is now located at 305 Washington Avenue SE, Albuquerque, New Mexico

- TELEMETERING
- MISSILE GUIDANCE
- GROUND ELECTRONICS SYSTEMS
- AIRBORNE ELECTRONICS SYSTEMS

TELE-DYNAMICS INC.

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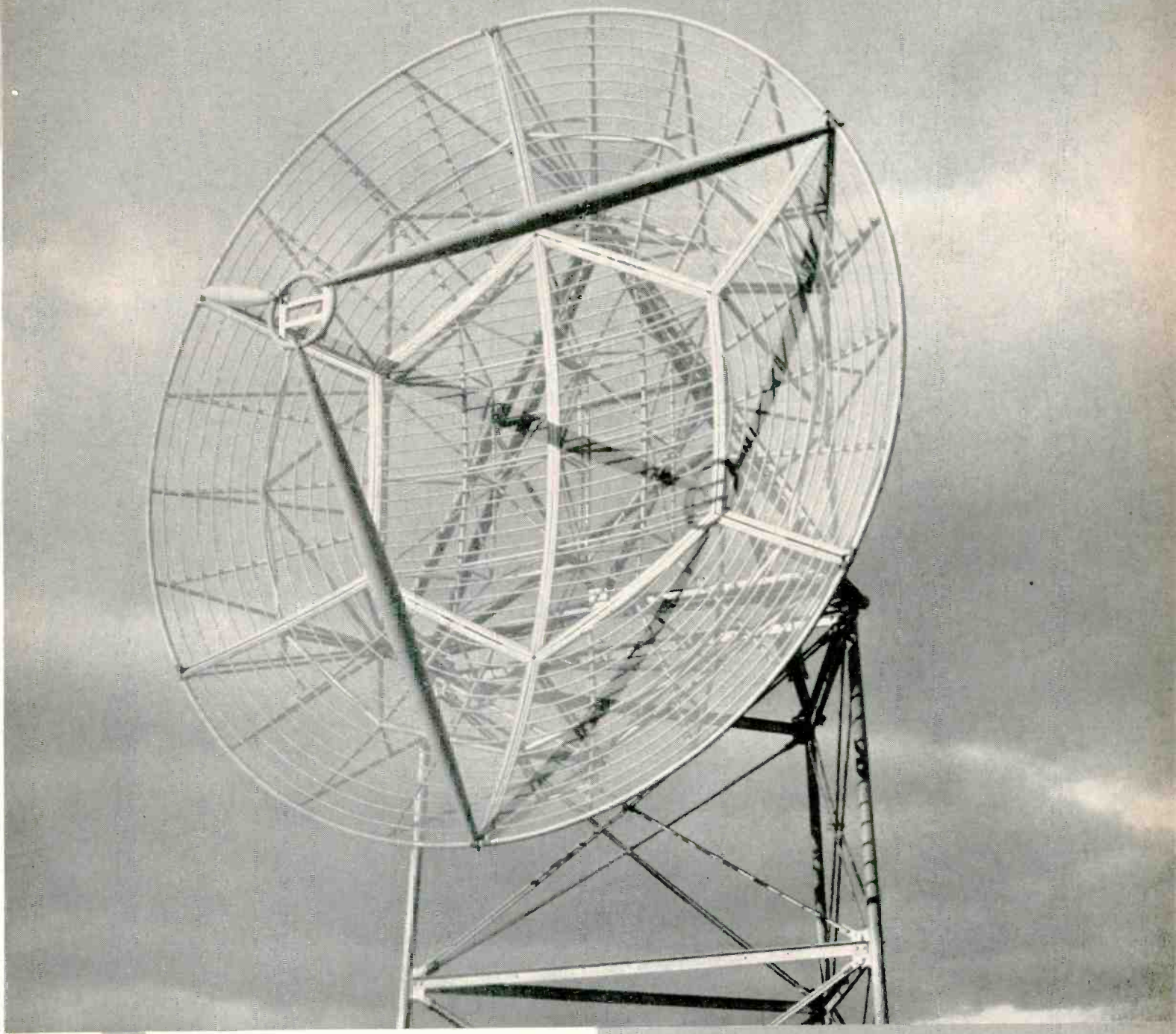
KENNEDY INTRODUCES

the 28 foot "TUF-SCAT" *antenna*



This new scatter antenna is specifically designed for the world's toughest weather conditions. Recently static load tested with over 32 tons (105 lbs./sq. ft.) on its surface, this big dish and tower have been carefully engineered and constructed to withstand winds in excess of 150 M.P.H. Even a 6" layer of ice won't disturb its performance. It is, in fact, the most rugged aluminum antenna ever built. Yet, its light weight, sectionalized aluminum construction keeps shipping costs down, makes assembly easy.

YOU CAN'T MISS US AT THE I.R.E. SHOW-BOOTH #2344

ANTENNA EQUIPMENT

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Tracking Antennas – Radio Telescopes – Radar Antennas –
"Trans-Horizon" Antennas: Ionospheric Scatter – Tropospheric Scatter

Transitron

Silicon

Transitron's diodes, voltage regulators and rectifiers are designed to operate over wide environmental extremes and meet the many varied requirements of electronic circuitry. Reliability is assured through hermetic sealing and exacting manufacturing standards.

Transitron's silicon units have established a record of dependability in such critical applications as guided missiles and jet aircraft. They feature low inverse leakages and high voltage operation and are recommended for high temperature applications where germanium and selenium are unreliable.

- Current ratings up to 2 amps
- Superior regulating qualities
- Rugged construction
- Small size
- Axial mounting

Send for Bulletin TE-1352

VOLTAGE REGULATORS

	Type	Voltage Range	Dynamic Resistance	Maximum Current @ 25°C (ma)	Maximum Current @ 125°C (ma)
Subminiature	SV-6	5.2 - 6.4	20	40	8
	SV-9	7.5 - 10.0	15	25	5
	SV-15	13.5 - 18.0	120	14	3
	SV-24	20.0 - 27.0	300	10	2
Miniature	SV-805	5.2 - 6.4	20	120	24
	SV-808	7.5 - 10.0	15	75	15
	SV-815	13.5 - 18.0	120	40	8
	SV-824	20.0 - 27.0	300	27	5
				(amps)	(ma)
Power	SV-905	5.2 - 6.4	.7	1.6	400
	SV-908	7.5 - 10.0	.8	1.0	250
	SV-915	13.5 - 18.0	3.0	.6	150
	SV-924	20.0 - 27.0	8.0	.4	100

"Leadership in semiconductors"

Germanium Diodes | Transistors | Silicon Diodes | Silicon Rectifiers

RECTIFIERS

	Type	Maximum Inverse Voltage	Maximum Forward Current (ma) @ 150°C	Maximum Inverse Current (ma) @ 150°C
Military	*1N256	570	200	.25
	*1N255	380	400	.15
	*1N254	190	400	.1
	*1N253	95	1000	.1
Miniature	TJ40A	400	200	.5
	TJ30A	300	200	.5
	TJ20A	200	200	.5
Stud Mounted	TM64	600	1000	.5
	TM47	400	3000	.5
	1N332	400	400	.2
	1N338	100	1000	.2
			(amps)	(ma)
Medium Power	TR402	400	20	5
	1N250A	200	20	5
	1N249B	100	20	5
High Power	TH402	400	35	5
	1N413A	200	35	5
	1N412A	100	35	5

*JAN types specified at 135°C

- Reliability at high temperature
- High power handling ability
- High efficiency
- Rugged construction
- Hermetic sealing

Send for Bulletin TE-1351

DIODES

	Type	Maximum Operating Voltage (volts)	Maximum Average Forward Current (ma) (@ 150°C)	Maximum Inverse Current (ua) @ volts (@ 150°C)
Military	*1N457	60	25	5 @ 60
	*1N458	125	25	5 @ 125
	*1N459	175	25	5 @ 175
High Conductance	1N484B	130	50	5 @ 125
	1N486A	225	50	25 @ 225
	1N488A	380	50	25 @ 380
			(@ 125°C)	(@ 125°C)
High Frequency	*1N251	30	30	10 @ 10
	1N252	20	40	10 @ 5
	S9G	40	25	10 @ 20
	Recovery time .15 usec			
			(@ 100°C)	(@ 100°C)
Fast Switching	SG213	200	12	50 @ 175
	SG211	80	12	20 @ 60
	Recovery time .3 usec			
	SG228	200	35	50 @ 175
	SG226	80	35	20 @ 60
	Recovery time 1 usec			

*JAN types

- Recovery times under .15 us
- High voltage ratings
- Operation up to 200°C
- High inverse resistance
- Subminiature size

Send for Bulletin TE-1350

Visit us at IRE Show Booth 3912-14

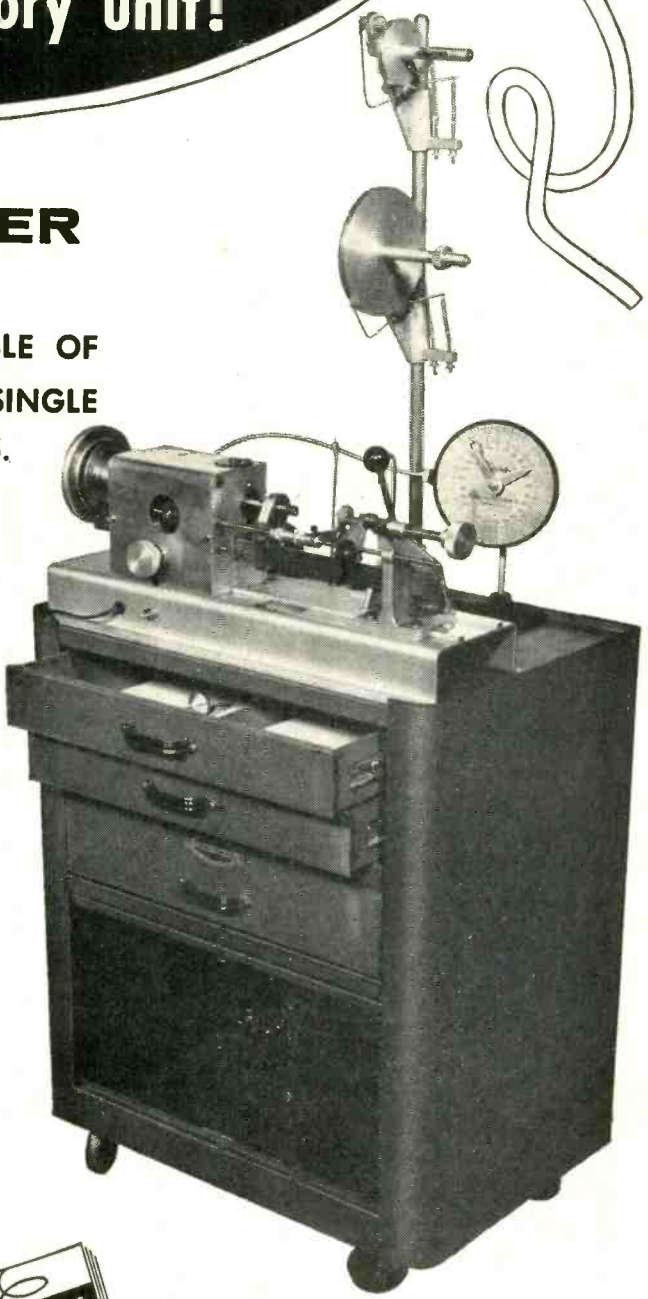
Transitron electronic corporation

wakefield, massachusetts

NOW... the world's most Versatile Coil Winder available as a complete laboratory unit!

MODEL W COIL WINDER

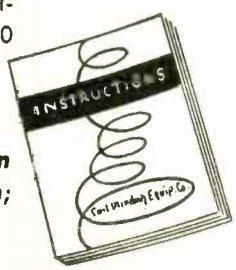
THE ONLY COMMERCIAL MACHINE CAPABLE OF WINDING LATTICE—BOBBIN—INTERLEAVED—SINGLE LAYER—BANK WOUND—INTERWOVEN COILS.



Now the world's most versatile coil winder made up in one mobile compact unit complete with all necessary equipment e.g. lubricants, wrenches, instruction book, etc. The model W is capable of winding every type of coil required in the electronic or industrial laboratory except toroids.

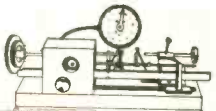
SPECIFICATIONS

⅛ HP motor and speed control—Gears from 25-100 teeth—Wire Guide for universal or lattice winding—Wire Guide for bobbins or layer winding—Wire Guide for single or multiple layer coils to 6" in length—3:1 reverse idler for bank winding and long multiple layer coils—Cams for continuous traverse adjustment, 0"-1½"—Large yoke for larger bobbins and transformers—Available with clock counter calibrated in ¼ turns or with drum type predetermining counter—Universal type arbor for coils with hollow cores—Pi spacing attachment with 1/32 index plate—Adjustable bank winding cam—Feeds for wire as fine as .001"—Rack feed range .00083" to .150" per turn (7-1200 TPI). Maximum distance from head to tailstock 8"—Layer wound coils using cam traverse 2 to 600 TPL. Net weight 140 lbs.



Model W with cabinet comes with 50 page instruction book complete with charts for universal computation; work sheets and nomographs.

Cabinet made of auto body steel with reinforced corners and ends; heavy duty ball bearing rubber tired caster with 2 foot brakes; size 17x25½x32" high; one cylinder lock secures all compartments.

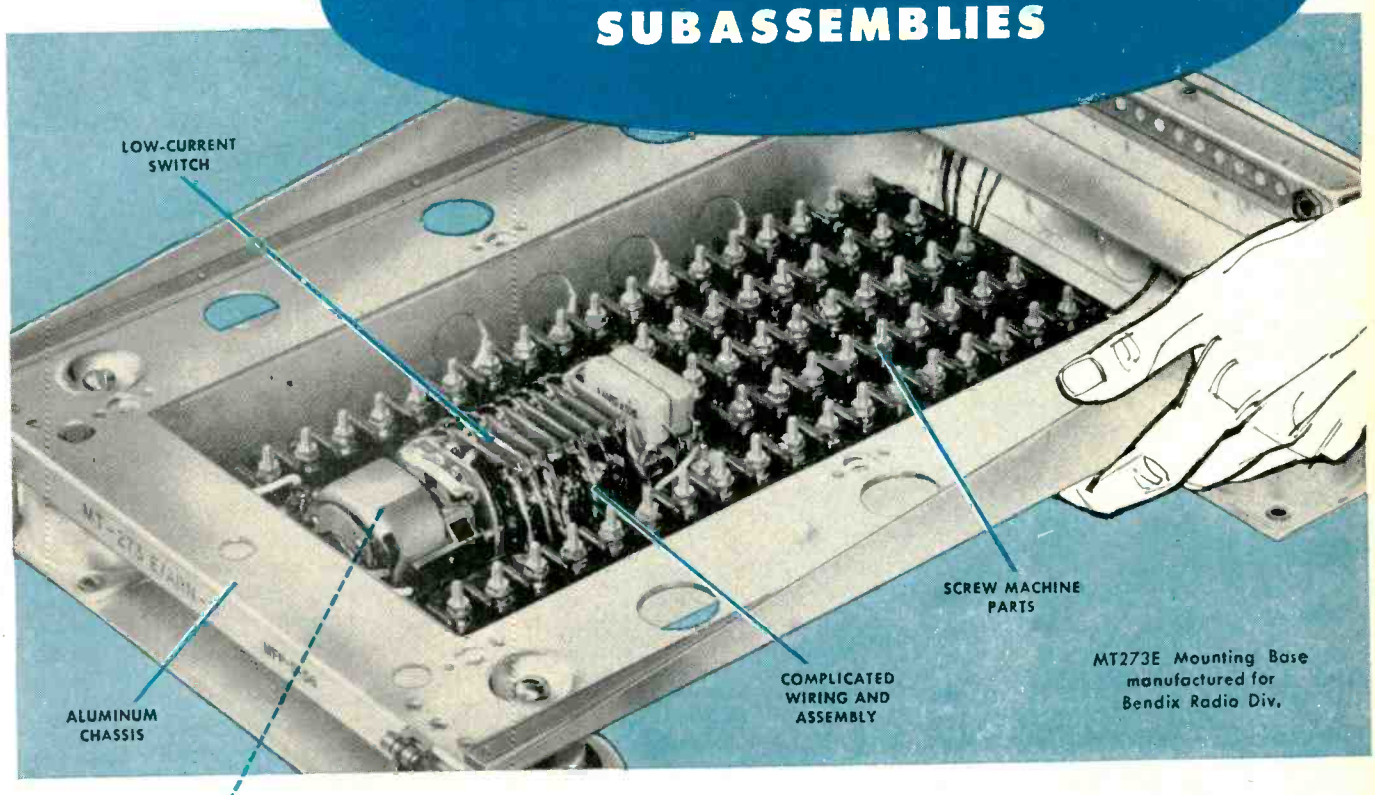


COIL WINDING EQUIPMENT CO., OYSTER BAY, N.Y. – OYster Bay 6-1285 CWEC

VISIT US AT BOOTHS 4502-4601—RADIO ENGINEERING SHOW

OAK can engineer and manufacture your

REMOTE-CONTROLLED SUBASSEMBLIES



. . . one *source* . . . one *responsibility* for your electro-mechanical requirements

OAK ROTARY SOLENOID*

*Mfd. under license from G. H. LELAND, INC.

Oak rotary solenoids are ideally suited as actuators for remote control of complex circuits under the severe environmental conditions of MIL-S-4040A, and other specifications which are typical of air-borne, mobile, or military apparatus. They are compact and rugged—being practically solid metal throughout. Oak rotary solenoids are exceptionally adaptable, too. They can be used to drive switches, gear trains, and many other mechanisms requiring a restricted rotary stroke with repetitive operation. Wire-saver circuitry is available to help you economize on wiring.

For the above subassembly, Oak stamps, draws, welds, and etches the aluminum chassis . . . builds the rotary solenoid switch . . . manufactures the screw machine parts . . . makes the complicated cable harness . . . assembles all the parts . . . then runs life tests, heat and cold checks, and humidity chamber trials.

Besides complete facilities, Oak has the knack for making complicated devices producible. Why not contact Oak engineers about your own requirements? Do it early in the design stage. Time and again, they have been able to suggest changes that resulted in lower costs and better operation.

Phone or Write Our Mr. Howard Olson, Today, on *Any Aspect* of Your Subassembly Projects.

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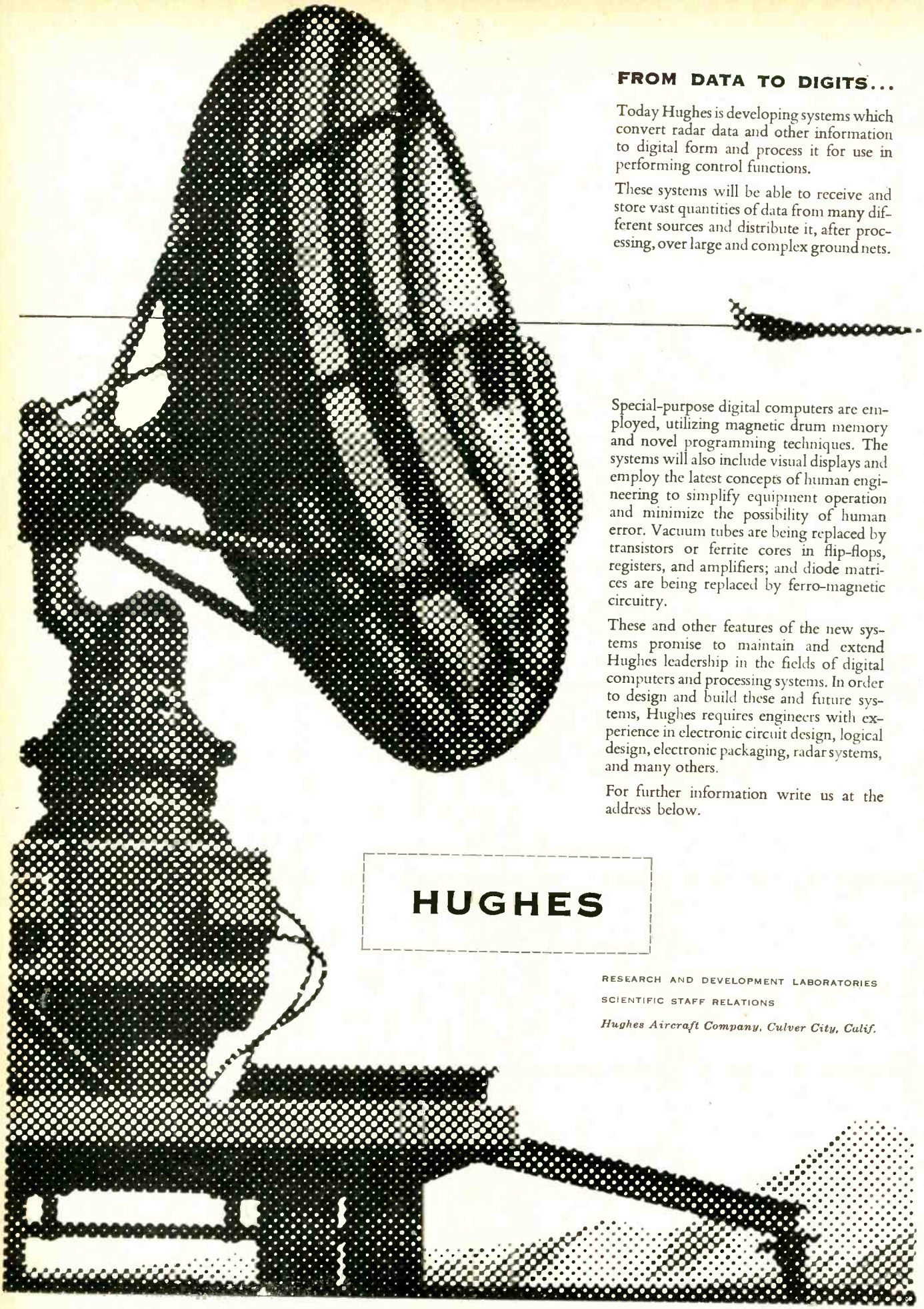

FROM DATA TO DIGITS...

Today Hughes is developing systems which convert radar data and other information to digital form and process it for use in performing control functions.

These systems will be able to receive and store vast quantities of data from many different sources and distribute it, after processing, over large and complex ground nets.

Special-purpose digital computers are employed, utilizing magnetic drum memory and novel programming techniques. The systems will also include visual displays and employ the latest concepts of human engineering to simplify equipment operation and minimize the possibility of human error. Vacuum tubes are being replaced by transistors or ferrite cores in flip-flops, registers, and amplifiers; and diode matrices are being replaced by ferro-magnetic circuitry.

These and other features of the new systems promise to maintain and extend Hughes leadership in the fields of digital computers and processing systems. In order to design and build these and future systems, Hughes requires engineers with experience in electronic circuit design, logical design, electronic packaging, radar systems, and many others.

For further information write us at the address below.

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Three unusual direct-display storage tubes by Hughes

MEMOTRON

FEATURES: bright display . . . constant and uniform intensity of presentation . . . no perceptible transient decay . . . simplifies photography. APPLICATIONS: transient analysis . . . spectrum analysis . . . direct comparison of wave forms. SPECIFICATIONS: 100,000 inches/sec. writing speed . . . stores traces until intentionally erased . . . erasure triggered by push-button, or programmed voltage . . . electrostatic focusing and deflection.

MEMO-SCOPE

Model 104, incorporating MEMOTRON, is a new memory oscilloscope with 5 optional preamplifiers to satisfy the most critical production, test and laboratory requirements.

TONOTRON

FEATURES: half-tone presentation . . . excellent grey scale . . . controllable decay rate . . . compact design. APPLICATIONS: closed circuit TV . . . instrumentation . . . P.P.I. . . . narrow band, slow scan TV. SPECIFICATIONS: 1,000 foot-lamberts brightness at 10 kv . . . electrostatic focusing . . . magnetic deflection . . . . 60 lines per inch resolution . . . writing speed of 150,000 inches/sec.

TYPOTRON

FEATURES: high brightness . . . permanent display until intentionally erased . . . rapid display of printed data . . . 63 character matrix. APPLICATIONS: digital computers . . . teletype reception . . . wherever printed data must be displayed rapidly for use by human operator. SPECIFICATIONS: writes up to 25,000 characters/sec. . . . permanent storage until erased . . . almost instantaneous erasure . . . electrostatic focusing and deflection.

See demonstrations of these tubes and MEMO-SCOPE *at the I.R.E. Show, booths 2801, 2803, 2805, Second Floor. For additional information write to:*

HUGHES PRODUCTS • ELECTRON TUBES
International Airport Station, Los Angeles 45, California

HUGHES PRODUCTS

Now!

New low cost oscillator covers entire audio band in one sweep of the dial

-hp- 207A Audio Sweep Oscillator—continuous output 20 cps to 20 KC—flat response, low distortion—may be motor driven or coupled to recording device

SPECIFICATIONS

Frequency Range:
20 cps to 20 KC, covered in one range.

Accuracy:
±4% including changes due to warm-up, aging components, tubes, etc.

Dial:
Six-inch diameter dial calibrated over 300° of arc.

Frequency Response:
±1 db entire frequency range.

External Frequency Control:
¼-inch shaft, extending from rear of instrument, rotation approximately 150° for full frequency coverage.

Output:
10 volts into 600 ohm rated load, balanced or 1 terminal at ground.

Output Control:
Decreases level continuously by more than 40 db.

Distortion:
Less than 1% over entire frequency range.

Hum Voltage:
Less than 0.1% of rated output. Decreases as output is attenuated.

Power:
115/230 volts, ±10%, 75 watts.

Dimensions:
Cabinet Mount: 7½" wide, 11½" high, 15¼" deep. Rack Mount: 19" wide, 7" high, 12½" deep.

Weight:
Approximately 25 lbs.

Price:
$275.00

Data subject to change without notice

Here at last is a low cost, high quality oscillator providing the time-saving convenience of continuous single-sweep frequency coverage from 20 cps to 20 KC. The instrument has high waveform purity, constant output, high stability and dial calibration which is essentially logarithmic. Band switching and resulting transients are eliminated. A flexible 10 volt output can be used balanced or with one side grounded.

Model 207A may be swept by hand, motor driven, tuned remotely or coupled to a recording device by means of a shaft extended through the rear of the cabinet.

Priced at just $275.00, this new *-hp-* oscillator is an outstanding value and particularly convenient for such audio tests as speaker frequency response and amplifier flatness, measuring characteristics of filter networks, complex coupled systems and industrial transducers, or automatic response measurements where response is recorded or viewed on an oscilloscope.

See the new -hp- 207A at the IRE Show, Booths 2509- 2511-2513.

550A — highly stable, wide band; 10 cps to 10 MC. For audio, supersonic, video, rf measurements. Output 15 mw/3 volts. Frequency response flat ±1 db. $490.00.

200AB — for audio tests, 20 cps to 40 KC. Output 1 watt/24.5 volts. Simple to use, compact, rugged. $130.00.

233A — carrier test oscillator covering frequencies 50 cps to 500 KC. Output 3 watts/600 ohms. $475.00.

200CD — popular precision instrument for audio and ultrasonic tests. 5 cps to 600 KC; output 160 mw/10 volts; 20 volts open circuit. $160.00.

11 additional -hp- quality oscillators

- outstanding value
- complete coverage 0.008 cps to 10 MC
- stable RC circuit pioneered by -hp-
- each instrument designed to do a specific job best

206A — very low distortion; for high quality, high accuracy audio tests. Covers 20 cps to 20 KC; output +15 dbm. $565.00.

200J — extreme accuracy for interpolation and frequency measurements. Covers 6 cps to 6 KC, output 160 mw/10 volts; 20 volts open circuit. $275.00.

205AG — time-tested convenience for high power tests, gain measurements. 20 cps to 20 KC 5 watts output. $440.00.

200T — custom-engineered for telemetry, carrier current tests. 250 cps to 100 KC, output 160 mw/10 volts; 20 volts open circuit. $350.00.

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World's most complete line of fast, accurate, easy to use oscillators!

202C — replaces famous 202B for low frequency measurements 1 cps to 100 KC. Output 160 mw/10 volts; 20 volts open circuit. $300.00.

202A — for servo, vibration, medical and other very low frequency measurements. 0.008 to 1,200 cps. Output 20 mw/10 volts. $465.00.

201C — specifically designed for high quality audio tests. Covers 20 cps to 20 KC. Output 3 watts/42.5 volts. $225.00.

4170

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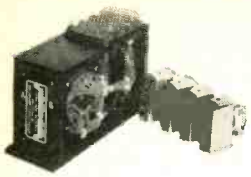
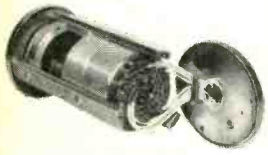
TYPICAL ASCOP SWITCHES

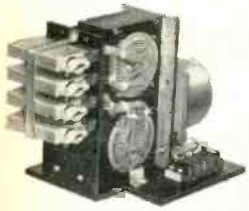


STRAIN GAUGE SAMPLING

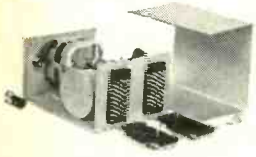
TELEMETERING



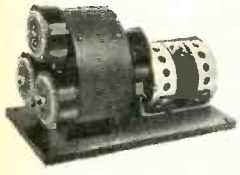
GUIDANCE



THERMOCOUPLE SAMPLING

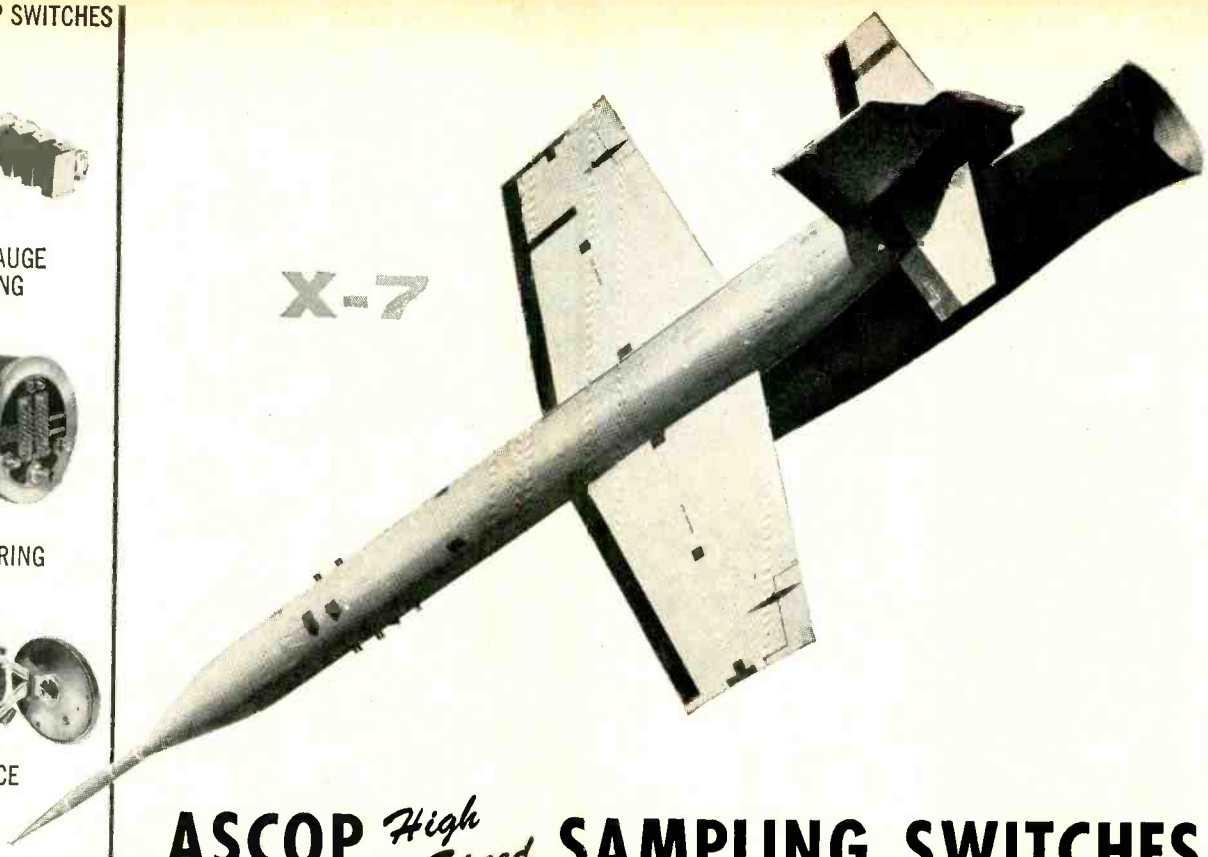


DRIFT COMPENSATION



RADAR DISPLAY

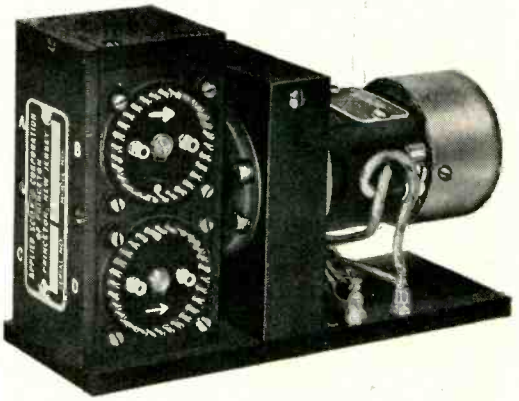
CRO DISPLAY



ASCOP *High Speed* SAMPLING SWITCHES

Help Spearhead Ramjet Research in the Lockheed X-7

The needle-nosed X-7 is playing a major role in the development of powerful new engines for Air Research & Development Command ramjet missiles. ASCOP high speed rotary sampling switches are employed in this "flying laboratory" to provide detailed information on *flight attitude, supersonic airspeed, temperature* and *stress*. As many as 100 measurements of aerodynamic behavior are provided by ASCOP Switches for transmitting to ground stations where the vital statistics are analyzed to contribute to better ramjet performance. ASCOP is the leading manufacturer of rotary sampling switches and has over 200 standard models for use in telemetering, drift compensation, thermocouple sampling, radar display and countless other applications. Write for complete details.



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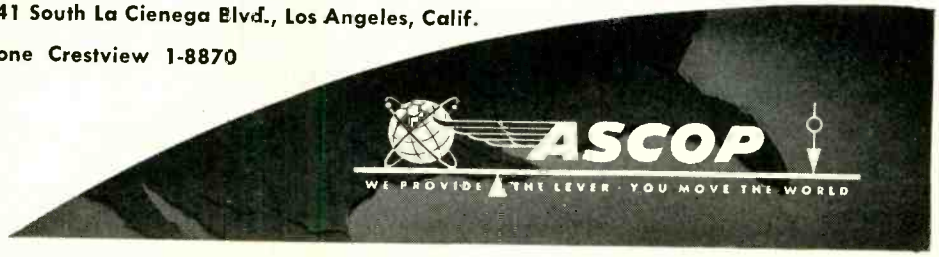

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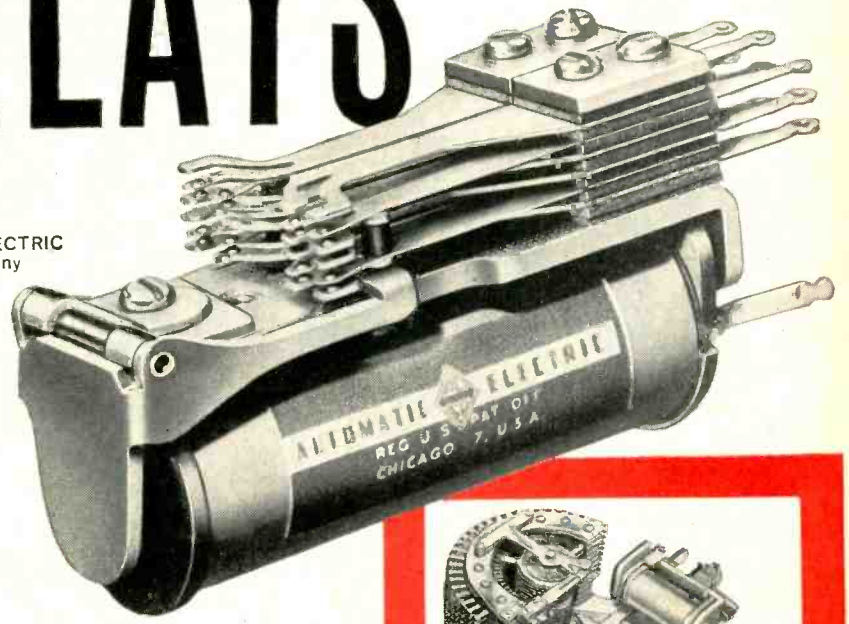

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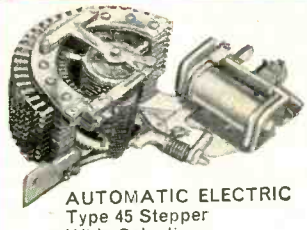

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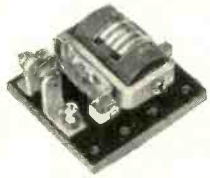

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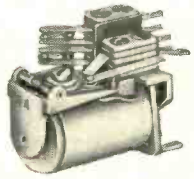

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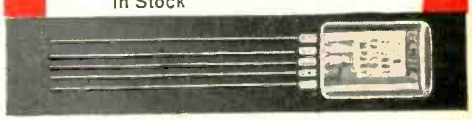

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No blue sky...just to back up our belief that you and Collins

We're going to build a proposition which we believe deserves your most serious consideration, if you are a mechanical or electrical engineer. This proposition is built on pure and simple fact—no high flown promises or broad generalities. Our proposition: you and Collins should get together. We present these facts to support it.

FACT NUMBER 1:

Collins Radio Company's sales have increased 10 fold in each of three successive seven year periods. 1933 sales were $100,000; 1940 sales, $1,000,000; 1947 sales, $10,000,000; 1954 sales, $100,000,000, and 1956 sales, $126,000,000. (Note graph.) This company *has grown, and is growing* at a phenomenal rate. Total employment is 9,000 of which 24% are research and development personnel.

You grow when the company you work for grows.

FACT NUMBER 2:

As shown in the graph at right, the employment of research and development personnel has increased steadily despite fluctuation in sales. Notice that even during periods of national sales regression Collins continued to strengthen its engineering staff.

Collins has based its growth on the solid foundation of stability in the engineering department.

FACT NUMBER 3:

At Collins, the ratio of engineers to total employees is extremely high, far higher than the average among established companies engaged in both development and production. First and foremost, Collins is an engineering company.

Engineering is king at Collins—never takes a back seat to production expediency.

FACT NUMBER 4:

Collins' reputation for quality of product is universally recognized. It has led to Collins' phenomenal sales record. At Collins there is no compromise when quality is at stake.

If you're the man we want, you'll get real satisfaction out of this quality-consciousness.

FACT NUMBER 5:

Electronics is Collins' only interest. In no way is it subsidiary to the manufacture of industrial or consumer products. Collins builds electronic equipment, not airplanes or vacuum cleaners. Every research, development and production facility is devoted to progress in electronics.

If electronics is your interest, you'll like the climate at Collins.

FACT NUMBER 6:

There is a limitless variety of fields and types of work for the Collins engineer. Recent Collins work in air and ground communication, and aviation electronics include developments in transhorizon "scatter" propagation; single sideband; microwave and multiplex systems; aircraft proximity warning indicator; aviation navigation, communication and flight control; broadcast; and amateur equipment.

There is big opportunity for your special talents.

Right now we are prepared to offer you a technical or supervisory assignment in one of many interesting fields. And the sky *is* the limit as far as responsibility and salary are concerned.

You will work in one of Collins' new research and development laboratories located at Cedar Rapids, Iowa; Dallas, Texas; and Burbank, California. Offices and subsidiary companies are located in New York; Washington, D. C.; Miami; Knoxville; Seattle; Hickman Mills, Missouri; Toronto, Canada; London, England; and South America.

All your moving expenses are paid. Company benefits are tops in the industry.

We repeat—if you are a mechanical or electrical engineer, you and Collins should get together. Take the first step now, send your resume today to:

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Fred Aiken
Collins Radio Co.
2700 W. Olive Ave.
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Collins Radio Co.
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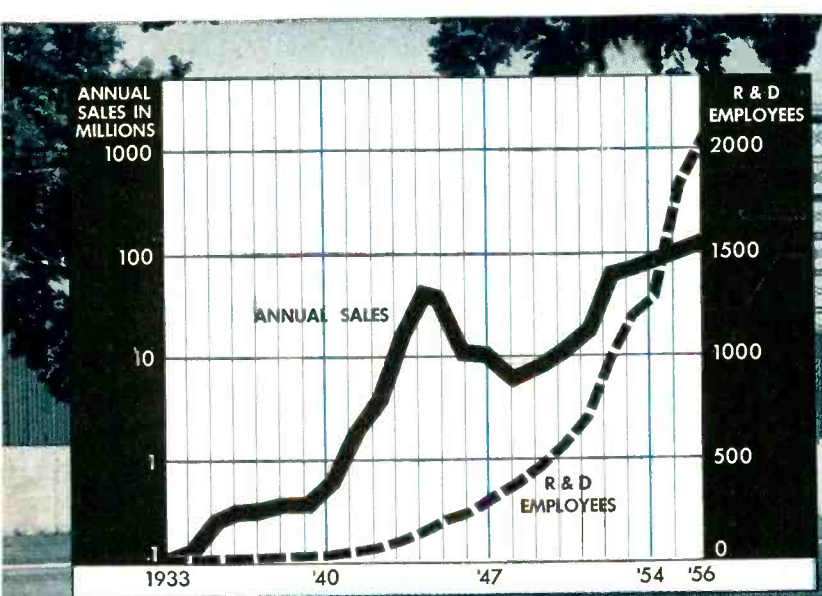
Dallas, Texas

black and white facts

should get together

Collins will be interviewing engineers and tech writers at the IRE Show in New York March 18-22. Call L. R. Nuss, CIrcle 5-7076, for a personal, confidential interview.



This graph shows the relationship between sales and employment of engineering personnel at Collins. Notice the steady increase in research and development employment despite sales fluctuations.

Collins new research laboratory building at Cedar Rapids, Iowa. Air-conditioned, shielded against radio waves, completely equipped.

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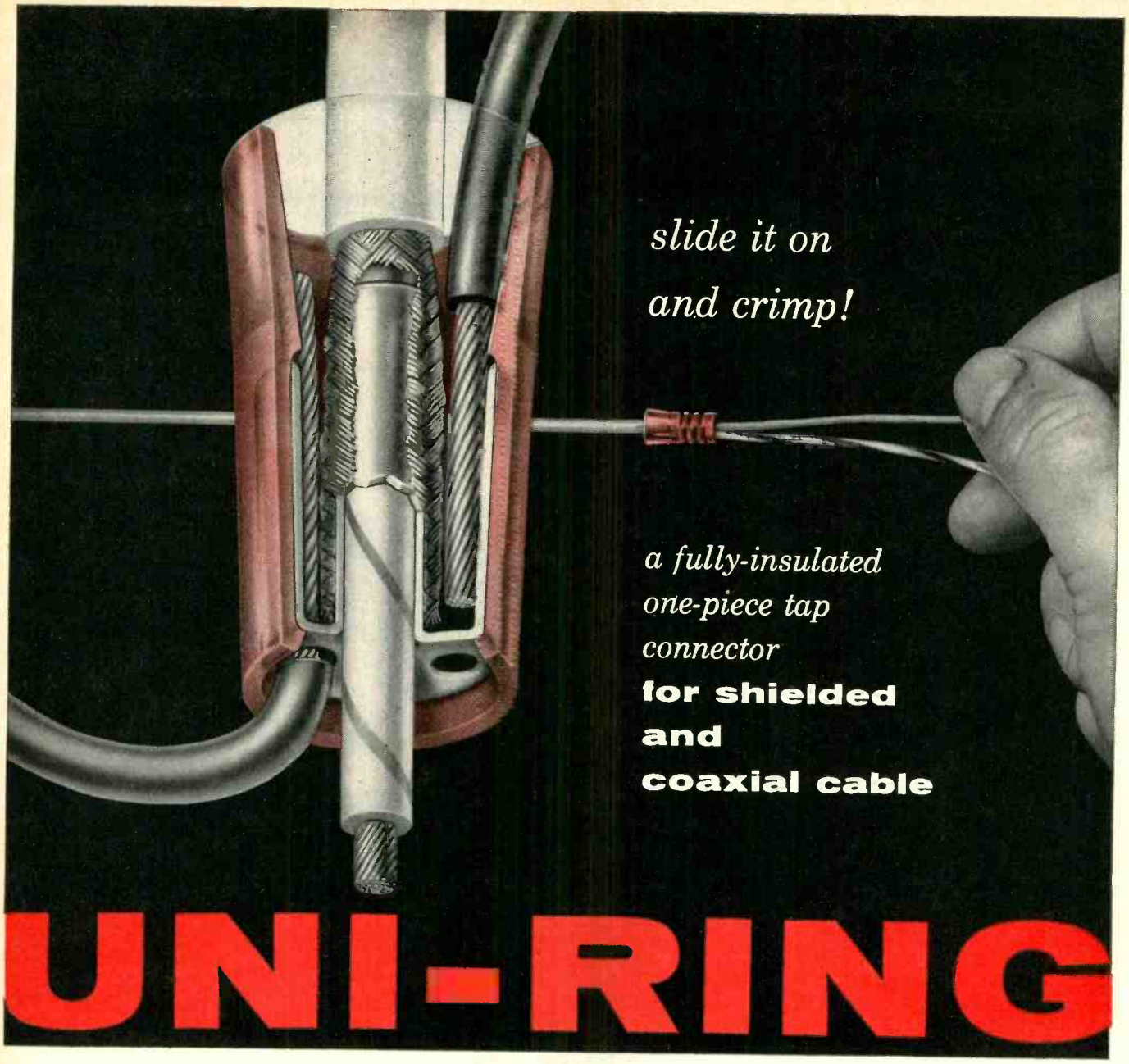

UNI-RING offers a tremendous saving in installation time over any previous method of tapping or terminating shielded or coaxial cable. As the inner ring slides under the shielded braid, the tap wire is held between the braid and the outer ring. Single or multiple taps, from either the front or back of the connector, can be accommodated . . . A single crimp, using the same basic HYTOOLS used for installing HYRINGS, completes the uniform, secure, and insulated assembly.

The protecting nylon insulation extends beyond both ends of the UNI-RING, eliminating metal-to-metal contact and preventing harmful wire-chafing in tight locations. The UNI-RING is color-coded to indicate conductor sizes.

UNI-RING's one-piece design insures electrical integrity, prevents heating, and eliminates noises caused by isolated metal parts.

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with ceramic tubes that can

Ceramic Receiving Tubes
Eimac, the world's largest manufacturer of transmitting tubes, enters the receiving tube field with a significant new concept—the stacked ceramic receiving tube. Design eliminates internal insulators and spacers. These new stacked ceramic tubes can withstand heavy shock and vibration with low noise output.

3CX100A5
Here is a new premium quality ceramic and metal 100-watt triode similar to the 2C39B. It is used as a CW amplifier or oscillator to 2500 megacycles, and in pulse applications to 3000 megacycles.

4K50,000LQ
This four-cavity externally-tuned klystron is typical of an extensive line of Eimac high and super power klystrons for UHF/microwave application. Water and forced air cooled, the Eimac 4K50,000-LQ will deliver 10,000 watts of power at frequencies up to 1000 megacycles.

2CL40A
A new, small ceramic high vacuum rectifier or clipper diode that can be air or liquid cooled. Under the latter conditions, average plate current is 120 milliamperes, with a peak inverse voltage of 16,000 volts.

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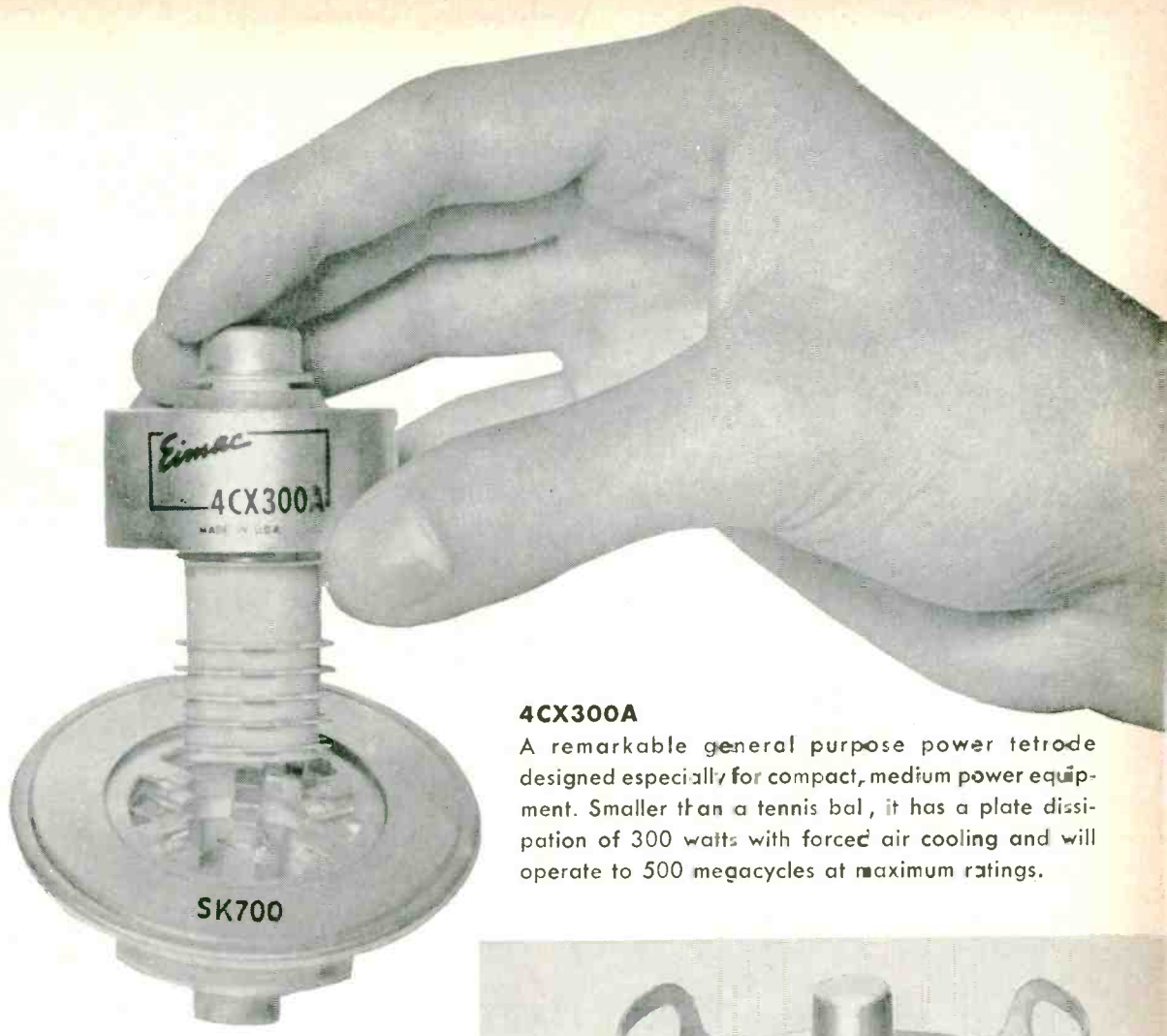

4CX300A
A remarkable general purpose power tetrode designed especially for compact, medium power equipment. Smaller than a tennis ball, it has a plate dissipation of 300 watts with forced air cooling and will operate to 500 megacycles at maximum ratings.

In recent years equipment manufacturers and users have been introduced by Eimac to a series of ceramic tube firsts unequalled in the industry: klystrons, negative grid tubes, rectifiers and receiving tubes.

Clean, and rugged...these tubes can stand up to shocks and temperatures no glass tube can. Design and production advantages are a boon to equipment manufacturers and users alike.

As first in the field, Eimac has developed ceramic tube manufacturing techniques that have evolved into well established processes.

See this line of "tubes that can take it" at the Eimac exhibit, Booth 2410-12, National I. R. E. Show and Convention, March 18-21.

Eimac

EITEL-McCULLOUGH, INC.
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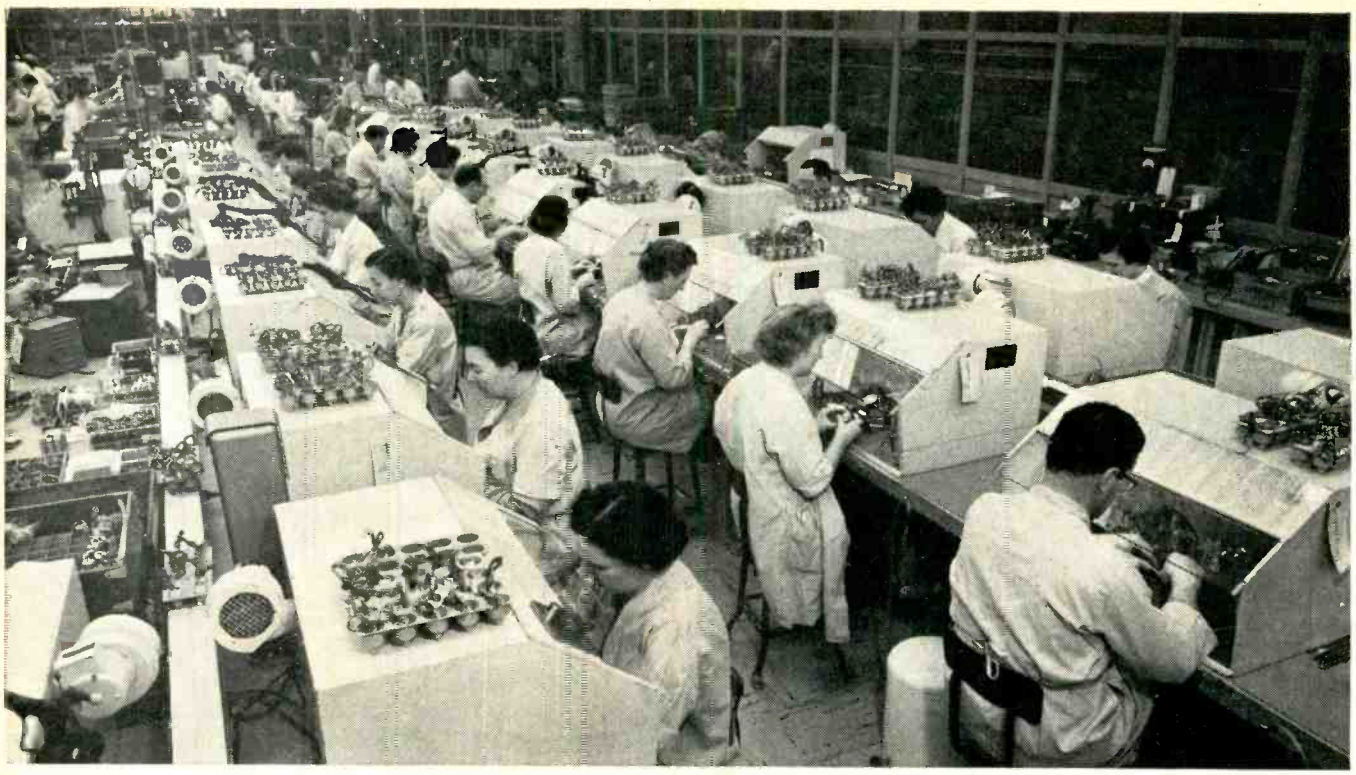
4CX5000A
This Eimac radial-beam power tetrode is especially suitable for single sideband operation. A rugged ceramic tetrode, it delivers 10 KW output in Class AB1 service and handles high inputs without going into the positive grid region.



Portion of Eclipse-Pioneer's synchro calibration and test facility.

WHY IT PAYS TO SHOP AT THE BENDIX "SUPERMARKET"

— NATION'S LARGEST PRODUCER OF SYNCHROS

SHAFT POSITION-TO-DIGITAL CONVERTERS

Eclipse-Pioneer Coded Commutator type shaft position-to-digital converters are miniature devices for converting Analog information to Binary Digital form. Designed for Digital control systems, data processing equipment, telemetering applications, or computers. Especially suited to oir-borne use.

Specifications:

	Model GS-1-A1	Model GS-2-A1
Type output	8 digit gray (Reflected Binary Code)	7 digit Natural Binary Code (double brush)
Shaft resolution	1 part in 256	1 part in 128
Current rating	.015 amps. (max.) per digit with non-inductive loading	.015 amps. (max.) per digit with non-inductive loading
Shaft speed	Max. continuous input of 150 revs. per minute	Max. continuous input of 150 revs. per minute
Input torque	0.2 ounce-inch (max.)	0.4 ounce-inch (max.)
Diameter of unit	15/16 inch	15/16 inch

In buying precision synchros, doesn't it make a lot of sense to insist on getting exactly what you want, when you want it—and at minimum cost?

Best way to be *sure* you get all three is to depend on the Bendix "Supermarket".

Our mass synchro production facilities . . . the nation's largest . . . are constantly turning out just about all types of synchros imaginable. This means we can offer you immediate delivery of most synchro types—and minimum cost on all synchro types, even for small quantity orders.

You can depend on the quality of Bendix synchros, too. They will equal . . . or exceed . . . the accuracy of any other synchros made today. Sound reasons why you'll be ahead to rely on the experience and mass-production facilities of *Bendix*.

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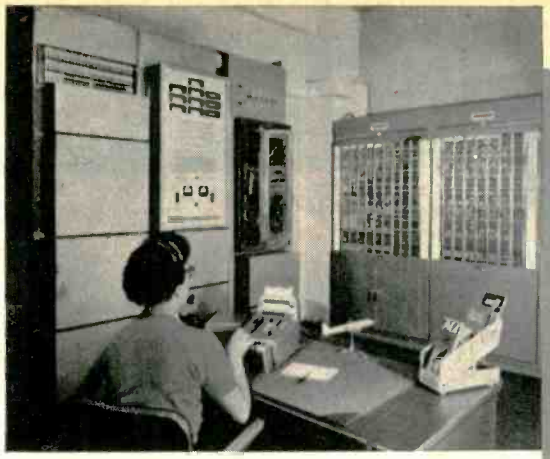


AMP'S PATCHCORD PROGRAMMING SYSTEM

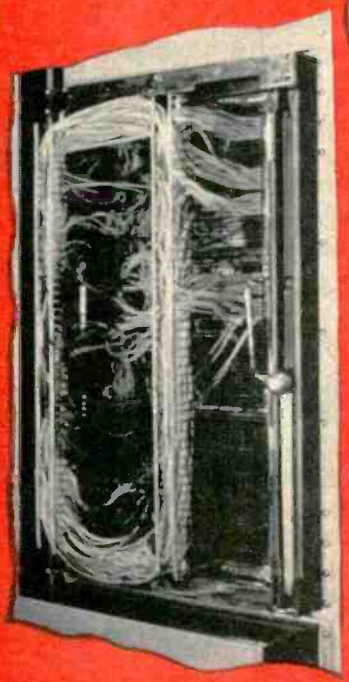
Speeds confirmation of airline reservations

A wide variety of AMP Taper Technique product provides long-life assurance of perfect electrical terminations and is a contributing factor in keeping electronic equipment compact. The AMP Patchcord Programming System offers a multiformity of internal wiring arrangements and connections and permits circuit versatility by use of prepatched, removable front boards.

A number of major airlines, including the Long Island City facilities of Pan American Airlines (shown above), have installed electronic equipment manufactured by Teleregister Corporation, Stamford, Connecticut to eliminate delay and uncertainty in air travel reservations procedure. AMP Taper Technique and AMP Patchcord Programming Systems are prominent in the design of this equipment.

AMP Taper Technique and AMP Patchcord Programming Systems have been utilized for years to solve problems inherent in the design of computers, business machines, and automatic control equipment.

Complete information is available on request.



You are cordially invited to visit our display at the IRE show in New York City, March 18th to 21st, 1957.
BOOTHS 2427-2429

AMP INCORPORATED AMP® *General Office: Harrisburg, Pa.*

Wholly Owned Subsidiaries: Aircraft-Marine Products of Canada Ltd., Toronto, Canada
Aircraft-Marine Products (G.B.) Ltd., London, England
Societe AMP de France, Le Pre St. Gervais, Seine, France
AMP—Holland N.V. 's-Hertogenbosch, Holland
Japanese Distributors: Oriental Terminal Products Co., Ltd., Tokyo, Japan

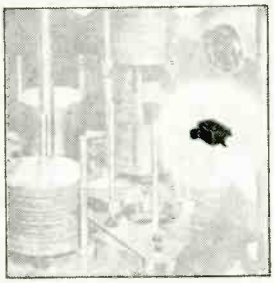
Want more information? Use post card on last page.

Switches have uses unlimited

Switches put "THINK" into this press transfer feed

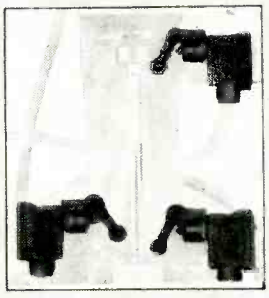
Here is a typical example of how a manufacturer improved his product. With MICRO SWITCH Precision Switches designed into the press, blanks are loaded and fed automatically, dangerous manual feeding is eliminated, mistakes are "erased" without interrupting production. This product improvement was due in no small measure to the help of MICRO SWITCH application engineers.

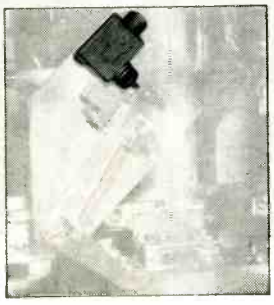
For more information for your design engineers, write for Catalog 83.



When a stack of blanks is nearly depleted, the descending elevator trips this switch which starts a motor and turns the six-station turret to the next full station for blanks.

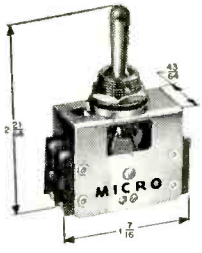
Plunger which picks up the blanks is controlled by switches shown. Upper switch stops the press if the blanks do not reach level of gripping fingers. Switch at left brings new stack of blanks into position. If stack doesn't come into position, the third switch stops press.





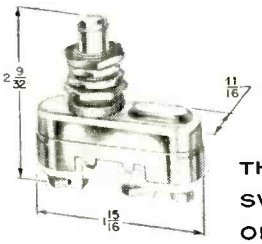
When two blanks stick together and feed into the press they trip this switch which actuates a solenoid and opens a trap door in the press bed. The blanks fall through, the press goes on uninterrupted.

SWITCH "REMEMBERS" CIRCUIT WHICH WAS LAST ACTUATED



This is the first of a new series of "electrical memory" toggle switches. The switch indicates through a pilot light or buzzer which circuit was last actuated. The assembly uses one pole of its four-pole circuitry to indicate which circuit was last operated. Use of this switch simplifies basic circuit designs of radar units, computers, aircraft control panels and other similar devices. Seal prevents entrance of liquids and dust. Basic switches are Underwriters' Listed at 5 amperes 125, 250 volts a-c, d-c rating at 28 volts-3 amperes at sea level, 2.5 amperes at 50,000 feet (inductive); 4 amperes at sea level and 50,000 feet (resistive); maximum inrush, 15 amperes.

Visit MICRO SWITCH Exhibit
Booths 2202-2212
at the I R E Show
New York Coliseum
March 18-21



THIS SWITCH OPERATES RELIABLY AT TEMPERATURES FROM −50° TO +1000° F

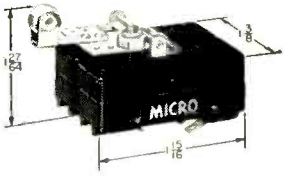
Use of laboratory-tested, heat-resistant materials makes this switch an extremely dependable component for use in applications where high temperatures are present. It will operate satisfactorily in a temperature range of −50° to 1000°F. Contact arrangements are single-pole double-throw. Switch is available in panel-mount design (shown) or with pin- or roller-plunger actuators.

(*Send for Catalog 77*)

A TWO-CIRCUIT SWITCH WITH ACCURATE REPEATABILITY

This switch uses a snap-action spring to provide quick make and break of both contacts in each double-break circuit. It is Underwriters' Listed for 10 amperes 125 or 250 volts a-c; ½ H.P. 125 volts a-c; 10 amperes 30 volts d-c.

(*Send for Catalog 62*)



TWO SWITCHES OPERATED BY A SINGLE LEVER ACTUATOR

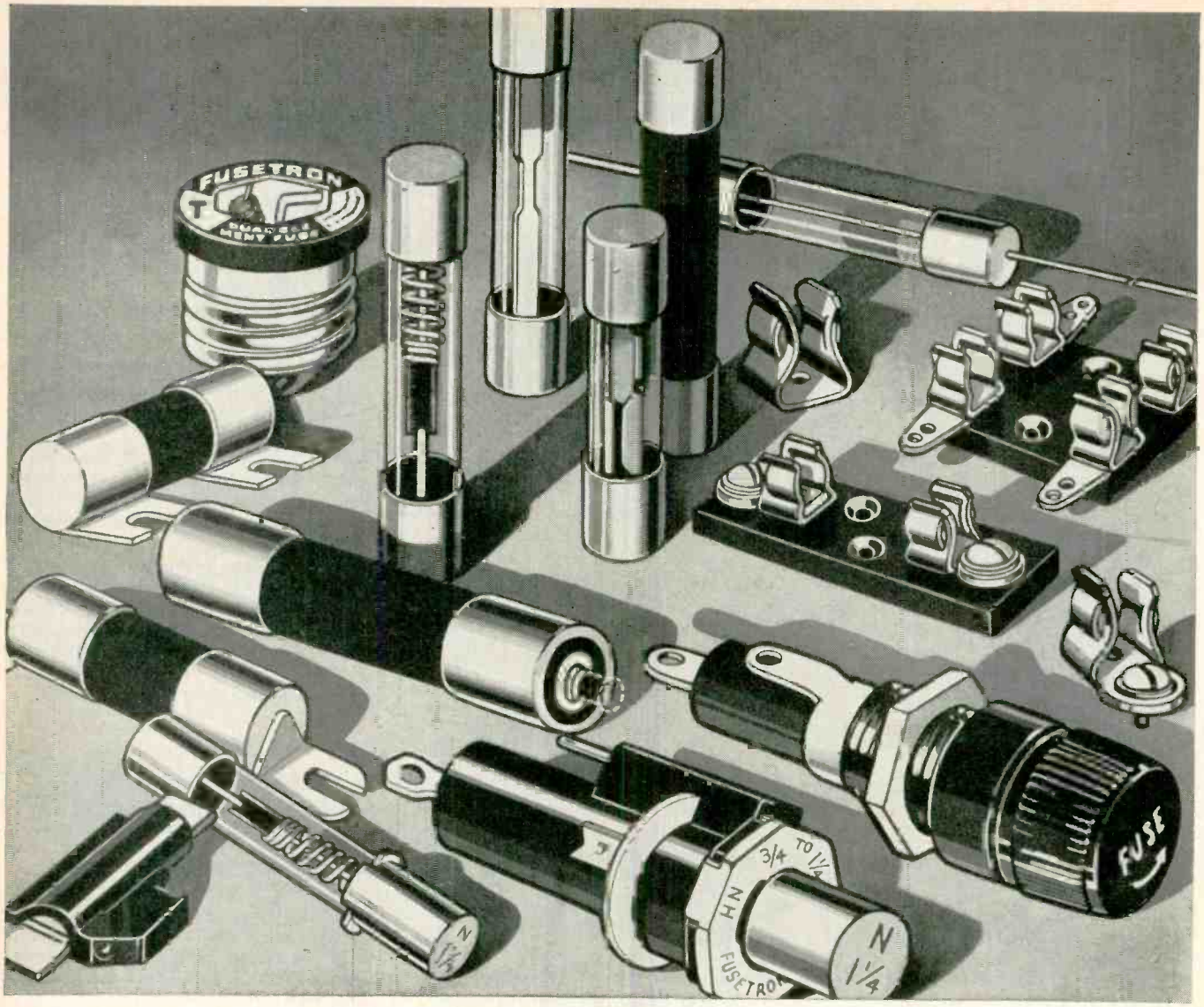
This is an assembly of two single-pole double-throw switches. It provides for switching of two isolated circuits at the same time. The basic units are listed by Underwriters' Laboratories at 15 amperes 125, 250 or 460 volts a-c; ½ ampere 125 volts d-c; and ¼ ampere 250 volts d-c.

(*Send for Data Sheet 100*)

MICRO SWITCH

A DIVISION OF MINNEAPOLIS-HONEYWELL REGULATOR COMPANY

In Canada, Leaside, Toronto 17, Ontario • FREEPORT, ILLINOIS



You can rely on BUSS FUSES to operate as intended.

Here's why— With BUSS fuses, dependable electrical protection isn't left to chance. BUSS fuses are tested in a sensitive electronic device. Any fuse not correctly calibrated, properly constructed and right in all physical dimensions is automatically rejected.

The result,—BUSS fuses provide maximum protection against damage due to electrical faults. And just as important, they eliminate useless shutdowns caused by faulty fuses blowing needlessly.

With a complete line of fuses available, it is just good business to standardize on BUSS. The "trouble-free" operation of BUSS fuses helps to assure that your product will operate as intended . . . thus, BUSS fuses help to maintain the reputation of your product for quality and service.

If you have an unusual or difficult protection problem, let the BUSS fuse engineers work with you and save you engineering time. If possible, they will suggest a fuse already available in local wholesalers' stocks, so that your device can be easily serviced.

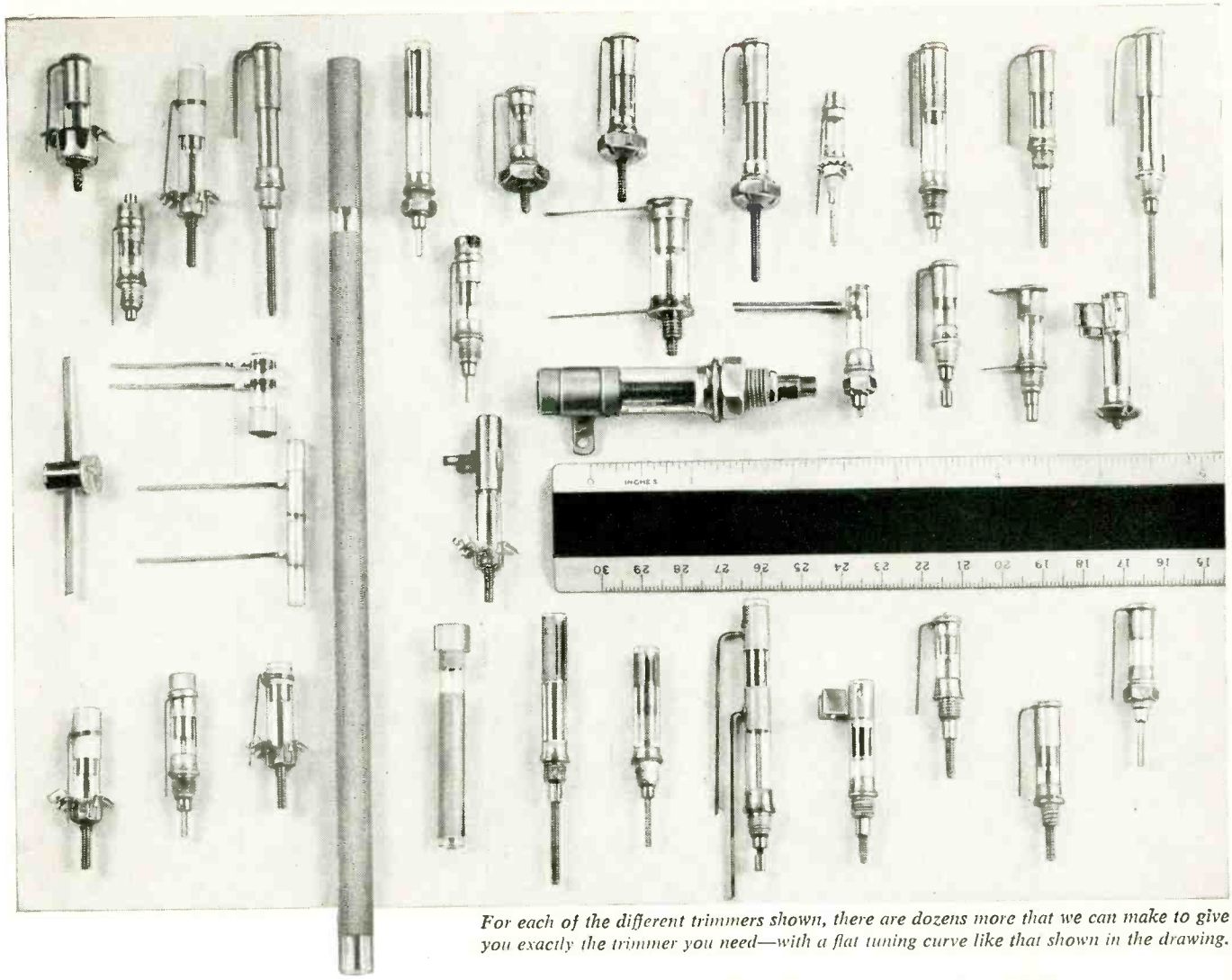
For more information on BUSS and Fusetron small dimension fuses and fuseholders . . . Write for Bulletin SFB, Bussmann Mfg. Co. (Div. of McGraw-Edison Co.), University at Jefferson, St. Louis 7, Mo.

BUSS fuses are made to protect – not to blow, needlessly

FUSETRON
TRUSTWORTHY NAMES IN ELECTRICAL PROTECTION
BUSS

Makers of a complete line of fuses for home, farm, commercial, electronic, automotive and industrial use.

357



For each of the different trimmers shown, there are dozens more that we can make to give you exactly the trimmer you need—with a flat tuning curve like that shown in the drawing.

Let us put our exceptional stability in a trimmer capacitor designed for your need

Just turn your requirements over to us and we'll design the type you need around the many important features that Corning Trimmer Capacitors alone combine.

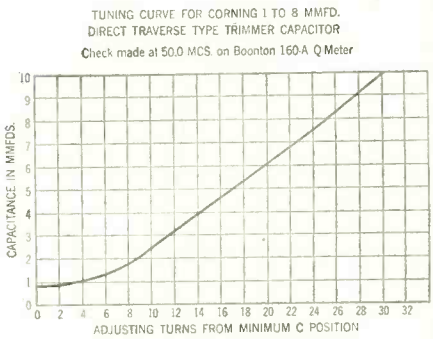
Or, if you have your design pretty much worked out and want a manufacturer, let us show you how we go about giving you what you want along with extra measures of miniaturization and stability.

Starting by permanently bonding metal to tubes of rugged glass, we give you trimmers that have negligible capacity change even when ambient temperatures vary greatly. Temperature coefficients are +50 ±50 ppm/°C. or +200 ±50 ppm/°C., depending on the core material used.

If you're working in critical applications, such as high frequency amplifiers and oscillator circuits, the Corning direct-traverse motion will simplify tuning. Because the tuning slug moves in and out without turning, you get no reverse loops. A mushroom end spring eliminates microphonics and capacity shift under vibration.

Or, if you're interested more in the general high frequency range, you can get Corning trimmers with rotary tuning slugs. This economical design comes in a wide variety of mounting styles, push-on mounts, and split bushings, with saddle clips, wire leads, pan terminals or solder spots.

You can get both the direct-traverse type and the rotary style in ratings from .3 to 12.0 mmfd. to your design. You can also get a capacity range of from 2 to 30 mmfd. in a slightly larger version of our direct-traverse motion.



Whatever you need, write, wire, or phone Corning for facts on how we can help you. If you'd like more information, circle the publisher's inquiry number for catalog sheets.

Other electronic products by Corning Components Department: Fixed Glass Capacitors*, Transmitting Capacitors, Canned High-Capacitance Capacitors, Subminiature Tab-Lead Capacitors, Special Combination Capacitors, Direct-Traverse and Midget-Rotary Capacitors*, Metallized Glass Inductances, Resistors.

**Distributed by Erie Resistor Corporation*

CORNING GLASS WORKS, 94-3 Crystal Street, **CORNING, N. Y.**

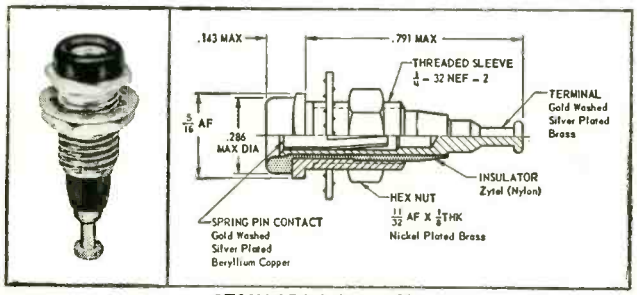
Components Department, Electrical Products Division

Corning means research in Glass

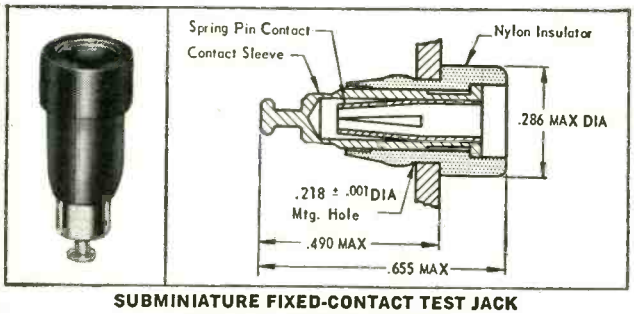
new...from Raytheon TEST JACKS

Now the most complete quality line in the industry . . .

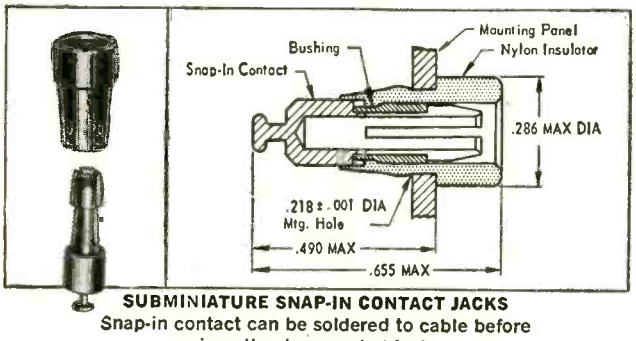
All your test jack needs from one reliable source—Raytheon. These brand new components offer a unique combination of highly desired features. Nine colors. Nylon insulators. Beryllium-copper contacts with silver-plated gold-washed solder terminals. Designed for extreme salt spray, humidity, temperature conditions. For standard .080" prods. These jacks conform to military specs. and are **competitively priced.**



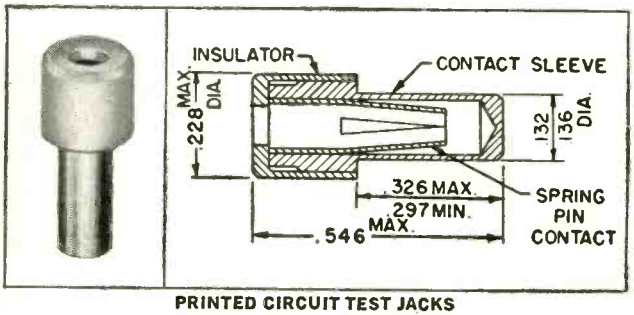
STANDARD TEST JACK
Rugged construction, superior design. Ideal for extreme shock and vibration conditions



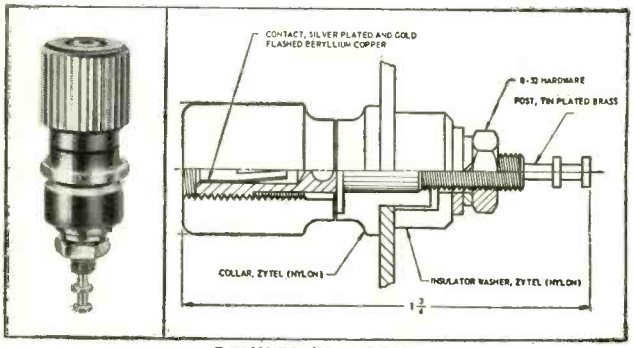
SUBMINIATURE FIXED-CONTACT TEST JACK
Fast, easy, press-fit assembly



SUBMINIATURE SNAP-IN CONTACT JACKS
Snap-in contact can be soldered to cable before insertion in mounted jack



PRINTED CIRCUIT TEST JACKS
Mount on any panel to ¼" thick



5-WAY BINDING POST
Compact, high strength. Incorporates jack for banana plug or standard .080" prod. Available in black or red

For complete information, please write Dept. 6120

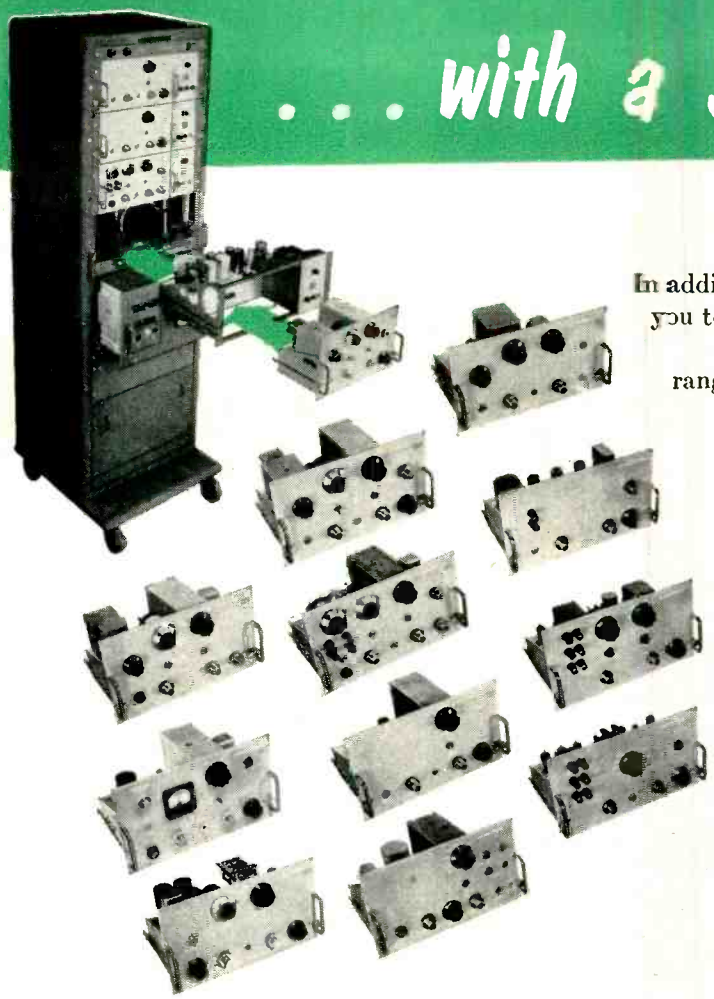
Excellence RAYTHEON *in Electronics*

RAYTHEON MANUFACTURING COMPANY
Commercial Equipment Division
Waltham 54, Mass.

See Raytheon's exhibit at Booth 2611-14 at the I.R.E. Show

Get what you really need in oscillographic recording

. . . with a SANBORN "150"

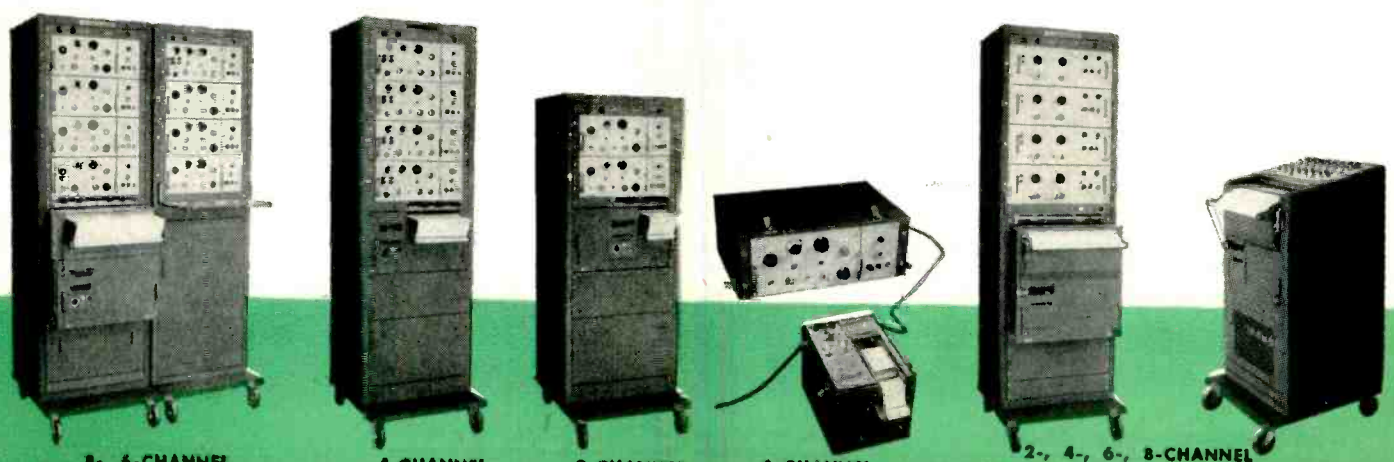


The specific advantages common to all Sanborn "150" systems are shown at the right. In addition, the fundamental design of the Sanborn "150" allows you to purchase and set up *only* what you need for your direct-writing oscillographic recording needs (in the 0–100 cycle range). There are no standard "150" recording systems. Each system in use today comprises (1) a basic assembly in the number of channels the user needs, and (2) a *choice* of interchangeable preamplifiers according to the nature of the immediate or anticipated measurements desired to be recorded by the user.

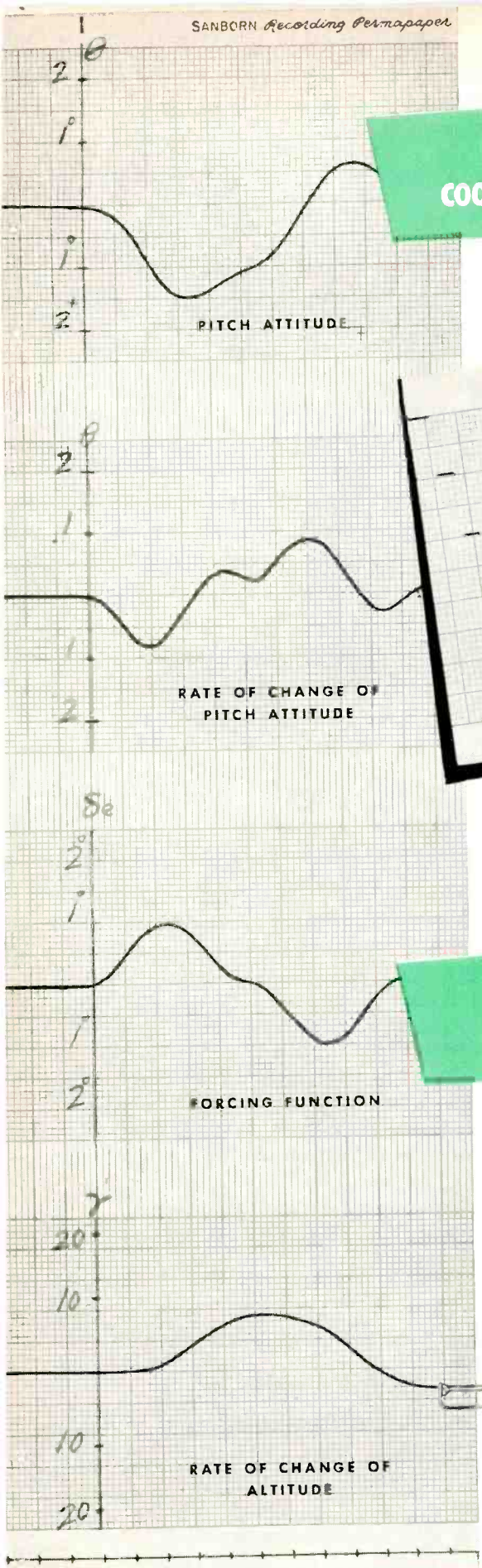
For example, the purchaser first selects either a 1, 2, 4, 6 or 8 channel Basic Assembly, each of which comprises a complete Recording Assembly in a metal mobile cabinet (or portable cases if 1-channel), a Paper Take-up Unit, and for each channel a Driver Amplifier with frame and Power Supply including Control Panel. Each Driver Amplifier is designed to receive, by simple plug-in connections, any of the eleven currently available Preamplifiers listed below.

To complete his "150" Recording System, the user then purchases the interchangeable Preamplifiers designed specifically for his recording requirements. Available "150" Preamplifiers cover a wide range of uses and include: AC-DC Carrier, Servo Monitor, Low Level DC Coupling, Log Audio, Chopper Stabilized DC, AC Wattmeter, RMS Volt/Ammeter, 400 cycle Frequency Deviation, and Frequency Meter. For those who wish to build special Preamplifier circuits to their own design, a Blank Preamplifier Chassis is available which may be used along with any of the standard Preamplifiers mentioned above.

AT I. R. E. SHOW
Booths 3601 and 3603
Dynamic display of differential transformers and velocity transducers, along with complete display and demonstration of Sanborn recording systems with interchangeable preamplifiers.

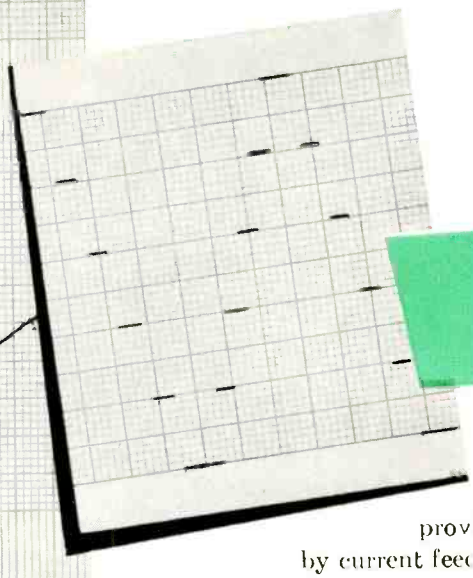


8-, 6-CHANNEL | 4-CHANNEL | 2-CHANNEL | 1-CHANNEL | 2-, 4-, 6-, 8-CHANNEL FOR ANALOG COMPUTER READOUT SYSTEMS



TRUE RECTANGULAR COORDINATE RECORDING . . .

Sanborn "150" recordings save you valuable analysis time, and minimize the possibility of errors in interpretation, by presenting data in *true* rectangular coordinate form. Without waveform curvature, "negative" time lines, etc., traces in multi-channel records can be easily and accurately correlated, during as well as after recording.

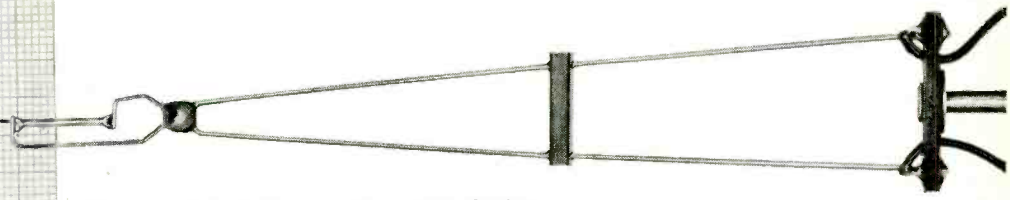


1% LINEARITY . . .

To meet your requirements for *accurate* recordings, Sanborn 150 systems provide over-all linearity of 1%. This is accomplished by current feedback driver amplifiers (one in *each* channel), and galvanometers of new design, featuring high torque (10 ma develops 200,000 dyne cm) and shorted coil frames. Maximum error over middle 4 cm of chart is 0.25 mm; over entire 5 cm chart width, 0.5 mm. Hysteresis effects have also been reduced in the recording galvanometer assembly, to further improve over-all recording accuracy.

CLEAR, SHARP, INKLESS RECORDING . . .

A third basic feature of all "150" recordings is that they are *inkless*, produced by hot ribbon stylus on heat-sensitive Sanborn Permapaper. The stylus removes the white opaque surface of the chart leaving the black undercoating to show through. Permanent and smudge-proof, the traces are characterized by sharp, blot-free peaks and notches.



For useful data on the 150 Series systems and equipment to meet your needs, write to Sanborn outlining your application requirements.

SANBORN COMPANY

WALTHAM 54, MASSACHUSETTS

INDUSTRIAL DIVISION

Patchwork has its place but . . .

The FIRST 6

In an era of stepped up competition, no manufacturer can hope to keep pace with the field while relying on obsolete "patchwork" instrumentation. . . . Almost hourly, electronics research is spawning new instruments designed to perform a specific function better, in less time, at lower cost.

But here's where your independent FIRST SIX* manufacturers' representative enters the picture. He represents what's new, what's right in electronic product design. What's more he's technically qualified to recommend and apply industry's newest product innovations advantageously to your instrumentation problems.

Today, "patchwork" — won't work! Better call in your independent FIRST SIX sales engineer. He'll back up his lines with a full measure of intelligent technical service . . . from recommendation to maintenance!

*** THE FIRST SIX — Six leading, independent manufacturers' representatives functioning cooperatively for the advancement of improved electronic instrumentation in industry.**

A. CROSSLEY ASSOC., INC.
Chicago, Ill.
Dayton, Ohio
St. Paul, Minn.

THE I. E. ROBINSON CO.
Philadelphia, Pa. — (Upper Darby)
Camp Hill, Pa.
Asbury Park, N. J.

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Detroit, Mich.
Cleveland, Ohio
Dayton, Ohio

HORMAN ASSOC., INC.
Washington, D. C.

J. D. RYERSON ASSOC., INC.
Syracuse, N. Y.

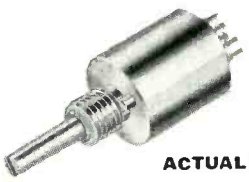
YEWELL ASSOC., INC.
Burlington, Mass.
Bridgeport, Conn.

DeJUR precision potentiometers

...THE ONE BEST ANSWER TO YOUR DESIGN PROBLEMS

SERIES C-050

SUB-MINIATURE ½" • SEALED CONSTRUCTION



ACTUAL SIZE

- One piece nickel plated bronze case and bearing.
- Electrical rotation—320°; Mechanical rotation—325°, or continuous 360°
- Voltage breakdown—1000 volts AC.
- Threaded bushing mounting.

SERIES C-078

MINIATURE ⅞" • GANGED MULTIPLES • INDEPENDENT PHASING

ACTUAL SIZE

- Unit height ⅜"; weight ½ oz.
- Independent linearity: ± 1% is standard.
- Linear or non-linear windings on flat card; res. tol. — ± 5% std., ± 1% on order.

SERIES C-158

INTERMEDIATE 1⅝" • GANGED MULTIPLES • INDEPENDENT PHASING

½ ACTUAL SIZE

- Independent linearity: ± 0.5% of total resistance is standard.
- Linear or non-linear windings std., ± 1% on order. on flat card; res. tol — ± 5%
- Rotation: electrical — 320°. Mechanical—325°.

SERIES C-200 (sleeve bearing) BC-200 (ball bearing)

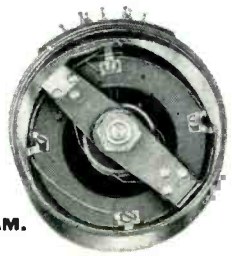
IN-FIELD GANGING • UNLIMITED MULTIPLES • ADJUSTABLE TAPS

2" DIAM.

- Resistance ± 5% standard; to ± 1% on special order.
- Linearity: ± 0.5% independent linearity is standard; ± 0.3% on special order for C-200; ± 0.2% on special order for BC-200.
- Mounting: Servo type or single hole mounting with optional non-turn device.

SERIES C-300

SINE-COSINE



3" DIAM.

- Independent brush contacts produce accurate sine and cosine outputs.
- Function accuracies of ± 1% are standard.
- Multiple ganged units are available.

SERIES KS-200 (sleeve bearing) K-200 (ball bearing)

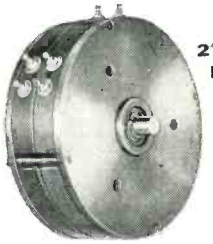
LONG FUNCTION ANGLES • CLAMP PHASING • HIGH RESOLUTION

2" DIAM.

- Resistance: linear, on triple Formvar copper mandrel.
- Independent linearity: ± 0.5% is standard; ± .1% on order.
- K-200 pots are completely enclosed and may be used as single or multiple ganged units.

SERIES HP-200, HP-300, HP-500

HIGH RESOLUTION • LONG FUNCTION ANGLES • GANGING MULTIPLES



2", 3", 5" DIAM.

- Linearity: ± .5% standard to ± .1% on order.
- Resistance: ± 5% standard to ± 1% on order.
- Rotation: 360° mechanical; 356° ± ½° electrical standard.

WRITE FOR COMPLETE TECHNICAL LITERATURE

Our engineering department can supply prototypes to meet unusual design specifications for tests and approval. Send us your specs for analysis. Electronic Sales Division, DeJUR-Amsco Corporation, 45-01 Northern Blvd., Long Island City 1, New York.

You're always sure with **DeJUR**

PRECISION POTENTIOMETERS

See our complete line at Booth 3911-13, I.R.E. Show

Continental Connectors

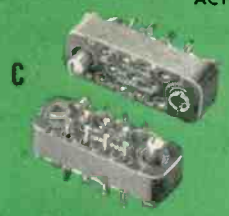
AMERICA'S FASTEST GROWING LINE

featuring the most important connector developments in recent years

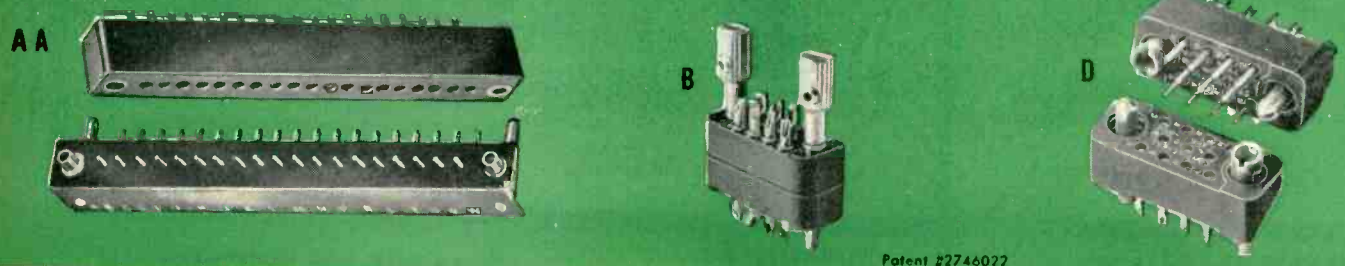
SEE CONTINENTAL AT BOOTH 3911-13, I.R.E. SHOW

PRINTED CIRCUIT CONNECTORS with "BELLOWS ACTION CONTACTS"

MICRO-MINIATURE CONNECTORS
ACTUAL SIZE



SUBMINIATURE CONNECTORS
ACTUAL SIZE



PRINTED CIRCUIT CONNECTORS A) New Series PC "Bellows Action Contacts" grip printed circuit board over 100% of board contact area. Contacts in single or double rows permit up to 56 connections. **AA)** Right Angle Printed Circuit Pin and Socket Connectors for dip soldering to printed circuit boards. Available in 4, 8 and 19 contacts.

B) POLARIZING SCREWLOCKS to prevent accidental disconnection due to vibration now available in Series 20 Miniature and Series SM-20 Subminiature Continental Connectors.

C) SERIES 22 MICRO-MINIATURE Connectors offer the ultimate in miniaturization without sacrifice of performance. Available with 7, 11, 14, 20, 26, 29 and 34 contacts for #22 AWG wire. Rating: 3 amps; Voltage: 1800V. RMS.

D) SERIES SM-20. Model shown has 11 contacts for #20 AWG wire. Available in 7, 11, 14, 20, 26 and 34 contacts. Rating: 5 amps; Voltage: 1900V. RMS.

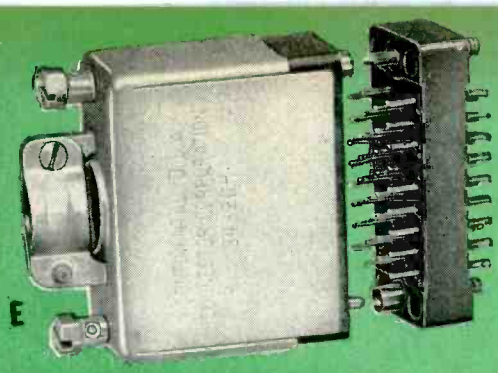
E) SERIES 20 MINIATURE CONNECTOR with Hood and Polarizing Screwlocks. Available with 7, 8, 9, 11, 14, 18, 20, 21, 26, 34, 41, 50, 75 and 104 contacts for #20 AWG wire. Rating: 5 amps; Voltage 2100V. RMS.

F) SERIES 20 with 50-ohm matched impedance coaxial contacts and 14 or 18 standard #20 contacts. Rating: 5 amps; Voltage: 2100V. RMS.

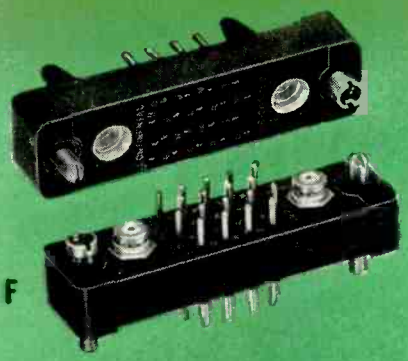
G) SERIES CCC 20 in stainless steel shells, recommended for airborne applications. 37 contacts for #20 AWG wire. (15 and 25 contacts on request.)

H) SERIES E-Z Easy Release Connectors with up to 34 solder cups or solderless taper pin contacts. Aluminum hoods, polarizing screwlocks and coaxial contacts available on order. Rating: 10 amps; Voltage: 4500V. RMS.

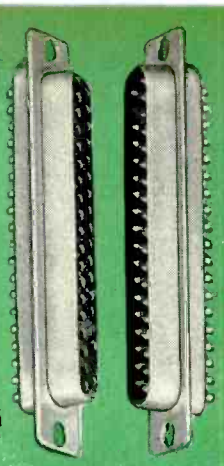
High precision, dependable Continental Connectors have achieved a reputation for excellence throughout the aircraft and electronics industries. The widest range of applications can be made from our standard line.



E



F



G

CONTINENTAL "SERIES 20" MINIATURE CONNECTORS

H

EASY RELEASE
Patent #2736870

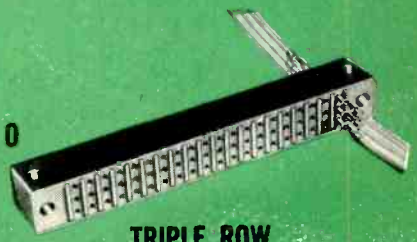
I

MINIATURE AN-TYPE

TAPER PIN TERMINAL BLOCKS

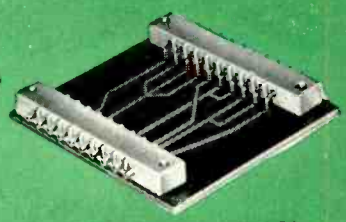
N

SINGLE ROW



O

TRIPLE ROW

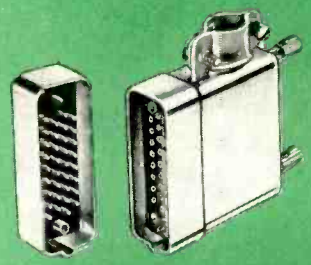


P

RIGHT-ANGLE CONNECTOR

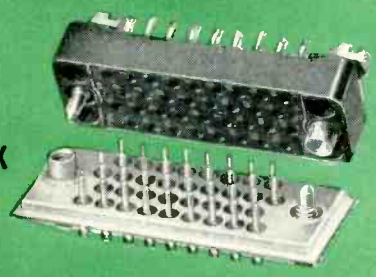
J

HERMETIC SEAL CONNECTORS

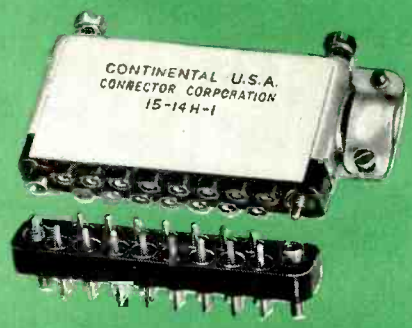


L

PROTECTIVE SHELLS



K



M

POWER CONNECTORS

I) SERIES 1300 MINIATURE AN-TYPE Connector with one-piece molded inserts. Rating: 7.5 amps; Voltage: 3000V. RMS. Two shell sizes: 3, 4, 5 contacts, and 15, 19, 27, 31 contacts.

J) SERIES HC-20 HEXAGONAL Hermetic Plug has solid glass insert. Choice of 4, 5, 7, 9 and 10 contacts.

K) SERIES H-20 Hermetic Plug for #20 AWG wire. Contacts individually compression sealed in glass. Fits Series 20 receptacles. With polarizing screwlock or guide pin and guide socket.

L) ANODIZED ALUMINUM SHELLS give complete protection against physical damage on Miniature Series 20 and Subminiature Series SM-20. Obtainable with or without corrosion-resistant stainless steel polarizing screwlocks.

(M) SERIES 14 Power Connector (illustrated with hood and polarizing screwlock.) Choice of 7, 9, 10, 15 or 18 contacts for #14 AWG wire. Rating: 10 amps; Voltage: 4500V. RMS.

N) SERIES 145-58 Single Row Taper Pin Terminal Blocks. Available in any combination of feed-through shorting or non-shorting terminals. Molded holes for stacking or mounting.

O) SERIES 145-48 Triple Stacked Taper Pin Terminal Blocks. Continental will supply stacked taper pin blocks in any combination of feed-through shorting or non-shorting terminals. Molded holes for right angle and perpendicular mounting.

P) SERIES 145-60 Taper Pin Terminal Blocks for Printed Circuitry. Precision tapered molded-in right angle terminals for dip soldering to printed circuit boards.

For special designs and technical data sheets on these connectors write Electronics Sales Div., DeJur-Amsco Corporation, 4501 Northern Blvd., Long Island City 1, N. Y.

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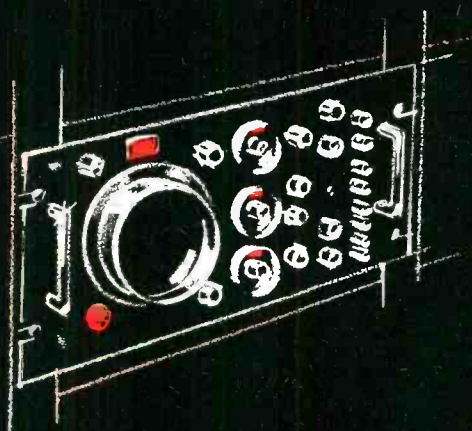
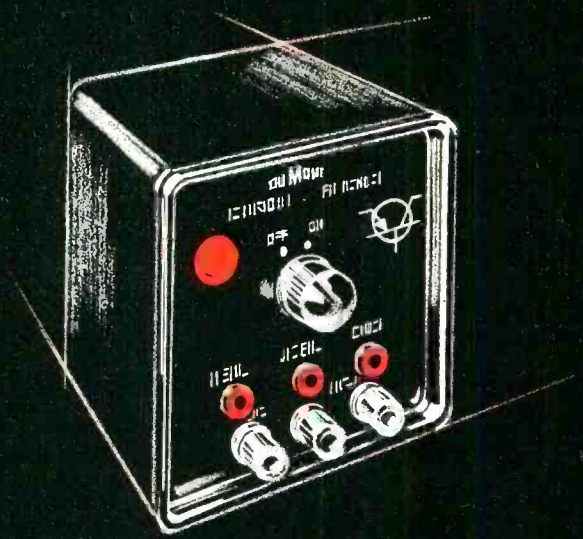
TYPE 403

Highest sensitivity oscilloscope commercially available. DC amplifier 1 mv full scale sensitivity.



TYPE 401

High gain. DC-150KC. Identical X- and Y-amplifiers. Calibrated sweeps.



TYPE 407

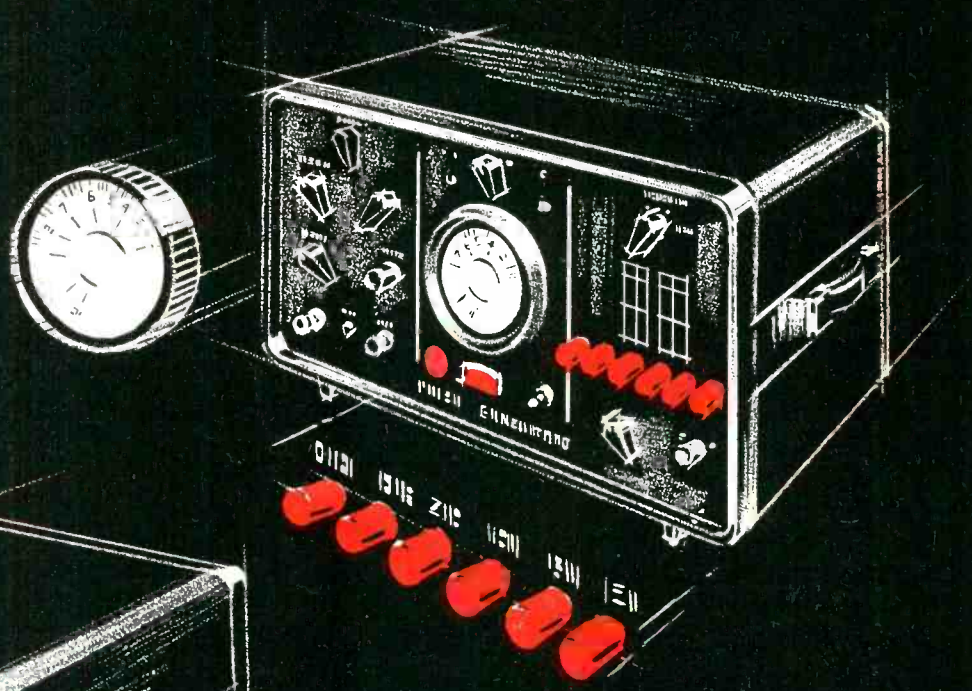
Transistorized low-noise pre-amplifier. Gain of 10. Battery operated. Self-contained. Size 4" x 3½" x 4⅞". Frequency response: 0.15 cps to 10 kc.

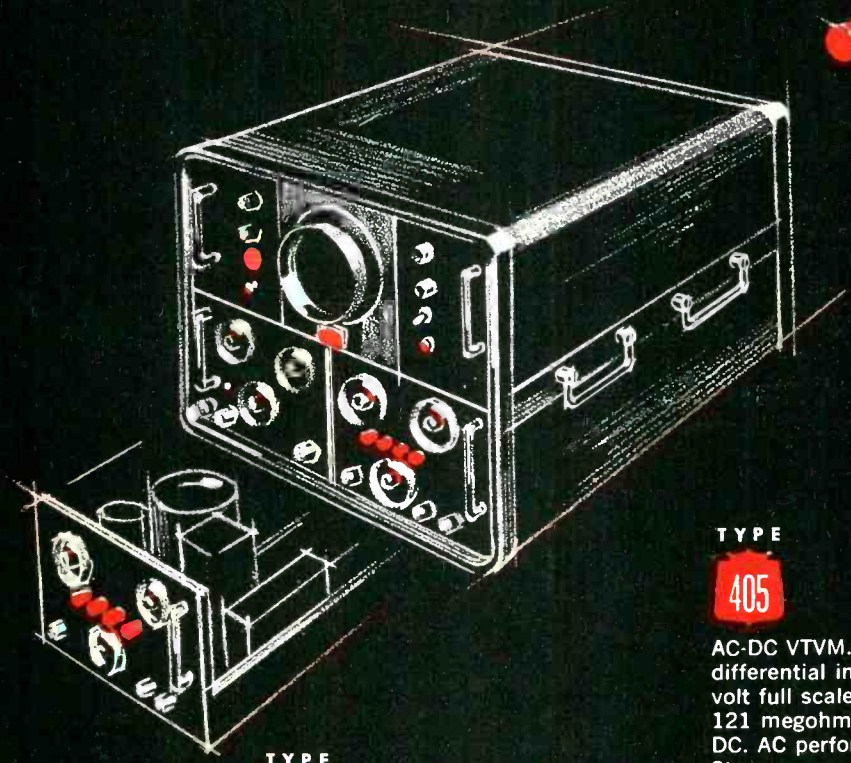
Sparkling new ideas materialize in the Du Mont 400 Series. These 6 new instruments are *current* models, ready right now. See and operate these instruments at the New York I.R.E. Show. Or ask for a demonstration at your convenience. Write for complete details.

6 ready now

TYPE 404

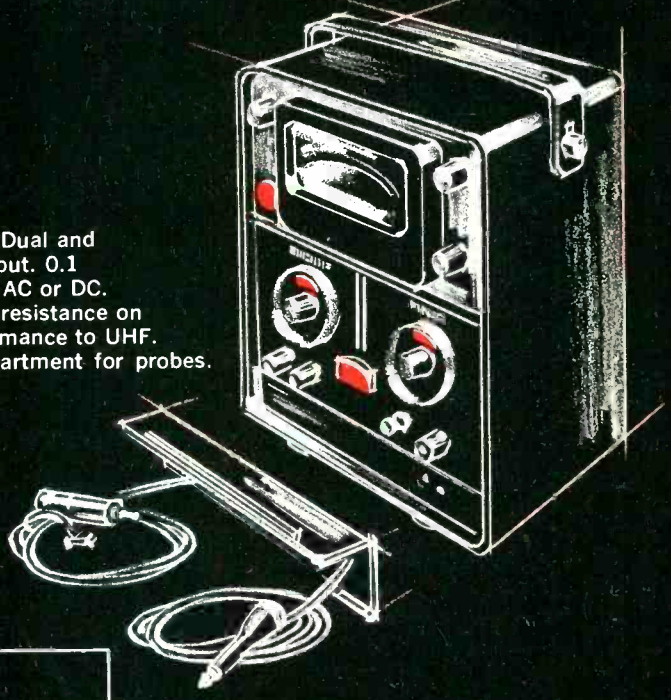
Jitter-free, hard-tube circuitry pulse generator. Pulse repetition rates up to 100,000 pps.





TYPE 405

AC-DC VTVM. Dual and differential input. 0.1 volt full scale AC or DC. 121 megohm resistance on DC. AC performance to UHF. Storage compartment for probes.



TYPE 410

High gain DC amplifier with 7 millimicrosecond rise time. High duty cycle calibrated sweeps. 24 KV accelerating potential. Building Block construction allows choice of performance characteristics.

WARRANTY

Every instrument in the Du Mont 400 Series carries a five-year guarantee.

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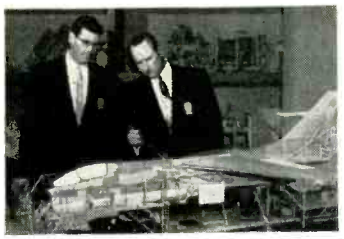
Engineers selected from their original groups for the Crusader project followed their assigned systems and sub-assemblies from preliminary design to flight test. Teamed with engineers from other groups, they lent mutual assistance, worked outside their own specialties, and enlarged their view of the program. At the same time, liaison was maintained with the original groups on methods, research and policy. This way, the Crusader became everyone's aircraft, and everyone learned. That's the value of the project-group system. Linking group with project, it coordinates the state of the art with the practical problems of project work. Joining engineers of one specialty with those of another, it offers each a better compromise and a wider view.



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. . . an internal thermal gradient of 1.2° C/watt or less!

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Furthermore, these transistors are normalized to retain their performance characteristics regardless of age. Write for engineering data. Delco Radio transistors are produced by the thousands every day.

TYPICAL CHARACTERISTICS

	2N173	2N174	
Properties (25°C)	12 Volts	28 Volts	
Maximum current	12	12	amps
Maximum collector voltage	60	80	volts
Saturation voltage (12 amp.)	0.7	0.7	volts
Power gain (Class A, 10 watts)	38	38	db
Alpha cutoff frequency	0.4	0.4	Mc
Power dissipation	55	55	watts
Thermal gradient from junction to mounting base	1.2°	1.2°	°C/watt
Distortion (Class A, 10 watts)	5%	5%	

DELCO RADIO DIVISION OF GENERAL MOTORS KOKOMO, INDIANA

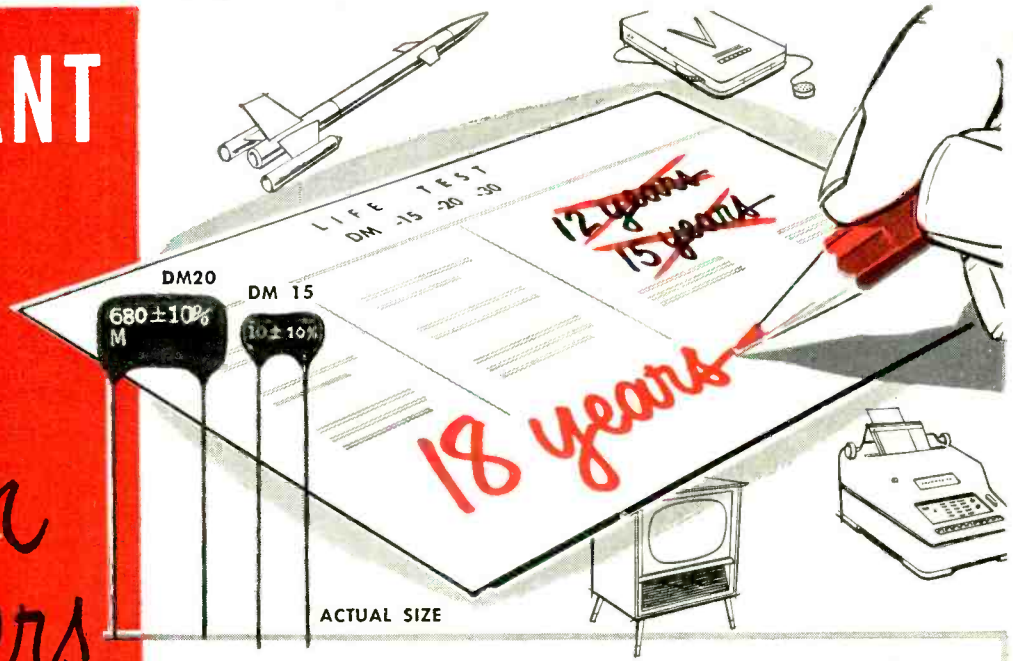
IMPORTANT NEWS

for design engineers

WHAT IS YOUR CAPACITOR APPLICATION PROBLEM?

We'll be glad to advise you.

Make your own test of El-Menco Dur-Mica Capacitors



El-Menco Dur-Micas

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El-Menco Dur-Mica Capacitors Can Now Assure You Of Dependable Performance Up To 18 Years!

Not An Extravagant Claim, But A Tested Fact. The latest series of rugged trials by El-Menco engineers found El-Menco DM15, DM20 and DM30 Dur-Mica Capacitors outlive and outperform all others. Under accelerated conditions of 1½ times rated voltage at 125°C ambient temperature; El-Menco capacitors continued to perform reliably after 12,000 hours. Translated into normal conditions, this indicates a lifetime of from 15 to 20 years!

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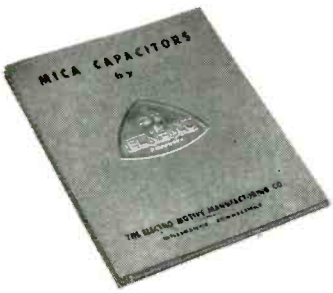
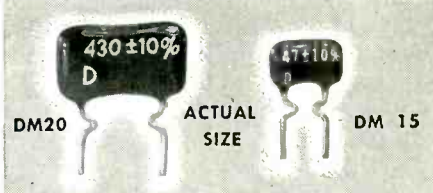


Write for FREE samples and catalog on your firm's letterhead.

El-Menco Dur-Mica DM15, DM20 and DM30 Capacitors Mean:

1. LONGER LIFE
2. POTENT POWER
3. SMALLER SIZE
4. EXCELLENT STABILITY — SILVERED MICA
5. PEAK PERFORMANCE

In addition to longer life, El-Menco Dur-Mica Capacitors with tougher phenolic casing assure greater stability over wide temperature range.



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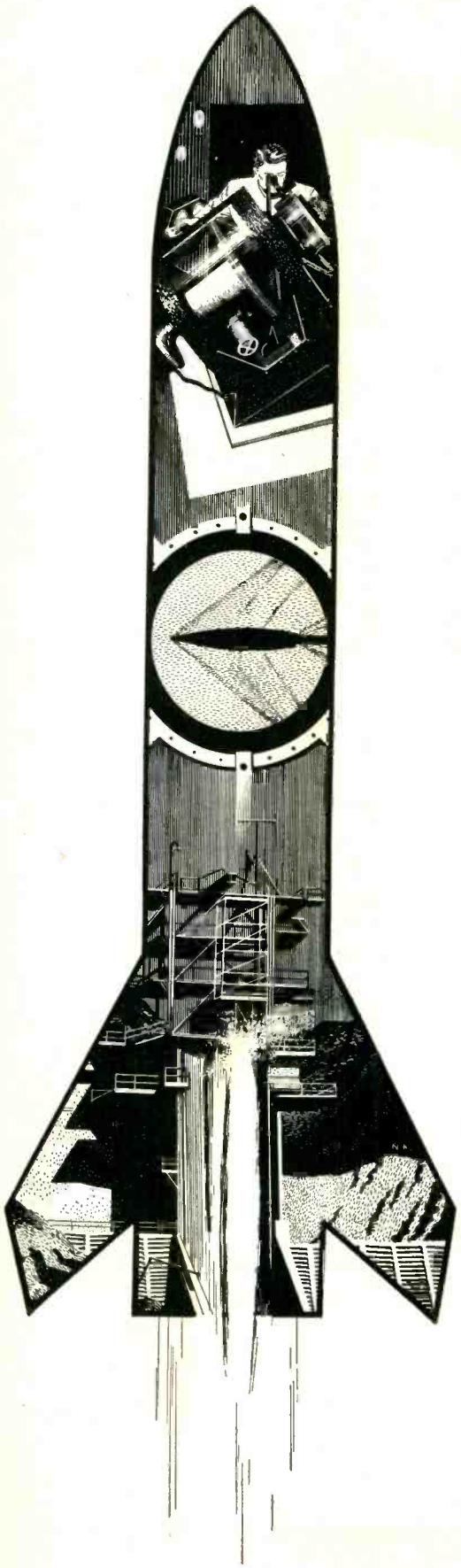
Special 111-conductor Rome cable solves tough guided missile problem



When project engineers at North American Aviation, Inc., needed a special telemetering cable for their advanced guided missile work at various missile test centers, Rome Cable Corporation was asked to make it.

The cable was a tough one to manufacture. The specifications called for exacting dielectric requirements, low-loss characteristics, adequate service life—and a total of 111 conductors—all contained by one heavy-duty jacket.

Because Rome Cable engineers are accustomed to solving tough cable problems like this, they readily produced the cable which met North American's rigid specifications. Rome RoLene—a polyethylene compound—proved perfect for insulating the 37 triplets inside the jacket, and it easily met the specification requirements calling for controlled capacitance and uniform wall thickness. Rome Synthinol, a tough polyvinyl chloride compound, proved to be an excellent jacket material.

Rome Cable can also help you

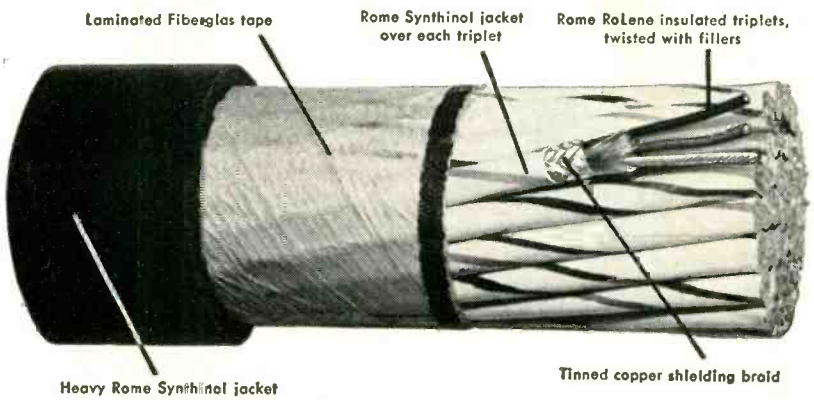
You can turn to Rome Cable with confidence for the right solution to *your* special cabling problems. Rome's competence in its field is, in part, a function of the following factors:

1. Engineering experience. Rome engineers regularly handle complicated specification problems. They've had years of experience dealing with electronic circuit problems.

2. Complete production facilities. The completeness of Rome Cable's manufacturing facilities is unique.

3. Uncompromising quality control. Latest devices, like the photoelectric gauge, are regularly used to assure highest quality. This particular gauge enabled Rome to maintain an exacting control on the diameter limits of insulations and jacket for this special cable.

Rome Cable's engineers can probably be of real help to you on your next cable problem, especially if it is a really tough one. For more information as to what we can do to help you, simply contact your nearest Rome Cable representative—or write to Department 850, Rome Cable Corporation, Rome, N. Y.



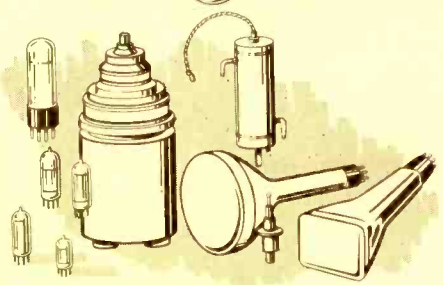
ROME CABLE

CORPORATION

TUBE DESIGN NEWS

GENERAL ELECTRIC

RECEIVING * POWER * CATHODE RAY



Snow-White Cleanliness Extends to 5-Star Tube Parts Manufacture, Inspection, Handling

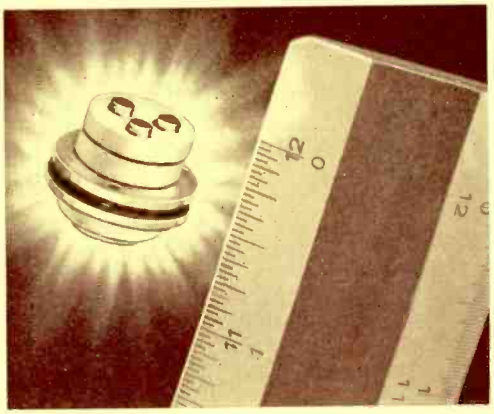
Broadened facilities for building G-E 5-Star high-reliability tubes under conditions of immaculate cleanliness, include dirt- and lint-free manufacture of the tube sub-assemblies.

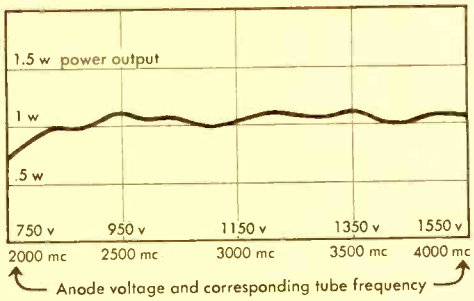
All areas of General Electric's 5-Star Tube factory now are air-conditioned and pressurized to keep out dust. Workers, inspectors, and foremen who build and handle parts, wear the same lint-free Nylon and Dacron garments as employees who assemble and test 5-Star Tubes.

Grids are wound and cleaned with virtually no chance that a particle of dust or thread of lint will adhere, to cause tube "shorting". Heaters are formed, coated,

(*Continued on Page 2, Column 1*)

New G-E Voltage-Tunable Magnetrons in Development Permit Fast Tuning over Wide Range with Steady Output





ABOVE, LEFT: the developmental Z-5112 voltage-tunable magnetron is only 5/8 in. high and 3/4 in. wide. ABOVE, RIGHT: preliminary tests prove essentially stable power output throughout 2000-mc tuning range.

Latest developmental type in a series of voltage-tunable magnetrons pioneered by General Electric, the Z-5112 indicates the advantages which this group of tubes offers to designers of military equipment.

Recent tests of the Z-5112 prove its capability for rapid, efficient tuning over an extended frequency range, from 2000 mc to 4000 mc—with power output .5 w to 1 w throughout.

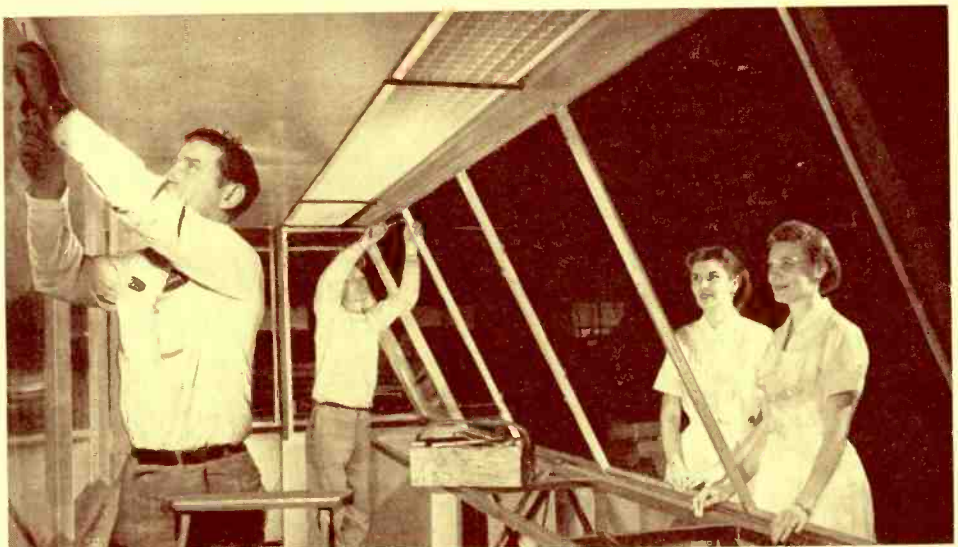
Counter-measures can benefit from this threefold tube advantage. Also, enemy jamming can be effectively circumvented by rapid tuning over a broad frequency spectrum with little or no reduction in signal power. With tube frequency a linear function of the anode voltage, the Z-5112 and other VTM types can be tuned merely by changing the potential of the anode. This makes for circuit simplicity.

Design benefits of General Electric voltage-tunable magnetrons now in development, are small size, light weight, and metal-ceramic construction. The latter adds strength, and gives high-temperature resistance. Tubes are designed to operate up to 60,000 feet altitude.

Besides being directly useful for counter-measure work, voltage-tunable magnetrons are suited to telemetering—for example, missile tracking; to FM altimeters; to air-navigation applications, broadband test equipment, and microwave communications generally.

Ask any G-E office listed on the next page for information on the development status of voltage-tunable magnetrons.

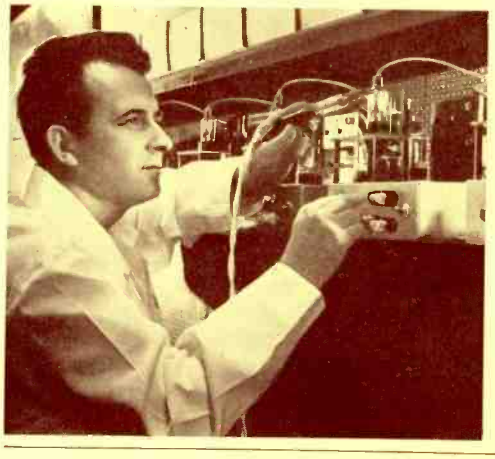
G-E Snow-White Workers Check Progress on Their 5-Star Tube "Factory", to Operate at March I.R.E. Show



Featured at General Electric's exhibit at the New York I.R.E. Show, will be the actual assembly of 5-Star Tubes in an air-conditioned, pressurized working area, housed in a transparent plastic "factory". Trained operators from General Electric's 5-Star Owensboro, Ky., factory will assemble the tubes . . . Another G-E show highlight: first public demonstration of voltage-tunable magnetrons, described elsewhere on this page.

'Lightning-Rod' Filament Shield for G-E High-Voltage Rectifier Tubes Increases TV Dependability

ABOVE: a special tungsten post shields G-E tube filaments from electrostatic pull of high anode voltages. BELOW: checking 1B3-GT and 1X2-A/B rectifier types during G-E flyback life test that further safeguards tube performance.



Among numerous steps taken to increase the reliability and long life of General Electric 1B3-GT and 1X2-A/B high-voltage rectifier tubes, mounting a "lightning-rod" shield beside the filament is important. Manufacturers of TV receivers thus are better protected against picture failures . . . . . in sets in production, on test, and in owners' hands.

G.E.'s tungsten shield, or post wards off electrostatic pull on the tube filament . . . . . thus minimizing pull-out and filament-to-anode shorts, and sharply reducing the incidence of broken filaments.

In addition, a highly adhesive filament coating further protects against arc-overs. Another special feature: the bulbs of G-E high-voltage rectifier tubes are ringed with conductive material to prevent vertical picture streaking that is caused by bulb charging.

To make sure that tube performance meets design targets, 1B3-GT's and 1X2-A/B's receive a 100% flyback test and a dynamic flyback life test—both at the top ratings for big-screen operation.

Realizing the importance to the TV industry of dependable, long-life rectifier tubes, General Electric is continuously improving its design, production, and test methods for these types.

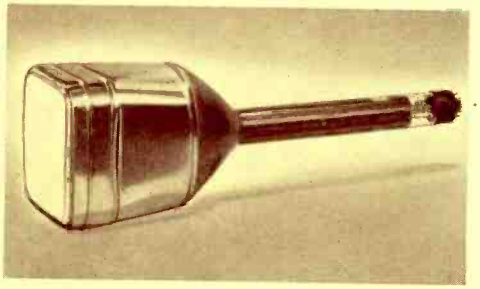
Snow-White Cleanliness, 5-Star Parts

(*Continued from Page 1*)

and heat-treated . . . . . other parts built and processed . . . . . under the same strict conditions of near-surgical cleanliness.

There are 35 General Electric 5-Star Tubes, 11 of them subminiatures, meeting substantially every military and industrial need. Two new miniature types for computers are included in the line.

RIGHT: 5-Star Tube heaters, after forming and coating, are placed in individual glass cylinders for inspection. This helps guard heaters from contact with dust or lint until the tubes are assembled, exhausted, and sealed off.



Special bulb design of Z-4399 optimizes resolution, accommodates several types of magnetic deflection yoke for presenting various kinds of information on face plate.

New Z-4399 High-Resolution Tube Accents General Electric's Facilities For Special C-R Tube Development

Used primarily in equipment to pinpoint enemy mortar locations for quick counter-fire, General Electric's Z-4399 C-R tube combines a group of features essential for its purpose—a 5½-in. square face plate that lends itself to a rectilinear coordinate display system; extremely high resolution; magnetic focus and deflection; a bright image brought about by aluminizing.

The tube's neck has been specially lengthened in order to (1) increase image resolution to a new standard of fineness and sharp definition, (2) accommodate several types of deflection yoke.

Designing C-R tubes such as the Z-4399 for specific military or industrial functions, is a job for which General Electric has extensive facilities in research, engineering skill, and equipment. Problems calling for the selection or origination of special C-R types are welcomed.

JUST PRINTED!

New, complete booklet on General Electric 5-Star Tubes — their design, manufacture, and testing. A "must" for designers who require maximum reliability in critical tube sockets. Ask for Booklet ETD-1425!

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All shook up over his second Microwave System

His first took 8 months to build — needed lots of engineering and special components. Now he wants a duplicate. Needs it yesterday. Here's the gasser — it's gonna take **another 7 months** to build. Calls for same amount of special construction. Yipes! — what to do?

No problem! Get it built by DeMornay-Bonardi with their standard "building blocks." D-B manufactures 924 types of microwave components, from 2.60 to 90 KMc/SEC — carries 'em in stock. With this wide choice, they can engineer a system in days. Seldom a special component needed, and when there is, only simple alterations do the job. That's why D-B can deliver any complete system in 5 weeks or less. They could have done it on the first one. No problem.

There's more for our engineer — he saves a lot of budget money in the deal. Because D-B isn't stuck with heavy design work or expensive trial-and-error methods, it sells a system for little more than the cost of components alone. D-B prices run from 25% to 50% less than custom shop prices — for a system guaranteed to work.

To get with it, all our fellow practitioner has to do is send us his electrical requirements and space allowance. We take it from there. New D-B catalog will be sent to company letterhead requests.

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. . . . YOU SHOULD KNOW
THERE IS A MORE ACCURATE
VOM

1½% accuracy . . .

mirror scale

to eliminate any possible parallax and give you readings with the same laboratory accuracy that is built into the instrument.

MODEL 630-A $54.50

This VOM is truly what laboratories buy when they must have the best. Model 630-A is prized in
782 industrial laboratories
115 research laboratories
237 development laboratories
and is owned by over 300 engineering consultants and used for critical production line testing and in the maintenance of automation equipment by over 1100 manufacturers of all types of products.

TRIPLETT FEATURES:

½% resistors—molded mounting for resistors and shunts allows direct connections without cabling. (No chance for shorts—longer life and easy-to-replace resistors in their marked positions.) King sized recessed knob for the single selector switch for both circuit and range—just turn and make reading.
Resistance ranges are compensated for greatest accuracy over wide battery voltage variation.

33 RANGES:

12 D.C.-A.C. Volts (20,000 ohms per volt DC, 5000 ohms per volt AC.); 5 Current Ranges; Resistance from .1 Ohms to 100 Megohms; Decibel and Output readings.

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The Smallest Complete V-O-M with Switch

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H-H Rheostats are designed for top performance and long life in military and commercial applications —

- **Smooth, long-life mechanical action**
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Constant pressure contact arm adjusts tension for complete continuous contact, eliminates backlash, prevents birding. High temperature gray vitreous enamel coating increases safety by its ability to withstand overload.

H-H rugged Gray Line Resistors meet all requirements for continuous, heavy duty commercial applications —

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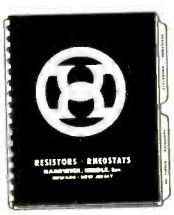
Stronger core affords extra dependability under extreme operating conditions. All wire connections on H-H Long Life Resistors feature all welded construction. The fixed, ferrule and adjustable types meet MIL-R-26 specifications.

H-H Blue Ribbon Resistors for Reliability in Applications with Space Limitations

H-H Blue Ribbon Resistors provide higher wattage ratings per unit, save space and weight wherever mounted. Ruggedized construction features high temperature, vitreous enamel, crazeless coating offering maximum moisture resistance. Aluminum thru-bar distributes heat uniformly along entire resistor length. Mounting studs are all corrosion resistant, and bracket assembly is vibration-proof.

Illustrated catalogs available on H-H Resistors and Rheostats include helpful engineering and installation data. Call or write for copies, now! Standard stock items available for immediate delivery from authorized local electronic parts distributors.



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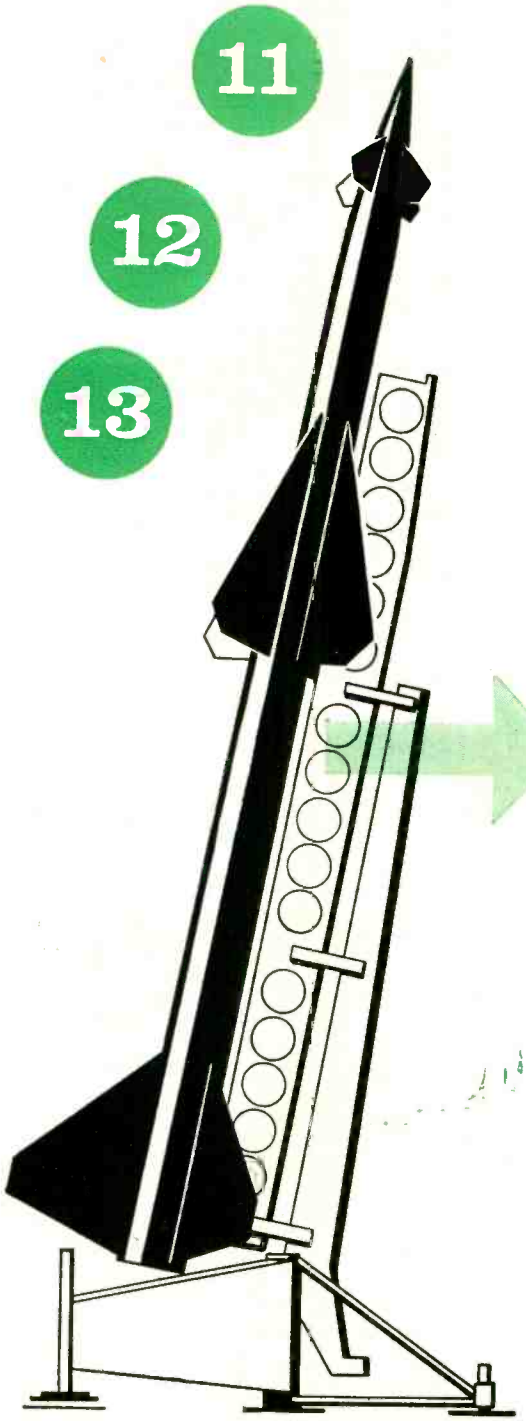

17
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19

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23 24 25

Sperry's Microwave Electronics Division provides a unique service: Developing and producing special radar subsystems and components for the electronic industry. ■ Microline® equipment ranges from single miniaturized components to complete microwave systems—together with complex antennas, precision test equipment, and automatic checkout instrumentation ■ Whether your immediate need is for one component or for the complete line, we will be happy to discuss your problem with you.

The equipment indicated on these pages together with many other Sperry developments will be on display at the Radio Engineering Show, New York Coliseum, March 18-21, Booths 1416-1422.

SYSTEMS

RADAR

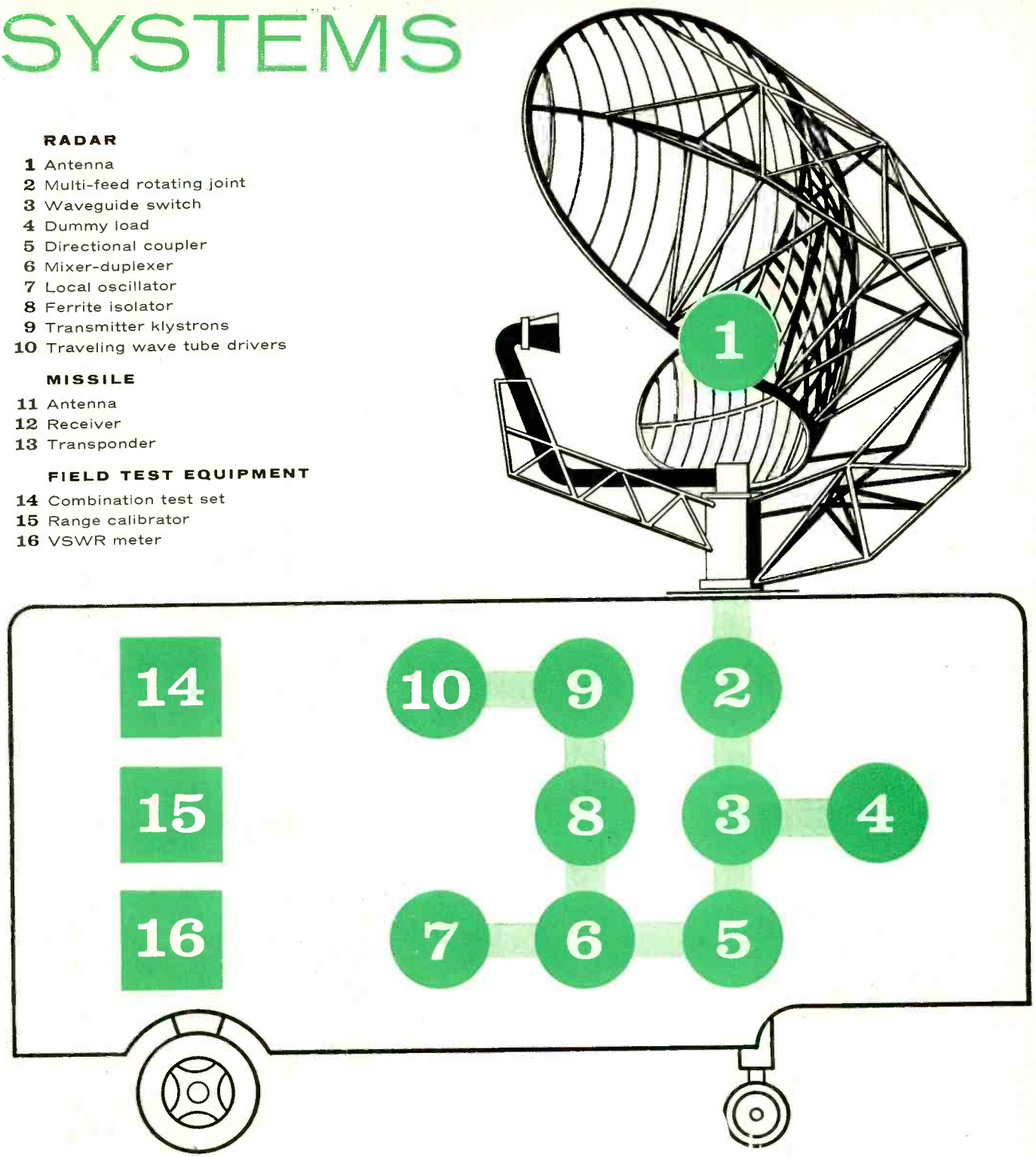
1 Antenna
2 Multi-feed rotating joint
3 Waveguide switch
4 Dummy load
5 Directional coupler
6 Mixer-duplexer
7 Local oscillator
8 Ferrite isolator
9 Transmitter klystrons
10 Traveling wave tube drivers

MISSILE

11 Antenna
12 Receiver
13 Transponder

FIELD TEST EQUIPMENT

14 Combination test set
15 Range calibrator
16 VSWR meter



SUPPORT EQUIPMENT

17 RACE (Rapid Automatic Checkout Equipment)
18 System evaluators
19 System performance monitors

DEPOT SUPPORT EQUIPMENT

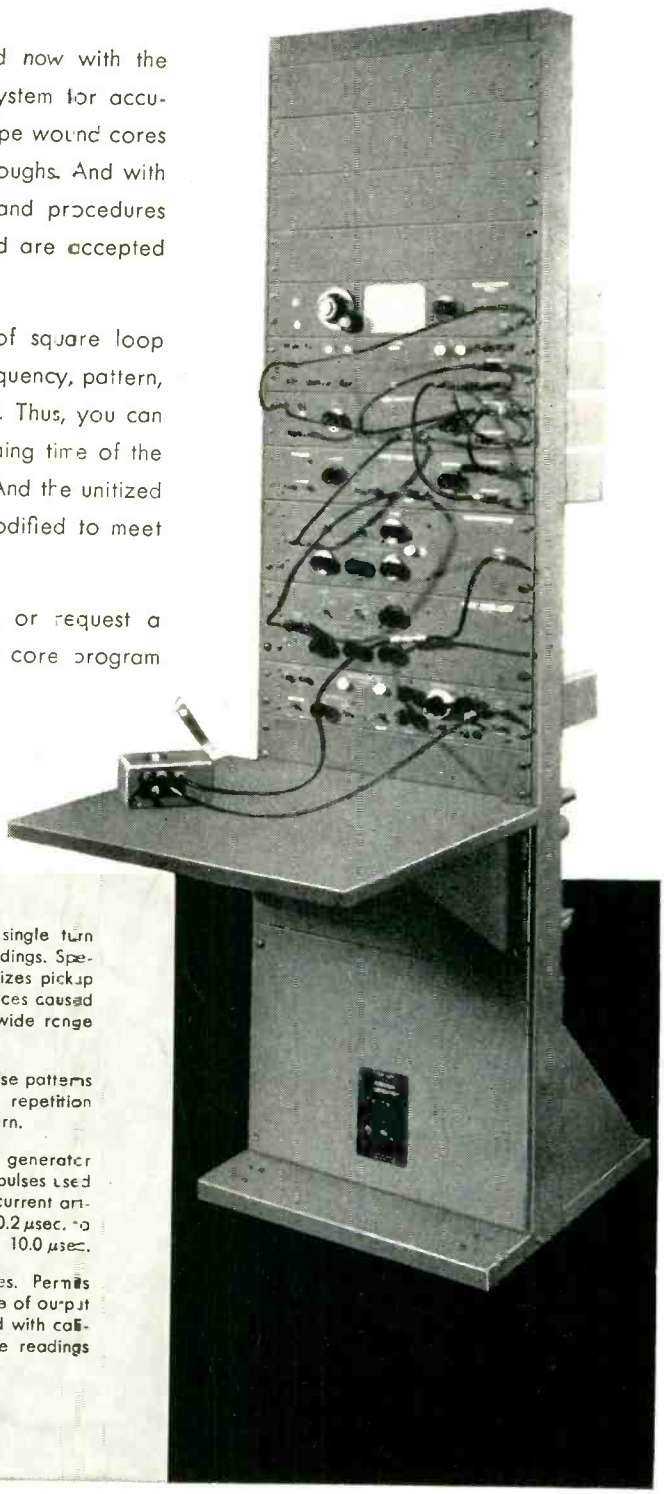
20 Peak power meter
21 Multi-pulse generator
22 Directional couplers
23 Ferrite isolators
24 Ferrite attenuators
25 Barretter mounts

HOW TO TEST CORES

You can get your core program off the ground *now* with the Burroughs BCT-301. This complete and flexible system for accurately measuring the operating characteristics of tape wound cores is the result of six years of core research at Burroughs. And with it, you get the benefit of advanced techniques and procedures which are now in everyday use at Burroughs, and are accepted practice among major core manufacturers.

Designed expressly for the individual testing of square loop cores, the BCT-301 allows precise control over frequency, pattern, amplitude, and rise time of the core driving signal. Thus, you can get extremely accurate measurements of the switching time of the core as well as the amplitude of the output pulse. And the unitized sections of the BCT-301 can be expanded and modified to meet new testing requirements as they arise.

Write for additional details on the BCT-301, or request a demonstration of how this new tool can get your core program off the ground *now*.



specifications

tools for engineers

core mounting jig:	Low-noise test mounting jig applies tight single turn loops around core for input and output windings. Special electrical and mechanical design minimizes pickup by the secondary as well as other disturbances caused by air flux. Adjustable pins accommodate wide range of bobbin sizes with equal precision.
pattern generator:	Provides extreme flexibility in generating pulse patterns applied to core, controlling pulse spacing, repetition rate of cycle, and number of pulses in pattern.
current drivers:	Two drivers convert voltages from pattern generator into positive and negative constant current pulses used for driving core. Front panel controls vary current amplitude from 0 to 1.0 ampere; rise time from 0.2 μsec. to 1.0 μsec.; pulse duration from 1.0 μsec. to 10.0 μsec.
calibrator:	Accurately measures currents and voltages. Permits measurement of driving current and amplitude of output voltage with an error of less than 1%. Used with calibrated oscilloscope, permits highly accurate readings of switching time.
power supply:	Provides seven regulated d-c voltages.

Burroughs

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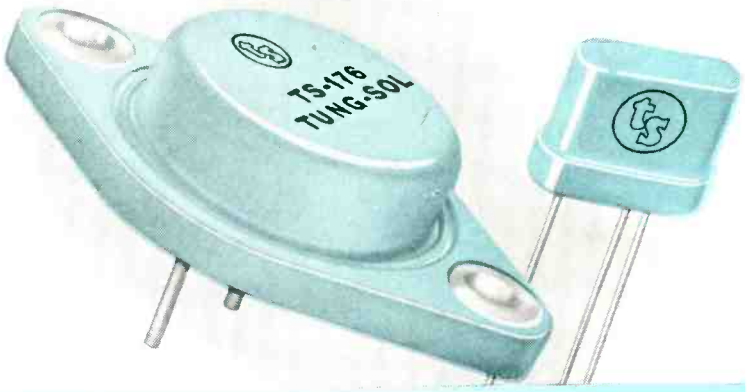
TUNG-SOL *Alloy Junction Germanium Transistors*

Reliability is the principal characteristic of these hermetically sealed Tung-Sol transistors now in volume production. Gain factor is extremely high over the operating ranges, with excellent heat dissipation. Design and construction methods provide a wider safety margin against the effects of shock, vibration, contamination and temperature. Rigorous testing of electrical and mechanical characteristics assures accurate maintenance performance and life standards. If your equipment designs call for transistors of these or related types, you will find Tung-Sol quality and dependability extremely valuable in maintaining your own output at highest levels.



HIGH POWER TRANSISTORS

	RATINGS (25°C)		TYPICAL CHARACTERISTICS (25°C)			
	V_c	P_c	Current Gain 500 MA Ice	Power Gain CL. A	Power Output CL. A	Distortion Max.
TS176	—30 Volts	10 Watts	50db	32 db	2.5 Watts	5%

Type TS176 PNP junction transistor is designed for high power audio service in mobile battery operated equipment. The collector is connected directly to the case for conduction cooling. Emphasis is given to efficient thermal design, high power sensitivity, low distortion at high current levels and reliable hermetic sealing.

TS612
TS613

These are high power units rated for non-audio applications such as series regulator and power switching. Collector-to-emitter voltage ratings range from 50 to 90 volts depending on circuit conditions.

MEDIUM POWER TRANSISTORS

	RATINGS (25°C)		TYPICAL CLASS B OPERATION (25°C)			
	V_c	P_c	E_{cc}	Power Output	Distortion Max.	Power Gain
TS616	—25 Volts	150 MW	—12 Volts	500 MW	5%	28 db
TS617	—25 Volts	150 MW	—12 Volts	500 MW	5%	31 db
TS618	—25 Volts	150 MW	—12 Volts	500 MW	5%	34 db

PNP alloy junction transistors designed and tested for medium power class B audio applications. Close parameter control, particularly at high collector currents, makes special matching within type classification unnecessary.

	RATINGS (25°C)		TYPICAL CLASS A OPERATION (25°C)			
	V_c	P_c	E_{cc}	Power Output	R_L	Power Gain
TS619	—25 Volts	75 MW	—12 Volts	2 MW	15,000 OHMS	44 db

PNP alloy junction transistors designed and tested for class A driver service in audio amplifiers. Close parameter control and hermetic sealing insure production uniformity and performance stability.

General Purpose Transistors: The following general purpose RETMA types are also available: 2N63, 2N64, 2N65.

Other semiconductor devices being developed for production include these important types:

Germanium transistors of both PNP and NPN types, designed for computer switching and radio frequency applications.

Germanium PNP medium power transistor with 350 milliwatt dissipation rating.

Gold bonded germanium computer diode.

Silicon power diode with diffused junction.

More Data? Requests for additional information about these—and other related types of transistors for special applications—should be addressed to: Semiconductor Division, 95 Eighth Avenue, Newark 4, N. J.

Technical Information Service. Upon request, your name will be placed on our special mailing list. You will automatically receive new Tung-Sol semiconductor data and product application notes as such information becomes available.

See You At The IRE Show! The Tung-Sol Booth is 2813-15. It will feature actual assembly of electron tubes and semiconductors.

CAREER OPPORTUNITIES

Tubes and semiconductor products are the foundation of the whole science of electronics. Tung-Sol offers attractive and responsible positions in research, design, development and production. Write to Director of Personnel, 95 Eighth Avenue, Newark 4, N. J.

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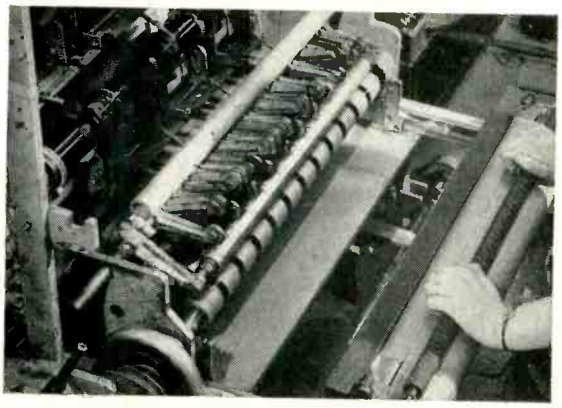

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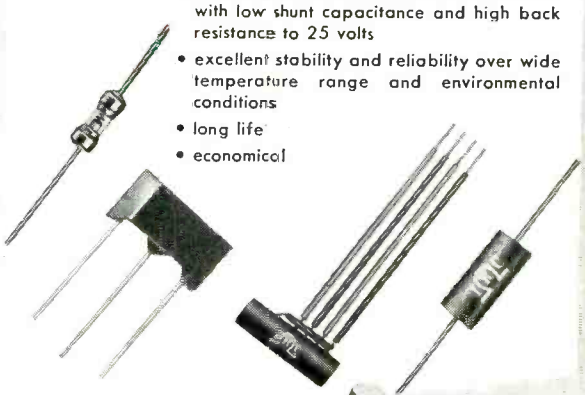
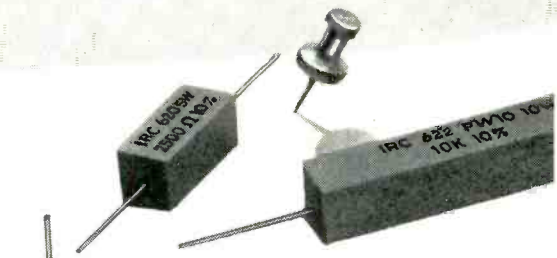
6 NEW ANSWERS TO TODAY'S

New IRC Dual Diodes

New answer to the bulk, higher cost, and assembly problems of vacuum tube diodes in low current applications.

- featuring balanced miniature selenium cells with low shunt capacitance and high back resistance to 25 volts
- excellent stability and reliability over wide temperature range and environmental conditions
- long life
- economical





Expanded line of axial lead resistors offering wider ranges, higher operating temperatures and easier assembly at lower cost.

- now available in 5, 7 and 10 watt ratings
- leads automatically secured to element for maximum terminol security
- sturdy rectangular ceramic case with special IRC insulating cement

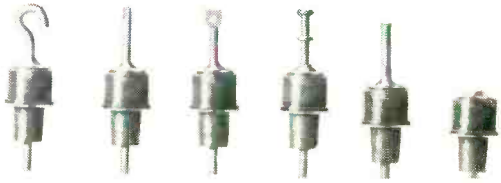
Power Resistor Line

New IRC Distributed Parameter Delay Lines

A compact, more uniform product for time delays of less than 1.0 microsecond at impedance levels of 4000 ohms or less.

- designed for mass production in a continuous process
- featuring high stability and uniform characteristics
- economical

New IRC Hermetic Sealing Terminals



Superior hermetic sealing and insulating performance in miniature units meeting a wide variety of space, electrical, and termination requirements.

- four body designs and six lead types
- excellent resistance to thermal shock, zero water absorption, physically tough, will not crack or craze.
- special fluoracarbon plastic body with superior electrical and mechanical characteristics

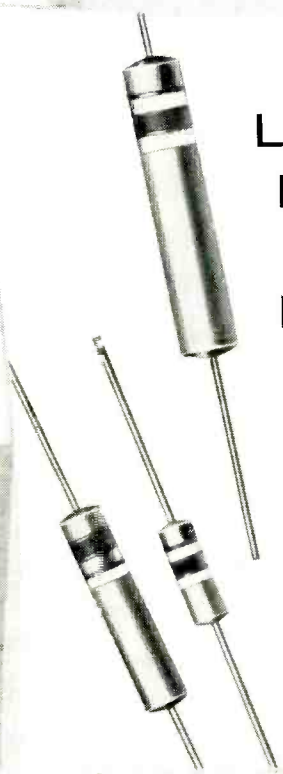
DESIGN AND COST PROBLEMS

Deposited Carbon Resistors

New molded resistor line providing a means of obtaining long-term stability up to 100 megohms with savings in cost and bulk.

- 1/8, 1/4, 1/2, 1 and 2 watt ratings
- excellent load life characteristics and resistance to aging
- conservatively rated at 70° C. ambient

Low Range BW Wire Wound Resistors



Now mass produced at low cost for transistor applications where the low volue and stability of a wire wound resistor is an important factor. Ruggedized unit to withstand rigors of modern installation techniques.

- fully insulated
- values from 0.24 ohm to 10 ohms

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Company _____

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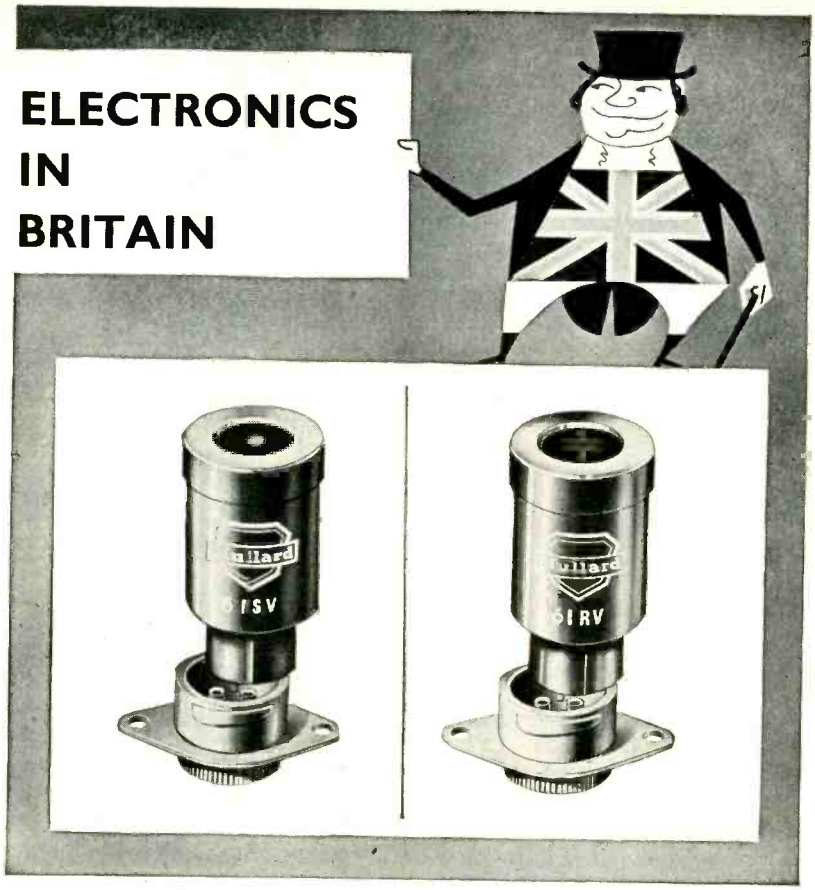
City _____ *State* _____

The British Electronics Industry is making giant strides with new developments in a variety of fields. Mullard tubes are an important contribution to this progress.



Principal Characteristics

	61SV	61RV
Peak spectral response	2.5μ	2.5μ
Spectral range	0.3 to 3.5μ	0.7 to 4.5μ
Cell resistance (average)	4MΩ	100KΩ
Max. applied voltage	250V	100V

Sensitivity

a. Tungsten light source at 2700°K	3.0mA/lumen	300μA/lumen
b. Black body at 200°C (radiation) energy 5.82μW; chopper frequency 800c/s; amplifier bandwidth 50c/s)	180V r.m.s./W peak to peak	1.66V r.m.s./W peak to peak

61SV/61RV

extra-sensitive infra-red photoconductive cells

Important among recent British achievements is the introduction by Mullard of two new photoconductive cells, the 61SV and the 61RV. These cells, specially designed for detecting infra-red radiations, combine an unusually high order of sensitivity with an extremely fast response, peaked at a wavelength of 2.5 microns. Their spectral range extends beyond the usual limits of infra-red detectors down to the red end of the visible spectrum.

The high signal-to-noise ratios of the 61SV and the 61RV make them ideal for measuring small temperature variations of relatively low heat sources down to 100°C. Additionally, their small size and rugged construction qualify them for the majority of infra-red applications in industry.

For further technical information and advice on the use of these outstanding photocells please write to either of the companies listed here.

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Rogers Majestic Electronics Limited, Dept. IC, 11-19 Brentcliffe Road, Toronto 17, Ontario, Canada.

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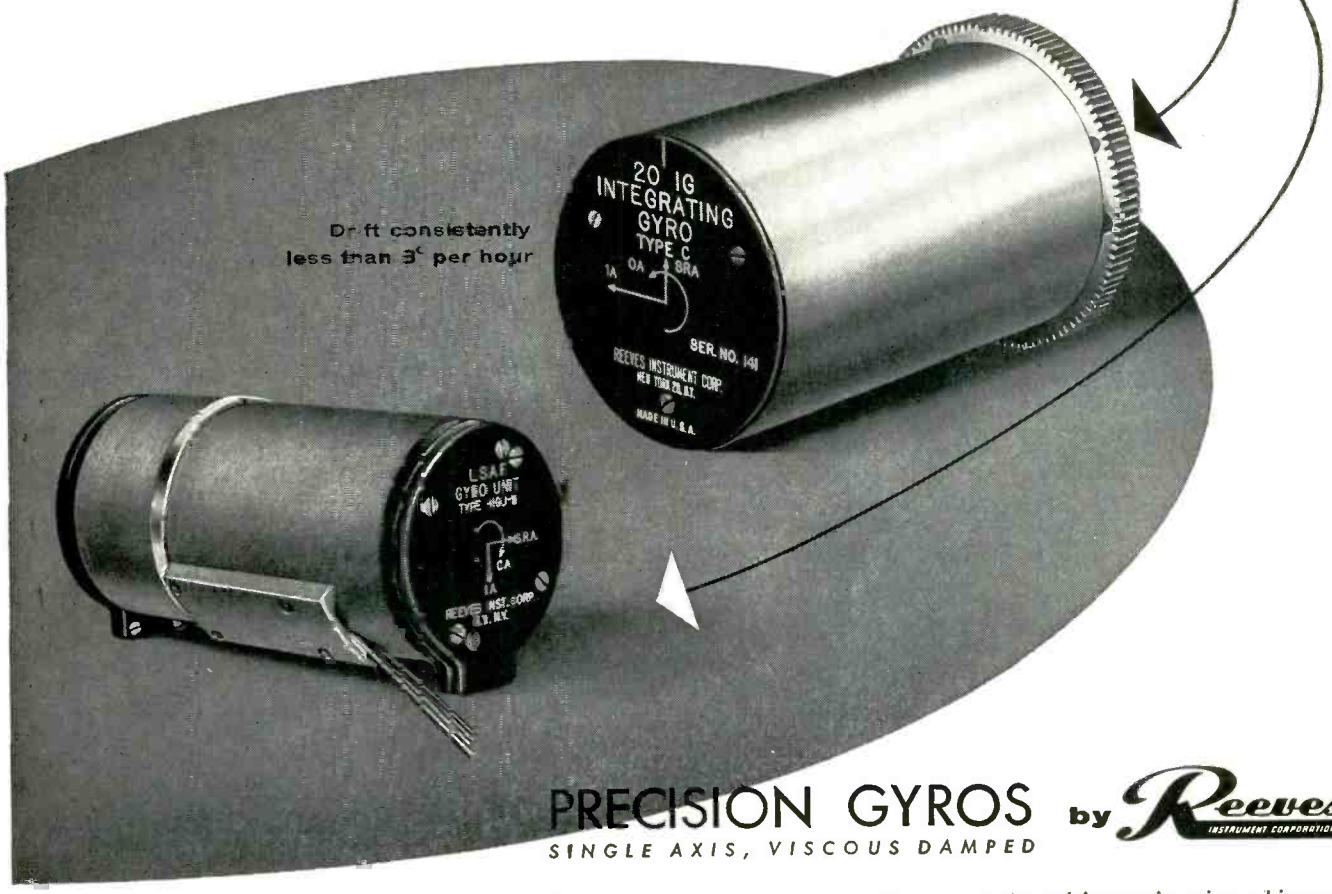

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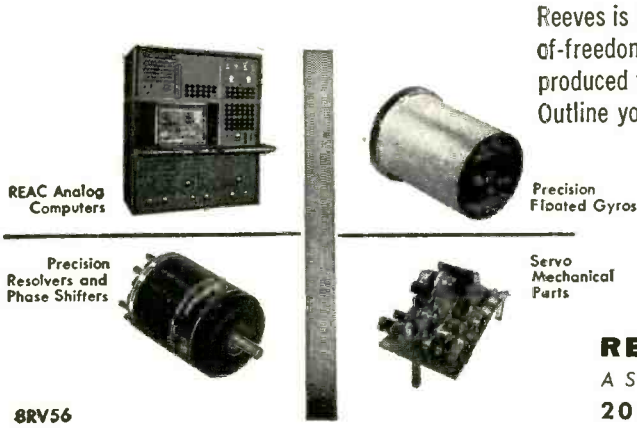

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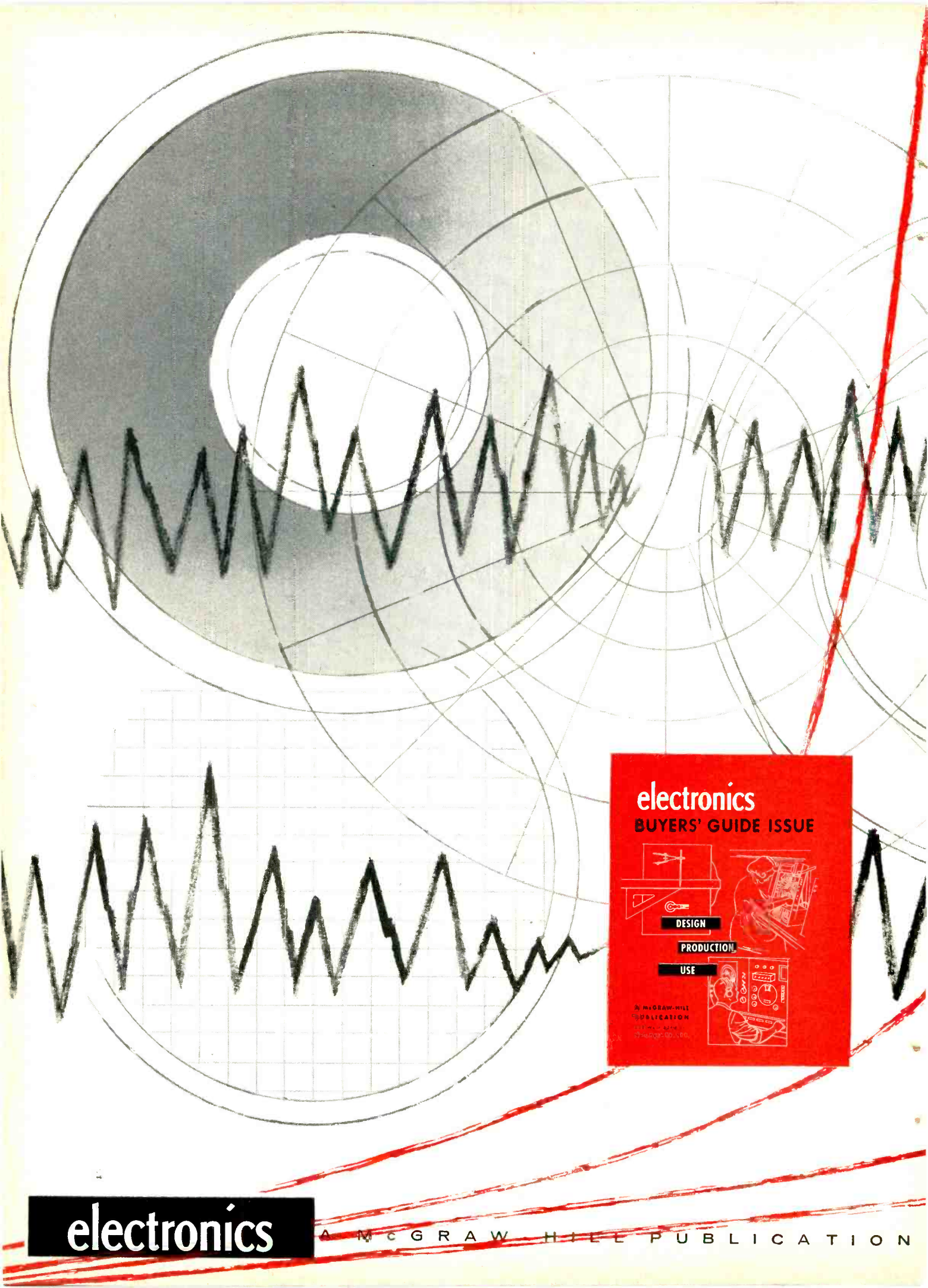

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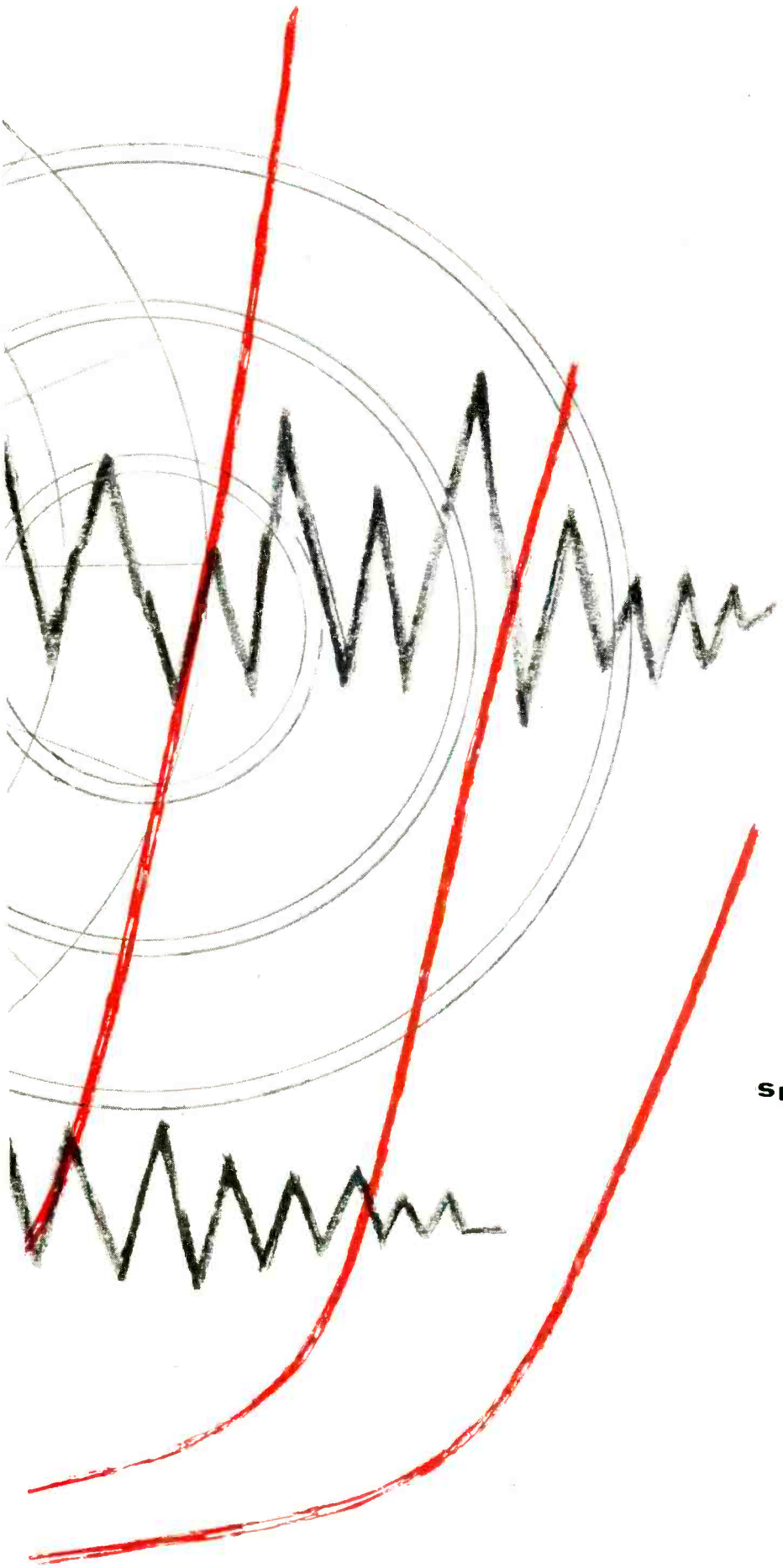

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2 • Facilitates Dynamic Balance Analysis

3 • Offers new possibilities for miniaturization of FM/FM Telemetry Ground Stations

1

new **Model PDA-1 Panoramic's Spectral Power Density Analyzer** — A tremendously flexible instrument that expands the utility and versatility of Panoramic's Spectrum Analyzers from Sub-Sonic through Microwave . . . automatically analyzes the energy distribution of random information. Ideal for evaluating noise, vibration and other changing phenomena.

2

new **Model SF-1 Panoramic's Synchronous Frequency Analyzer**—A versatile, direct reading instrument that has many application possibilities . . . automatically tracks a frequency component derived from a rotating or oscillating source and simultaneously provides a visual plot of component frequency vs. component amplitude. Excellent for dynamic balance analysis.

3

new **Model TMC-307 Panoramic's 7-Point Frequency Calibrator**—Designed specifically for telemetering applications, the TMC-307 sequentially furnishes *seven* equally spaced frequencies per channel for all RDB channels within end limits of ± 7.5% . . . within ± 15% for the upper five channels. Other end limits and spacings can be furnished. Channel and frequency point switching may be either manual or automatic. Accuracy is 0.02%. Occupying only 10½" panel space, the Model TMC-307 offers new possibilities for miniaturized ground station equipment.

Pioneers in the field of spectrum analyzers from sub-audio to microwave, unparalleled sweep generator systems and highly reliable frequency calibrators, Panoramic instruments have accelerated completion of research and development projects and helped to clear production test bottlenecks.

Now, Panoramic again leads the way with these three new instruments, highly versatile and far reaching in application.

SEE these significant new instruments . . . get a glimpse of new equipment to come . . . learn how Panoramic's instrumentation for testing, checking or measuring problems can help you . . . in the laboratory, on the production line, or in military applications. You are also cordially invited to witness dynamic demonstrations and to discuss with our engineers technical characteristics and applications of panoramic instruments.

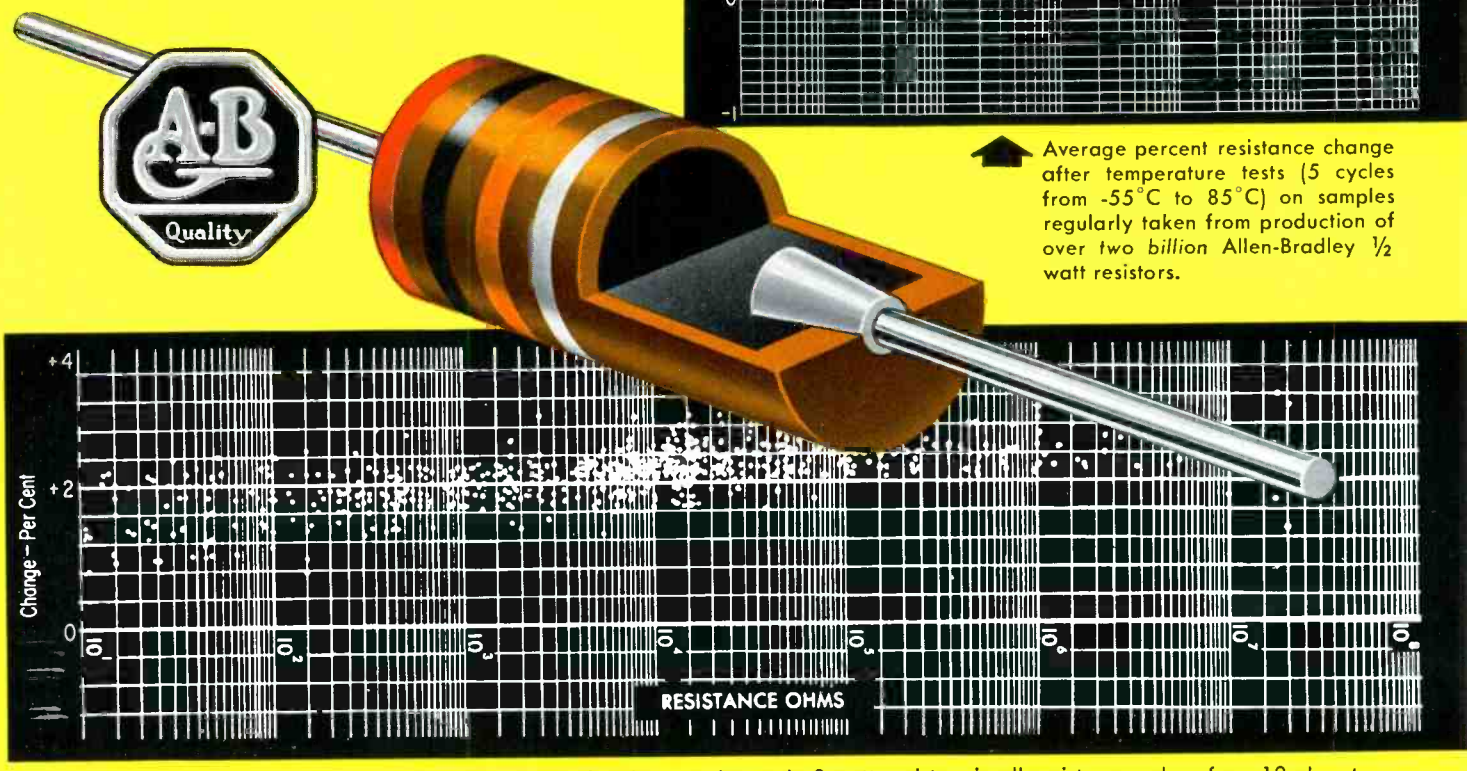
If you cannot attend the show, write, wire or phone for information. A Panoramic Applications Engineer is always available to discuss specific problems.

PANORAMIC
RADIO PRODUCTS, INC.

Panoramic Radio Products, Inc.
10 South Second Avenue, Mount Vernon, New York
Phone: Mount Vernon 4-3970 • Cables: Panoramic, Mount Vernon, New York State

fantastically uniform

Average percent resistance change after temperature tests (5 cycles from -55°C to 85°C) on samples regularly taken from production of over *two billion* Allen-Bradley ½ watt resistors.



Graph showing the consistency of resistance change in 2 watt resistors in all resistance values from 10 ohms to 100 megohms during humidity test at 95%, 55°C for 113 hours.

Allen-Bradley fixed resistors are available in 1/10, 1/2, 1, and 2 watt sizes, in all standard RETMA resistance values.

...billion after billion!

To maintain this uniformity, Allen-Bradley quality control engineers take samples of resistors from production continuously and test them. The results of these tests, as shown by the graphs on this page, are amazing. One graph, covering 1248 tests of samples from production totaling over two billion resistors, shows an average resistance change of only ½ of 1% after five cycles from -55°C to 85°C! Another graph, plotting production sampling of 100 million resistors in a humidity test at 95%, 55°C for 113 hours, shows only a slight deviation in resistance.

So far as electrical characteristics and mechanical configuration are concerned, Allen-Bradley resistors have no equal. That's why they are so decidedly preferred by electronic engineers throughout the world.

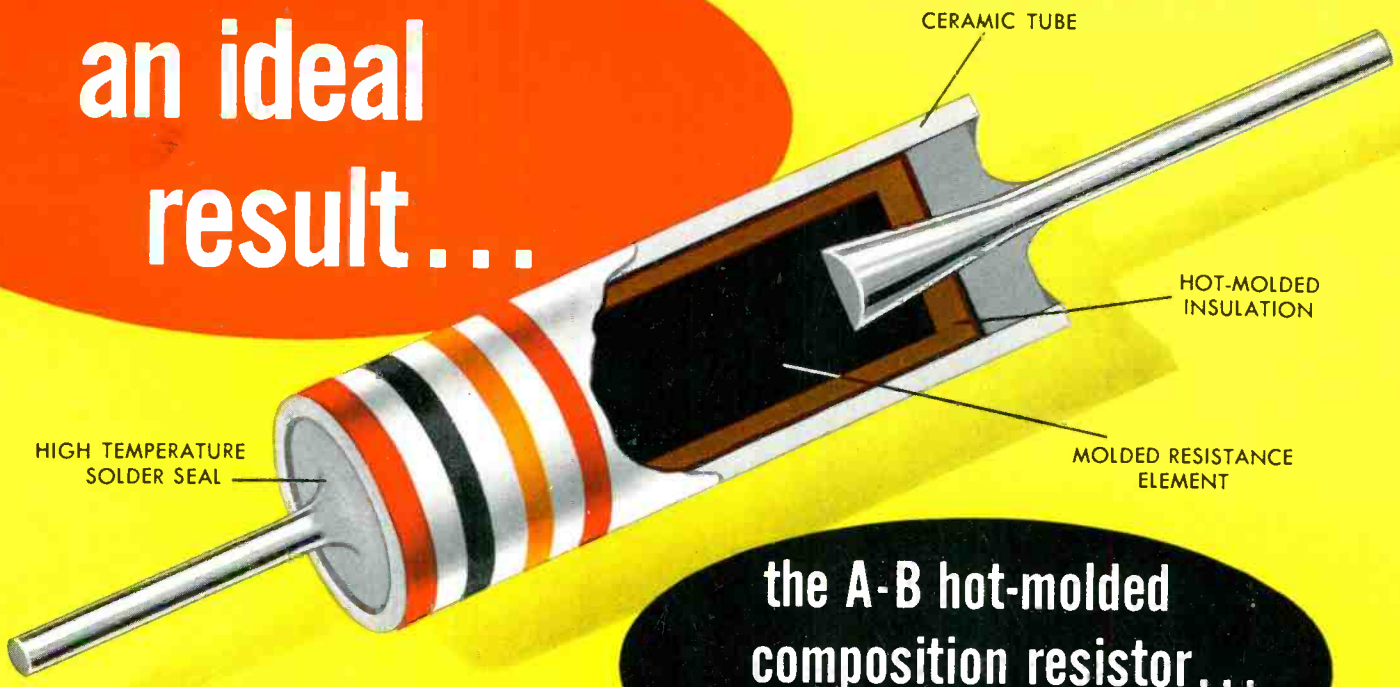
Allen-Bradley Co., 222 W. Greenfield Ave., Milwaukee 4, Wis.
In Canada—Allen-Bradley Canada Limited, Galt, Ont.

ALLEN-BRADLEY

HOT-MOLDED COMPOSITION RESISTORS

QUALITY

an ideal result...

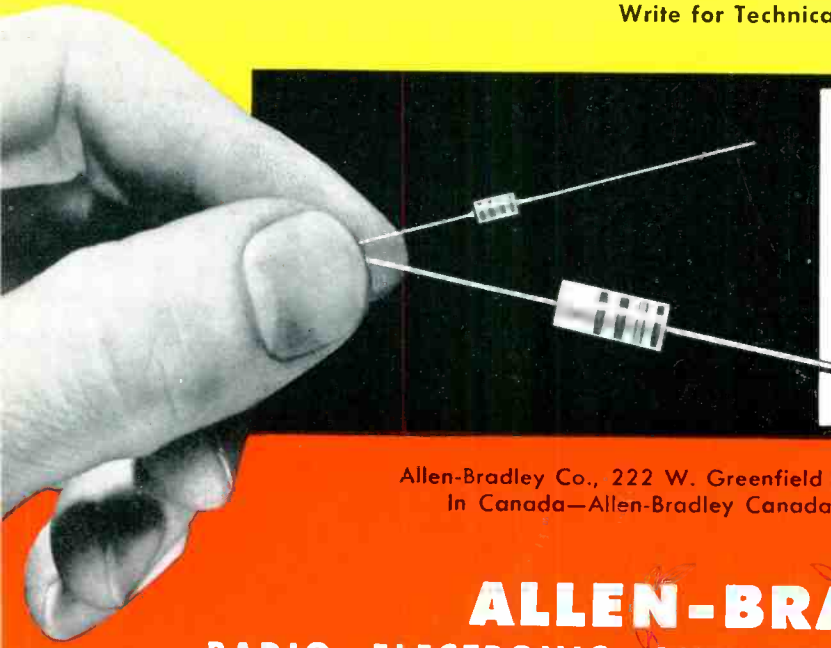


the A-B hot-molded composition resistor... *HERMETICALLY SEALED!*

● Here's a line of composition resistors that assures you virtually ideal characteristics *plus* complete freedom from catastrophic failures. Because of their ceramic enclosure and high temperature hermetic end seals, these hot-molded composition resistors are unaffected by humidity and moisture. Furthermore, they have an extremely low noise level. All microphonic noise, occasionally encountered in composition resistors due to shock and vibration, has been eliminated. Their unusual rugged construction, and uniformity of size and configuration make these resistors ideal for mechanical handling.

Special techniques have made it practical to increase the operating temperatures beyond the rating heretofore considered "good practice." The Type ES, 1 watt resistor can be operated safely at 165° C without load; the Type TS at 110° C under the same conditions. Available in tolerances of 2% and 5%; in resistance values from 2.7 ohms up.

Write for Technical Data



Allen-Bradley Hermetically Sealed, Hot-Molded Composition Resistors, Type TS (1/8 watt) and Type ES (1 watt)

Allen-Bradley Co., 222 W. Greenfield Ave., Milwaukee 4, Wis.
In Canada—Allen-Bradley Canada Limited, Galt, Ont.

ALLEN-BRADLEY

RADIO, ELECTRONIC, AND TELEVISION COMPONENTS

Oxygen-free high conductivity copper... *in convenient* rod form

Tube manufacturer ends rejects by using PB&B O.F.H.C. copper rod

A major manufacturer of transmitting tubes was getting rejects of approximately 2 per cent in finished tubes, due to microscopic leaks in a copper part made from extruded rod. Each reject meant loss of a tube worth nearly $100. This source of high vacuum leakage was impossible to detect before assembly. Since switching to O.F.H.C. hot rolled rod, supplied by PB&B, rejects from this cause have completely vanished.

Need *certified grade* O.F.H.C.® copper rod—for use in vacuum tubes or other electrical or electronic equipment?

We can supply you quickly from stock, to highest quality standards. You'll find this material useful and economical in many special applications. It is pre-forged and hot rolled, to produce a dense, homogeneous grain structure free from microscopic porosity. It is not subject to hydrogen embrittlement during hydrogen atmosphere brazing. We certify its conductivity to be at least 98% I.A.C.S.

Cold-straightened rod, in diameters of ¾", 1", 1¼", 1⅜", 1½" and 1⅝", to standard hot rolled tolerances, is regularly stocked in "as rolled" condition. You can order in random lengths, or we can cut to your specifications.

Write today for a quotation on your particular requirements.

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PHILADELPHIA BRONZE & BRASS CORP.
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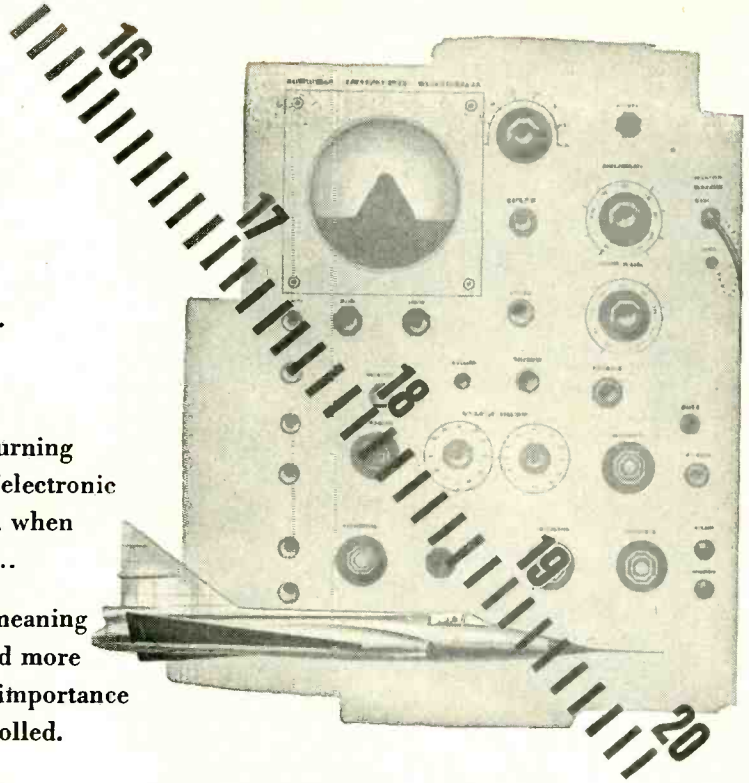
—a subsidiary of

P.R. MALLORY & CO. Inc.
MALLORY

SECOND OF A SERIES

How to get reliability



Got the automation jitters?...worried about turning complex manufacturing operations over to an "electronic brain"?...worried about what can happen when one component in the control system fails?...

Reliability takes on a new and different meaning as American industry becomes more and more automated. Here are a few thoughts on the importance of reliability and how it can be controlled.

All of us are going to have to pay more attention to "reliability."

We'll have to pay more attention to individual "devices" within a system.

We'll have to guard ourselves carefully when we design the entire system.

The industrial pendulum is swinging more and more toward automatic controls, servo-mechanisms, computers, and automatic "watchers." As it does, the reliability factor becomes more and more important. Let's see why. For example, you probably have three radios at home. If one fails because a soldered joint comes apart, your home life is probably not disrupted to any alarming degree. But... consider the automatically controlled steel mill. One soldered joint failing, unless all controls are installed in duplicate (which is expensive) could tie up the entire production process for valuable minutes, if the maintenance crew has second sight. For hours, if automatic trouble-indicating and locating systems are not installed (and these are expensive, too). Last, but not least, lend a thought to the dependence of guided missiles and man-made satellites upon the reliability of electronic circuits and components. So... let's start to examine "reliability." Let's begin by looking at this definition which is currently popular in the technical field:

The reliability of a particular component or system of components is the probability that it will do what it is supposed to do under operating conditions for a specified operating time.

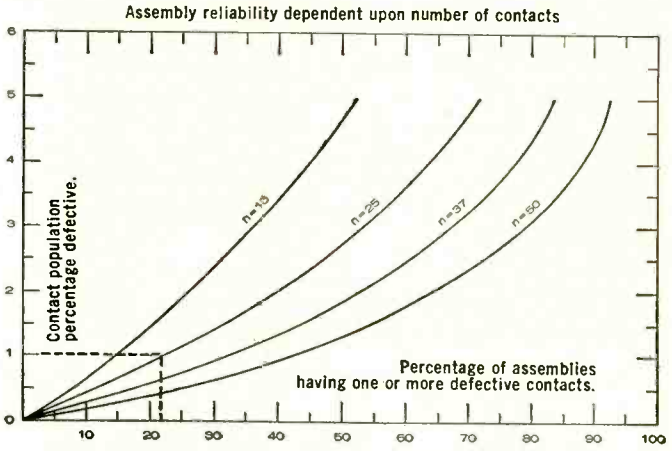
Now... this is a relatively well-accepted definition, and it offers the key to the problem of coping with failure control. Take the word "probability" in this definition. Let's discuss its implication.

Many of today's systems, simple or complex, are a chain of components. So picture a system as a chain with its successive links. In the field of statistics the over-all reliability of the chain is the mathematical product of the reliabilities of the individual links...

Overall Reliability, $R_o = r_1 \times r_2 \times r_3 \ldots r_n$

Now, let's consider a system made up of 100 different components, each of which has a reliability of 99%. In applying the formula, multiplication of .99 by itself 100 times gives an over-all reliability for the system of only 36.5%. Two out of three systems you have put together will probably fail!

Cannon becomes involved with this problem because our main business is making electric connectors. So, let's look at the following chart that covers contact reliabilities and reliability of the assembly in which they are mounted.



This chart illustrates the reliability of four connectors having 15, 25, 37 and 50 contacts respectively. As an example, assume that the contacts have a contact population of 1% defective (1 in 100 defective . . . this percentage is considered a fairly high standard in most fields). On the 15-contact assembly, we find from our chart that 14% of the connector assemblies would have one or more defective contacts! With 25 contacts, 22% would have one or more defective contacts. With 50 contacts, 41½% . . . is your hair starting to curl? Obviously, a 99% contact reliability standard for guided missile components is absolutely unacceptable. And, in between the simplest system and that of a guided missile, are hundreds of assemblies and systems whose reliability factors must be analyzed with utmost care.

But all is not lost! There's another side to the picture. With proper care, analysis, and control, our Cannon organization has actually achieved, in special "missile quality" contacts, a known level of only 2.85 x 10^{-3}% defective . . . only 1 part in 35,000! Naturally, we don't achieve that with all our contacts . . . but we do try to design and manufacture the utmost in reliability required for specific applications.

We have pictured this chart to show the direction we must all take, whether we're talking about connectors, other components, or systems. It boils down to two steps . . .

- The number (n) of components must be kept low . . . *simplicity*.
- The level of component reliability must constantly be improved . . . *hard work for all of us*.

Now . . . if we refer to our reliability definition on the previous page we note the phrase "do what it is supposed to do." So be sure *you* define these objectives for your component assembly, or system . . . failure to do so carefully can cause undue failure or the expenditure of unnecessary dollars for needless, excessively-reliable parts or design.

Further on in the same definition, we note the words "operating conditions." This brings up many new points for consideration. Here we are concerned with such things as temperature, pressure, humidity, corrosive atmosphere, stray electric and magnetic fields, low and high frequency noise, shock and vibration. Do your design standards need upgrading? Are your components designed and then tested to meet the operating conditions you specify . . . or are they designed to meet "average" conditions? Are you using adequate "safety factors"?

In a simple component, manufacturers have always looked for, recognized, and corrected faults when they occurred. We use component quality control to achieve and maintain Cannon's world famous product quality. But in complex systems such component quality control is not enough. Actually . . .

Reliability control over the system is needed. It should be all-encompassing. When you get right down to it, *reliability* is the product of procedures, equipment, and people . . . in the design, manufacture, testing, control of quality, transportation, and use of products or systems.

Do you have a reliability control system?

Here are a few of the steps that are needed to get a reliability control system operating:

1. Determine Your Requirements. Specify the environment, operating time, performance limits, and the percent of reliability required. Allow an adequate safety factor keeping in mind the end use of the finished product.

2. Collect Reliability Data. Set up facilities for the continuous accumulation of data on component or system failures and their causes.

3. Establish quality control and test procedures which show high degree of correlation with end-use conditions.

4. Analyze. Determine if reliability requirements are being met. Establish the most important causes of failure by analyzing the data you collect.

5. Improve. Take action to eliminate the most important defects or causes of failure. Reduce the failure rate to the required level.

6. Maintain Continuous Vigilance. You have emphasized system design . . . you have used statistical analysis of failures . . . now exert continuous and critical control to be sure your "improvements" actually improve reliability. Examine new and unforeseen failure sources. Review and modify your requirements with changing conditions.

*

We at Cannon Electric are proud of our historical emphasis on quality and reliability. Since 1915 we have adhered to a design philosophy embracing the highest quality and reliability in each and every Cannon Plug for the specific application for which it is to be used. *If we can't design to that principle, we don't make it!* In manufacture, we are proud of our know-how in depth, proud of our fine quality control systems, proud of our personnel and proud of our reliability control group.

Whenever *you* have an electric connector reliability problem . . . in design, engineering, production, or prototype phases . . . we would appreciate the opportunity of discussing it with you.

Cordially,

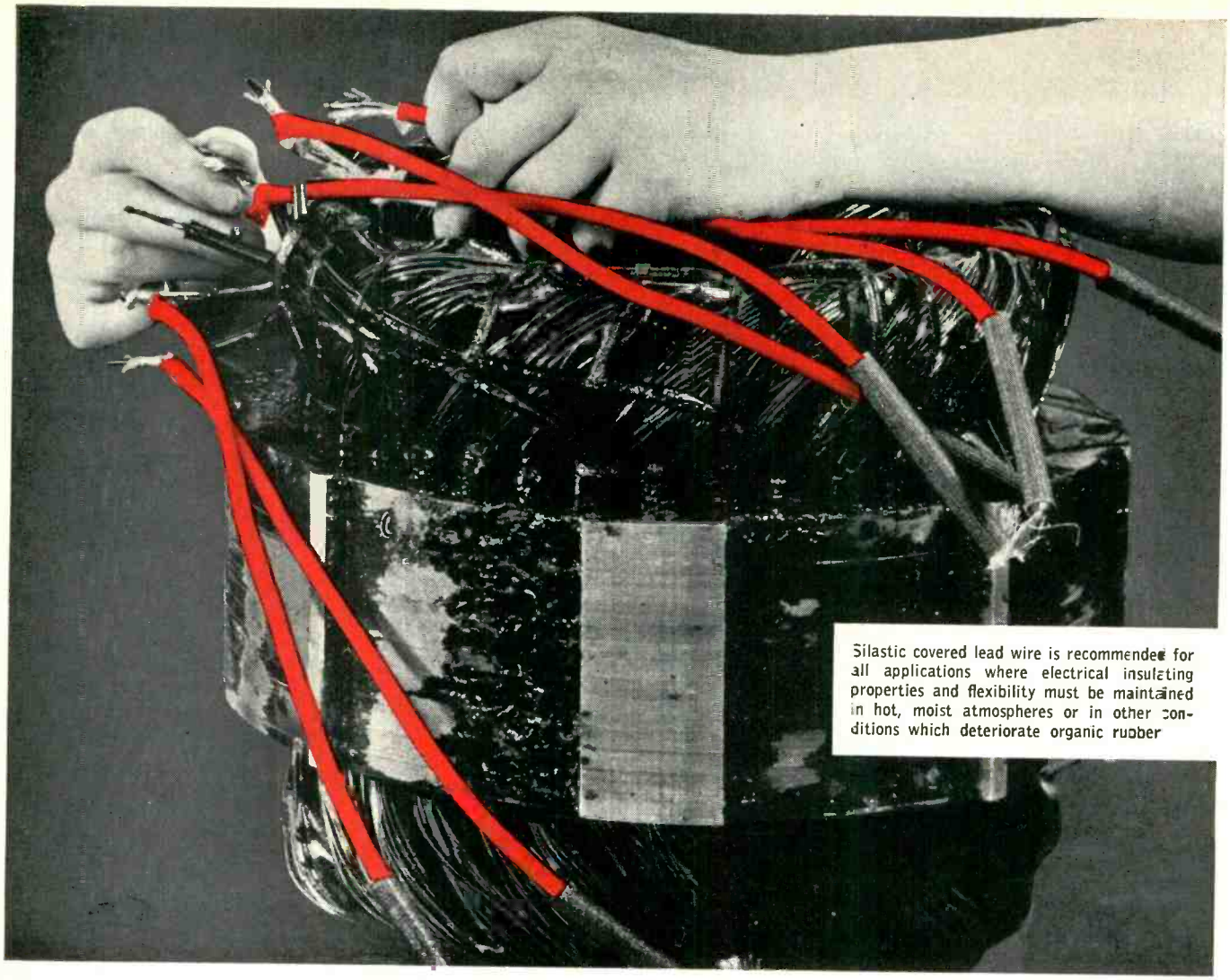
Robert J. Cannon *President*

CANNON ELECTRIC COMPANY
3208 Humboldt St., Los Angeles 31, California

CANNON PLUGS

Eight plants around the seven seas!

Please Refer to Dept. 120



Silastic covered lead wire is recommended for all applications where electrical insulating properties and flexibility must be maintained in hot, moist atmospheres or in other conditions which deteriorate organic rubber

SILASTIC covered cable stays flexible at 500 F

SILICONE RUBBER

Even after repeated exposure to temperatures as low as —130 F or as high as 500 F Silastic*, Dow Corning's silicone rubber, retains its flexibility, dielectric strength and resistance to ozone, weathering, moisture, certain hot oils and corrosive atmospheres. That's why Silastic, employed as a covering for all types of electric wire and cable, assures the ultimate in reliable service. Ask any leading rubber fabricator.

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Please send me latest data on Silastic

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*T M REG U S PAT OFF

Typical Properties of Silastic for Wire and Cables

• Temperature range, °F	—130 to 500
• Tensile strength, psi	600 to 900
• Elongation, %	150 to 300
• Insulation Resistance, megohms/1000 ft.	1000 to 3000
• Dielectric strength, volts/mil	300 to 500
• Dielectric Constant, 10^2 cycles per second, nominal	3.2

If you consider ALL the properties of a silicone rubber, you'll specify SILASTIC.

first in silicones

DOW CORNING SILICONES

DOW CORNING CORPORATION • MIDLAND, MICHIGAN

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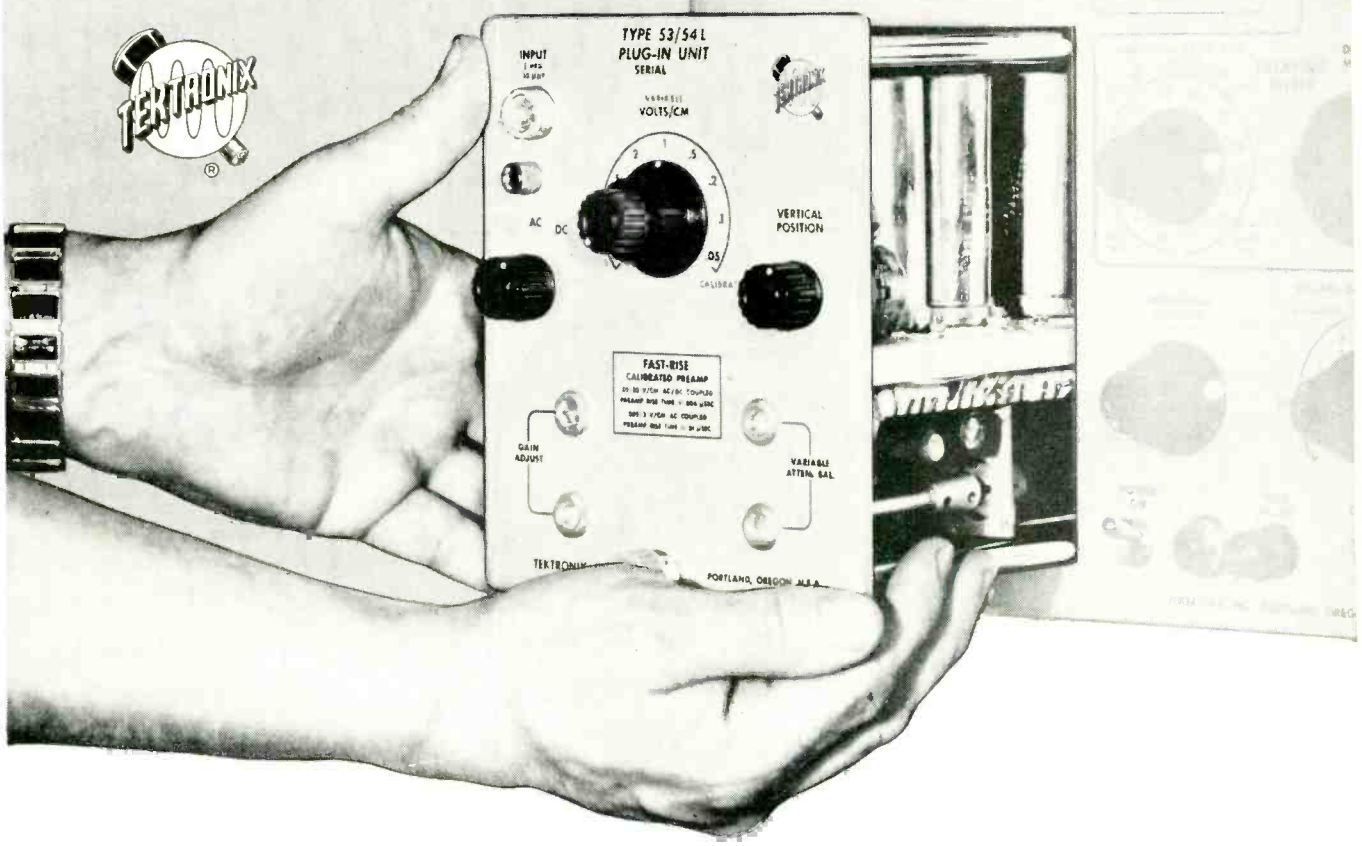
Another *NEW* Plug-In Unit

to *increase* the value of your Tektronix Type 541 and Type 545 Oscilloscopes



High Sensitivity for Fast-Rise Applications—The new Type 53/54L Fast-Rise High-Gain Preamplifier plugs into your Type 541 and Type 545 Oscilloscopes, increasing the calibrated vertical deflection factor to 5 millivolts/cm. At the higher deflection factors (5 millivolts/cm to 50 millivolts/cm), risetime is 0.015 μsec and vertical passband is 3 cycles to 24 mc. From 50 millivolts/cm to 50 volts/cm characteristics are the same as the Type 53/54K Unit . . . risetime 0.012 μsec, passband dc to 30 mc. Input capacitance is 20 $\mu\mu$f direct, 8 $\mu\mu$f with the 10x attenuator probe furnished with Type 541 and Type 545 Oscilloscopes. Other probes with higher attenuation ratios are available to reduce input capacitance to as little as 2.5 $\mu\mu$f.

Type 53/54L Fast-Rise High-Gain Unit $185

First shipments are expected to be made during July, 1957. Please keep in touch with your Tektronix Field Engineer or Representative for current details.

OTHER PLUG-IN UNITS FOR TYPE 530-SERIES and TYPE 540-SERIES OSCILLOSCOPES

Type 53/54A—Wide-Band DC Unit	$ 85
Type 53/54B—Wide-Band High-Gain Unit	125
Type 53/54C—Fast-Rise Dual-Trace DC Unit	275
Type 53/54D—Differential High-Gain DC Unit	145
Type 53/54E—Low-Level Differential AC Unit	165
Type 53/54G—Differential Wide-Band DC Unit	175
Type 53/54K—Fast-Rise DC Unit	125

Prices f.o.b. Portland, Oregon

SEE THE TYPE 53/54L UNIT AND OTHER NEW TEKTRONIX INSTRUMENTS AT THE IRE SHOW, BOOTHS 3028, 3029 AND 3030.

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P. O. Box 831 • Portland 7, Oregon
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NOW...

a completely new subminiature paper tubular capacitor

Because the terminal is mechanically retained in the case, independent of the captive solder seal, the new design permits perfect positioning with uniform accuracy.

Hermetically sealed with Sangamo's new "Innerseal" terminal...for higher reliability...for longer service life

Here is today's latest development in miniaturized military type capacitors—a newly designed terminal for Sangamo subminiatures. This Sangamo engineering development offers many advantages over conventional seals.

The "Innerseal" structure seats and locates itself exactly on the case. Terminals cannot be cocked at angle, extend out of case, or be pushed too deeply into case and cause cupped ends or section damage. It permits optimum performance and reliability through greater flexibility of internal design.

The solder is confined and automatically sealed. Solder or flux cannot run down inside case to cause life failures due to contamination. There are no cracked terminals due to solder time variation.

Write for full information—ask for Engineering Bulletin TSC-117, or

SEE THIS NEW CAPACITOR AT THE I. R. E. SHOW

VISIT SANGAMO BOOTH 1213

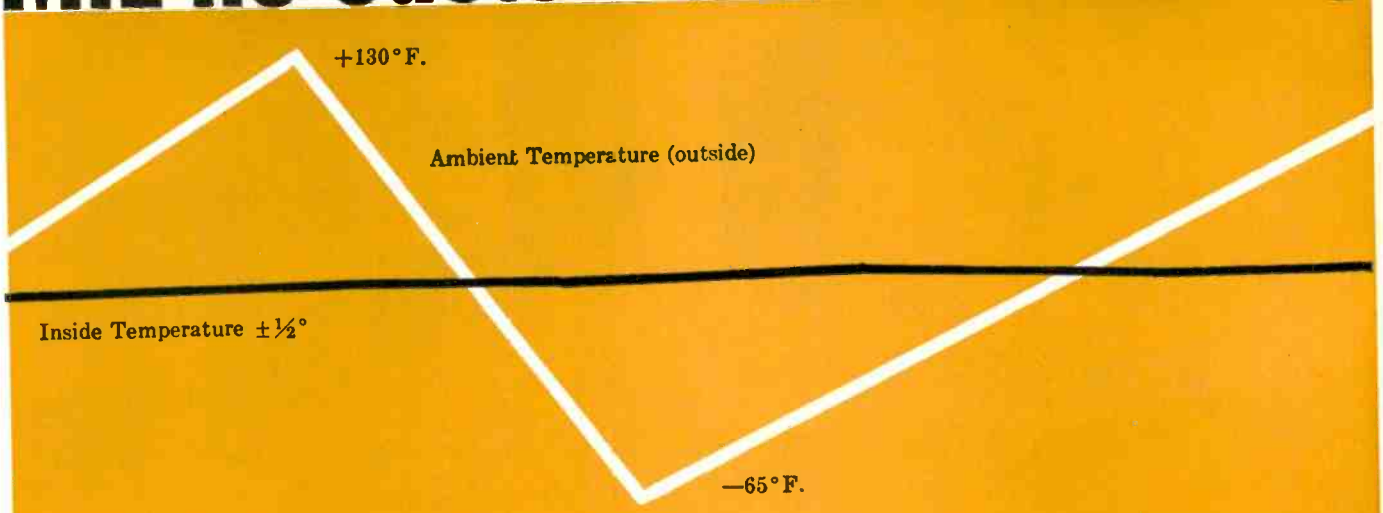
SC57-3

SANGAMO ELECTRIC COMPANY

Electronic Components Division

SPRINGFIELD, ILLINOIS

MIL-AC Custom Air Conditioning



Condition: MIL-E-5272* Today, electronic systems can function under the most difficult environmental conditions (MIL-E-5272*), by using highly specialized air conditioning equipment.

Custom air conditioning is our business at Ellis and Watts. For example, we recently designed and built MIL-AC Units for Radome installations operating in ambient temperatures from −65°F. to +130°F. These air conditioning units maintain temperatures within ±½° F., with continuous dehumidification under varying internal load conditions. Because of antenna sweep height of unit was restricted to 36″.

MIL-AC Units are self-contained, compact, lightweight, readily air-transportable. They can be designed to cool, heat, humidify, dehumidify, filter, and can incorporate air-cooled or water-cooled condensers. Units are manually or automatically controlled. We are staffed with specialists who will analyze your requirements, submit a proposal, complete your installation promptly and to your complete satisfaction.

Write for helpful load calculating Nomograph and other technical data for use in making time-saving preliminary calculations.

*Military specification dealing with the following climatic and environmental conditions: Temperature, humidity, altitude, salt spray, vibration, fungus, sunshine, rain, sand and dust, explosive atmosphere, acceleration and shock.

Typical MIL-AC Unit. MIL-AC configurations, features and functions to suit your specific requirements.

ELLIS AND WATTS PRODUCTS, INC.

P.O. Box 33, Cincinnati 36, Ohio.

Ellis and Watts also design and build custom air conditioners, liquid coolers and heaters, dehumidifiers, wave guide dehumidifiers, laboratory temperature and humidity control units.

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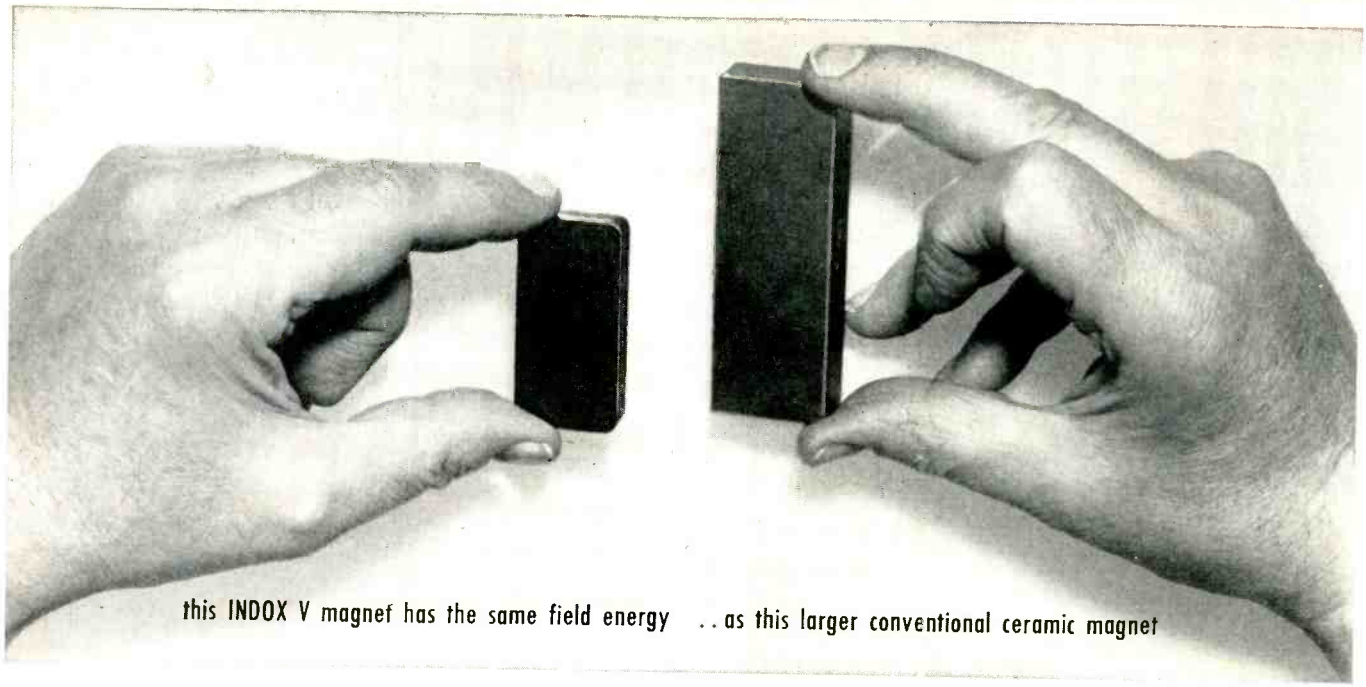


this INDOX V magnet has the same field energy .. as this larger conventional ceramic magnet

NEW, high energy Indox V ceramic permanent magnets

.. they're 3½ times stronger than conventional ceramic magnets

Indox V — another first from the research and development laboratories of The Indiana Steel Products Company — is available to magnet users *immediately*. This unique, new, magnetic material offers these important advantages . .

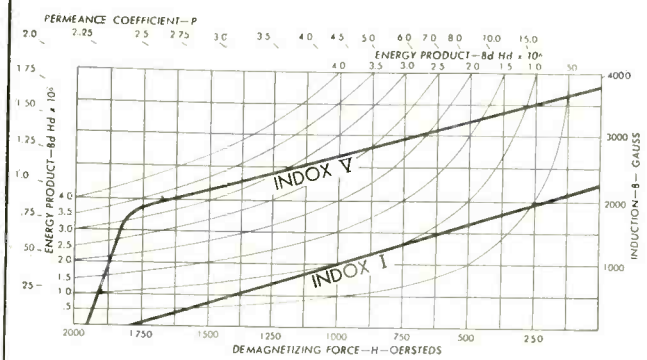
Indox V requires no critical materials. It is a highly oriented barium ferrite . . using inexpensive, noncritical, raw materials that are constantly available. Shortages in times of emergency cannot occur.

Indox V requires less space, weight to do same job. Volume and weight comparisons show that the energy of Indox V far exceeds Indox I . . and is comparable to Alnico V, the strongest permanent magnet material commercially available.

Indox V offers high resistance to demagnetization. Indox V magnets can be designed for applications where extremely high demagnetizing forces exist . . without irreversible losses occuring. This means it can be used where other types of magnets have been impractical . . for example, in stators of medium-size electric motors where electromagnets are now being used.

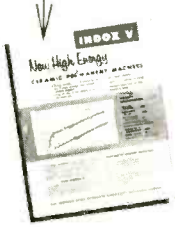
.. ideal for:

- D-C motors
- Synchronous drives
- Traveling wave tubes
- High-fidelity loud-speakers
- Eddy current drives
- Tractive devices where size is important



Comparison of demagnetization and energy product curve for conventional Indox I ceramic magnets and the new, high energy Indox V magnets.

JUST PUBLISHED! *This two-page data sheet gives detailed information on new high energy Indox V. Use this coupon to request your copy. Ask for Bulletin 16-A3.*



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.. the world's largest manufacturer of permanent magnets

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INDIANA PERMANENT MAGNETS

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sierra

Peak-reading and average-reading WATTMETERS—POWER MONITORS

Sierra 195A-Z Termination Wattmeter

TERMINATE RF COAX SYSTEMS

MEASURE RF POWERS

MEASURE INCIDENT, REFLECTED POWERS

MATCH ANTENNAS, LOADS

SIERRA TERMINATION WATTMETERS

Sierra 195A series Peak-Reading Termination Wattmeters are rugged, conservatively rated instruments specifically designed for measuring peak powers and terminating rf coaxial systems in testing and adjusting pulse transmitters and oscillators. They are designed for maximum reliability and minimum rf leakage. Three basic models cover 250 MC to 1000 MC and have characteristics given alongside. All require a 110 v 60 cps power source.

Sierra 185A series Average-Reading Termination Wattmeters are also offered for average-power measurement or termination on rf coaxial systems. The table at right gives models, frequency coverage, etc. No auxiliary power is required.

BI-DIRECTIONAL POWER MONITORS

Sierra Power Monitors are convenient, versatile instruments for measuring incident or reflected power, or precise matching of loads to lines. A twist of the wrist selects incident or reflected power, or any power range. Compact, rugged construction makes these instruments ideal for portable field applications or laboratory use.

Peak-Reading Sierra 194-A Bi-Directional Peak Power Monitor reads 0-1/3/10/30 Kw from 200 MC to 1215 MC. Minimum pulse width 1.0 μsec, minimum repetition rate 400 pps, accuracy ±10% full scale. Insertion VSWR 1.10 maximum. Requires 110 v 60 cps power source.

Average-Reading Sierra 164 series Bi-Directional Power Monitors cover 25 MC to 1000 MC with as few as two plug-in elements. Each plug-in covers broad frequency range and has full scale power ranges of 1, 5, 10 and 50 watts or 10, 50, 100 and 500 watts. Power is read direct on linear scale within ± 5% full scale. Insertion VSWR less than 1.08 (Type N connectors) except on 1 watt ranges. 50 ohm impedance available with Type N or UHF connectors. No auxiliary power required.

Sierra 194A-A

MODEL 195A PEAK-READING WATTMETERS

Model	Frequency	Peak Power, Kw	Max. Average Power	Connector
195A-Z	250-1000 MC	0-1/3/10	15 watts	N
195A-X	250-1000 MC	0-10/30/100	100 watts	LC
195A-Y	250-1000 MC	0-100/300/1000	500 watts	LC

MODEL 185A AVERAGE READING WATTMETERS

Model	Frequency	Power Range, Watts	Max. Power Dissipation	Connector
185A-15FN	20-1000 MC	0-5/15	15 watts	N
185A-100FN	20-1000 MC	0-30/100	100 watts	N
185A-500FN	20-1000 MC	0-150/500	500 watts	N

Note: 185A series accuracy ± 5% full scale maximum VSWR 1.2. 195A series accuracy ± 10% full scale, pulse width 1.0 μsec minimum, repetition rate 400 pps minimum. Female connectors standard.
Sierra also manufactures calorimeter wattmeters; details on request. Data subject to change without notice.

Sierra Electronic Corporation

A Subsidiary of Philco Corporation

3885 Bohannon Drive DAvenport 6-2060 Menlo Park, California, U.S.A.

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IRE Booths 3905-3907

4085

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Motor - Gear - Trains

3:1 to 150,000:1 Ratio Range • Up to 18 Foot Pounds Torque

- Motors available: DC, 60 or 400 cycle, PM, split series, series, shunt, single phase and 2-phase. All are reversible.
- Available with either governor or brake.
- 1000 hour life minimum.
- Designed to meet MIL-E-5272A.
- Precision gearing throughout.
- Can be furnished up to 125°C.
- Designed for continuous duty or intermittent duty applications.

MOTOR GEAR TRAIN									Size	Overall Length Inches-Max.	Motor Type	Mounting	Oster Type
Gear Ratio	No-Load Speed	Nominal Voltage D.C.	Voltage Range D.C.	No-Load Current	Normal Speed	Normal Load OZ.IN.	Normal Current	Operating Temp. Range					
5.68:1	1800	28	24-32	0.4	1800	5.0	1.0	−55° To +85°C	13	3.777	P.M. GOVERNOR	FACE	13R-9102-08
17.9:1	600	28	24-32	0.4	600	12.0	1.0	−55° To +85°C	13	3.930	P.M. GOVERNOR	FACE	13R-9102-06
32.3:1	300	28	24-32	0.4	300	12.0	1.0	−55° To +85°C	13	3.935	P.M. GOVERNOR	FACE	13R-9102-02
67:1	150	28	24-32	0.4	150	12.0	0.6	−55° To +85°C	13	4.092	P.M. GOVERNOR	FACE	13R-9102-05
85:1	150	27.5	—	.25	130	50.0	0.7	−55° To +85°C	13	4.095	P.M.	FACE	13R-9101-11
109:1	100	28	24-32	0.4	100	32	0.6	−55° To +85°C	13	4.094	P.M. GOVERNOR	SYNCHRO	13R-9102-12
109:1	180	27.5	—	0.4	175	30	0.5	−55° To +100°C	13	2.843	P.M.	FLANGE	13R-9104-01
125:1	75-90	28	—	.25	70-85	20	0.3	−55° To +71°C	13	3.920	P.M.	FACE	13R-9101-13
157:1	60	28	24-32	0.4	60	12.0	0.6	−55° To +85°C	13	4.095	P.M. GOVERNOR	FACE	13R-9102-03
285:1	48	35	—	.25	40	160	0.6	−55° To +71°C	13	4.038	P.M.	FACE	13R-9103-01
333:1	30	28	24-32	0.4	30	12.0	0.6	−55° To +85°C	13	4.317	P.M. GOVERNOR	FACE	13R-9102-04
410:1	15	27	25-29	0.3	15	8.0	0.3	−55° To +85°C	13	4.400	P.M. GOVERNOR	FACE	13R-9102-11
1043.8:1	5-10	27	24-30	0.15	7	30	0.2	−55° To +71°C	13	4.450	P.M. BRAKE	FACE	13R-9105-01
1044:1	5-10	27	24-30	0.15	7	30	0.2	−55° To +71°C	13	3.910	P.M.	FACE	13R-9101-12
2214:1	3-4	6	—	1.2	3.4	30	1.2	−55° To +71°C	13	4.454	P.M.	FACE	13R-9101-04
3241:1	5.5	35	—	.35	5.5	18	0.4	−55° To +71°C	13	4.454	P.M.	FACE	13R-9101-03
5933:1	1.3	30	—	.13	1.3	30	0.15	−55° To +71°C	13	4.816	P.M.	FACE	13R-9101-10
21,707:1	2-3	120	—	.25	2-3	12	0.25	−55° To +71°C	13	3.475	P.M.	FLANGE	13R-9101-16
322:1	80	110	—	0.2	30	240	0.3	−55° To +71°C	15	3.815	SPLIT SERIES	FLANGE	15R-9201-01
407:1	22	27	—	0.2	20	8	0.2	−20° To +50°C	15	3.989	SPLIT SERIES	SYNCHRO	15R-9201-03
433:1	30	26	—	0.6	25	260	1.2	−50° To +80°C	15	3.110	SHUNT	FACE	15R-9201-02
955:1	33	27	—	0.6	12-18	420	1.0	−55° To +50° C	15	4.419	SPLIT SERIES	FLANGE	15R-9201-08
26:1	240	27.5	24-29	0.65	240	40	1.3	−18° To +71°C	17	5.315	SHUNT GOVERNOR	SYNCHRO	17R-9251-01
4.26:1	1800	28	—	0.6	1800	12	1.85	−30° To +55°C	24	4.640	SHUNT GOVERNOR	FACE	24R-9451-01

Speed tolerance on governed motors is ±2% over voltage and an ambient temperature range. Closer speed tolerance units can be designed to fit the particular application.

Many other variations available. There is an Oster motor-gear-train to fit your exact specification. Consult Oster specialists today, sending your detailed requirements.

Other products include servos, synchros, AC drive motors, DC motors, servo mechanism assemblies, synchro indicators, servo torque units, reference and tachometer generators, actuators, motor driven blower and fan assemblies and fast response resolvers.

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Engineers For Advanced Projects:
Interesting, varied work on designing transistor circuits and servo mechanisms. Contact Mr. Zelazo, Director of Research, in confidence.

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Fast, convenient, dependable

precision wave analyzers frequency-selective voltmeters

Sierra 121A Wave Analyzer

Sierra now offers exactly the instruments you need for wave analysis, wire carrier and microwave subcarrier applications.

Sierra 121A Wave Analyzer is a highly selective, double superheterodyne receiver covering frequencies from 15 KC to 500 KC and providing wave analysis data directly in voltage and dbm at 600 ohms. The instrument offers the selectivity required for use with new single sideband carrier systems.

Sierra 158A Wave Analyzer is similar but covers frequencies from 500 KC to 10 MC.

Both analyzers have high selectivity, accuracy of ± 2 db, spurious response at least 50 db down, and a signal-measurement range of 77.5 μv to 97.5 volts. The instruments are supplied in cabinet mountings which are readily adaptable to relay rack mounting.

SPECIFICATIONS — SIERRA VOLTMETERS

Model	Frequency Range—kc	Selectivity		Accuracy		Direct Reading in dbm	
		Down 3db	Down 45db	Frequency	Measuring	Balanced	Unbalanced
101C	20-500	± 550 cps	± 2900 cps	Note A	± 3 db	Note D	600 ohms
103B†	3- 40	± 400 cps	± 3000 cps	± 0.5 kc	± 3 db	Note D	600 ohms
104A	5-150	± 300 cps	± 1500 cps	± 1 kc	± 3 db	Note D	600 ohms
108B	15-500	± 550 cps	± 2900 cps	± 3 kc Note B	± 2 db Note C	135 ohms Note D	600 ohms
114A	100-800	± 550 cps	± 2900 cps	Note A	± 3 db	Note D	600 ohms

All Sierra Carrier Frequency Voltmeters feature built-in calibration oscillators and circuits for level calibration, have aural monitoring jacks, and (except 103B) are furnished with Sierra Model 149A Precision Spiral Scale Dials.

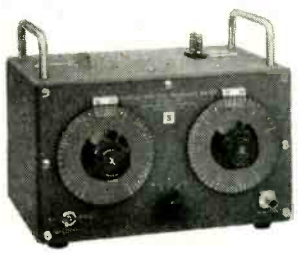
† Contains carrier re-insertion ascillatar for monitoring suppressed carrier systems. Furnished with planetary drive dial. Note A. Ranges from ± 2 KC at low end of dial to ± 3 KC at upper end. Note B. ± 1 KC in the 48 KC to 256 KC region. Note C. ± 1 db for + 30 db to — 40 db attenuator steps on 135 ohm balanced measurements. Note D. All models may be converted for 135 and 600 ohm balanced line measurements by convenient plug-in bridging transformer, Model 130D.

Sierra 101C Carrier Frequency Voltmeter

For carrier system and other field or laboratory work between 3 kc and 800 kc, Sierra offers 5 accurate, stable, tuned vacuum tube voltmeters. All are direct reading in voltage and dbm at 600 ohms from —80 dbm to +42 dbm.

Line Bridging Transformer

Model 130D Dual Impedance Line Bridging Transformer converts VTVM and wave analyzer inputs from single-ended to balanced operation. Covers 3 kc to 500 kc, bridges both 135 and 600 ohm balanced lines.



Impedance Meter, Line Fault Analyzer

Sierra 166 Impedance Meter (at left) measures impedance on high noise circuits, 30 kc to 300 kc; measures on "hot" lines through coupling capacitor.

Sierra 124 Line Fault Analyzer pinpoints shorts, opens or grounds on open wire lines. Direct reading, range ½ to 200 miles, accuracy ¼ mile.

Data subject to change without notice.

sierra

Booths 3905-3907

4084

Sierra Electronic Corporation

A Subsidiary of Philco Corporation

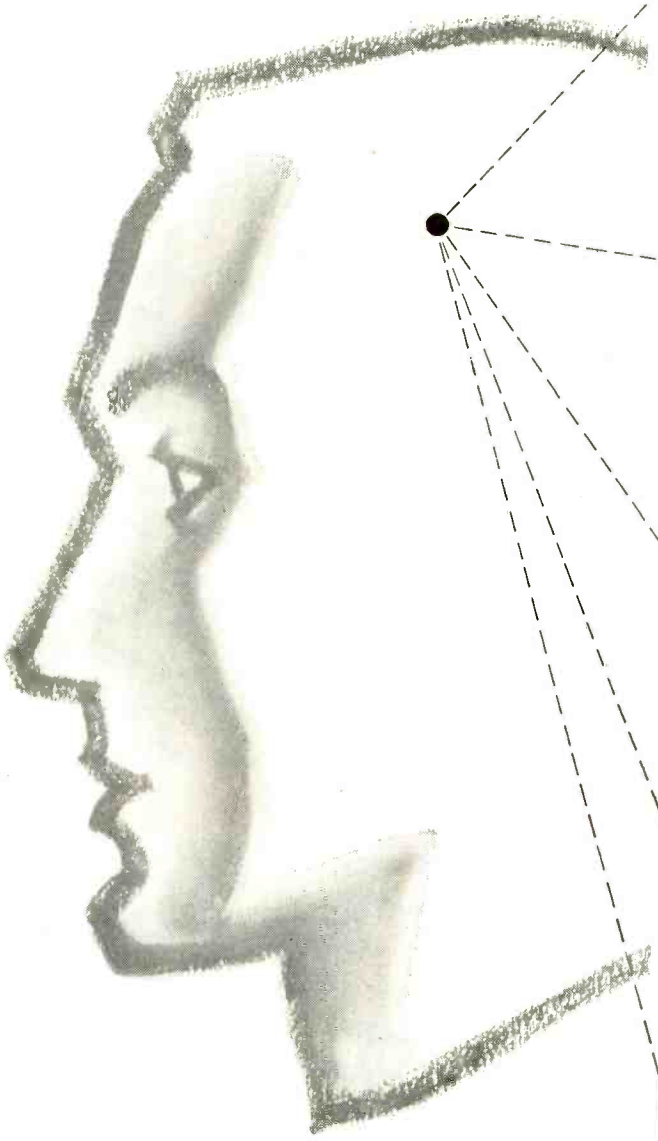
3885 Bohannon Drive DAvenport 6-2060 Menlo Park, California, U.S.A.

Sales Representatives in Major Cities

Canada: Atlas Radio Corporation, Ltd., Toronto, Montreal, Vancouver, Winnipeg

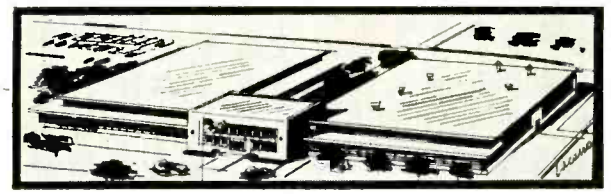
Export: Frazar & Hansen, Ltd., San Francisco, New York, Los Angeles

From the idea . . .



. . . to automated mass production

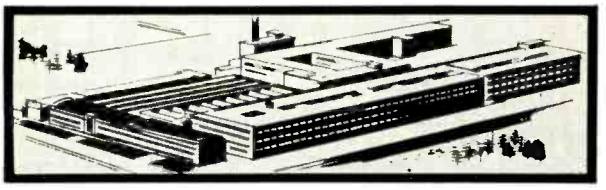
Headquarters for the Division, the Waltham Laboratories, in Waltham, Massachusetts, specialize in advanced systems related to guided missiles, avionics, radar, data processing and electronic warfare.



The Electronic Defense Laboratory, Mountain View, California, is a special development facility devoted to research, technical development and rapid fabrication of ground-based electronic warfare systems.

The Microwave Physics Laboratory, at Mountain View, California, is devoted to the investigation of new magnetic materials and ionized gaseous media for microwave control devices used in radar, communications and electronic countermeasures systems.

The Microwave Tube Laboratory, Mountain View, California, is engaged in developing and producing special tubes such as klystrons, traveling wave tubes, backward wave oscillators, and related devices.



Buffalo Engineering Laboratory and manufacturing facilities for the Division occupy some 170,000 square feet of floor space in this industrial center. The Laboratory specializes in the development of advanced communications techniques and equipments.

The Sylvania ESD family is equipped to carry out your electronics development programs . . . large or small.

Backed by the corporation as a whole, Sylvania's Electronic Systems Division has a long record of successful problem solving in both military and industrial electronics. It has made many important contributions in the fields of avionics, guided missiles, countermeasures, communications, radar, computers and control systems.

Staffed with top-ranking scientists and engineers, backed by extensive research facilities and modern automated mass production capabilities—the Sylvania Electronic Systems Division is a major contributor to our national arsenal for defense. Intensive specialization in the Weapons Systems concept has resulted in utmost organizational efficiency, as well as the highest order of technical and management competence.

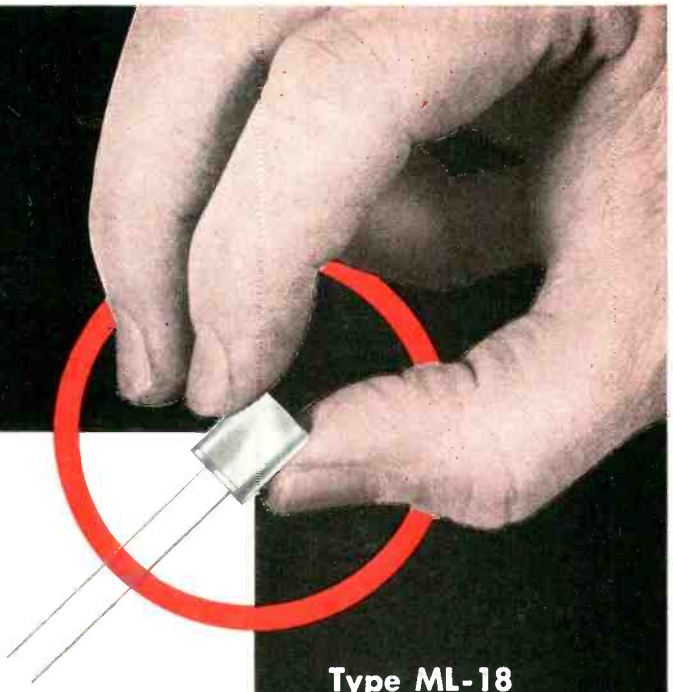
Whether your project requires management or technical experience for complex integrated systems, subsystems, equipments or special components, from initial concept through mass production, Sylvania engineers will be glad to discuss methods of solving your specific problems.

SYLVANIA

SYLVANIA ELECTRIC PRODUCTS INC.
Electronic Systems Division
100 First Avenue, Waltham, Mass.

LIGHTING • RADIO • TELEVISION • ELECTRONICS • ATOMIC ENERGY

bigger things in smaller packages...



Midland

CRYSTALS

pack king-size performance in finger-tip space

"Make it smaller — and make it BETTER!" Miniaturization is a military necessity and an industrial demand for all electronics equipment.

Midland meets it with frequency control crystals of Lilliputian proportions and titanic efficiency. Like their "big brothers" that made Midland first choice in two-way communications the world over, Midland miniatures and sub-miniatures are masterpieces of accuracy, stability and uniformity — everything you want in a crystal — guaranteed by Midland's Critical Quality Control.

Have a special crystal problem? Whether it's in miniaturized or conventional application, our engineering staff is ready to help (including development and production of crystals tailored to your individual requirements.) Get in touch with us.

Type ML-18

Range: 5.0 mc — 150 mc
Wire pin diameter: .017 ± .001
Wire pin length: 1.500 ± .062
Fixed pin diameter: .040 ± .002
Fixed pin length: .234 ± .030

Whatever your crystal need, conventional or highly specialized, when it has to be exactly right, contact...

Midland MANUFACTURING COMPANY, INC.
3155 Fiberglas Road • Kansas City, Kansas
WORLD'S LARGEST PRODUCERS OF QUARTZ CRYSTALS

Solve core problems quickly, economically with

FERRITE COMPONENTS by GENERAL CERAMICS

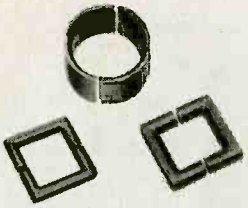
HUNDREDS OF STANDARD PARTS
plus CUSTOM DESIGNING TO SPECIFICATIONS

STANDARD ANTENNA RODS

THREADED TUNING CORES

STANDARD EI CORES

CUP AND TOROID CORES



TELEVISION COMPONENTS

RECORDING HEADS

Computer and Automation Systems Designers!

Ferramic memories provide a new design concept in the area of computers and automation. Magnetic memories combine increased speed, accuracy and reliability with light weight, compact size. Write for bulletins on cores or complete memory planes.

Performance proven magnetic ferrites available for every electronic application

General Ceramics ferrites for television, radio and instrumentation offer designers and engineers a wide range of economical standard components. All are application tested for highest efficiency electrically and mechanically. The fact that leading electronic manufacturers specify Ferramics is due to the program of continuing research and equipment modernization by which General Ceramics keeps pace with the industry's needs as to quality *and costs!* Bulletins are available; write to General Ceramics Corporation, Keasbey, New Jersey, Dept. E.

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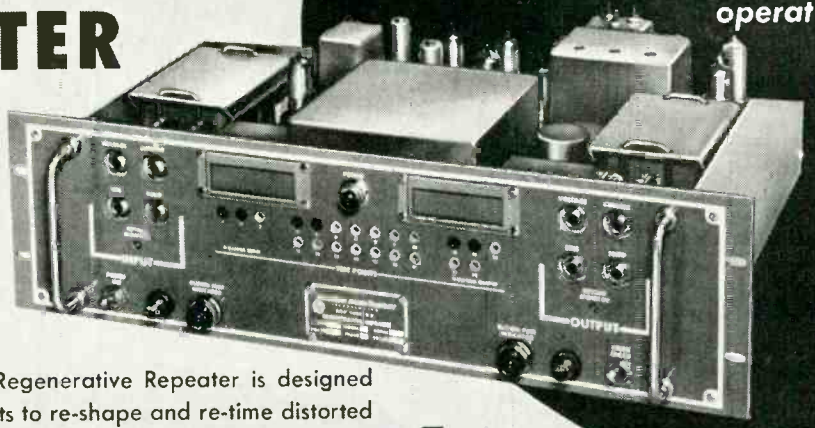
Manufacturers of FERRAMIC CORES, MAGNETIC MEMORY CORES, MEMORY PLANES, MICROWAVE FERRITES, SOLDERSEAL TERMINALS, HIGH TEMPERATURE SEALS, STEATITE, ALUMINA & CHEMICAL STONEWARE

NEW NORTHERN RADIO REGENERATIVE REPEATER

Type 207 Model 1
the most advanced in the industry!

for teleprinter, half duplex and synchronous binary operation



The new Northern Radio Regenerative Repeater is designed for use in telecommunication circuits to re-shape and re-time distorted signals for local use or retransmission. Special provision has also been made for use of this unit on half duplex circuits — where it will not only regenerate the ordinary teleprinter signals but also faithfully reproduce such special signals as "break" signals and "mark restoration" information.

Further provision has been made for use of this Regenerator with synchronous binary signals on either single channel circuits or multi-channel time division multiplex systems. Provision is made to synchronize this unit from an external source.

- **Maximum Acceptable Signal Distortion:** new circuitry accepts up to 47% mark or space distortion.
- **"Floating" Input & Output Circuits:** completely electronic output, no relays.
- **Greater Timing Circuit Stability:** time base derived from highly stabilized L-C oscillator.
- **Switch Selection of Speeds:** 60, 75, 100 words per minute.
- **Adaptable to Any Speed:** low-pass filter & frequency-determining elements are plug-in units.
- **Completely Self-contained:** includes power supply and line battery.
- **OUTSTANDING DUPLEX FEATURES:**
  - — faithfully reproduces "break" signals
  - — transmits "break" signal in case of line failure
  - — protected against "space lock-out"
  - — output can be open-circuited with no excessive rise in line voltage & no harm to the Repeater
  - — 22 front panel test points for equipment function and 8 jacks for input & output line, equipment, current and voltage measurements

Input Keying Signal Requirements:	(1) Neutral keying, positive or negative sense (a) on-off 60 ma pulses (40 ma min) (b) on-off voltage pulses 10-100V into 100K ohms (2) Dry contact keying
Frequency Stability of Time Base Generator:	Less than 1 point range loss for ± 10% line voltage variation or ± 20° C ambient change from 25° C
Sampling Time:	Approximately 50 microseconds
Output:	Electronic tube outputs: (a) neutral 65 ma max. into 2K ohms (b) polar 33 ma (max.) into 2K ohms
Output Distortion:	(a) Signal bias distortion less than 0.5% (b) Signal element random jitter less than 1% (c) Signal history (duty cycle) distortion less than 0.5% (d) Total distortion less than 2%
Power Requirement:	125 watts approx: 110/220V, 50/60 cps
Mounting:	Standard 19" rack mounting, 5¼" panel

Write for free 67-page catalog. See us at Booth 1423, IRE SHOW

Pace-Setters in Quality Communication Equipment

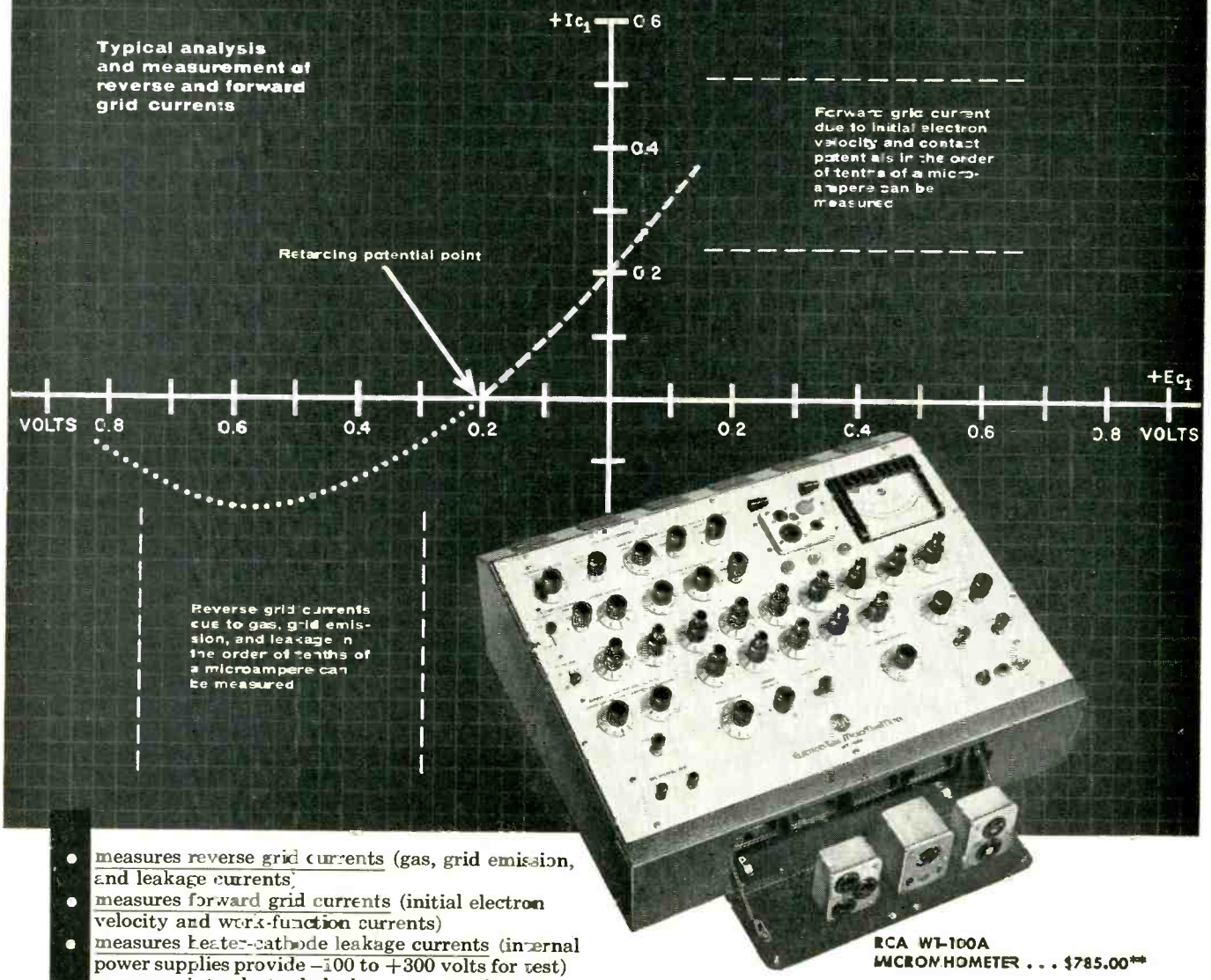
NORTHERN RADIO COMPANY, inc.

147 WEST 22nd ST., NEW YORK 11, NEW YORK

In Canada: Northern Radio Mfg. Co., Ltd., 1950 Bank St., Billings Bridge, Ottawa, Ontario.

Electron-Tube Transconductance (gm) Tester measures Electrode Currents as low as 0.0000001 ampere!

RCA WT-100A MicroMhoMeter enables equipment design engineers to measure electron-tube grid and interelectrode-leakage currents for critical circuit applications



- measures reverse grid currents (gas, grid emission, and leakage currents)
- measures forward grid currents (initial electron velocity and work-function currents)
- measures heater-cathode leakage currents (internal power supplies provide −100 to +300 volts for test)
- measures interelectrode leakage currents between any combination of electrodes (internal power supplies provide −100 to +300 volts for test)

RCA WT-100A MICROMHOMETER . . . $785.00**

** User Price (optional)

RCA WT-100A Electron-Tube MicroMhoMeter is a laboratory-quality instrument which brings a reliable concept of tube-testing technique to users of tubes—on the production line, in the laboratory, and in circuit design. Uniquely designed, compact, and self-contained, the WT-100A offers versatility and accuracy comparable to that of more elaborate and complex laboratory equipment used for measuring transconductance and electrode currents. For detailed brochure, write RCA, Commercial Engineering, Section C19W, Harrison, N. J.

SPECIAL FEATURES OF THIS REMARKABLE INSTRUMENT

• Measures true transconductance with better than ±3% accuracy • Built-in shorts test for any combination of tube elements • Measures transconductance up to 100,000 μmhos—in 6 ranges • Measures transconductance of *low-plate-resistance* types and *high-perveance* types • Measures *control-grid-to-plate, screen-grid-to-plate,* and *suppressor-grid-to-plate* transconductances • Measures heater currents including 600-ma series-string TV types • Built-in calibrating circuit—no null meters or extra devices required • Has easy-to-read meter for all measurements • VoltOhmyst*-type circuit for current measurements—has full-scale, reading of 3 μamps on lowest current range • Electronically protected burn-out-proof meter • Regulated power supplies for all dc voltages • 250-ma dc supply for filaments of battery operated tube types.

*Registered U.S. trademark

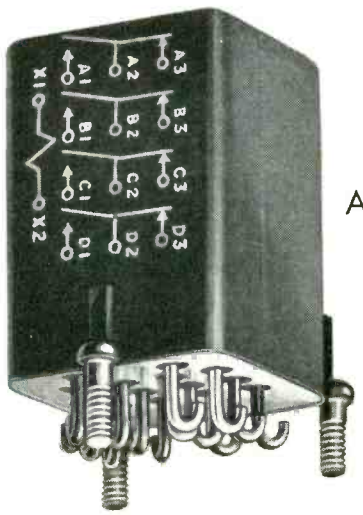
TEST EQUIPMENT

Radio Corporation of America
Components Division, Camden, N.J.

NEW 10 Amp Relay

30g to 2000cps 60 Amp Overload 80 Amp Rupture

Type CH-12D



Actual Size

Here are the facts:

Contact Rating: 10 amperes resistive at 30 volts d-c and 115 volts, 400 cps
Overload—60 amperes
Rupture test—80 amperes

Contact Arrangement: 4 PDT

Coil: 26.5 volts d-c, 170 ohms (other resistances are available)

Temperature: −65°C to +125°C

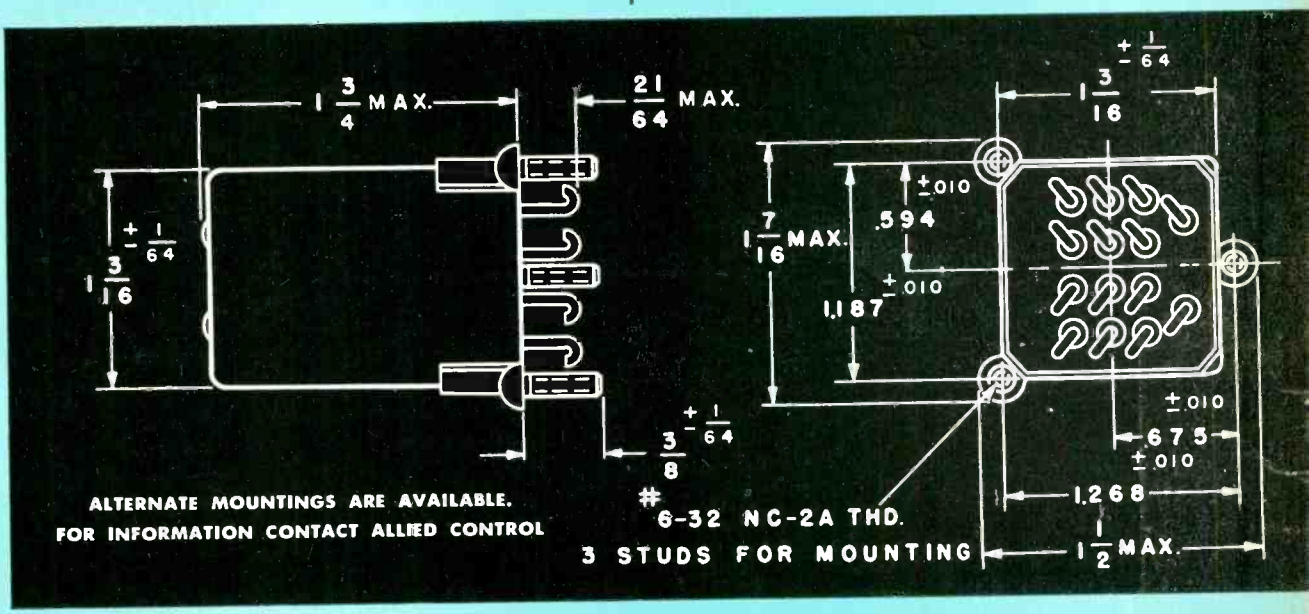
Vibration: 30 g to 2000 cps

Operating Shock: 100 g.

Weight: 5 oz.

Military Specifications:
Meets test conditions of—
Mil-R-5757B • Mil-R-6106A • Mil-R-25018

For more information, write for Bulletin CH



ALLIED CONTROL

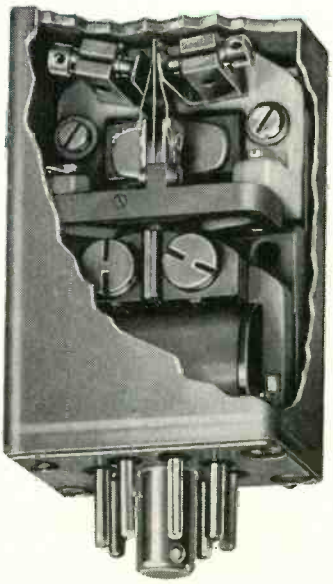
ALLIED CONTROL COMPANY, INC., 2 EAST END AVENUE, NEW YORK 21, N. Y.

ALLIED'S NEW

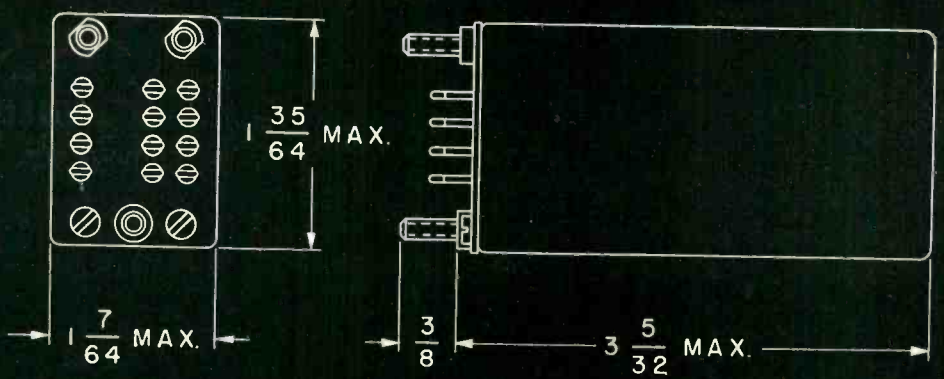
Allied Types
Trls 163-169

Actual Sizes

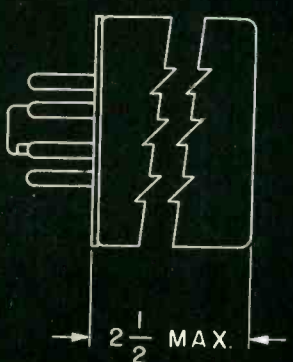
This new polarized relay, designed and manufactured by Siemens & Halske Company of Germany, is now available from Allied Control, and in the near future will be produced by Allied with the technical assistance of Siemens & Halske.



Allied Types
Trls 193-199



Trls 163-169 with SOLDER TERMINALS



Trls 193-199
with OCTAL BASE

AL 172

Sealed POLARIZED RELAYS

Specifications for Allied's Types Trls 163-169 and Trls 193-199

Type Number		Trls 163 Trls 193	Trls 164 Trls 194	Trls 165 Trls 195	Trls 166 Trls 196	Trls 167 Trls 197	Trls 168 Trls 198	Trls 169 Trls 199
Description	Positions	2		3	2	2	3	2
	Operation	Magnetic Latch						
		High Contact Pressure	High Sensitivity	Null Center	Magnetic Latch	Spring Biased	Null Center	Spring Biased
Contact Arrangement		SPDT		SPDT	DPDT	SPDT	DPDT	DPDT
"Operate" Excitation (Std.)	Amp. Turns	7	2	2.2	5.5	5	4	15
"Operate" Power Trls 163-169	μ Watts	500	40	50	300	250	160	2250
"Operate" Power Trls 193-199	μ Watts	610	49	61	375	300	195	2750
"Working" Excitation	Amp. Turns	15	4	6	10	10	10	25
"Release" Excitation	Amp. Turns			2.2		2.4	4	5
Max. Rate of Operation	Oper./Sec.	200	200	200	200	100	200	100

Shock and Vibration: The degree of shock and vibration resistance is related to the type of operation, the adjustment, the coil input power and the application. Contact Allied Control for ratings for your specific application.

Contacts:	Silver, General Purpose 2 amp., 28v d-c resistive load
	Platinum Alloy A. Low-Level Applications up to .5 amp.
	Platinum Alloy B. Heavy Duty Applications above .5 amp.
	Max. Continuous Current 5 amps.

Dielectric Test Voltage	Coil to Frame	500v rms.
	Contact to Contact	350v rms.
	Contact to Frame	500v rms.
	Winding to Winding	150-500v rms.
Standard Coils	Resistances from 1.1 to 18,000 ohms	
	Max. number of windings	3
	Max. Continuous Loading	1 watt
Temperature	Max. Ambient	85°C

ALLIED CONTROL

ALLIED CONTROL COMPANY, INC., 2 EAST END AVENUE, NEW YORK 21, N.Y.

ALLIED CONTROL'S

New

CRADLE RELAYS

These new telephone type relays meet the requirements of modern equipment for a small versatile and economical relay. Designed and manufactured by Siemens & Halske Company, Germany, the cradle relay series are now available from Allied Control. In the near future these relays will be produced by Allied with the technical assistance of Siemens & Halske. • For complete information on these relays write for Bulletin 52.

Specifications

Pull-in Power at 25° C:
.035 watt to .140 watt

Contact Arrangements:
up to 6 make or 6 break or 4 pdt

Contact Rating:
1 or 5 amp, 30v d-c or 115v a-c

Max. Coil Loading:
1.5 watts

Coil Voltages:
From 1v d-c to 140v d-c

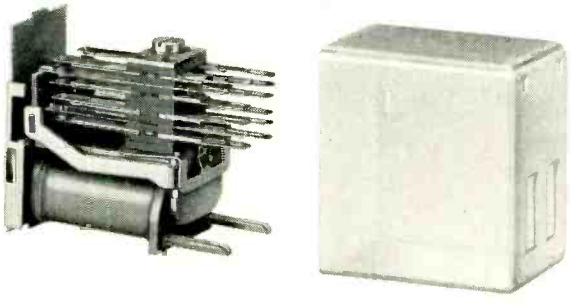
Coil Resistance:
From 1.3 ohms to 15,000 ohms

Speed of Operation:
10 ms max. at 1 watt

Shock: 25 G's

Vibration:
10-55 cps at .062" double amplitude
55-500 cps 8 G's

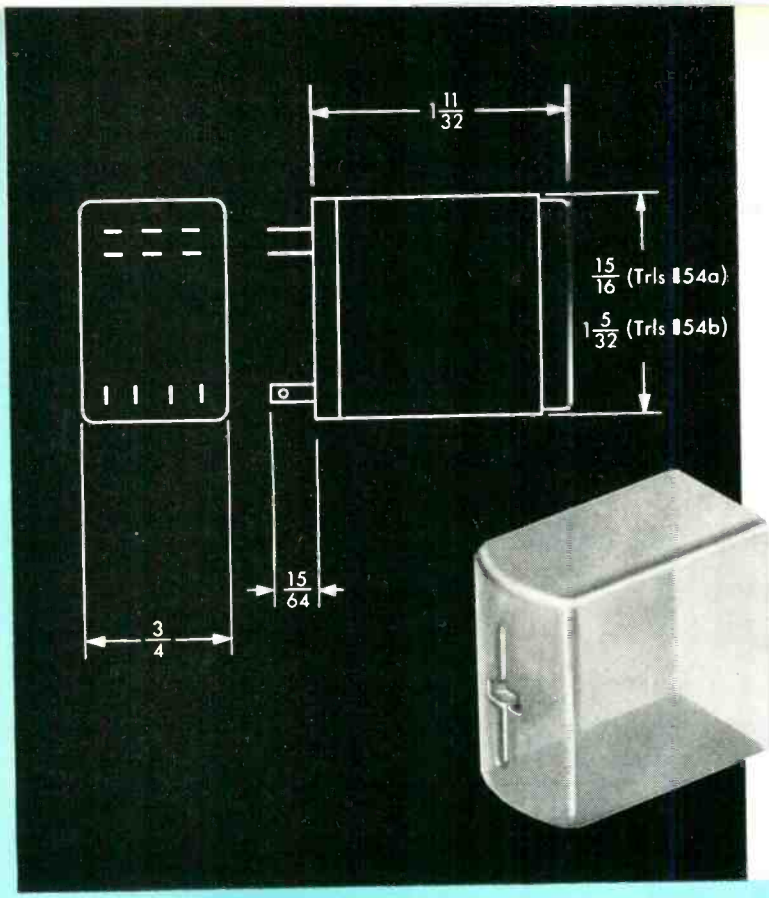
Actual Size



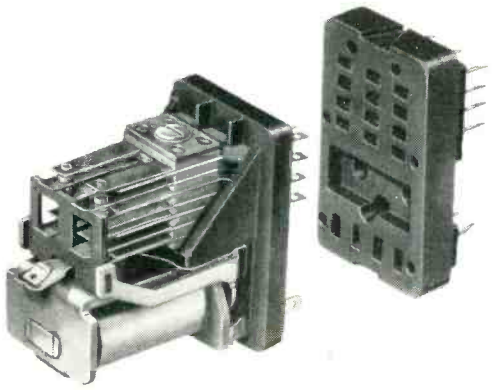
ALLIED TYPE Trls 151
Available in two sizes (x or y) with solder terminals and transparent dust cover.

For Types Trls 151 and 151H low capacitance wire contact pile-ups are also available.

AL174

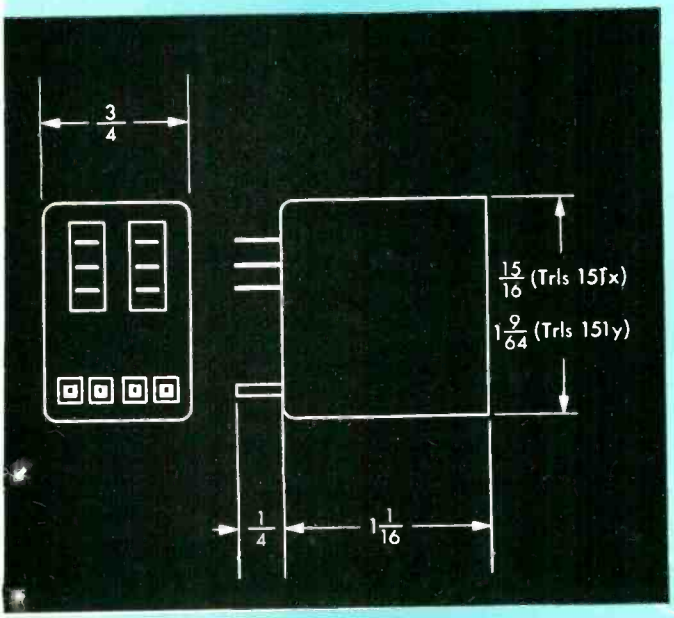


ALLIED
TYPE Trls 154
Available in two sizes (a or b) with plug-in base, transparent dust cover, and special socket.



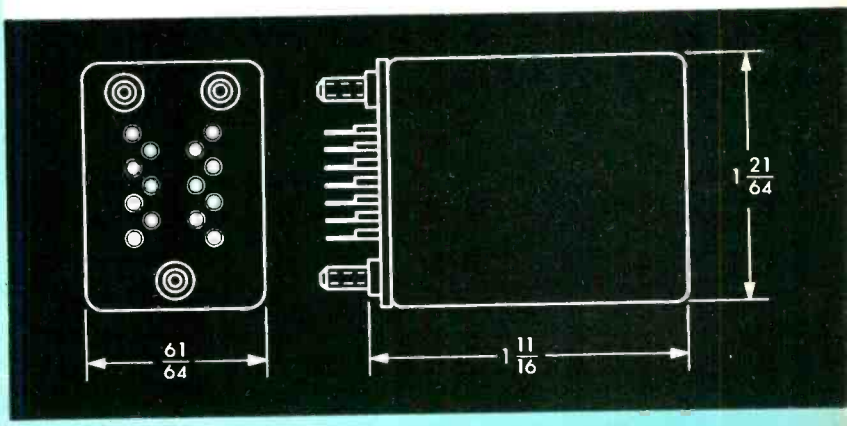
Actual Size

DIMENSIONS SHOWN ARE MAXIMUM



ALLIED
TYPE Trls 151H
This is an hermetically sealed version of Allied's Type 151.

Actual Size



ALLIED CONTROL

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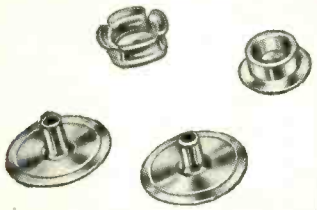
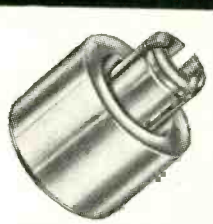


MINIATURE BATTERY CONNECTORS

For use with small "B" batteries; afford quick and positive polarized electrical connections and worthwhile space savings on small electronic equipment.

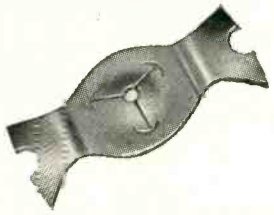


POLYETHYLENE MOUNTING FOOT

No mar no scratch glide for use on TV receivers, record changers and small appliances. Assembles into round hole in either wood or metal cabinets.

FISHTAIL RATCHET PLATE

Made in a wide range of sizes to hold on smooth metal, die-cast or plastic studs. For use on refrigerators, radio cabinets, washing machines and other products to hold medallions, name plates, etc.



VIBRATOR GROUNDING FASTENERS

Holds 1½" dia. beaded or non-beaded vibrator. Vibrator Can grounded to chassis. Holding prongs designed to hold several types of Cans.

RUBBER FOOT

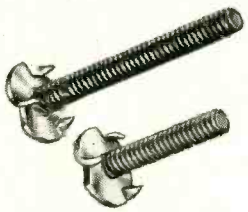
Snap-in Rubber Foot for Record Changers and Phonograph Mountings eliminates threaded member, lock washer and nut thereby speeding assembly time and reducing costs.

NYLON COIL NUT

Designed to snap into a TV tuner and receive a 4-40 or 4-48 coil adjusting screw. No coil form or coil form fastener required.

SPEAKER MOUNTING BOLT

Pronged head prevents bolt from turning in speaker panel during application of nut and lock washer, permits one-side attachment providing production-line savings.



NYLON SNAP-IN NUT

Serves as insulator between "hot TV chassis" and cabinet. Snaps into square chassis hole and secures to cabinet with sheet metal screw.

PLUG BUTTONS

Made to snap into hole sizes ⅛" to 3". Can be embossed with ornamental or functional designs. Removable. Supplied with various finishes, in a variety of shapes and sizes.

QUICKEY FASTENER

Eliminates need for welding or swaging studs to sheet metal stampings, facilitates nesting, eliminates damage in transit because Quickey snaps in just before final assembly.

TRIMOUNT STUDS

Designed to hold two or more thicknesses of material together. Easily installed by hand. Insure vibration proof attachment. Permanent or removable attachment. Wide variety of shapes and sizes.

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Parts illustrated are representative of the thousands of different specialized fasteners and allied devices designed and manufactured in volume by United-Carr and its subsidiaries for leading manufacturers of electronic equipment. United-Carr's wide and varied experience with special fastening problems in the automotive, aviation and appliance fields provides an unequaled background of technical knowledge which may well be applicable to your special needs.

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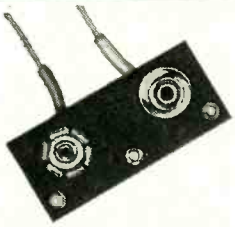
Ucinite Electrical Assemblies



BATTERY CONNECTORS

Wired snap-on units for use with batteries equipped with United-Carr electrical snap fasteners. Wiring to customer's specifications.

BANANA PINS

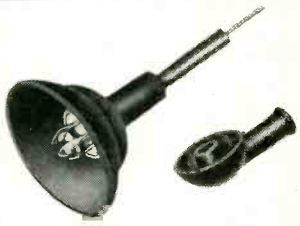
Four sizes of plugs with one-piece beryllium copper springs. Adaptable mounting ends in threaded, staking, or solder lug types. Similar Mating Jacks also available.

SHOCK MOUNTS

Offered in several sizes—brackets and durometer of rubber bushings can be varied. With threaded Teenuts or plain bushings. Insulated versions if needed.

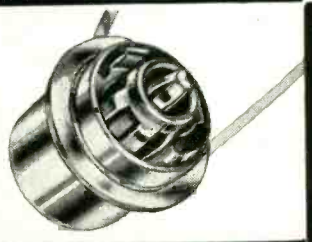
ANODE CONNECTORS

Plug button contacts for positive firm connections. Corona resistant neoprene or silicon shields in straight or right angle types. Wiring to customers specifications.



TUBE CAPS

Positive gripping, heat treated steel springs in corona resistant metal housing. Insulated or non-insulated. Wired to specifications. Type shown has silicon shield for special application.

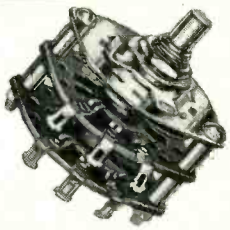


MAGNETRON CONNECTORS

For heater and heater cathode terminals of magnetrons. Available in many variations to answer specific needs.

SWITCHES

Oak type switches manufactured as a licensee. Variety of rotary and push-button assemblies to specifications.



SNAP SWITCHES

Precision, momentary contact push-button switches. Small and dependable. Several circuit arrangements. Water tight version shown.

TEST JACK

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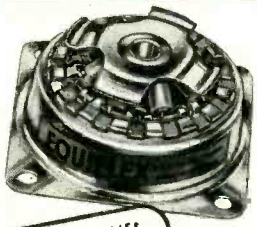

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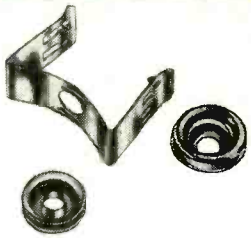

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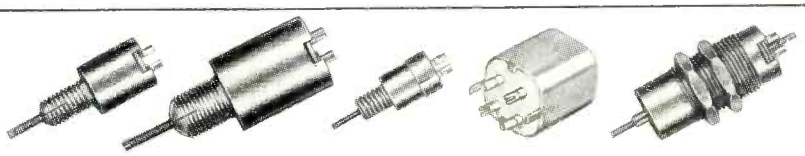
Miniaturized. Highly shock resistant. Mechanically enclosed, completely shielded for maximum reliability.



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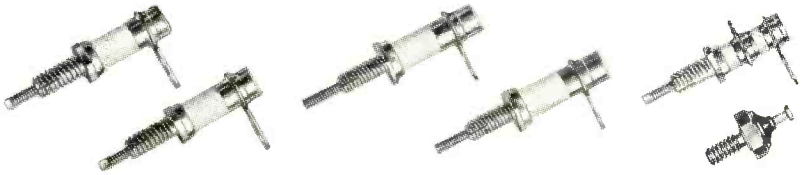
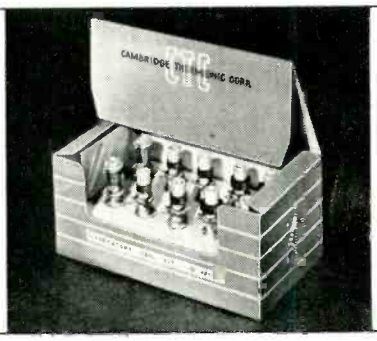
Miniaturized Variable Ceramic Capacitors that outperform much bigger capacitors. (*Extreme right*): Stand-Off Capacitors with ceramic dielectric. Rugged R-F by-pass capacitors for high quality equipment. Shock-, vibration-, humidity-resistant.



CTC QUALITY WOUND COILS IN STANDARD VALUES
Precision wound on slug-tuned ceramic coil forms, with silicone Fibreglas collars and mounting hardware. Available in bulk or in kit form (illustrated).



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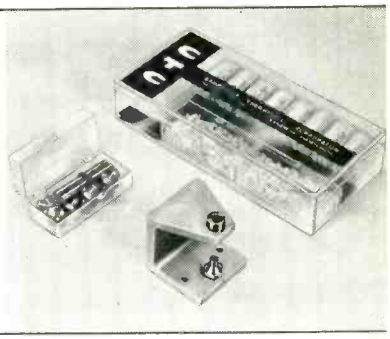
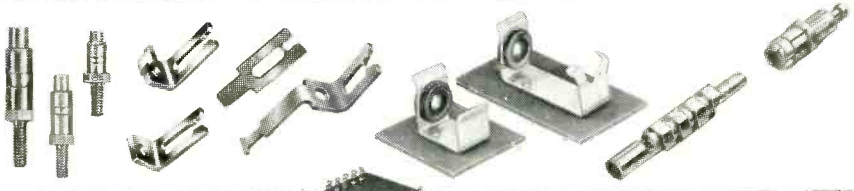
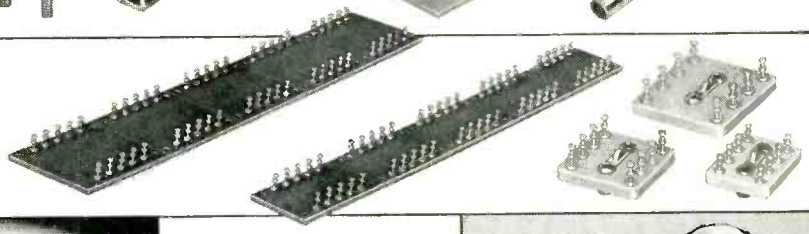
Design your electronic equipment around standard components, using four convenient CTC kits: Coil Form Kit, Coil Kit, Choke Kit, Solder Terminal Kit (illustrated).



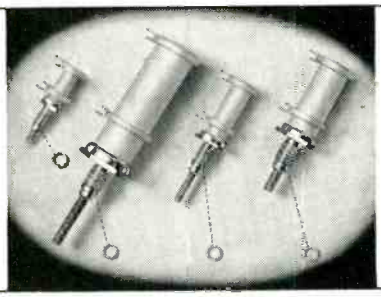
CTC QUALITY DIODE CLIPS
Seven different types, including spring-loaded units primarily for holding fragile diode pigtail leads from .005″ to .085″ in diameter. CTC also offers lines of quality battery clips and miniature plugs and jacks.



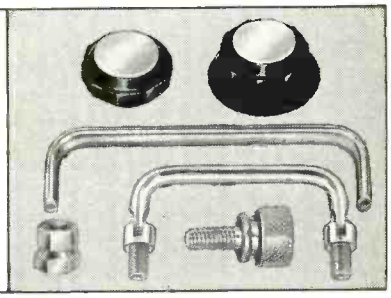
CTC QUALITY TERMINAL BOARDS
Custom-made, standard all-sets, standard ceramics. Variety of materials available — paper, cloth, nylon, glass laminates — phenolic, melamine, epoxy, silicone resins. Moisture — and fungus-proofed.



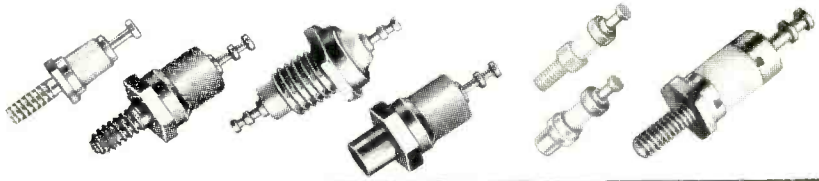
CTC QUALITY PERMA-TORQ COIL FORMS
Constant-tensioning devices for tuning cores of standard CTC ceramic coil forms. Keeps coils tuned as set despite shock, vibration.



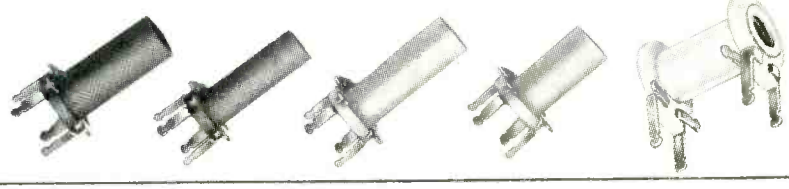
CTC QUALITY KNOBS AND PANEL HARDWARE
Selected materials, carefully processed and finished. Metal parts polished before plating. Hard-wearing surfaces, lasting lusters.



CTC QUALITY INSULATED TERMINALS
Wide variety of stand-off and feed-through models in Teflon and ceramic. Extremely resistant to shock, vibration, moisture and temperature. Solder terminals hold even after prolonged soldering operations.

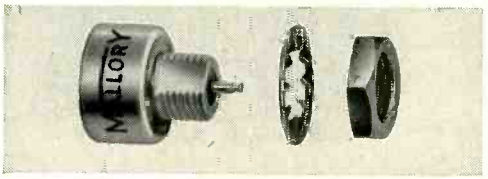


CTC QUALITY PRINTED CIRCUIT COIL FORMS
Phenolic and ceramic types. Can be soldered after mounting. Available as forms alone or wound as specified. Two- to six-terminal models.



for dependable service
under extreme conditions...

Mallory Tantalum Capacitors



MILITARY AND INDUSTRIAL services require component dependability under extreme conditions of temperature and shock. Mallory research and production made possible the Mallory XT line of tantalum capacitors, now thoroughly performance tested and proven for this kind of service.

Mallory XT capacitors were the *first* made to withstand vibration shock to 2000 cps., and temperatures to 175° C. (the highest standard rating). On special order Mallory XT capacitors can be furnished for continuous duty at 200° C.

Mallory tantalum capacitors were *first* to employ a true hermetic seal—metal to glass—without use of rubber or synthetic materials, and are absolutely impervious to immersion. Only Mallory makes available such a broad range of capacity and voltage ratings.

Complete information on Mallory XT capacitors can be had by asking for a copy of the paper—"Typical Expected Performance Characteristics of Extreme Temperature Range Tantalum Capacitors." Data on subminiature capacitors, including the newest tantalum type, can be had by requesting technical bulletins on Mallory types TAP, TAW and TNT.

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electronics

W. W. MacDONALD, Editor

MARCH 1 • 1957

CROSS TALK

▶**WHO'S THE BOSS?** • • • "If the Russians agreed to permit aerial inspection but insisted that it be in full swing within a year we might not be able to put up the necessary equipment. Or, if we could, it might be very inefficient equipment indeed."

So says a prominent manufacturer of aerial reconnaissance apparatus, and thus points up a situation which concerns most manufacturers of electronic equipment and the military as well—the extreme difficulty of getting together on quantity production which meets the needs of both.

The industry says it can't finance, design, buy materials and components and deliver finished equipment complete with maintenance manuals on schedule if the military persists in doling out orders in mere sample quantities, changes the specs every odd Wednesday and then fools around with payment for the merchandise. The military says it can't store huge quantities of gear, has to make changes to keep pace with possible technical advances elsewhere and must safeguard the interests of the taxpayer by carefully checking bills.

Both are probably right; there has to be much give-and-take between industry and government in a democracy at peace. But there is one thing we think can and should be corrected. It should be possible for a manufacturer who already has what he thinks is a firm order to get straight answers when he needs them without having to ring doorbells all the way up to the Secretary of Defense. And we know of many instances where there have been literally dozens of men in between, presumably with authority, who wouldn't say either yes or no. Or, if they did, were later reversed.

▶**PREVIEW** • • • IRE's annual show in New York has always been good but it will be still better this year, if for no other reason than that the new Coliseum is a dream for exhibits.

Saw the boat show there just recently (and parted with a few bucks for a little day-sailer called a "Thistle") and the facilities are just about perfect. The place will take our kind of a crowd with ease.

▶**ASK THE CUSTOMER** • • • Whenever it seems that nothing new can be added to electronic consumer goods that will stimulate demand just ask any intelligent user who will hold still for questions.

We squeezed just one the other day and here's what he said: "How about doing something with portable radios so I don't have to aim the things or their antennas like a gun? Can't someone make a tv set with a station selector that moves without subjecting me to the danger of a sprained wrist? Has anybody thought about combining one of those little transistor radios with a hearing aid?"

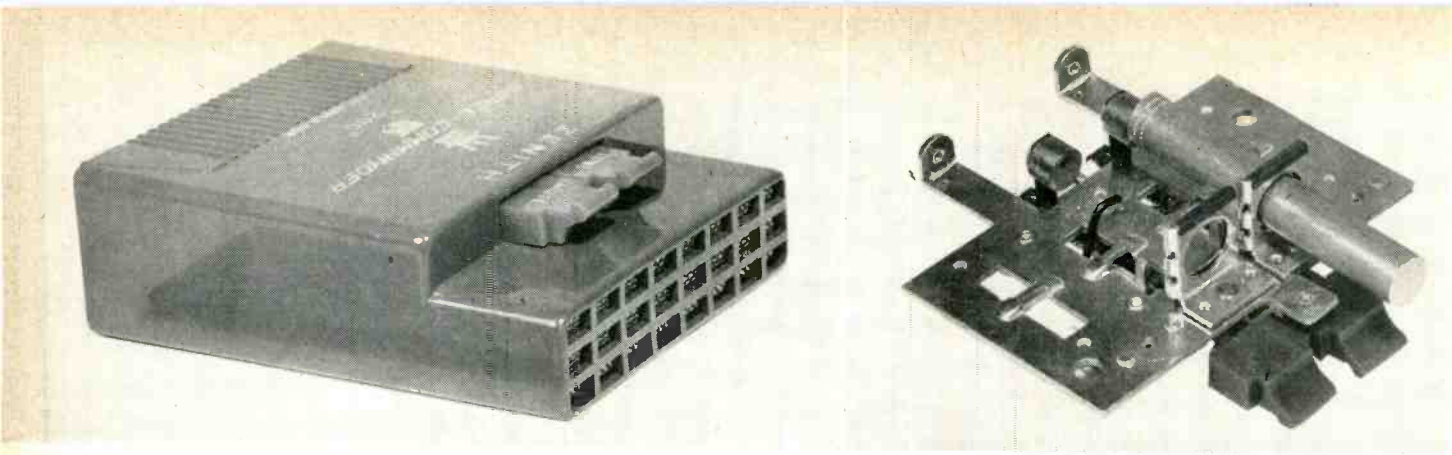
LOOKING AHEAD . . .

Revolution in photo-engraving business is now not far away; more direct methods of converting art into cuts are coming fast

Electronic typesetting is also making progress, but will remain longer in the experimental stage

Photographic reconnaissance is nearing its altitude limit; there are heights above which intervening atmosphere distorts pictures despite excellent lens systems

High-speed light modulator in which refractive index of water column is varied at ultrasonic rate may provide new kind of radar photography



Complete two-channel transmitter, showing grille for ultrasonic output, and mounting details of aluminum rod, steel hammer and bent plastic-covered wire used as damper to terminate vibration of rod when pushbutton is released

ULTRASONIC GONG

By ROBERT ADLER, PETER DESMARES and JOHN SPRACKLEN

Research Department
Zenith Radio Corp.
Chicago, Ill.

THE ACOUSTIC signaling method of operating television receiver controls remotely insures that signals are confined by walls, so that all receivers can be built alike. Multiple control functions are easily accommodated by the use of several frequencies. Most important, acoustic signals can be produced mechanically, eliminating the need for a battery or other power reservoir in the transmitter.

Although an acoustic signaling system could be made to operate with signals in the audible range, it is questionable whether a system using fairly loud audible sounds would be acceptable to the public. The use of acoustic signals in the ultrasonic range avoids these difficulties without sacrificing the advantages of acoustic signaling.

Choice of Frequency

At ultrasonic frequencies, absorption in air produces losses in addition to the inverse-square-law attenuation which exists at all frequencies. Absorption loss varies with temperature and humidity and increases rapidly with frequency. For example, at 80 F and 37-percent relative humidity, absorption loss is 0.2, 0.5 and 0.9 db per foot for 20, 40 and 80 kc respectively. Thus, at 40 kc the absorption loss for a 30-foot distance is 15 db under these conditions. Absorption loss sets an upper limit to the range of useable frequencies.

A cylindrical aluminum rod, vibrating in its fundamental longitudinal mode, is a simple and efficient source of ultrasound in air. If such a rod is struck at one end by a hammer moving along its axis, it emits a long-sustained note of well-defined frequency. For example, a rod 2½ in. long and ⅜ in. in diameter has a fundamental resonant frequency of about 40 kc; its vibration decays as in Fig. 1. The time constant is 0.23 second, corresponding to a Q of about 29,000. The internal damping of aluminum is so small that a large part of the vibrational energy stored in the rod by the impact is radiated.

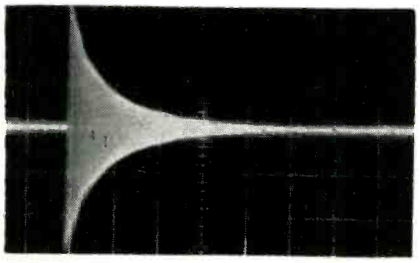


FIG. 1—Undamped output of aluminum gong decays in less than 1 sec. Each division horizontally represents 0.2 sec

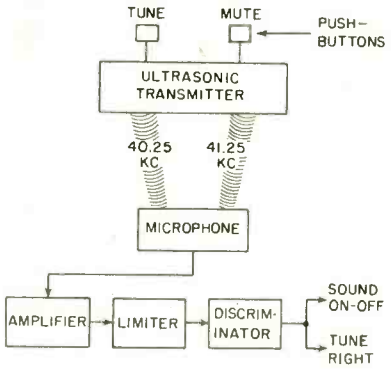


FIG. 2—Two-channel ultrasonic control system. Single tune button steps tuner switch in one direction only, hence button must be pushed 11 times to get next lower vhf channel

Discrimination

With a signal of so sharply defined frequency, it would seem best to build a highly selective receiver and discriminate against undesired signals on the basis of frequency alone. This is not practical, however, because the resonant frequency of an aluminum rod decreases substantially with increasing temperature. At 40 kc this decrease equals 5.5 cps per degree F. Since receiver and transmitter will not always be accurately at the same temperature, compensation is only partly possible and receiver selectivity would have to be reduced considerably.

Special alloys could be used in place of aluminum to provide transmitter frequencies which are not

SUMMARY —— Aluminum rods struck with pushbutton-actuated hammers generate slowly decaying single-frequency signals of four different values in vicinity of 40 kc. Electrostatic microphone in receiver acts with special control circuit to operate relays that turn set on, mute sound or tune in either direction. Frequency tripling, limiting, frequency selection and integration provide discrimination against jingling of keys and other acoustic interference. Simpler two-button version has only tune and mute control channels

CONTROLS TV SETS

affected by temperature, but another factor must be considered—the wide range of amplitudes, of signals as well as interference, to which the receiver will be subjected. Under practical conditions direct line of sight from transmitter to receiver does not always exist. The sound may arrive at the receiver by an indirect path which includes several reflections.

Standing-wave patterns arise which often reduce the received signal. On the other hand, strong ultrasonic interference is generated by any impact between small pieces of metal; jingling coins, rattling keys or opening a cigarette lighter produces surprising amplitudes in the ultrasonic range and this interference may be generated close to the receiver.

Receiving System

Figure 2 shows a receiving system which is well adapted to the interference situation in homes. The receiver consists of a microphone, a high-gain amplifier, a limiter and a discriminator. The discriminator circuit is so constructed that positive and negative voltages of equal magnitude appear simultaneously on two separate output terminals. The control circuits are connected to these output terminals through integrating networks. Figure 3 shows the voltages at the two discriminator outputs as a function of input frequency.

This receiver is similar to a conventional f-m receiver, capable of accommodating a wide range of input levels. The voltages plotted in Fig. 3 are quite independent of the input level as long as it exceeds the minimum required to saturate the limiter.

Two transmitter frequencies cooperate with the single discriminator. Each frequency corresponds to one of the two output voltage peaks. It is thus impossible for any interfering signal to generate a larger discriminator output than that which is produced by the transmitter, no matter how strong the interfering signal may be at the microphone. The control circuits are arranged to operate only if the discriminator output voltage exceeds a predetermined threshold, indicated in Fig. 3, for a certain minimum period of time; this period is defined by the time constant of the integrating network. To be mistaken for the desired signal, an interfering signal must have a frequency within the narrow band over which the discriminator curve exceeds the threshold (about ± 250 cps out of 40 kc), must last long enough to be accepted by the integrating network and must not be accompanied by other frequencies which would fall near the second

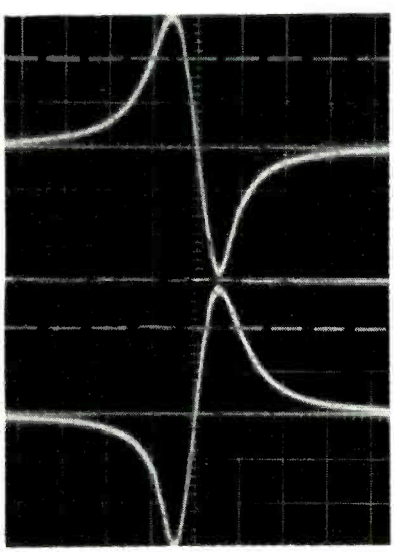


FIG. 3—Discriminator output voltages for two-channel system. Center frequency is 40.75 kc. Horizontal scale is 800 cps per division. Dashed lines indicate relay operating thresholds for sound on-off (upper curve, for 40.25-kc channel) and for tuning motor (lower curve, for 41.25-kc channel)

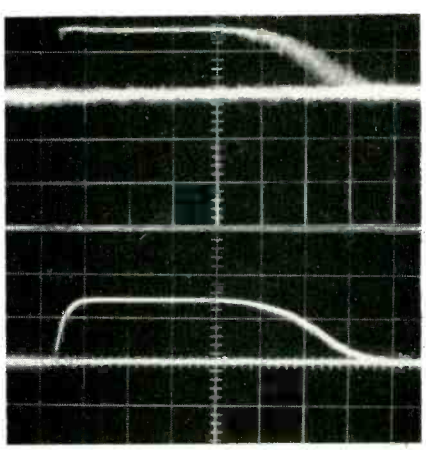


FIG. 4—Output voltage at one discriminator terminal before (above) and after integration. Horizontal scale is 800 cps per division from 40.75-kc center scale

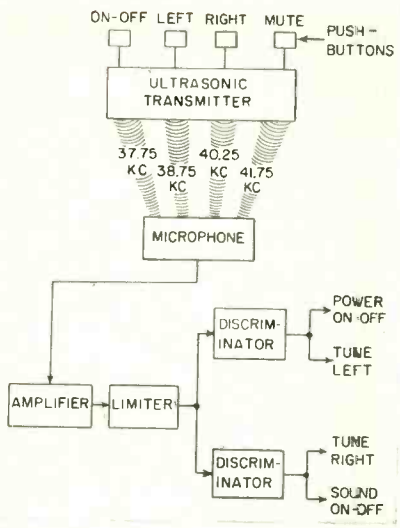


FIG. 5—Four-channel control system. Two tuning buttons permit going direct to desired new station

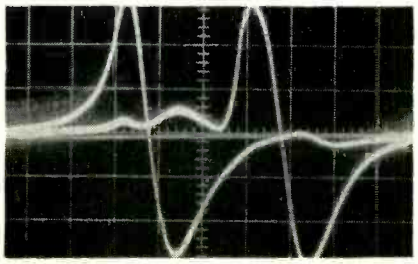


FIG. 6—Discriminator output voltages for four-channel system, where both discriminators operate from common limiter. Crossover for first curve is at 38.25 kc; second curve drops to zero at 40.75 kc

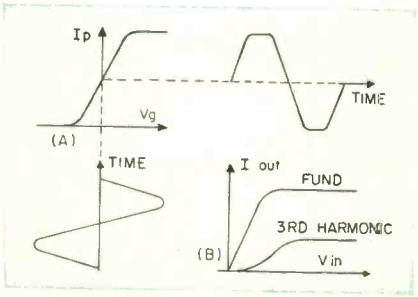


FIG. 7—Limiting and frequency-tripling actions of two-channel receiver

discriminator peak. This last-mentioned property makes the receiver insensitive to hiss and other broad-spectrum noises.

Integrating Action

Figure 4 illustrates the output voltage at one of the discriminator terminals, before and after integration, when a desired signal is received. The unintegrated output rises abruptly to the full level allowed by the limiter, remains at that level until the input signal begins to drop below limiting and then gradually returns to the zero level. Random noise and acoustic noise combine to produce a fluctuating zero line. The integrating network cleans up the fluctuations and changes the abrupt step at the beginning to a gradual rise. These curves were photographed with the transmitter only a few feet from the receiver; limiting under these conditions lasts longer than one second. When the transmitter is moved farther and farther away, the curves of Fig. 4 do not go down in amplitude but merely last for shorter periods until, at the extreme distance, the integrating network prevents the lower curve from reaching the threshold and the control circuits cease to operate.

Interference, such as that produced by jangling keys, consists of closely spaced pulses of many different frequencies. In the presence of such interference, unintegrated discriminator output varies rapidly with time, showing a jagged curve which may include peaks of both polarities reaching or approaching the maximum level.

After integration, however, very little output signal is left because no single frequency is maintained long enough.

Four-Function System

In some television receivers, more than two remote control functions are needed. Figure 5 shows how four functions are provided by a remote-control receiver which has two separate discriminators; the microphone, amplifier and limiter are common to both. It is quite practical to operate two discriminator circuits from a single limiter tube by connecting their primary tuned circuits in series. The voltages developed in these circuits represent a substantial part of the available anode voltage, but the two discriminators never operate simultaneously, so that voltage overload effects are not a problem.

Undesired coupling between the two primary tuned circuits is introduced by the output capacitance of the limiter tube, but this can be neutralized by taking advantage of a small controlled amount of inductive coupling between the two coils in the two tuned circuits.

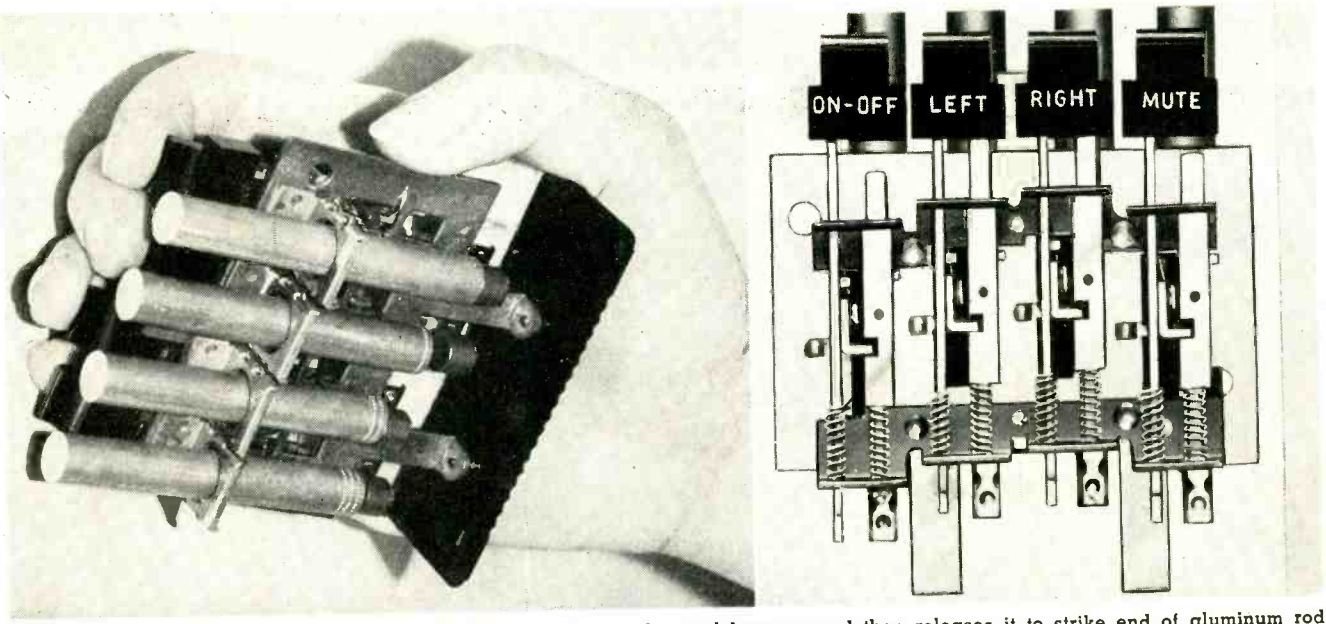
Figure 6 shows the output voltages observed on the two discriminators. A disturbance appears in the response curve of each discriminator in the vicinity of the center frequency of the other discriminator, but the disturbances are far below the threshold and therefore of no significance.

The control circuits employ relays which are operated by the plate current of triodes. A large negative bias is applied to the grid of these triodes to define the threshold which the discriminator output voltage must exceed. To render the control circuits fairly independent of the triode characteristics, bias voltages of the order of 20 volts and discriminator peak outputs of about 30 volts are used. To obtain output of both polarities, a center tap on each discriminator load resistor is returned to the source of bias voltage, so that a total discriminator output of about 60 volts is required. To insure operation even under highly unfavorable circumstances, limiting should occur with input signals of no more than 10 μv, considering the sensitivity of the microphone employed. A voltage gain of about 10^7 or 140 db is thus required.

To obtain a gain of 140 db at a single frequency would require rather expensive shielding and decoupling. This is avoided by using the limiter simultaneously as a frequency tripler. Figure 7A illustrates how this is done; the limiter tube (6BN6 or equivalent) has a transfer characteristic which resembles a step function. A sufficiently large input signal produces an anode current of substantially square waveform.

Frequency Tripling

In Fig. 7B, the amplitudes of the fundamental and of the third harmonic components of the anode current are plotted against input signal amplitude. To limit on the third harmonic requires a larger input signal and the limited output current is only one-third as large as the fundamental component, but even with these disadvantages tripling in the limiter remains quite practical. The simple receiver shown in Fig. 2, which employs only



Opposite sides of four-channel transmitter. Pushing a button cocks steel hammer and then releases it to strike end of aluminum rod and produce ultrasound used for actuating microphone mounted above picture tube in receiver

one discriminator, uses this circuit.

In the more complex receiver illustrated in Fig. 5 it is desirable to keep the output impedance of the limiter tube as high as possible to avoid interaction between the two discriminators. Also, limiter anode current should be kept low to obtain close control over the discriminator output levels. This is more easily accomplished with a limiter in which the input and output frequencies are the same. For this reason, a separate triode tripler stage precedes the limiter in this receiver.

Frequency tripling not only reduces shielding requirements but also decreases the cost of the discriminator circuits. To obtain the output characteristics illustrated in Fig. 3 and 6, the tuned circuits in these discriminators must have Q's of about 80 and must be stable with respect to temperature and aging. To accomplish this at 120 kc is much less expensive than to reach equal performance at 40 kc.

Complete Control Circuit

Figure 8 shows the circuit of a receiver for four control functions. A tuned circuit in the second pentode plate insures good waveform at the input grid of the tripler triode. This operates with grid-leak bias at low anode voltage and produces about 1.5 v third harmonic output with 1.5 v of fundamental input. The following 6BN6 operates only as a limiter with relatively low anode current, feeding the two discriminators. The 6CM7 relay control tube for each discriminator contains two dissimilar triode sections; the larger section operates the sound-on-off relay, which requires more driving power than the

FIG. 8—Four-channel receiver circuit. Separate 25Z6 full-wave rectifier (not shown) provides power here, but two-channel version obtains power directly from television receiver in which it is used

Photograph of solar flare taken at Sacramento Peak Observatory, Sunspot, New Mexico. The solar flare ionizes the atmosphere, resulting in changes that are detected by two radio receivers

By ROBERT H. LEE
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SOLAR-FLARE

SUMMARY —— Two radio receivers, operating at 27 kc and 18 mc, intercept signal disturbances occuring in the D-layer of the ionosphere during a solar flare. The detection system indicates an increased signal caused by sudden lightning bursts and an attenuated signal caused by cosmic-noise absorption. Pulse analyzers discriminate against background noise, interfering radio stations and unwanted atmospheric disturbances. Signals are chart recorded on a time-sharing basis

WHEN a solar flare occurs, there is often a rapid increase in the radiation that ionizes our atmosphere, to form the ionosphere. This radiation is probably Lyman alpha (1,216 Angstroms), or some shorter wavelength. The effect is most commonly known as a sudden ionospheric disturbance or a sudden short-wave fadeout. A severe disturbance can cause a complete blackout of short-wave long-distance communication. This fading is caused by increased absorption of the radio waves as they pass through the D-region of the ionosphere at a height of about 80 kilometers.

Two distinct types of radio signals are used to detect and study these solar-flare effects. The system is shown in Fig. 1.

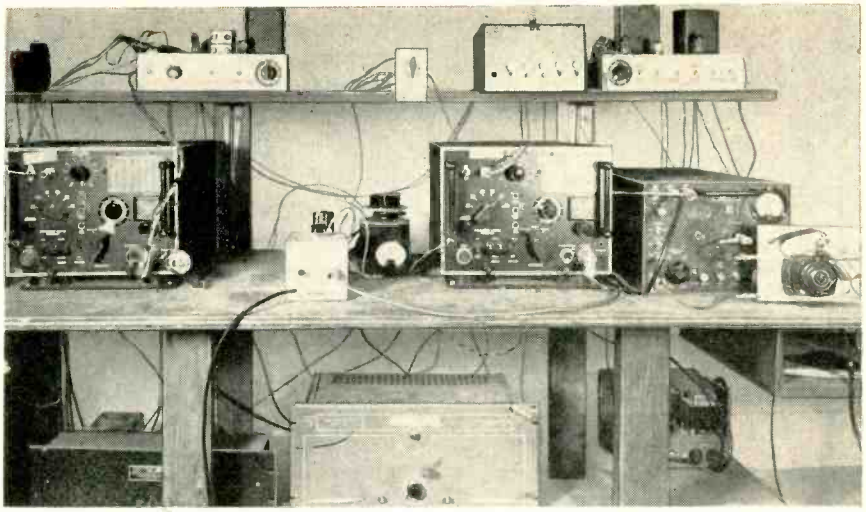
The first receiver, operating near 27 kc, detects any important sudden enhancement of atmospherics and records the frequency and intensity of lightning bursts from various parts of the world. When a solar flare occurs, the reflecting ability of the D-region of the ionosphere on the sunlit side of the earth is improved suddenly and there is an increase in the strength of the received signals. The decay in signal strength is much slower, indicating the recovery of normal ionization in the D-region.

The second method of detection records galactic or cosmic radio noise coming to us from space. This noise, in coming through the ionosphere, is partially absorbed. When a solar flare occurs, absorption is suddenly increased. This is called a sudden cosmic-noise absorption. The region around 18 mc is a reasonable compromise frequency for this measurement.

If a considerably higher frequency is used, the absorption becomes smaller and is difficult to measure. If a lower frequency is used, the interference from radio stations and atmospherics becomes more severe.

Noise-free locations are difficult to obtain and man, and considerable effort was spent in designing equipment that would discriminate against unwanted pulse signals.

Antenna array for solar-flare detection uses two parallel half-wave folded dipoles, spaced one half-wave apart and driven in phase



Solar flare detection equipment includes from left to right, a 27-kc receiver, noise calibrator, 18-mc receiver (second i-f), ARR-7 receiver (r-f and first i-f) and motor-driven radio frequency scanner. The two signal-interference rejectors are on top shelf, on both sides of timer. Chart recorder is not shown

DETECTION FOR IGY

The 27-kc receiver signal is caused by individual bursts of atmospheric noise due to thunderstorms. If the thunderstorm is sufficiently distant from the receiver that reception takes place by multiple reflections from the D-layer, the signal strength is increased at the time of a solar-flare. Also there is an extension of the area over which signals are received.[1]

At 27 kc, serious interference is created by power-leaks, brush-type electric motors and other electrical appliances. For this reason the receiver uses a shielded-loop antenna to null out main powerline noise. This receiver, the Navy model DZ-2, was designed as a direction finder and is available complete with loop antenna.

An infinite-impedance detector was added to the receiver with the front end modified to permit the loop antenna to be used remotely.

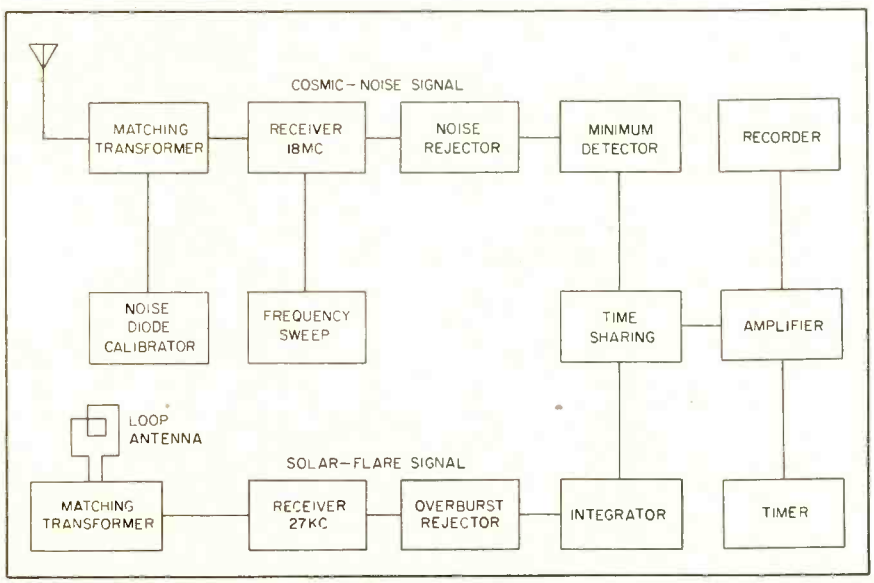


FIG. 1—Block diagram of solar flare and cosmic-noise detector

Background Noise

In spite of the use of the loop antenna, there is still an appreciable amount of noise received. If an ordinary averaging circuit were used, the atmospherics would be lost in the low-level background.

Fortunately the atmospherics, though infrequent, are greater in amplitude than most of the peaks of the background hash after nulling the main source of powerline noise. This permits use of a base clipper to prevent the low-level signals from reaching the signal-integrating device. This clipper can be the same diode that permits the charge and discharge time constants of the integrating circuit to be different.

Noise Discrimination

An atmospheric burst encounters the circuit shown in Fig. 2. The burst from the infinite-impedance detector in the receiver appears as

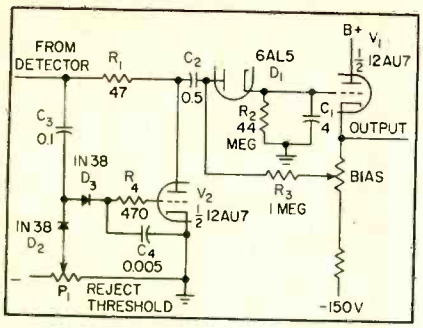


FIG. 2—Integrator and noice-rejection circuits in the 27-kc receiver

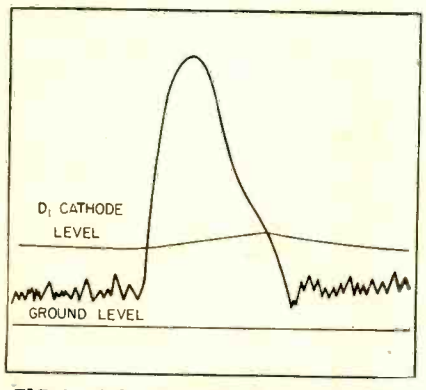


FIG 3.—Solar flare signal from the 27-kc receiver

a positive pulse as shown in Fig. 3. When the amplitude becomes great enough, D_1 conducts and the pulse charges C_1 through capacitor C_2 and limiting resistor R_1. As the amplitude of the burst drops, D_1 opens and C_2 is charged through R_3 to a new level so that the diode bias is restored. Also the charge lost by C_2 during the charging of C_1 is restored. The system is now ready for the next burst to be received at some undetermined later time.

The voltage on capacitor C_1 reaches equilibrium at a value given by average of pulses above clip level $\times$ R_2/R_1, assuming that C_2 can reach equilibrium between pulses.

Amplitude Selection

In addition to clipping out some of the base-level noise, it may be desirable to reject local thunderstorm bursts. This can be done by amplitude selection and is accomplished by V_2 in Fig. 2. In this application V_2 is biased beyond cutoff by the d-c restoring circuit C_3, D_2, P_1.

If a positive burst of sufficient amplitude occurs, V_2 conducts, causing the burst to appear as a drop across R_1. The voltage waveform presented to the integrator then appears as in Fig. 4A.

The C_1 charging current waveform will be the same as that portion of the voltage waveform above the D_1 cathode level. Thus the system rejects bursts above the amplitude selected at P_1, except for that part of the leading and trailing edges which are below the rejection level.

The trailing edge of an atmospheric burst has somewhat less slope than the leading edge, so most of the charge accumulated from a rejected burst comés from the trailing edge. The trailing edge can be eliminated by D_3 and C_4. When a large burst comes from the receiver, C_4 is charged through D_3 to nearly the peak value of the burst. Then, as the burst drops off, D_3 opens, leaving C_4 to discharge through R_4 and the back-resistance of D_3. By choosing capacitor C_4 properly, the voltage waveform presented to the integrator will be as shown in Fig. 4B. Only a small spike represented by the part of the curve above D_1 cathode level shows up as capacitor charge.

There will be smaller bursts present in a local thunderstorm against which the system cannot discriminate. Therefore, the best that can be hoped for is that there will be some discrimination against storms not in the immediate area, but too close to be received by D-layer reflection.

Cosmic-Noise Signal

The signal for the 18-mc receiver is galactic or cosmic radio noise generated in the galaxy. In coming through the ionosphere the noise is attenuated, depending on the ionization present. When a solar flare occurs, the attenuation is increased.[2]

At approximately 18 mc, automobile ignition, power line noise and radio stations are the chief sources of interference. One cannot discriminate against background since this is what is to be measured.

Cosmic Signal Level

The rejection technique for ignition and power line noise is similar to that used with the 27-kc receiver to reject local thunderstorm bursts. However, the rejected noise burst must be reduced only to the average level. If it is reduced too far, it will cause a decrease in the recorded signal level and would be worse than no rejection at all, since we are looking for decreases. Reduction is accomplished by returning the cathode of the noise-rejection triode to a point which varies as the average noise level, rather than to ground as in the 27-kc rejector.

Radio Interference

The rejection circuitry just described, satisfactorily removes impulse-type interference from the receiver output. However, there remains the problem of interfering radio stations.

To overcome this interference, the tuning dial of the receiver is mechanically driven so that it sweeps back-and-forth over a range of about 30 kc. Radio station interference can be eliminated by the circuit shown in Fig. 5.

Capacitor C_4 is charged slowly in a positive direction through R_5. When the potential reaches the volt-

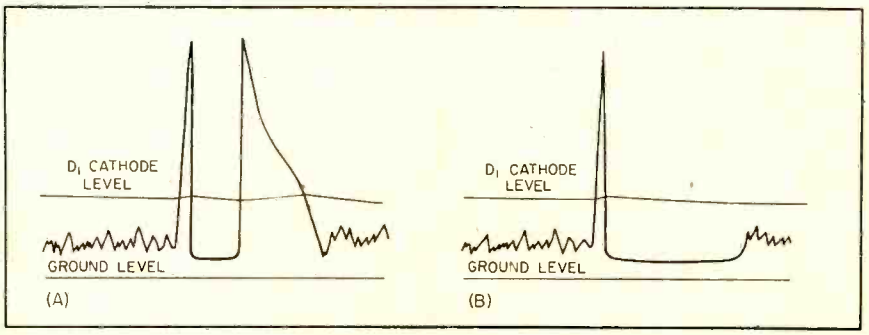


FIG. 4—Output of basic amplitude selector for rejected burst (A) and after pulse elimination (B)

age level of the cathode of V_2, D_4 conducts and prevents the capacitor from charging further. If an interfering signal causes the cathode of V_2 to go positive, D_3 opens and C_4 starts to charge slowly.

As soon as the interference is gone, D_3 conducts and rapidly discharges C_4 down to a level determined by the background noise as averaged in R_8, C_8. If the charge rate of C_4 is slower than the sweep rate on the tuning dial, the recording will be nearly a straight line representing the base noise level, ignoring the interfering radio stations.

The receiver used in the experimental system is an ARR-7 working into a DZ-2 receiver, making it a double conversion superhet with i-f of 456 and 88 kc. The first r-f stage of the ARR-7 was changed from a 6SK7 to a 6AC7 to improve the noise figure.

Antenna

The antenna array consists of two horizontal, parallel half-wave folded dipoles, spaced one half-wave apart and driven in phase. The dipoles are placed one-tenth wavelength above a ground screen.

The vertical gain of the antenna is useful primarily as a means of discriminating against interfering signals arriving at low angles above the horizon.

Chart Recorder

The present method of recording uses a pen recorder utilizing a time sharing system to record the output of both receivers on the same chart. A chart recording of a solar-flare is shown in Figure 6. The 18-mc receiver output has its zero point toward the bottom of the chart. Increasing signal level moves the pen upward. The 27-kc record has its zero at about the center of the chart. Increasing signal level causes the pen to move upward. At the time of a flare, the sudden cosmic noise absorption recording line deviates toward the lower part of the chart and the sudden enhancement of atmospherics record moves toward the top.

Interference on the 27-kc record goes in the same direction as the flare-signal record. For the 18-mc record the interference goes in the opposite direction from the cosmic-noise signal.

Sudden short-wave fadeouts may be recorded by connecting an RC averaging circuit, time constant of 3 or 4 minutes, to the cathode of V_2 in Fig. 5. This averaging circuit is then isolated by a cathode follower.

Three of the finished units will be in operation during the International Geophysical Year 1957-58, at the High Altitude Observatory, Boulder, Colo., at Sacramento Peak Observatory, Sunspot, New Mexico and at McMath-Hulbert Observatory at Lake Angelus, Mich.

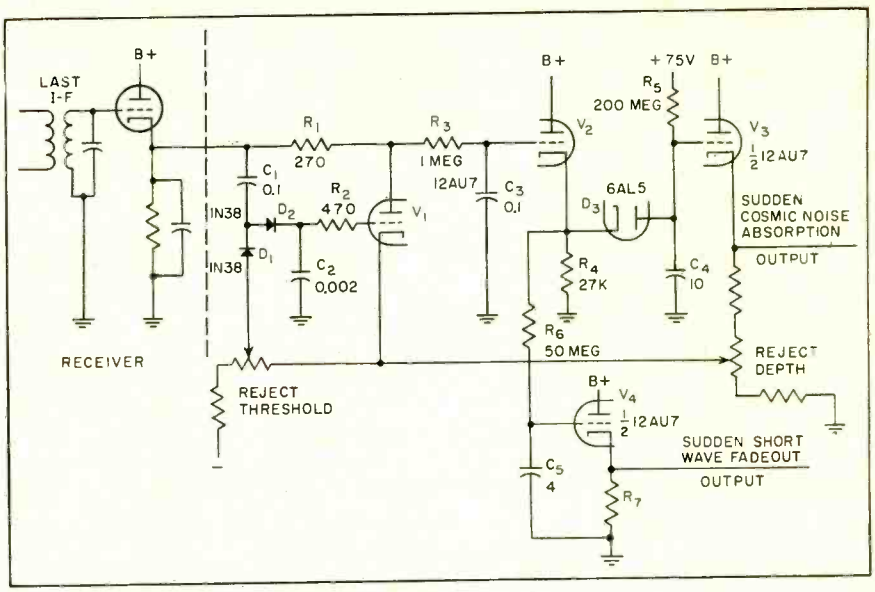


FIG. 5—Radio-interference rejector for the 18-mc receiver

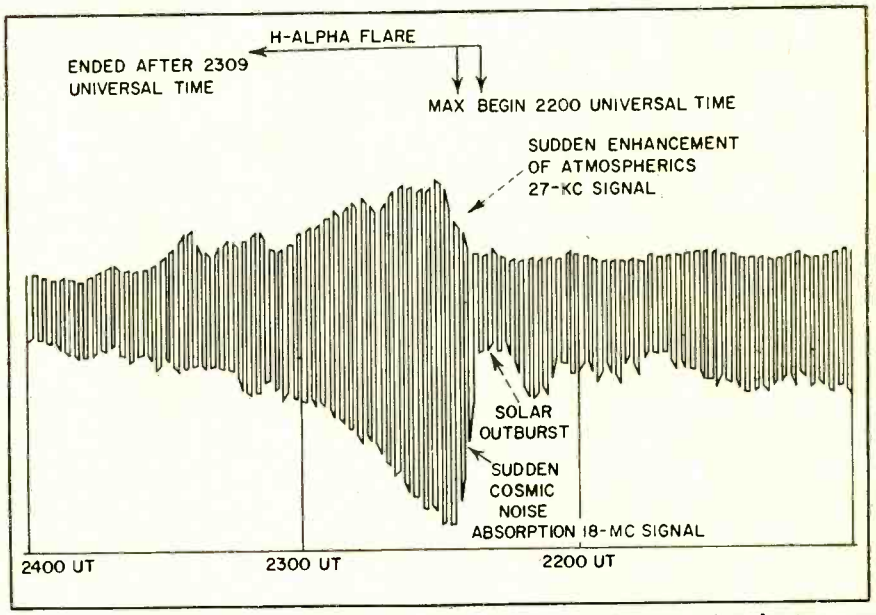


FIG. 6—Chart recording of solar flare shown in photograph. The two signed traces are recorded in universal time

The work described here was supported by the National Committee for the International Geophysical Year 1957-58, through a National Science Foundation grant. The author wishes also to express appreciation to William Wright of High Altitude Observatory for his assistance in construction and testing of this equipment.

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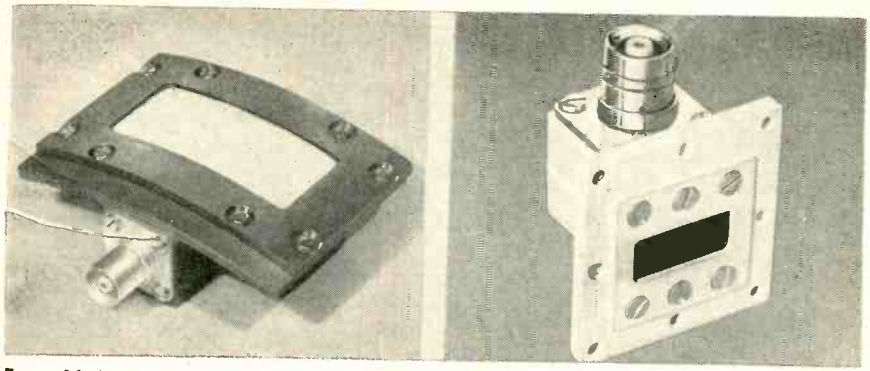
(1) M. A. Ellison, The H-alpha Radiation from Solar Flares in Relation to Sudden Enhancements of Atmospherics on Frequencies Near 27 kc. *J. of Atmospheric & Terrestrial Phys.*, 4, p 226, 1953.

(2) C. A. Shain and A. P. Mitra, Effects of Solar Flares on the Absorption of 18.3-mc Cosmic Noise. *J. of Atmospheric & Terrestrial Phys.*, 5, p 316, 1954.



Assembled missile beacon antenna elements for S-band (left) and X-band (right) frequencies. Similar slot elements with different curvatures and matching sections accommodate different missile diameters

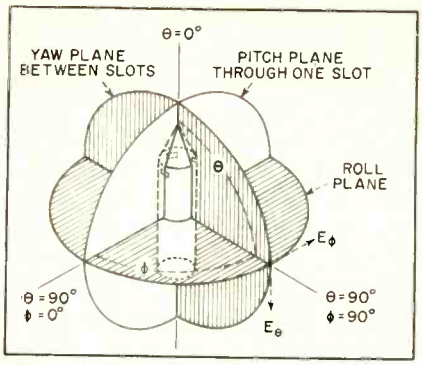


FIG. 1—Radiation pattern coordinate system for missiles. Antenna array of three elements gives best pattern coverage

BEACON ANTENNAS

IMPEDANCE matching and radiation patterns of a single-slot antenna were made on a large, flat ground plane and on a 15-inch diameter, 3-foot long cylinder. Configuration selected for the S-band system was a T-fed slot whose overall mounting depth was less than 1½-inches.[1] The exciting element consisted of a 0.165-inch diameter stub which is a continuation of the center conductor of the feed section into the cavity.

The X-band antenna is similar to the S-band antenna except that the shunt bar is eliminated leaving a stub-excited slot element. The feed stub was machined from coin silver rod and press fitted to a UG-568/U receptacle.

Radiation Patterns

A radiation pattern coordinate system for missiles is shown in Fig. 1. Calculations and measurements of radiation pattern substantiated previous results.

As shown in Fig. 2, the magnitude of the field at point P due to the contributions of antenna elements 1, 2 and 3 may be computed from the measured radiation pattern of a single element using the following steps:

(1) Plot measured patterns of single antenna on cylinder using polar reference angles at $\phi = 0$, 120 and 240 degrees.

(2) At each interval of ϕ record magnitude of field for each antenna element E_1, E_2 and E_3.

(3) Add E_1, E_2 and E_3 vectorially.

$$E_t = E_1 + E_2 \angle B_1 + E_3 \angle B_2$$

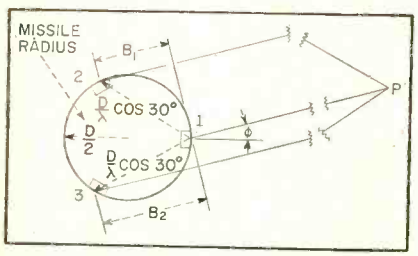
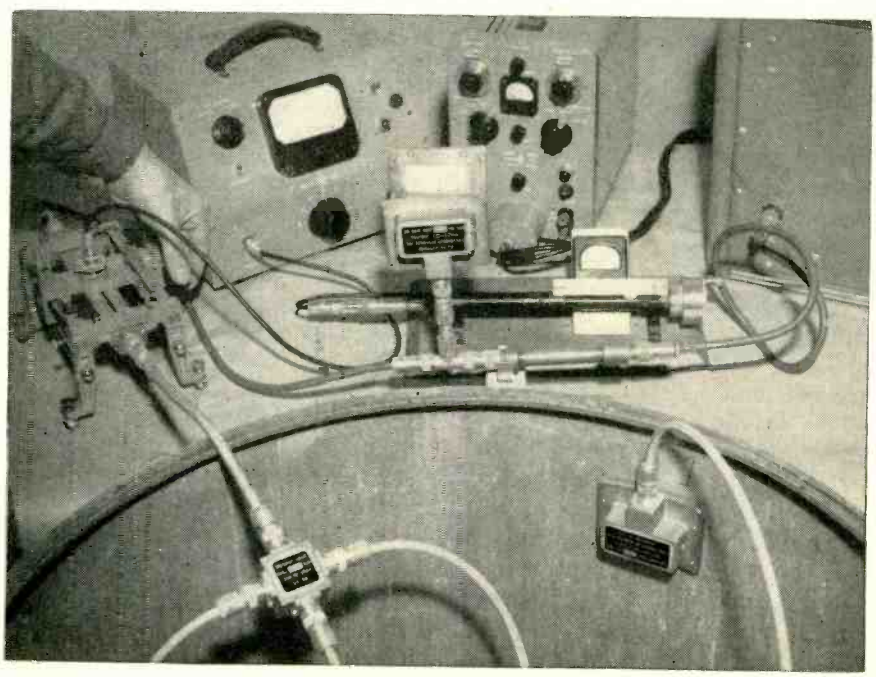


FIG. 2—Magnitude of the field at point P is computed from measured radiation patterns of a single element



Matching line transformer, at upper right of photograph, feeds power to a four-sided feed block. The power is divided to the three antenna elements and impedance is matched at the junction of the feed block

SUMMARY —— S-band and X-band antenna arrays consisting of three elements, equally spaced and circumferentially mounted on the missile, are fed in phase with polarization parallel to the missile axis. Radiation patterns for missile diameters ranging from four to 48 inches show better coverage and fewer small nulls than patterns of any other array up to and including 12 elements. Calculations, measurements of radiation patterns and techniques for impedance matching are given to assure best reception from or transmission to a circularly-polarized earth-mounted antenna

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Evansville, Indiana

For Guided Missiles

Where $\angle B_1 = \frac{D}{\lambda} \cos 30 \sin(60 - \phi)$

and $\angle B_2 = \frac{D}{\lambda} \cos 30 \sin(60 + \phi)$

(4) Plot magnitude of E_t obtained from Step 3 for each interval of ϕ used in Step 2.

Roll-plane patterns of multi-slot S-band arrays, plotted in Fig. 3, indicate that additional slots in excess of three merely increases the number and severity of the nulls present and pancakes the pattern. Calculations, plotted in Fig. 4, indicate that circumferential mounting, gives very superior coverage in the roll plane as compared to axially-mounted slots.

The principal plane patterns of a 3-slot S-band array have nulls in all three planes for the principal polarization which are covered by at least some cross polarization and the nulls fore and aft in the pitch and yaw planes are very sharp. However these sectors of possible circular polarization are small since the field patterns for both polarizations are changing rapidly, thus making the spherical coverage consist largely of linear polarization.

In these sectors there is an equal probability that the circularity of polarization will be of the correct sense suitable for reception from or transmission to a circularly-polarized earth-mounted antenna system.

The array of three elements gives the best pattern coverage on all sizes through 48-inches diameter. A two-slot array, circumferentially mounted, was used on the 4-inch diameter missile.

Optimum antenna cavity dimensions and diameter of exciting stub and shunt bars were determined by impedance measurements on a single-slot element. Temperature requirements narrowed the choice of slot cover materials to the ceramics family and Alsimag 35 was selected for the cover. High-temperature polyester-bonded fiberglas covers could be used as an alternate material for 500 F maximum temperature requirement. The impedance of the single-slot antenna with a ⅛ inch thick ceramic cover is approximately 17 ohms resistive

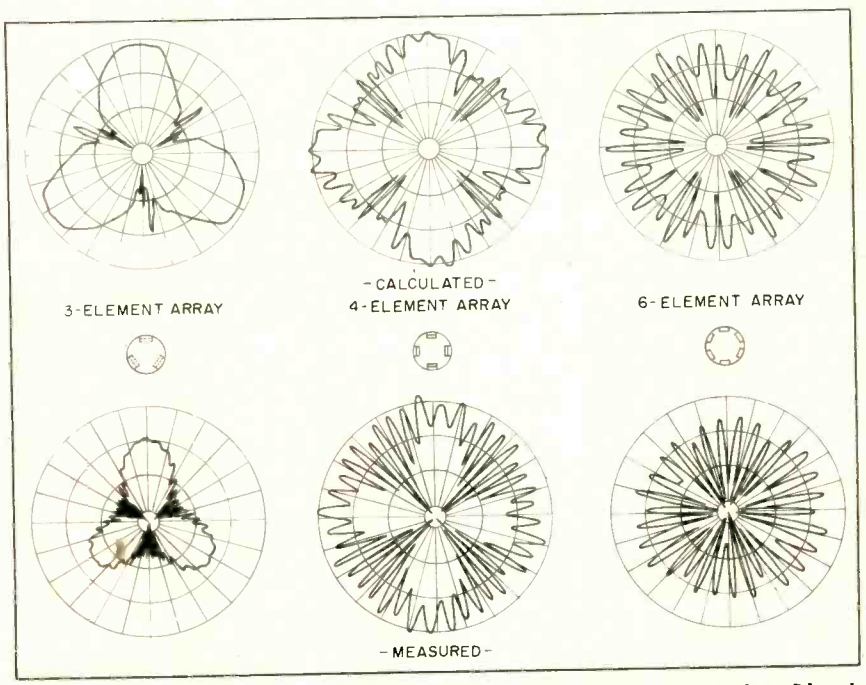
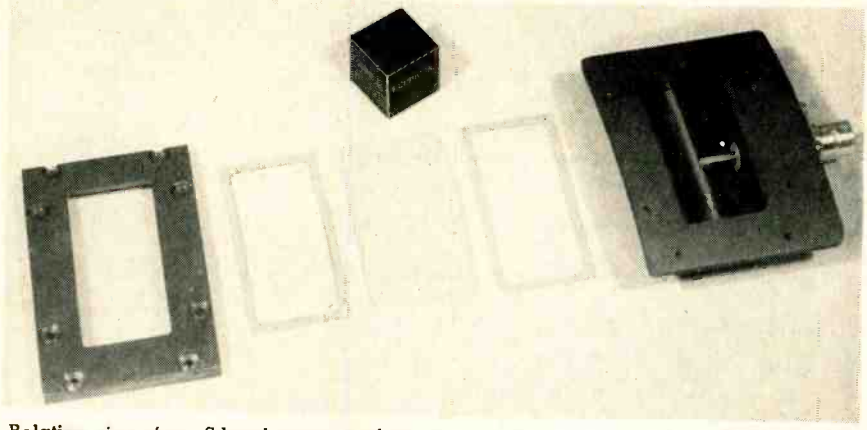


FIG. 3—These roll-plane patterns for 40-inch diameter missile show that S-band antenna elements in excess of three increase the number and severity of nulls

* Now with Cook Research Laboratories, Skokie, Ill.
† Now with Westinghouse Air Arm Division, Baltimore, Md.



Relative size of an S-band antenna element compared to a one-cubic-inch block. The T-fed slot is covered with Alsimag 35 ceramic window

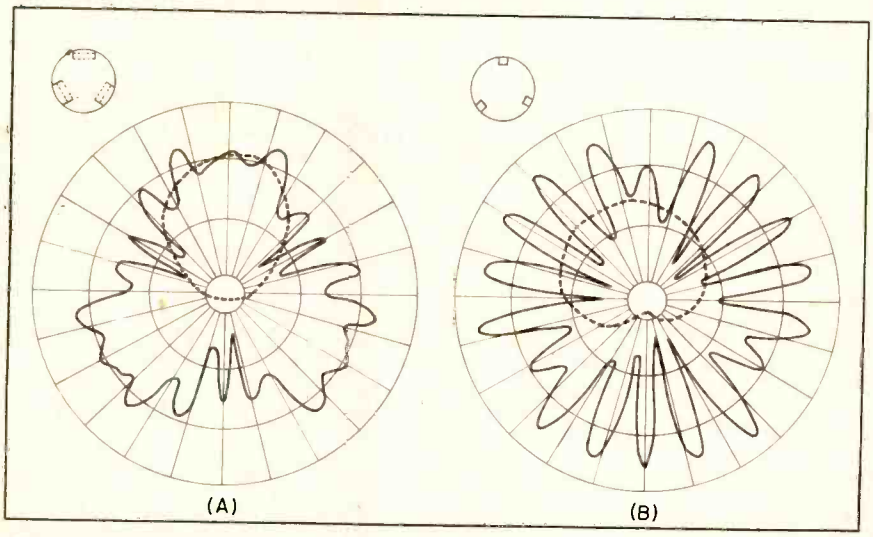


FIG. 4—Calculated roll-plane patterns for 15-inch diameter missile indicate that circumferentially mounted slot elements (A) give very superior coverage in roll plane as compared to axial mounting (B)

and with a $\frac{1}{16}$ inch thick cover approximately 23 ohms resistive.

The definition circle for 1.8:1 vswr on the impedance plots is drawn for the frequency band 2,835 mc to 2,965 mc and the circle for 1.2:1 vswr is drawn for the band 2,892 mc to 2,922 mc.

A matching line transformer, consisting of a 27-ohm coaxial line approximately 0.21 in length, feeds power to a four-sided feed block which consists of three short 50-ohm sections. The power is divided to the three antenna elements and impedance is matched at the junction of the feed block. All interconnecting cable lengths are accurately maintained for proper power distribution. Fig. 5 shows a typical impedance plot for a 15-inch diameter missile.

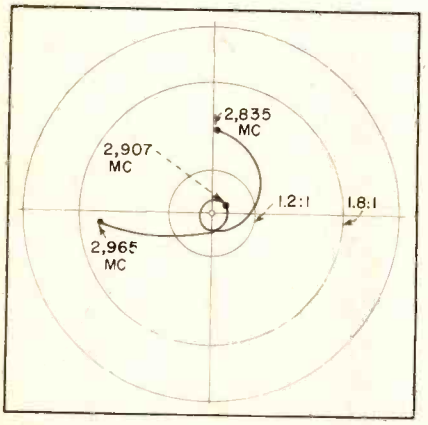


FIG. 5—Impedance plot of three S-band antenna elements on 15-inch diameter missile with 27-ohm line transformer approximately 0.21-inch long incorporated inside feed block

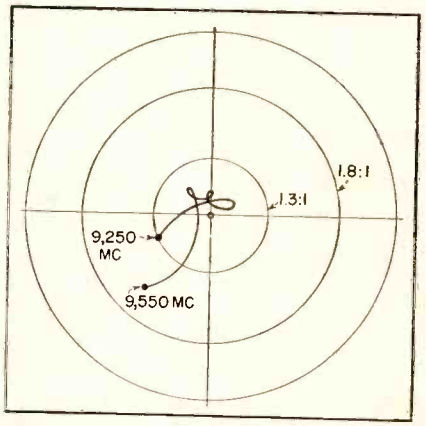


FIG. 6—Impedance plot of three X-band antenna elements mounted on 15-inch diameter missile was obtained by optimizing the overall diameter and length of the stub excited slot elements

X-Band Impedance

Very little success was realized using line-transformer methods to match impedance. Difficulty was encountered in controlling the degree of transforming action and the close tolerances required were impractical for production. Difficulty was also experienced with the fringe capacity introduced by a step-up or step-down in diameter of transformer center conductor and stub at the entrance to the cavity By eliminating this step-up or step-down in diameter and optimizing the stub over-all diameter and length, a matched condition was obtained over the required bandwidth. The impedance plot is shown in Fig. 6.

The antenna array system is adaptable to waveguide feed by attaching a waveguide-to-coaxial adaptor, constructed from a short section of RG-52/U waveguide, a UG-40A/U choke flange, a UG-568/U receptacle with press fitted probe and a receptacle block.

Since the S-band and X-band beacon-antenna systems bracket C-band, it is comparatively simple to extrapolate an antenna system design for the C-band frequency.

Development of those systems was sponsored by the U. S. Army Signal Corps Engineering Laboratories, Ft. Monmouth, New Jersey under contracts DA-36-039 SC-52,611 and DA-36-039 SC-15,522.

Thanks are due the Signal Corps for permission to publish this material and to B. H. Baldridge, Engineer Supervisor of Electronics Research, Inc. for his guidance and assistance.

References

(1) R. R. L. Staff. "Very High Frequency Techniques", 1, p. 188, McGraw-Hill Book Co., Inc., New York, 1947.

(2) Antenna Research Laboratory, Inc., Final Report on Antenna for S-Band Beacon on Aerobee Missile.

Color equipment can be adjusted by operator at control console

MONOCHROME SLIDES BROADCAST COLOR

By EDWARD L. COVINGTON

Engineering Dept.
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Tulsa, Oklahoma

SUMMARY — Two complementary colors can be broadcast from a tv transmitter using monochrome slides having well-defined transitions. In addition, special circuits permit continuous transmission of a yellow-green color stripe for color receiver adjustment during monochrome broadcasts

With increased numbers of color tv receivers being installed and only occasional color programs on the air during convenient servicing times, a system is desirable for providing a continuous color test signal. A narrow strip of color on the extreme edge of the picture permits proper receiver adjustments during monochrome transmissions.

A system permitting use of monochrome slides to produce color reduces the cost of programming. A station backlog of slides thus becomes useful for color work. The system to be described satisfies both of the above requirements. The equipment is divided into two rack-mounted units referred to as the subust generator and the bicolorimiter.

Broadcasts of either of the above signals require a standard color subcarrier reference burst. The subcarrier signal and burst keying pulses are generated by conventional circuits. The subust generator produces the color stripe signal. To create the stripe, the burst timing pulse is delayed by approximately 3.5 μsec as shown in Fig. 1.

It then triggers the stripe keying stages to produce a signal identical to and in phase with the reference burst, but delayed by the amount of DL_1. This signal is combined with burst in the adder stage to produce the waveform shown in Fig. 2.

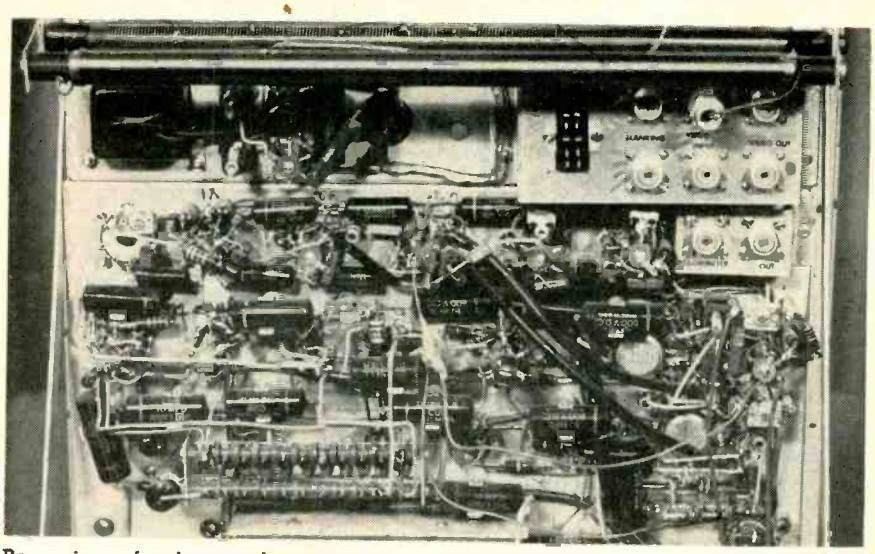
When the burst-stripe signal is added to the televised picture, the stripe appears on the extreme left edge as a narrow vertical bar, yellow-green in color. It can be seen by slightly reducing the width of the receiver raster. Normal width adjustment prevents the stripe from being objectionable during normal viewing, because it is masked by the sides of the screen.

Bicolorimiter

The bicolorimiter provides for the addition of two-color information to the monochrome slide signal. As is evident from Fig. 3, colors opposite each other on the NTSC vector diagram are complementary. It is therefore practical to split the phase of the subcarrier and produce color combinations that are pleasing to the eye.

The schematic diagram Fig. 4 shows that two delay lines are used, DL_1 delays the luminance information to coincide with the chrominance signal at the mixing point. Tapped along its length, DL_2 provides a selection of subcarrier phase with reference to burst.

These delay lines, originally developed by the KVOO engineering



Rear view of color supplement chassis reveals construction of various delay lines

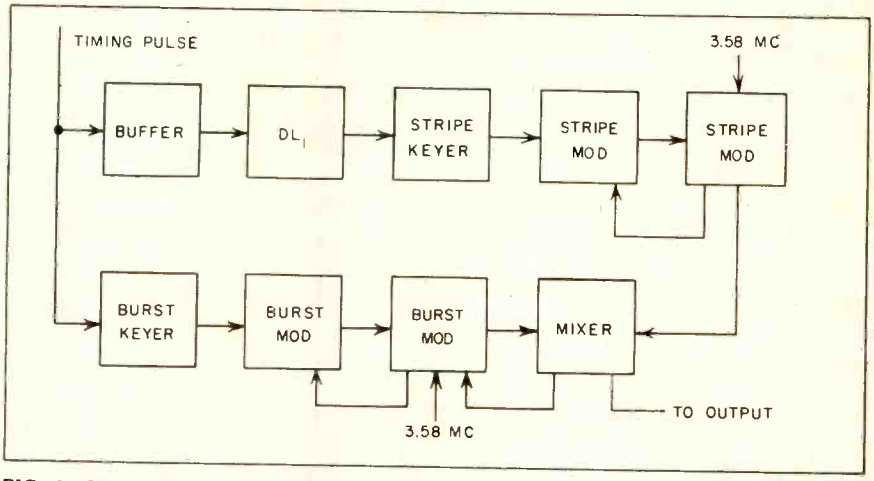


FIG. 1—Block diagram shows how the stripe and burst-forming stages are connected

department for another purpose introduce up to one-microsecond delay with acceptable video bandwidth. They consist of 200 turns of number 18 double Formex insulated copper wire wound in a spiral groove machined in a $\frac{3}{4}$-in. copper tube form. The wire spiral produces inductance and the proximity of the wire to the copper form provides the capacitance for this distributed-constant type delay line.

Increasing Capacitance

The cutting tool used to machine the spiral groove was specially ground to make a round bottom increasing the capacitance between the wire and the form. The form is slotted lengthwise to prevent a shorted-turn effect. This slot makes it convenient to tap the line at the desired delay point.

Since the characteristic impedance is inversely proportional to the square root of the shunt capacitance ($Z_0 \propto \sqrt{L/C}$) a convenient method of lowering the impedance to the desired 75 ohms is to increase the distributed capacitance by the application of printed circuit type silver paint in strips along the length of the delay line form.

After the correct impedance is established, the line is given a protective coating of Glyptal. The particular lines have been in use, in various experimental circuits, for six years and appear to be rugged and stable in this type of application.

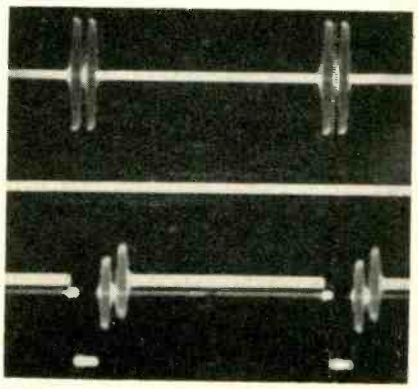


FIG. 2—Burst-stripe mixer output (above) and burst-stripe added to monochrome video (below) shown on an oscilloscope

Pulse Circuits

Video, preferably from an automatic level-setting device, is applied to the grid of video amplifier V_1. The amplitude is further increased by V_2 to the point of some compression. This permits sharp clipping of the signal by V_3, which was selected for its narrow cutoff-to-saturation characteristic.

The output of V_3 becomes a keying pulse that is amplified by V_4 and applied to phase inverter V_5. Pulses at the output of V_5, which are 180 deg out of phase, are applied to the suppressor grids of V_9 and V_{10} to cause them to alternate between conduction and a cutoff condition.

From the output of V_4 the pulse is also applied to an output stage to be used for montage purposes, increasing the scope of the station special-effects keying amplifier.

Subcarrier Circuits

The 3.58-mc c-w subcarrier from the subust generator is applied to the input end of DL_2. Taps permit color selection since the subcarrier phase is dependent on the distance from the input end of the line. The signal is then applied to the con-

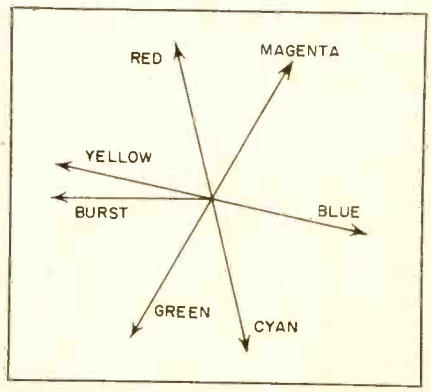


FIG. 3—Vector diagram relates colors showing complementaries at 180 degrees making the device usable for slides

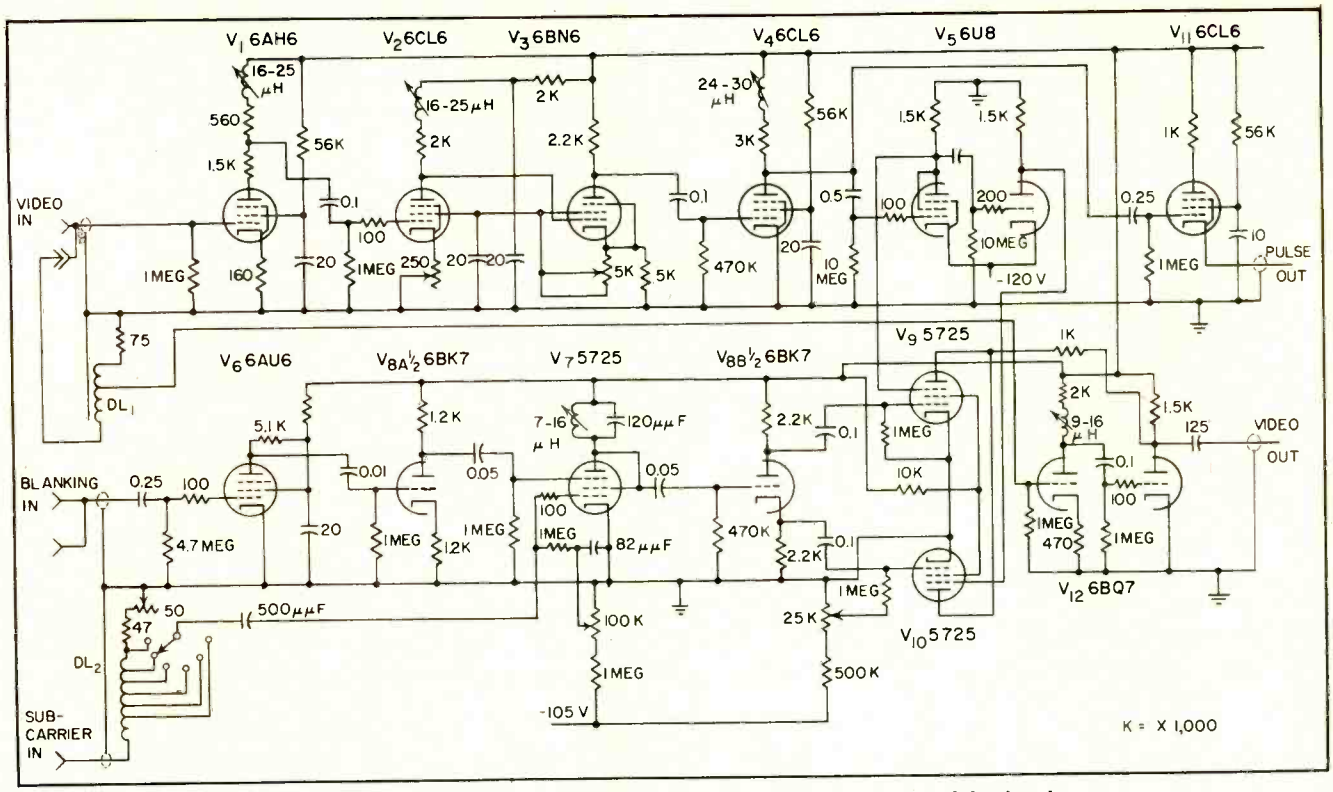


FIG. 4—Circuit diagram of the bicolorimiter that adds two-color information to a monochrome slide signal

trol grid of subcarrier amplifier V_7.

To prevent subcarrier from appearing during the blanking interval, the station blanking, which is amplified by V_6 and V_{8A} is applied to the suppressor grid of V_7. Subcarrier amplitude, or color saturation, is controlled by adjusting the control-grid bias of V_7.

Blanked subcarrier from V_7 appears at phase inverter V_{8B}. Signals of opposite phase from the plate and cathode of V_{8B} are applied to modulator stages V_9 and V_{10}. By the action of the keying pulses, subcarrier of one phase will appear during the time video exists above the clip point as shown in Fig. 5.

When the video potential is below the clip point, subcarrier of the opposite phase will appear at the common plate load. As the keying pulses are of opposite polarity, they cancel at the plates leaving only the subcarrier. To correct for a difference in tube characteristics, a d-c balance adjustment is provided in the grid circuit of V_{10}.

Luminance Channel

Video at the unit input is connected through DL_1. The line is tapped at a point to provide luminance delay equivalent to that of

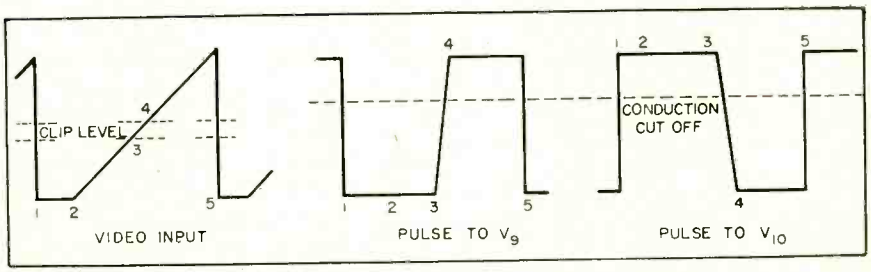


FIG. 5—Pulse circuit waveforms show how video input keys V_9 and V_{10}

the keying circuits. It is then amplified by the first section of V_{12}. From V_{12A} the signal is coupled to the output stage V_{12B} whose plate load is common to V_9 and V_{10}. Isolation is provided by the 1,000-ohm resistor between the plates.

Slide Types

The most useful slide material contains definite, flatly shaded whites, greys and blacks common to most lettered slides. Gradual grey or brightness transitions must be avoided to assure sharpness of clipping action. The ideal clip point is just above the grey material. Here, the whites appear as one color and the greys will appear as the color 180 deg from that of the whites. The blacks reveal little, if any color because of the luminance value. Slides containing only pure blacks and white are also excellent, but the only noticeable color will be that of the white areas, for reasons of luminance.

The output of the unit is treated as a regular camera signal for switching, since burst is added at the switcher output. With this arrangement it is possible to use the bicolorimiter signal in superimposures with monochrome studio or film cameras. Key inserts may even be used with the bicolorimiter pulse itself providing the keying signal.

The author acknowledges with thanks the original ideas of J. M. Bushnell, chief engineer and the aid and suggestions of James McDanield, Aubrey Decker and the KVOO-TV engineering staff.

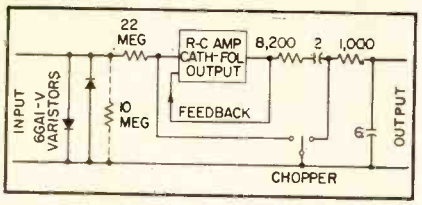


FIG. 1—Simplified diagram of amplifier shows chopper-stabilized and conventional feedback paths

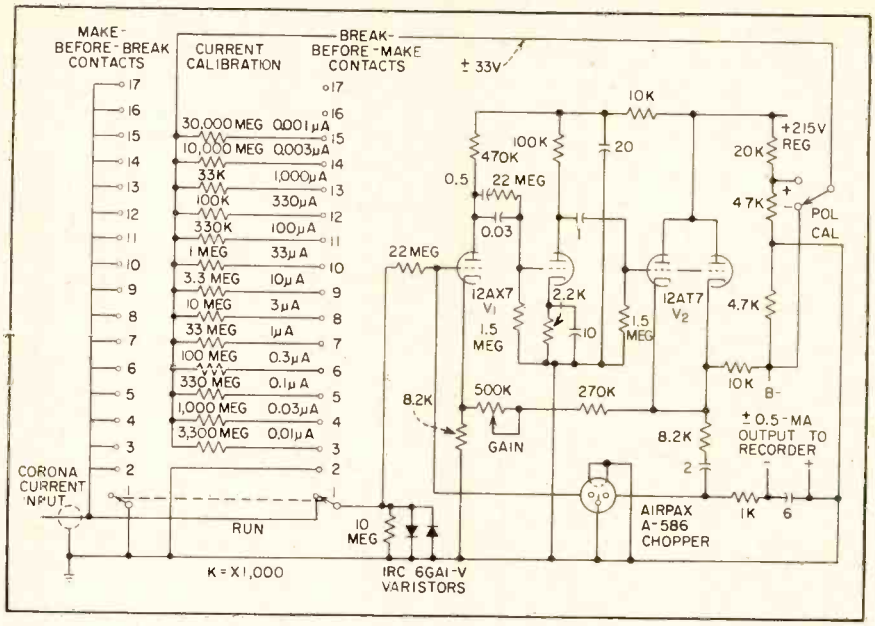


FIG. 2—Logarithmic amplifier includes calibration circuit currents, shown at left. Corona current reaches amplifier through 50 feet of shielded cable

Measuring Corona

SUMMARY —— Chopper-modulated feedback signal stabilizes amplifier for measuring radioactive corona-point currents in fair weather. Output signal to recorder is essentially logarithmic, for both polarities of current, in the range from 10^{-9} to 10^{-5} amperes. Built-in calibration remains practically constant through months of service

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Amplifier drives Esterline-Angus recorder from output of radioactive corona point on top of flagpole. Typical fair weather value of corona current is 0.03 μa

IN an investigation of atmospheric electricity, several years ago, a bipolar logarithmic amplifier[1] operating an Esterline-Angus recorder was used to measure current of either polarity, in the range from 0.1 to 1,000 μa, from a nonradioactive corona point at the top of a flag pole in disturbed weather.

Recently the nonradioactive corona point was replaced with one containing 320 micrograms of radium 226 so measurements could be made in fair weather too.[2] The typical value of current from the point is 0.03 μa and the minimum current of interest is about 0.001 μa.

While the old amplifier could be adjusted to record the current down to 0.001 μa, in the new range

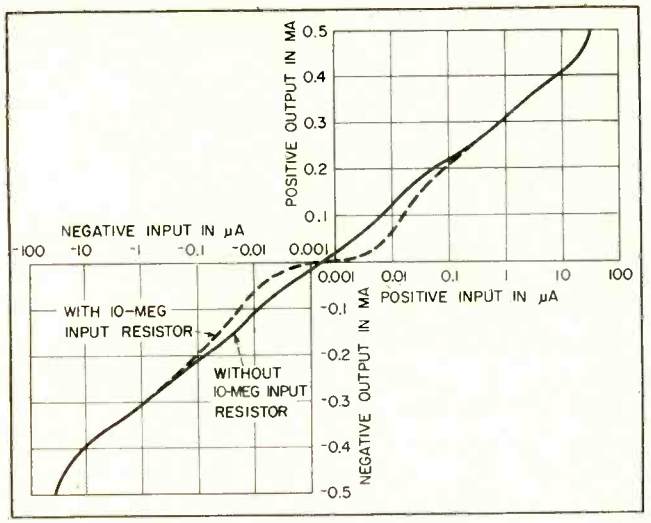
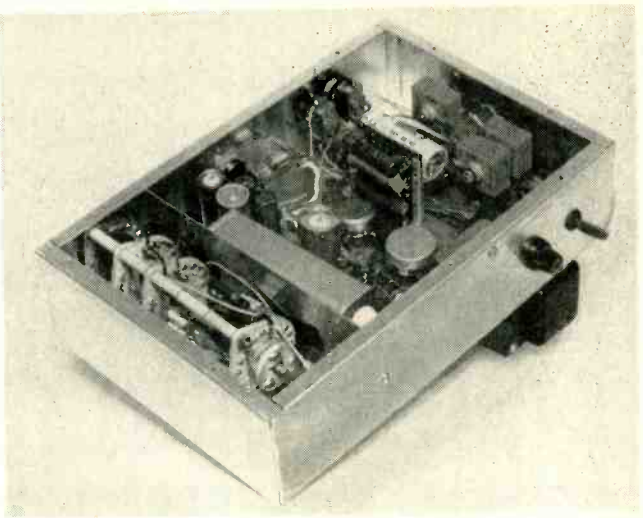


FIG. 3—Overall transfer characteristic of logarithmic-response amplifier with and without input resistor



Underside view of amplifier shows calibration switch at left of chassis in shielded section

From Radioactive Point

of sensitivity it was not satisfactory. Although a majority of the diodes (9004) had suitable logarithmic characteristics, for satisfactory operation the amplifier tube, a 954 pentode, following the diodes should have a grid current of much less than 0.001 μa over extended periods of time. One-fifth of new tubes began with a satisfactory grid-current characteristic, but only about a tenth of them would maintain this characteristic through months of service.

Revised Circuit

In a drastic revision, current-sensitive resistors were substituted for the logarithmic diodes, and a chopper-modulated three-triode feedback-stabilized amplifier was substituted for the d-c amplifier. The new circuit is shown in simplified form in Fig. 1 and in detail, with calibration current circuits, in Fig. 2.

When the 10-megohm resistor is shunted across the input, then the calibration is as shown in the dotted curve of Fig. 3; without the resistor, the solid curve applies. The calibration remains practically constant for months—maximum output current deviations are about two percent of full scale.

Except for the input, the amplifier is a standard R-C type operating as a carrier-frequency amplifier. Feedback around the amplifier stabilizes its gain. The carrier is established by a 60-cps chopper which also synchronously rectifies the output in a shunt rectifier circuit.

Logarithmic Response

The novel portion of the circuit is the input device, a pair of IRC 6GA1-V varistors shunted in opposite polarity. These varistors exhibit a logarithmic response as shown in the overall transfer characteristics in Fig. 3.

The 22-megohm resistor between the varistors and the chopper raises the shunt resistance seen by the varistor pair, preserving their logarithmic response. It also prevents shorting of charge stored in the cable capacitance.

Although changing temperature would alter the calibration, an input current change of about 2.4 percent per degree C for the same output indication, the equipment at present operates in a basement in which temperature fluctuations are small. The six-microfarad capacitor across the output minimizes the recorder pen vibration at fairly large currents.

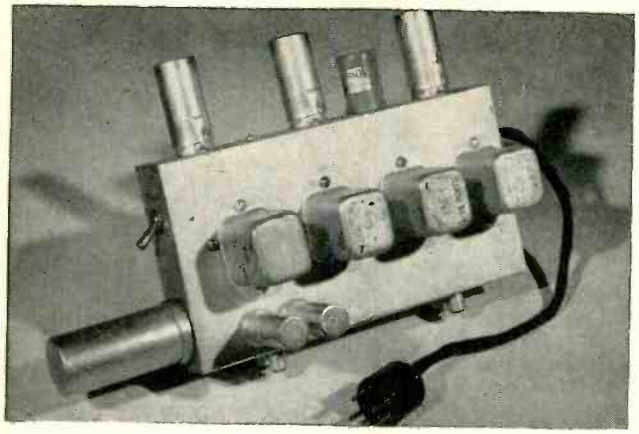
In disturbed weather, currents of 10 μa are common. Since a current greater than 30 μa had never been recorded, when the range was extended at the lower end in the new amplifier, it was decreased at the upper end. Actually, the varistors lose their logarithmic characteristic at about 10 to 13 μa.

Twice in seven years, lightning has struck within 200 feet of the corona point, but unfortunately in neither case has the recorder been turned on. It was hoped to observe the current, perhaps up to 1,000 μa just before a lightning strike, but as yet the recorder has not gone off scale at 30 μa.

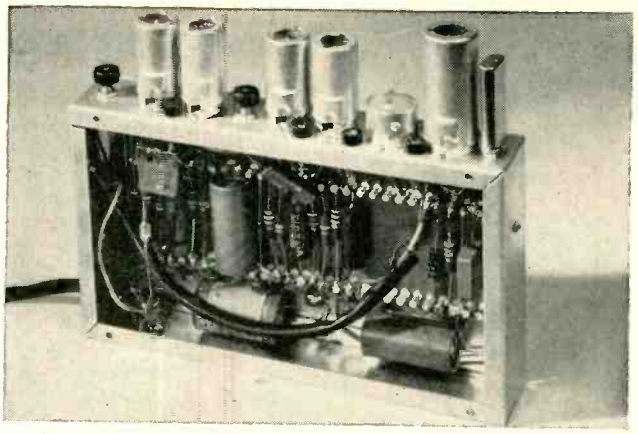
The circuit has been in continuous use for 18 months. Except for tube replacement and chopper replacement about every six months, it has required no attention and has been entirely satisfactory in the new range of ±0.001 to ±30 μa.

References

(1) Seville Chapman and L. Bogdan, Bipolar Logarithmic Current Amplifier, Electronics, p 136, Jan. 1953.
(2) Seville Chapman, Electrostatic Field Measurements, Corona Discharge and Thunderclouds, C.A.L. Report No. 68, Mar. 1956.



Developmental sync generator for RCA ITV-5 timing circuit, shown in Fig. 2, uses blocking-oscillator counters



Prototype sync generator for RCA ITV-6 equipment is similar to circuit of Fig. 6, except for master oscillator

SIMPLE SYNC CIRCUITS

SUMMARY —— Industrial television systems can use simplified three or four-tube sync-generator circuits because of nonstringent pulse-timing requirements. Three representative designs used in commercial equipment are described. Fourth type, for airborne military application, generates sync electromechanically with serrated-edge wheel and magnetic pickups

By HAIG A. MANOOGIAN
Assistant Editor
ELECTRONICS

SIMPLIFIED CIRCUITRY makes industrial-television systems compact, light-weight and low-cost. Compared to conventional broadcast-type equipment, the less stringent timing requirements of industrial equipment offer the greatest opportunity for circuit simplification, permitting use of sync generators with as few as three or four tubes. This article presents a few of the many types of simple sync-generator circuits used in itv systems of various manufacturers.

Basic System

In their simplest form, sync generators usually comprise a master oscillator, operating at twice the line frequency of 15.75 kc, and a countdown chain that divides by 525 to produce 60-cps field-frequency pulses in synchronism with the master oscillator pulses. Of several possible countdown circuits, blocking oscillators are frequently used because each division can be accomplished by a single triode section and a saving in B-supply current can be realized. Blocking oscillators conduct only during the short pulse portion of their cycle; at all other times they are cut off.

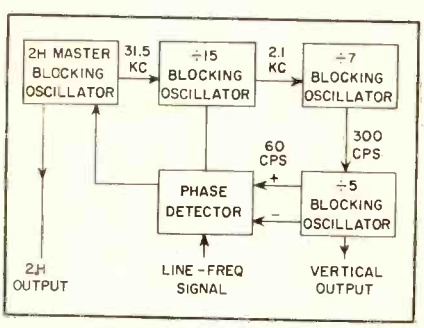


FIG. 1—Typical sync generator uses blocking-oscillator dividers

The sync generator shown in block form in Fig. 1 is a typical blocking-oscillator countdown timing system. Figure 2 shows an application of this system in the RCA ITV-5.

Blocking oscillator V_{3A} generates the 2H frequency of 31.5 kc, which is divided down to 60 cps by blocking oscillators—15 by V_{2B}, seven by V_{2A}, and five by V_{1B}. The 60-cps vertical-rate pulse is taken from the cathode of V_{1B}. Amplifier V_{3B} serves as a buffer stage for the 31.5-kc pulse output from the master oscillator.

Phase detector D_1D_2 compares the 60-cps pulses at the cathode and plate of V_{1B} with the 60-cps line-

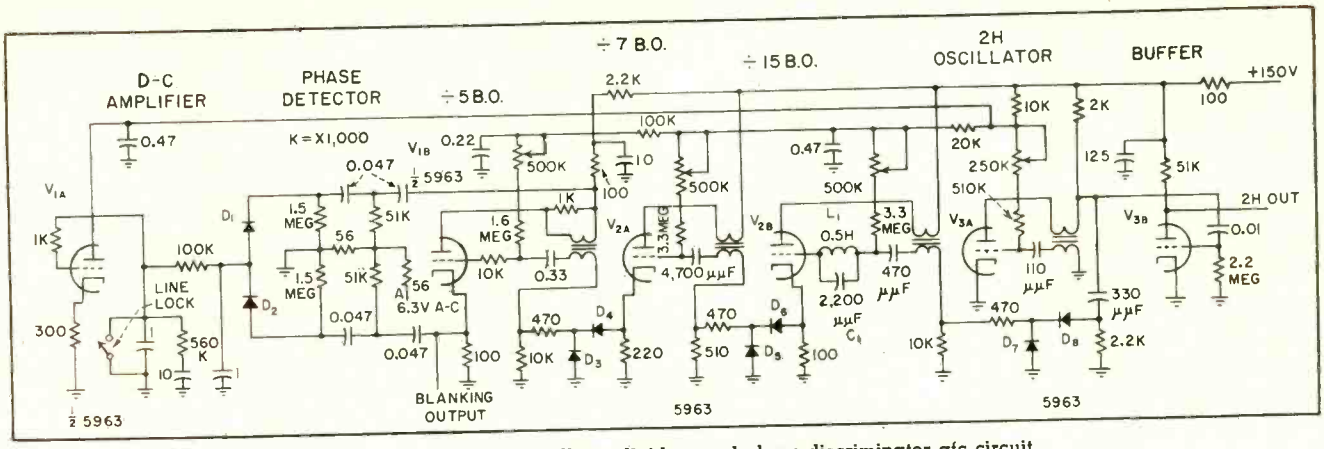


FIG. 2—Three-tube sync generator has three blocking-oscillator dividers and phase-discriminator afc circuit

TIME ITV SYSTEMS

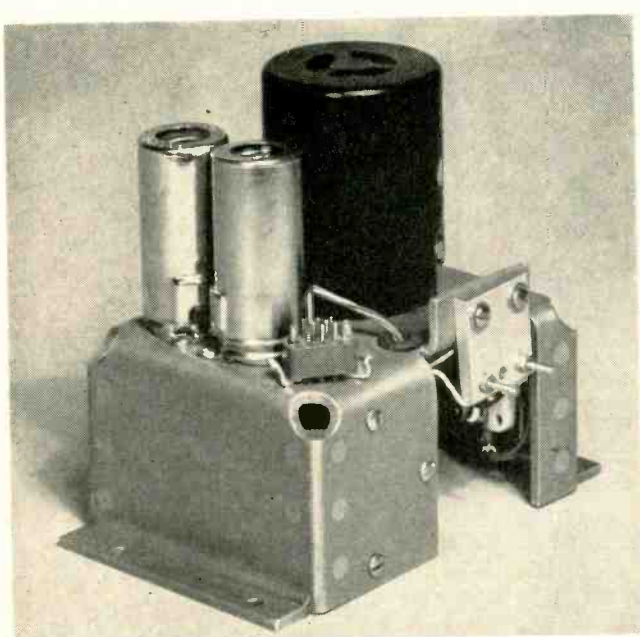
frequency signal introduced at point *A*. The resulting d-c error voltage is applied as an afc signal to the grid circuits of the 2H oscillator and dividers through d-c amplifier V_{1A}.

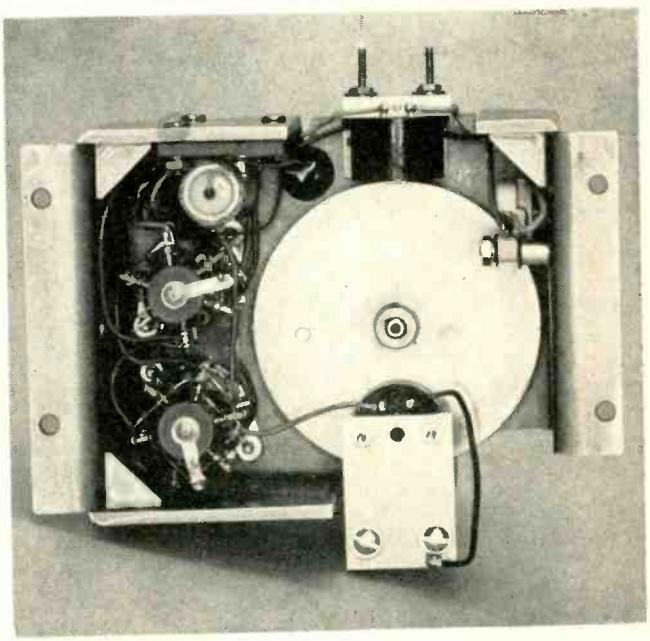
Hartley Master Oscillator

Another form of blocking-oscillator divider sync generator is represented by the block diagram of Fig. 3. A Hartley circuit is used as the master oscillator to assure extreme frequency stability when it is expedient to operate the sync generator unlocked from the power-line frequency.

In the circuit diagram of Fig. 4, V_{1A} operates at 31.5 kc. Plate current pulses through R_1, in series with the plate supply feed to the oscillator tank circuit, trigger ÷3 blocking oscillator V_{2A}. The output of this stage is divided by seven, five and five, by V_{2B}, V_{3A}, and V_{3B} respectively. The 60-cps vertical-rate frequency is obtained from the cathode of the last divider, V_{3B}.

Positive and negative current pulses from the cathode and plate





Mechanical tone wheel assembly is used in sync generator for Avion's airborne navigation-situation display television system. Chassis is made extra rigid to minimize timing errors from flexing and vibration

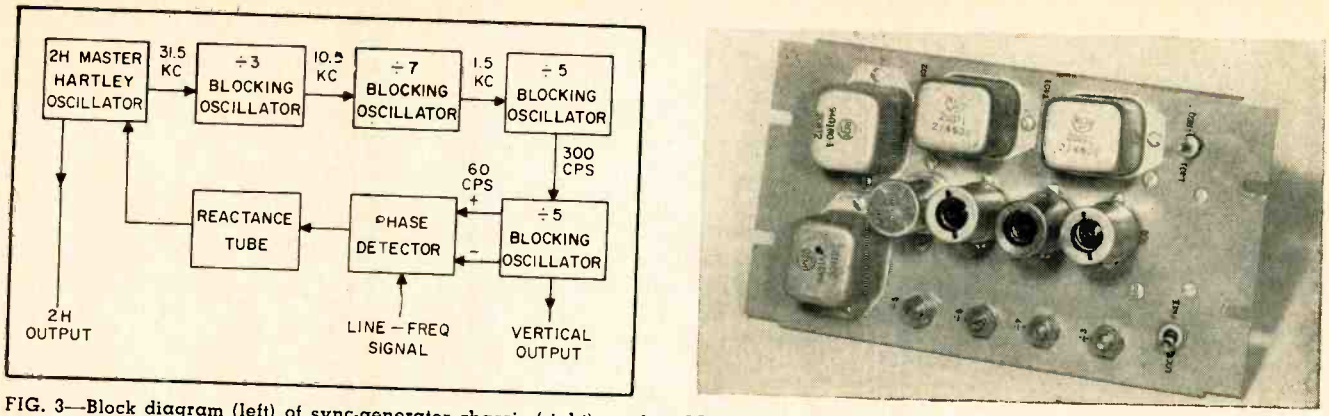


FIG. 3—Block diagram (left) of sync-generator chassis (right) used in GPL PD-150 industrial-television system

circuits, respectively, of V_{3B} are compared to the 60-cps line-frequency reference sine-wave voltage at point A in a conventional phase-discriminator network, similar to that in Fig. 2. The output of this network is a d-c voltage whose polarity is determined by whether the pulse frequency is higher or lower than the reference frequency and whose amplitude is proportional to the frequency deviation. This control voltage is applied to the grid of reactance tube V_{1A} when S_1 is in the lock position. The reactance tube changes the frequency of the Hartley oscillator to produce a minimum error signal in the feedback loop.

When S_1 is in the free-running position the error signal is shorted out.

As used in the GPL PD-150 itv system, this sync generator holds frequency over a range of ±2 cycles of the reference line frequency and will pull into lock within a range of ±1 cycle of the reference line frequency, with S_1 in the lock position.

Triggering Stability

One of the most serious problems encountered in the use of blocking oscillators in frequency-divider chains is that the large amplitude pulses, which occur when a blocking oscillator fires, kick back into the circuit of the blocking oscillator that is providing the trigger and upsets its operation. Unless extreme care is taken in the triggering circuit employed, kickback will cause both the preceding and following blocking oscillators to fire together.

In the circuit of Fig. 2, the pulse-steering networks consisting of D_3D_4, D_5D_6 and D_7D_8 prevent interaction of V_{1B} on V_{2A}, V_{2A} on V_{2B} and V_{2B} on V_{3A}. In addition, the trigger-

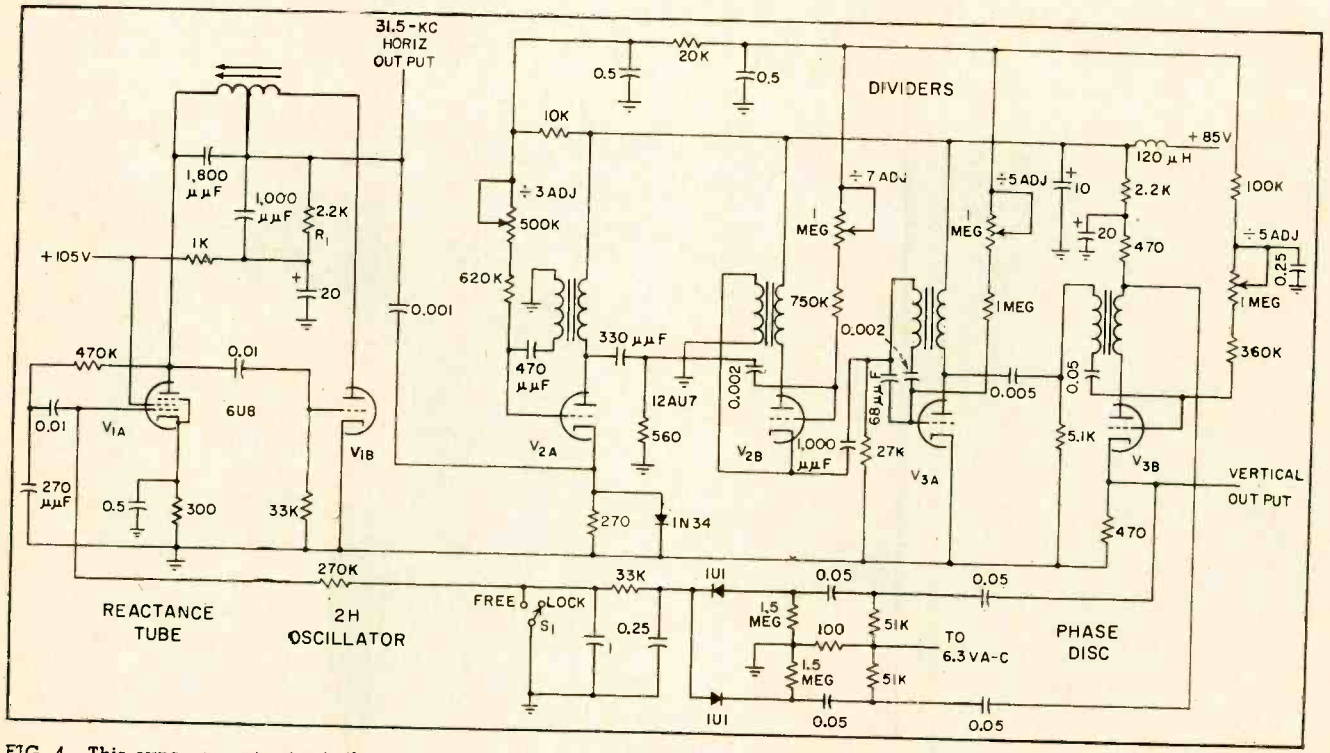


FIG. 4—This sync generator is similar to that in Fig. 2, except for Hartley master oscillator and reactance-tube afc. Grid capacitor-charging circuits of V_{2A}, V_{2B}, V_{3A} and V_{3B} are returned to a positive voltage to increase triggering stability

ing stability of the ÷15 stage is further improved by the tuned circuit comprising C_1 and ringing choke L_1, in the grid circuit.

The kickback problem is circumvented, in the circuit of Fig. 4, by employing the overshoot (Fig. 5) from one blocking oscillator as the trigger pulse for the following stage. Thus, the previous blocking oscillator has finished its cycle and is in a stable cut-off condition before the following blocking oscillator fires. This method can be used since it is not imperative that the leading edges of the field-frequency pulses coincide exactly in time with the leading edges of the line-frequency pulses.

A further increase in triggering stability is obtained in Fig. 4 by returning the grid capacitor-charging circuits of V_{2A}, V_{2B}, V_{3A} and V_{3B} to a positive voltage rather than to ground. In this way, the grid voltage for each tube approaches cut-off at a steeper angle and a larger difference is obtained between the peak voltages of adjacent trigger pulses.

Phantastron Dividers

To obtain more stability than that afforded by the blocking-oscillator divider chain in the ITV-5 equipment, a sync generator based on phantastron-type frequency dividers was developed for use in the RCA ITV-6 equipment. The prototype circuit, shown in Fig. 6, has a master oscillator that operates either free-running, line-locked or crystal-controlled, a two-stage phantastron divider that counts down by 525 and a phase-detector afc circuit for line-locked operation.

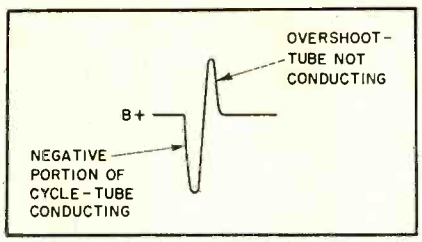


FIG. 5—Positive portion of blocking-oscillator plate waveform is used to trigger next divider stage without pickback

With S_1 in the line-lock position, V_{1B} operates as a synchronized 2H blocking oscillator. The 31-5-kc output signal across R_1 is applied to the phantastron circuit comprising V_{2A}, V_3 and V_{2B}, which counts down by 25. The 1,260-cps output from the screen of this divider is in turn applied to the second phantastron, V_{4A}, V_5 and V_{4B}, which counts down by 21 to the vertical field repetition rate of 60 cps.

Figure 7 shows, on an expanded time scale, the timing relation in the ÷25 and ÷21 counters. Note that the duration of the 60-cps vertical output pulse corresponds exactly to one cycle of the ÷25 counter or 25 2H pulses. This removes all jitter from the vertical blanking, as the vertical output pulse, after amplification and shaping, becomes the vertical blanking pulse.

Flyback Stability

As the flyback is the least stable portion of the operating cycle in the phantastrons, the start of the rundown and the start of the flyback are locked to pulses from the next highest counter. For the ÷25 counter, the trailing edges of the cathode and screen pulses correspond with the leading edge of the plate waveform that in turn corresponds with the leading edge of a 2H pulse. Thus, the following ÷21 counter is triggered at a time corresponding to the trailing edges of these cathode and screen pulses.

Reliable synchronization on the differentiated trailing edge of the cathode pulse is achieved by taking the pulse via V_{4A} and C_1 in Fig. 6. The triggering edge, which corresponds with the trailing edge of the vertical output pulse on the cathode of V_5, is made to correspond with the leading edge of a 2H pulse. Capacitor C_2 makes the leading edge of the vertical output pulse also correspond with the leading edge of a 2H pulse, by adding the small differentiated pulses shown

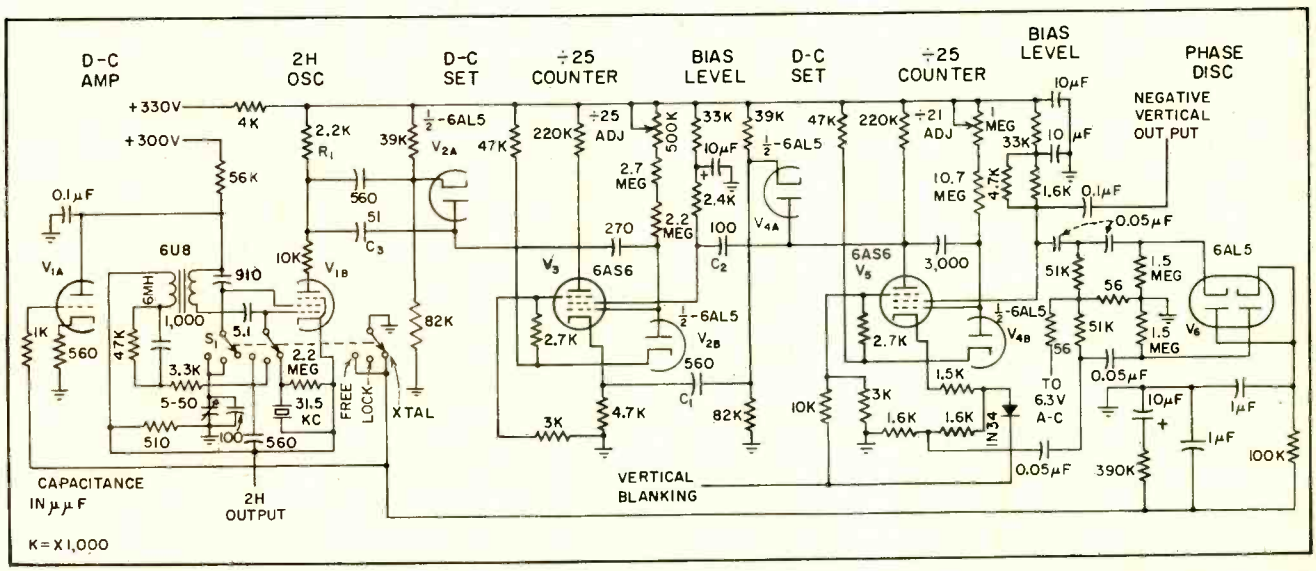


FIG. 6—Four-tube sync generator has phantastron-type dividers and line-locked, free-running or crystal-controlled oscillator. All jitter is removed from 60-ips output pulses by making their duration correspond exactly to 25 2H pulses

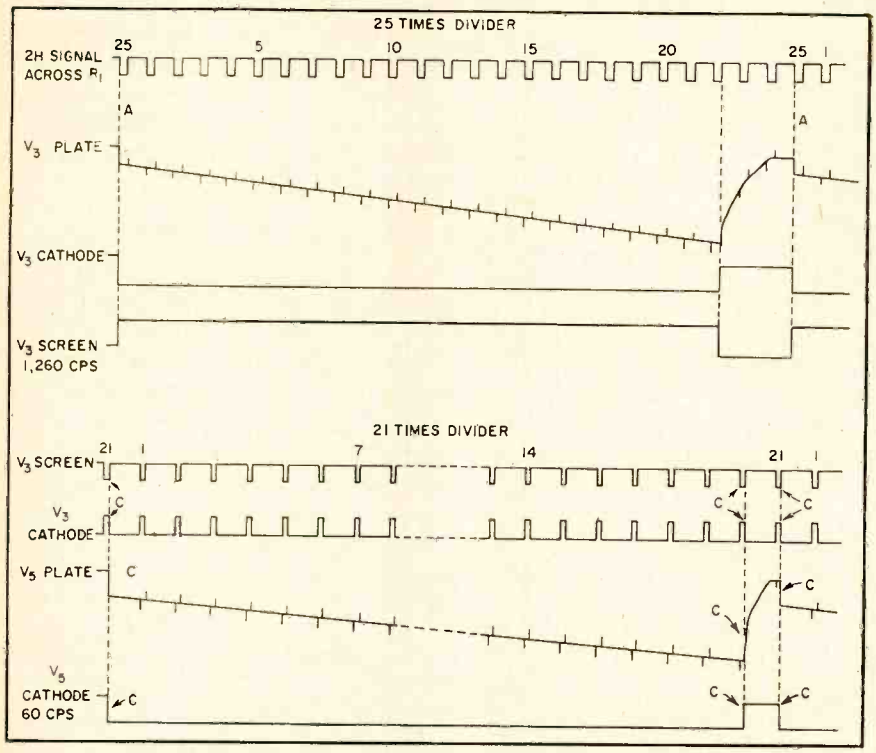


FIG. 7—Timing relationships of phantastron dividers used in circuit of Fig. 6

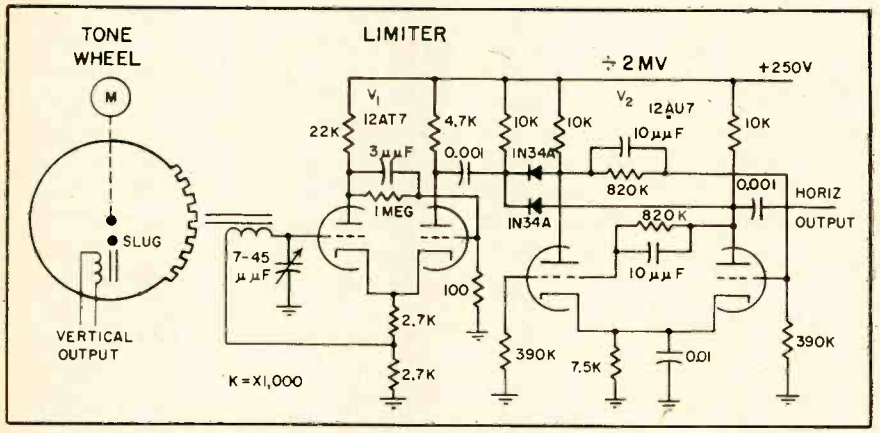


FIG. 8—Electromechanical sync generator has tone wheel with 525 teeth, for horizontal sync, and slug in wheel face, for vertical sync generation

in Fig. 7 to the waveform on the plate of V_5.

Negative 60-cps pulses are taken from the cathode of V_5 and positive pulses from the plate. These pulses are compared with the power-line frequency in phase detector V_6. The resulting d-c error voltage is applied as an afc signal to control-tube V_{14} to lock the master-oscillator frequency to the line.

With S_1 in the free-running position, V_{1B} operates as a free-running blocking oscillator. The latter two modes of operation require the power source to be hum-free to avoid the appearance of slowly moving hum bars in the monitor picture.

Mechanical Sync Generator

Developed for use in Avion airborne closed-circuit-tv fighter-situation-display equipment, the circuit of Fig. 8 differs from previously discussed sync generators in that a mechanical sync generator provides horizontal and vertical sync eliminating the need for a divider chain.

The system uses a 525-line, 50-field, 25-frame standard to enable the sync generator to be synchronized with the 400-cps line frequency of aircraft power sources.

Since the 400-cps line frequency can vary as much as ± 5 percent, the camera and kinescope deflection signals are obtained from common sweep generators. Use of synchronized sweep circuits, rather than triggered circuits, permits continued operation in case of sync failure, with only a slight loss of resolution and a slight increase in flicker.

The usual master oscillator is replaced by two magnetic pickup units and a tone wheel driven by a 6,000-rpm synchronous motor. One pickup generates a 52,500-cps signal from the 525 teeth on the wheel's circumference and the other pickup generates a 100-cps signal from a slug imbedded in the face of the tone wheel. The signals are essentially sinusoidal with approximately 30-v peak-to-peak amplitude.

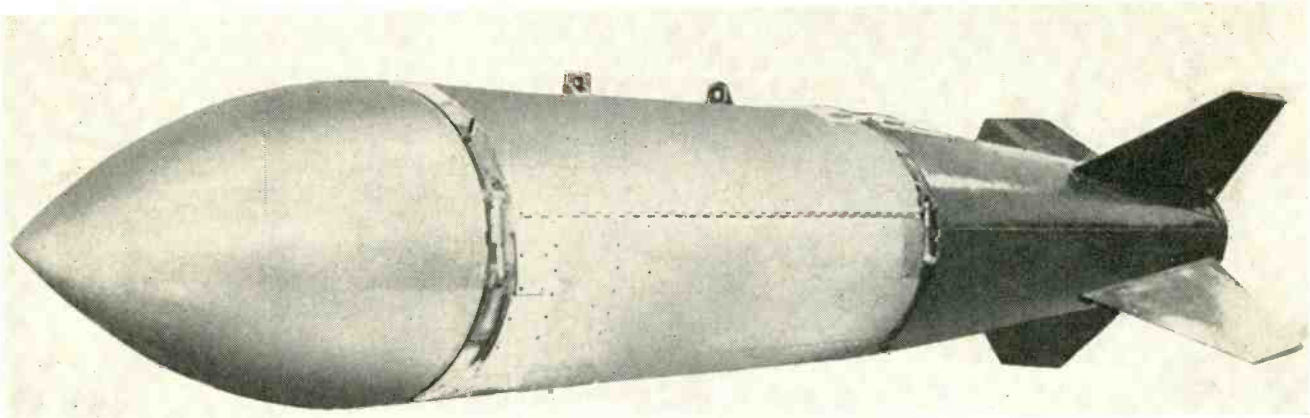
The 100-cps signal is used, without shaping, to synchronize a vertical blocking oscillator that counts down by two to the vertical field repetition rate of 50 cps.

The 52,500-cps signal contains some amplitude modulation due to mechanical irregularities in the teeth and runout of the tone wheel. To prevent time jitter of the horizontal sweeps from this cause, limiting along with a countdown by two is performed by biastable multivibrator V_3.

The 26,500-cps 2H output of V_2 is integrated and applied to a horizontal afc circuit that divides by two to obtain the desired horizontal repetition frequency of 13,125 cps. Every other pulse from V_2 is compared with a H pulse from the kinescope yoke. The resulting error signal is applied to the horizontal sweep generator.

Though a 6,000-rpm motor is used in this prototype, later equipments will use a 3,000-rpm motor to provide vertical field rate and 2H sync signals directly from the tone wheel without frequency division.

The author thanks Lester Flory of RCA Laboratories, Charles Taggert of General Precision Laboratory. Inc. and Sam Romano of Avion Division, ACF Industries Inc. for their cooperation in making available the information on which this article is based.



Explosive bolt connectors for nose and tail assemblies release parachutes for center section containing audio system

AIR-DROP SYSTEM BROADCASTS MESSAGE

SUMMARY —— High-power sound equipment is designed to be dropped from air to deliver prerecorded message. System including tape reproducer, 500-watt amplifier and five loudspeakers provides three-minute message intelligible over half-mile circle around drop point during descent

By F. C. FISCHER, A. A. GERLACH and D. S. SCHOVER

Cook Research Laboratories
Division of Cook Electric Co.
Skokie, Illinois

MODERN military tactics require a means of communicating propaganda or instructions to large groups of soldiers or civilians inaccessible by conventional radio transmitters.

This article describes the results of a program to develop a high-power loudspeaker system capable of being carried and dropped by high-speed, high-performance aircraft at altitudes to 60,000 feet. The system is designed to be as inexpensive as possible consistent with reliable one-shot operation. The loudspeaker system provides a minimum of three minutes of intelligible speech over a ground area equal to a half-mile diameter circle during a parachute-braked terminal-phase of its descent. A minimum articulation score of 80 per cent is required over this ground area in an ambient noise environment on the ground of 85 db of random or propeller-driven aircraft noise.

The loudspeaker system consists of a 500-watt amplifier and horn system broadcasting a tape recorded message. This equipment is housed in a 3-section bomblike container, shown in a photograph.

The conical tail section contains the brake parachute with its firing device and the main parachute. The cylindrical center section consists of an aluminum framework housing power, audio, acoustical and control systems. The nose section contains the nose parachute and serves to protect the speaker horn assembly during storage and while unit is being carried aboard an aircraft.

Physically the assembled missile is 119 in. in length and 19 in. in diameter.

Operation

When the missile is released from the aircraft two switches apply operating voltage to aneroid switch contacts and open all safety shorts on explosive devices used to separate the sections of the missile.

When the missile reaches a preset

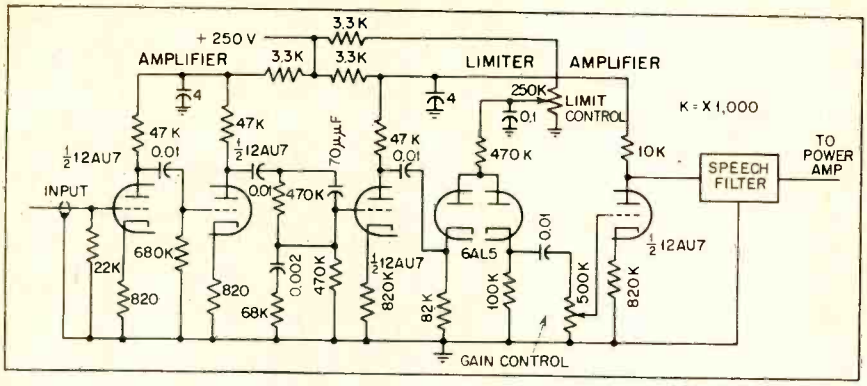


FIG. 1—Preamplifier for tape playback unit provides drive for 500-watt amplifier

altitude the aneroid switches initiate an internally programmed control sequence. The brake parachute is opened first. At a time sufficient to slow the missile from a velocity of 1,000 feet per sec to 100 feet per sec, the tail section is separated from the midsection, releasing the main parachute.

Three and one-half seconds later, the nose cone is separated from the midsection, releasing the nose parachute.

When the center section of the missile reaches an altitude of approximately 4,000 feet the sound reproducer system is placed in operation. The center section descends to earth at a rate of 14 feet per sec broadcasting its 3-minute tape recorded message during the descent.

Electronic Equipment

The electronic system consists of magnetic-tape transport, preamplifier, 500-watt power amplifier and battery power supply. The magnetic-tape transport shown in a photograph is a compact light-weight playback unit designed to reproduce messages recorded on ¼-inch plastic tape. Standard 3-inch NARTB spools, capable of holding approximately 200 feet of tape are used to give a total message time of 5.5 minutes at a tape speed of 7.5 inches per second. Signal-to-noise ratio is 60 db with wow and flutter of 0.25 percent. The 6¾ by 5 by 5-in. unit weighs 3 lb 10 oz.

The preamplifier shown in Fig. 1 utilizes a three stage R-C coupled amplifier compensated to give a flat frequency response. This is followed by a 6AL5 diode limiter feeding a fourth stage of amplification which in turn feeds a speech filter designed to obtain maximum intelligibility.

The power amplifier, Fig. 2, has one 12AU7, half of which is used as an amplifier and the second half as a phase inverter feeding a pair of 6AQ5's in push pull. The final stage is a class-AB_1 500-watt amplifier employing two type-813 output tubes. The over-all frequency response of this system, including playback unit, preamplifier and driver to the grids of the 813 amplifier, is flat within ±5 db from 200 to 5,000 cps.

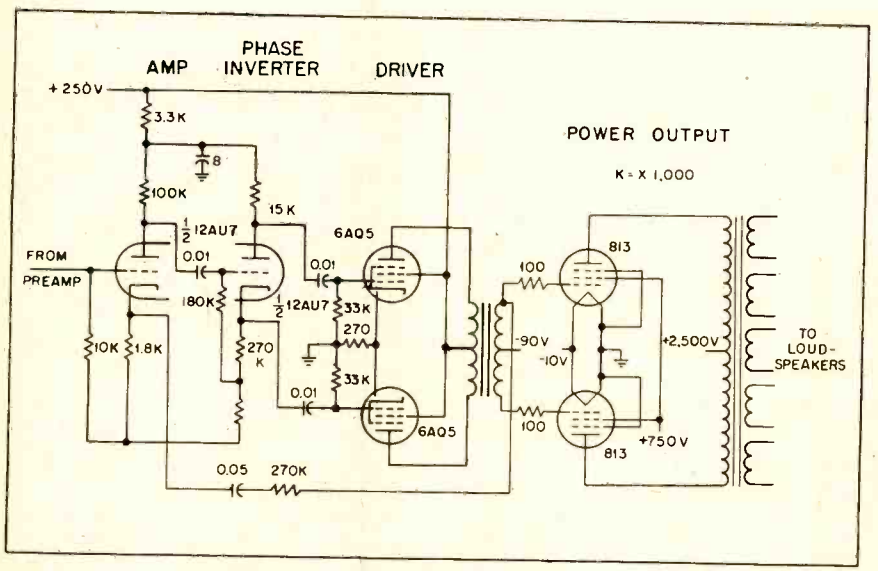


FIG. 2—Two type-813 tubes are used in push-pull to provide 500-watt power-amplifier output to five loudspeaker drivers

Power Source

Voltage requirements of the system are supplied by a mercury-cell battery pack. This high voltage supply consists of 12 series-connected batteries giving a total no-load voltage of 2,880 volts. Each battery contains 180 mercury cells, series-parallel connected to give a no-load voltage of 240 volts per battery and capable of supplying a total load current of 400 ma. Each of the twelve batteries weighs about 20 pounds and is 12 inches high with a four-inch rhombic cross section.

Mercury-cell packs are also used to supply the 90-volt power-amplifier bias voltage and recorder drive-motor requirements. All filament voltage is supplied from five type BB-238 U wet cells.

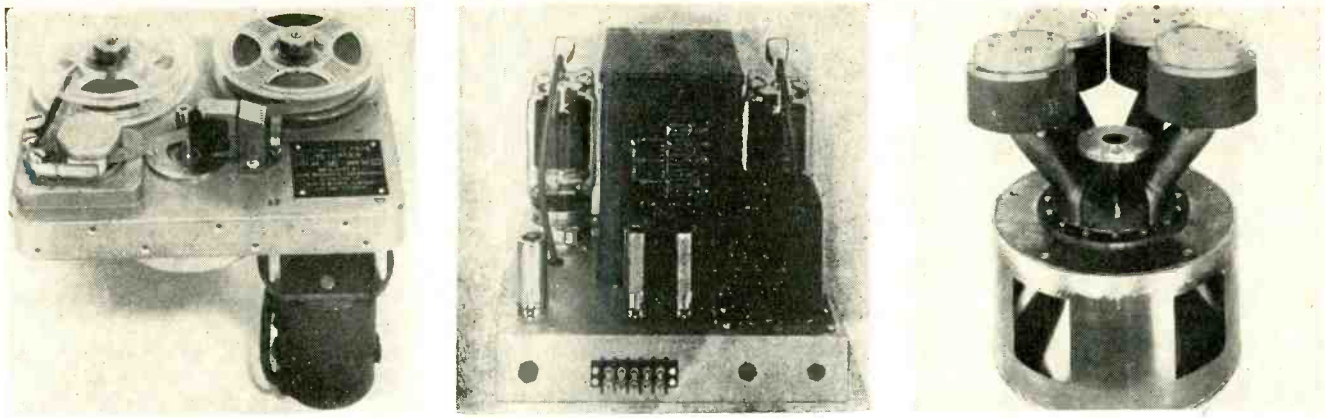
Electroacoustical System

The output of the power amplifier feeds an electroacoustical system located at the nose end of the missile center section. This system utilizes five permanent-magnet drivers.

A brass manifold couples the acoustical output of the five drivers to the horn. This manifold section consists of five identical throat sections with an approximate exponential flare and a cross-section transitional from a circular to a 70-deg pi section curved to accommodate the mounting space requirements of the drive units. The horn taper is exponential and roughly tangent to the throat taper at the matching plane.

This combination results in a satisfactory impedance characteristic over the speech range. A mouth diameter of 15½ inches provides a beam width of approximately 50 deg at 1,000 cps.

In preparing the taped message



Tape player (left), amplifier (center) and loudspeaker drivers (right) are major components of droppable sound system for air-to-ground communications. Tape reels hold enough tape for over five minutes playing time at 7.5 inches per second

used in the reproduction system, speech characteristics are modified for maximum intelligibity. Acoustical flight tests indicate an approximate 6 db per octave frequency attenuation above 600 cps which is corrected by employing frequency preemphasis in the recording process.

With an average power input to the drivers of 500 watts, power peaks in excess of the rated value of the driver units are present. To avoid possible damage to the drivers, speech clipping is employed during recording.

Use of this technique increases the effective sound power output of the system with no degrading effect on the speech intelligibility. A bandpass filter is employed to reduce the output of all frequencies outside of the 300-cps to 3,000-cps speech band.

System Evaluation Tests

System evaluation tests consisted of several missile drops. Reports of 100-percent intelligibility were obtained well outside of the half-mile diameter test circle. An observer located one mile off the speaker axis with the system at an altitude of about 4,000 feet reported 100-percent intelligibility of the message from the sound system even though his hearing was impaired by an intercom head set he was wearing at the time.

The final system evaluation test demonstrated the feasibility of the droppable method of sound transmission by the high intelligibility obtained with less power than is required by the usual airborne systems.

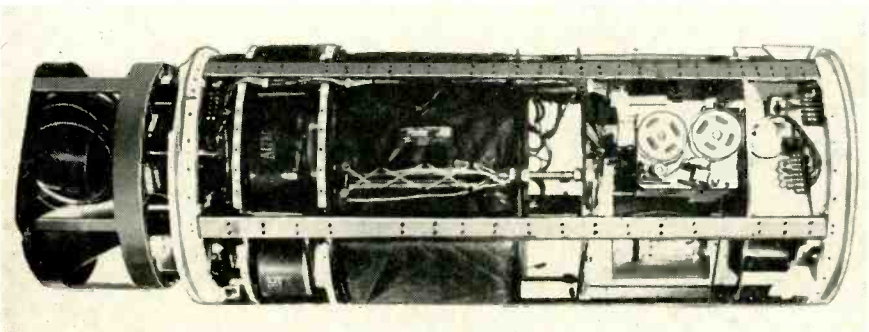
Further Development

Subsequent to the development of the present model of the droppable loudspeaker system, considerable progress has been made in the development of improved air stream modulating horn drivers. In the light of these developments it may be advantageous to incorporate an air-modulating driver into the sound system. Although such a modification would not appreciably reduce the over-all power requirements of the sound system, the resulting pneumatic power source should be more compact and less expensive. In this type of system a 10 to 20-watt audio amplifier would be required for modulating the air stream. An amplifier of this size could be transistorized, effecting a substantial reduction in the size and weight of the amplifier assembly, in addition to lowering the battery voltage requirements for the equipment.

These design changes would result in a lighter and more compact package, which in turn would decrease the requirements of the final descent parachute. A modification of the present assembly could be accomplished which would facilitate handling and transporting the units in a bomb cluster arrangement. It is conceivable that one aircraft could carry and drop as many as ten of these units which could cover a large ground area with a minimum risk as to the loss of aircraft and personnel.

The final model of the loudspeaker system is the result of the coordinated effort of many individuals. Credit is due to F. P. McGowan, C. J. Pelc, James Penick and other members of the Instrumentation Section of the Cook Research Laboratories.

The authors would also like to express their appreciation to members of the Communication and Navigation Laboratory of the Wright Air Development Center who sponsored the work on the droppable loudspeaker system. We are particularly indebted to R. L. Biles, L. Theroux and R. Kellogg for their continued guidance and support.



Audio section of droppable sound system. Loudspeaker horns are at left and tape reproducer at upper right. Padded center section provides heat for batteries

Ground-Controlled Drone

By FORREST WARREN and CARLTON CORDEN

Project Engineer *Systems Group Engineer*
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San Diego, Calif.

SUMMARY — Roll and pitch data systems control drone target used for missile testing at near-sonic speeds. Programmed turns and climb and dive controls permit operator to maneuver plane over preselected course or to test avoidance techniques

MISSILE flight testing requires a target for near-miss attacks capable of speeds comparable to those of a manned aircraft and also capable of changing course to test avoidance of the missile.

The Firebee turbojet drone is a reusable target controlled from the ground. At completion of a test flight, a parachute is released to lower the drone to the ground for recovery.

Control System

An automatic stabilization and control system permits the drone to maintain stable flight and to follow the commands of the remote-control operator. Position of the drone is recorded through a radar tracking system and radar plotting board. Maneuvers are initiated by a remote-control box.

Provisions are incorporated in the airborne part of the control system to receive and decode command signals by means of a radar control receiver and decoder unit. These signals actuate the aircraft control surfaces through the autopilot and control engine throttle.

Stabilization and control of the drone in flight is accomplished by ailerons for roll, elevators for pitch, and rudder for sideslip. The system is shown in Fig. 1. Automatic stabilization is provided about the roll and pitch axes. The sideslip or rudder trim control is commanded by the remote operator.

The autopilot data system consists of two cascades of low-impedance a-c bridges, the roll data system and the pitch data system.

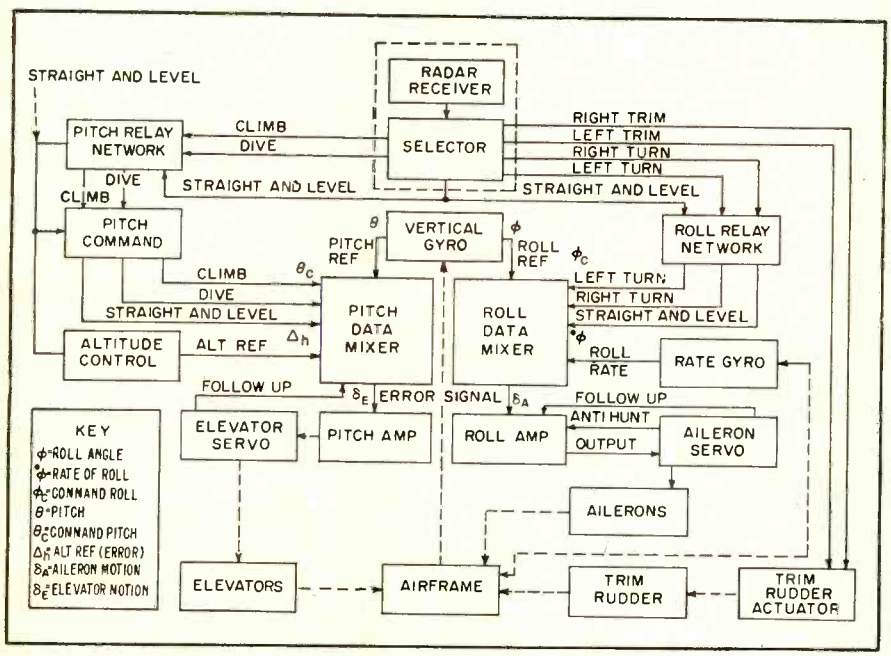

FIG. 1—Block layout of airborne equipment for remote control of drone

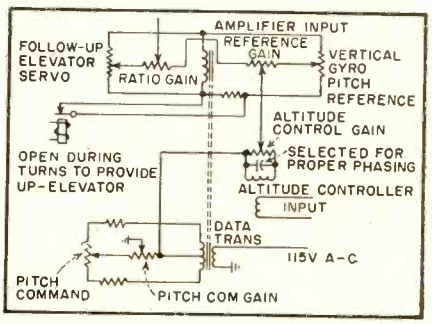

FIG. 2—Displacement bridge of airborne equipment pitch data system is operated from gravity-erecting vertical gyro

The pitch data system, Fig. 2, consists of a displacement bridge which contains the vertical gyro and follow-up pick-offs, a pitch command bridge, and an altitude controller pick-off, the outputs of and follow-up pick-offs, a pitch error signal.

The roll data system shown in Fig. 3 consists of the roll-displacement and roll-rate bridges, and the displacement and rate follow-up units. These outputs are combined to form a roll error signal which is supplied to the roll amplifier.

The functions of the autopilot and remote control system are best illustrated by a typical mission. After release from the mother plane, approximately five seconds is allowed for the drone to pick up sufficient flying speed and to damp out initial launching disturbances. The remote operator then transmits a straight-and-level command.

In the drone, a synchro is clutched to an evacuated aneroid element giving an output propor-

TESTS MISSILES

THE FRONT COVER

Turbojet drone dropped from plane is ground-controlled target for missile tests

tional to deviations from the reference altitude at which the straight and level command was transmitted. The output of the altitude controller is combined with the pitch attitude and elevator position signal to provide the elevator trim position necessary to maintain level flight.

When sufficient airspeed has been attained, a climb command is transmitted by the operator.

In the drone, the climb signal actuates a motor driving a potentiometer in the pitch data system and introduces an error voltage to the vertical gyro. Balance in the data system is achieved when the drone assumes the commanded pitch attitude. During climbs, the altitude controller is rendered inactive. Prior to transmitting a turn command, the operator commands straight-and-level. This allows the drone to level out and regain airspeed lost during the climb.

A left-turn command is transmitted by momentarily holding the control stick to the left. In the drone, the left-turn relay is locked electrically through the climb, dive, and straight-and-level relays. In the event that the pilot does not command straight-and-level before the turn, the altitude controller will be automatically engaged. Closure of the turn relay creates an unbalance in the roll-data system containing the vertical gyro and the roll-rate gyro. Simultaneously, the pitch system is unbalanced slightly to provide up-elevator.

The angle of bank is preset to 45 deg at altitudes below 30,000 ft and 30 deg above 30,000 ft. An bank angle is normally selected automatically by a barometric switch in the drone. The turn will continue until a straight and level, climb or dive command is given.

Vertical Turn

Due to the high speed of the drone, conventional horizontal turns were not considered desirable because of the excessive time required to perform a course reversal. A programmed vertical turn was decided upon.

This required gyro precession about both axes on command. This unit acts as a normal data reference to furnish roll and pitch information. When a course reversal is commanded, a program timer takes control and the gyro is precessed in pitch to cause the drone to perform a partial loop. The gyro is then precessed in roll, righting the airplane, and ultimately pulling up to level the drone at approximately the same altitude as at start of turn, but in reverse heading.

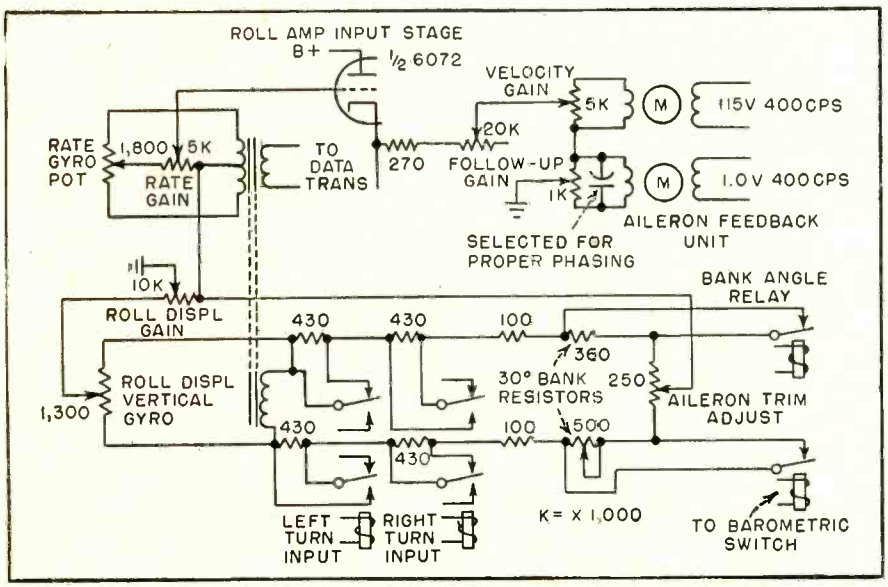

FIG. 3—Roll data section is controlled by vertical gyro and roll rate gyro

Wide-Range Analyzer

SUMMARY ——Sweep generator in conjunction with heterodyne sprectrum analyzer measures attenuation characteristics of frequency-selective networks. Equipment can measure band-stop regions down to attenuations of 100 db within the range of 20 cps to 20 kilocycles. Bandwidths below 10 cps are obtainable

MEASUREMENT of attenuation characteristics of filters and other frequency selective networks is facilitated by a composite instrument comprising a swept heterodyne spectrum analyzer used as an indicator for a sweep generator.

By placing a network between the generator and the indicator, curves may be traced showing relative gain against frequency.

This system responds to fundamental components only because of the tuned indicator. Hence harmonics, hum and other spurious are effectively eliminated from the transfer functions plotted.

The function of the audio sweeper and audio analyzer shown in block form in Fig. 1 is to convert the output of the swept r-f oscillator to the audio band and present it at a uniform amplitude and convenient impedance level.

Other bands may be examined with similar instruments.

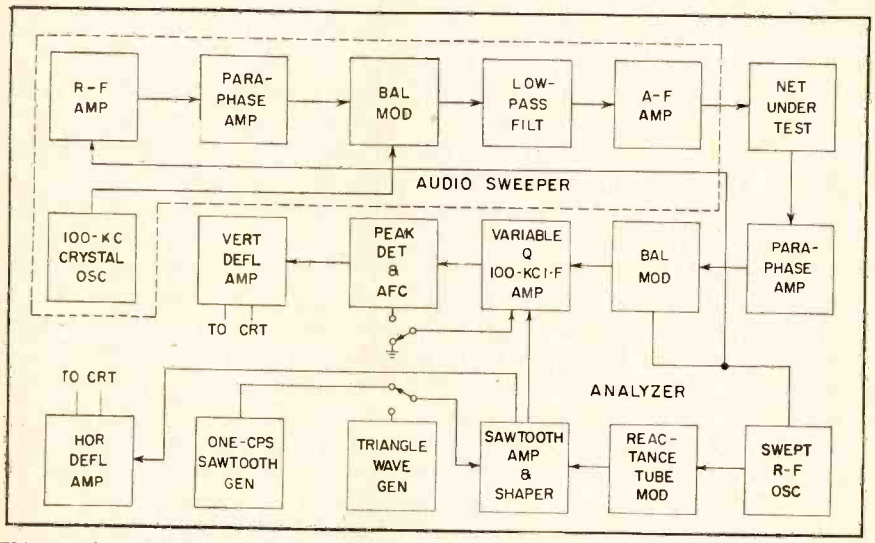

FIG. 1—Block diagram of audio sweeper and network analyzer

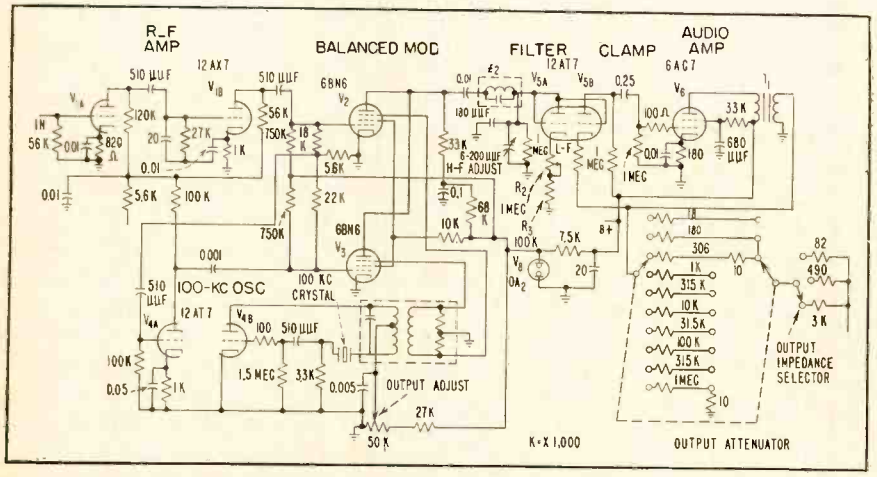

FIG. 2—Slave sweeper provides signal to drive network under test

System

By heterodyning the swept r-f oscillator output with a fixed frequency equal to the analyzer i-f, the difference frequency arithmetically tracks the frequency being examined by the analyzer. Adjusting the inductance Z_1 of the crystal-controlled oscillator in the sweeper unit of Fig. 2 for maximum amplitude on the crt shifts the fixed beat frequency for precise registration that occurs when the crystal-oscillator frequency is at the center of the i-f bandpass.

Thus the panoramic indicator is locked to the sweeper output and samples a small band defined by plus and minus one-half the i-f bandwidth about the instantaneous output frequency.

The operating controls which determine the center frequency, sweep width and choice of linear or logarithmic scanning modes are located on the analyzer. They provide adjustment of the swept oscillator frequency excursions and self-frequency.

The sawtooth modulating wave is obtained from the external triangular-wave generator or the one-cps time-base generator. It also drives the horizontal deflection stages and establishes a calibrated linear incremental or directly read logarithmic frequency scale on the crt.

The sweeper unit input stage

Traces Precise Curves

By EDWARD F. FELDMAN

Senior Engineer
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Mount Vernon, New York

Panoramic sonic analyzer serves as selective indicator for sweep generator in the 20 to 20,000-cps range when measuring attenuation characteristics of networks

V1A is an r-f amplifier operating in the 80-100-kc band. It is driven at low level from a loosely coupled secondary winding on Z_7 in the analyzer of Fig. 3 to preclude excessive loading and potential oscillator instability. After further amplification and phase splitting in V_{1B} and V_{4A}, the conversion to audio is effected in the pair of 6BN6's, V_2 and V_3 arranged as balanced modulators.

The modulator-tube suppressor grids are driven in opposite phase through the transformer-coupled output of the crystal-controlled 100-kc oscillator V_{4B}. Suppression of the high-level 100-kc component is vital to prevent over-driving the output amplifiers and to minimize i-f response in the analyzer. Network, Z_2, is parallel tuned to 100 kc and constitutes the voltage divider, with C_1 and C_2, which attenuates any unbalanced i-f output of the modulators. These capacitors also form a series resonant combination with the inductor of the r-f trap in the coil.

Capacitor C_2 adjusts the amount of treble boost.

The combination of C_2 and R_2 plus R_3 in parallel with R_1 is aligned for optimum bass frequency response. The diode connection of V_{5A} in conjunction with C_3 is a clamp tending to hold the grid of the audio amplifier V_{5B} negative to prevent horizontal oscillator flyback pulses, which cause shock transients in the output, from drawing grid current causing a minor blocking condition affecting gain.

The feedback from the secondary of T_1 to the cathode of V_{5B} serves to improve the bass response by counteracting the transformer low-end fall-off. Overall response is within 1 db to 40 cps and to 20 cps is within 3 db of mid-band gain. Harmonic distortion introduced by the diode does not deteriorate the instrument response as traced on the selective indicator because of the narrow-band i-f filter. With a minimum dual-stage bandwidth of 10 cps, sufficient harmonic rejection may be obtained fundamentals down to 20 cps.

A range of 100 db in steps of 10 is obtained in the output attenuator. Looking back from the output impedance selector, the impedance is roughly 20 ohms at all attenuator settings. The nominal output impedances provided are 100, 500 and 3,000 ohms.

Receiver

The analyzer, shown in Fig. 3, is a superheterodyne receiver with its local oscillator periodically frequency modulated. Audio frequency input signals are attenuated and divided into two equal and opposite components which feed the grids of the balanced modulators, V_3 and V_4. The local oscillator V_{15A} output is connected to the common cathodes of the 6SJ7 converters. Signal frequencies and heterodyne difference components are produced push-pull while the in-phase local oscillator outputs cancel in the plate circuits.

The 100-kc modulator output

Rack-mounted triangular-wave generator and signal alternator provide variable scan and ability to compare signals for precise measurements

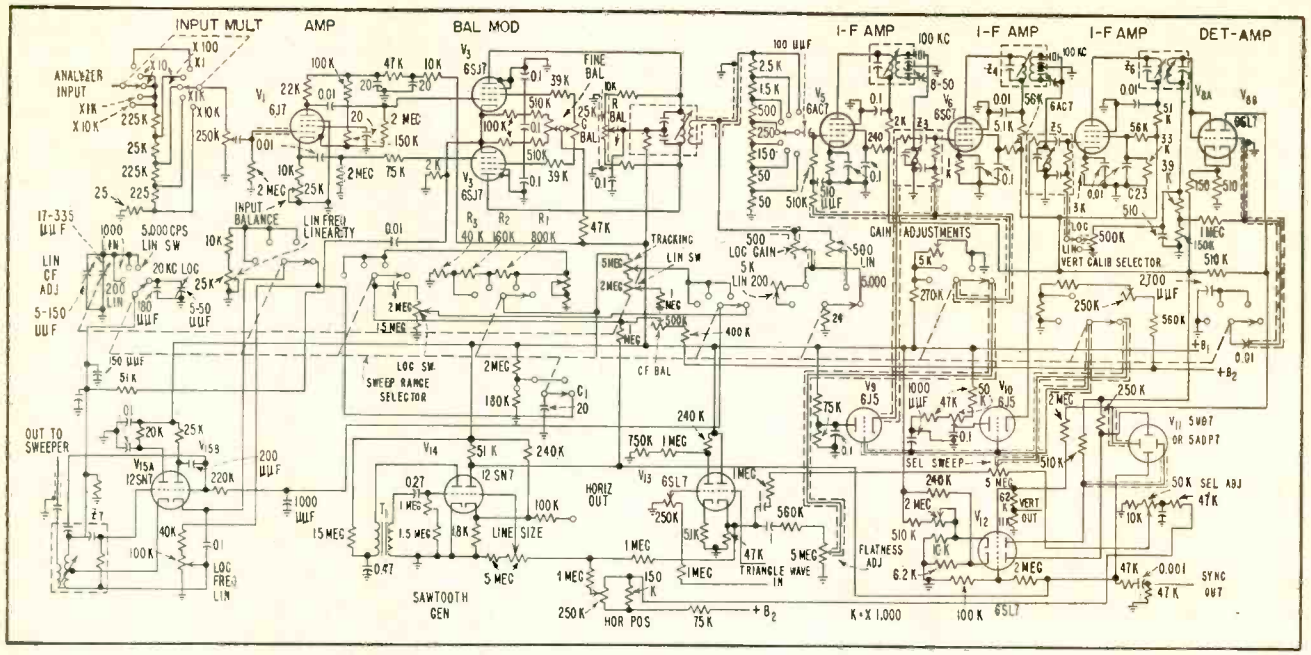


FIG. 3—Analyzer accepts input from network under test and displays its response

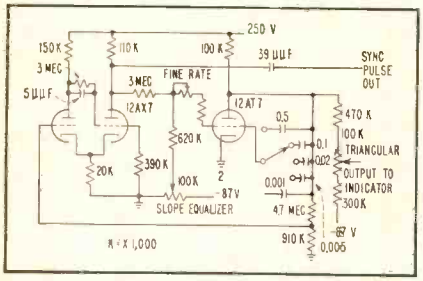


FIG. 4—Triangular-wave generator provides accurate sweep for indicator

eliminates any response to the input frequencies. The balance controls are adjusted for minimum local oscillator response near zero frequency where it sweeps through the i-f.

A Miller-effect reactance stage, V_{15B}, is connected across the tank circuit of the grounded plate local oscillator. As the sawtooth waveform from the time base generator drives the reactor grid, the impressed tuning capacitance varies directly as the instantaneous gain multiplied by the plate to grid capacitance. The 200 $\mu\mu$f capacitor serves to multiply the inherent Miller effect of the triode reactance tube.

Scanning Modes

Logarithmic frequency scan from 40 cps to 30 kc is obtained by addition of an integrating R-C network in the cathode of the reactor including the 20 μf capacitor, C_1. The ±10 percent ferquency modulation of the local oscillator is in excess of the usually achieved linear excursion with a high-Q reactance network. Since curvature of μ and r_p characteristics of the triode affect the resultant frequency calibration over the broad band utilized in the log sweep, each crt screen is plotted individually.

Only the one-cps scan rate derived from the sawtooth generator, V_{14}, may be employed with the broad-band log scan because of the dependence of the reactor integrator network upon sweep time. The variable-rate bidirectional sweep mode could not be used with the nonlinear scan mode because the forward and return traces would not coincide.

Expanded linear analysis provides magnification of a small spectrum to note critical regions. Excursions of 5-kc, 1-kc and 200 cps are provided with continuously variable center frequency from 0 through 20 kc. The sweep widths are fixed by the resistor divider chain, R_1, R_2, and R_3 which pick off the desired fractions of the sawtooth amplitude.

Bandwidth of the i-f amplifiers is determined by the dual 100-kc crystal filters of V_8 and V_9. A pair of cathode follows V_9 and V_{10} reflect the variable resistance into the i-f crystal loading network and govern the overall Q.

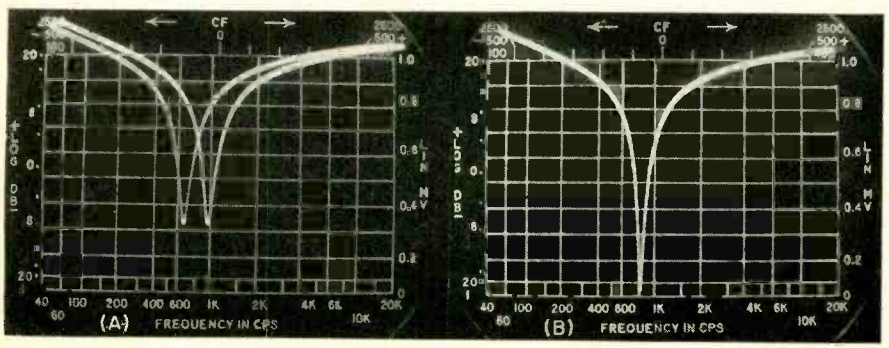


FIG. 5—Curves show excessive forward and reverse scan rate (A) and correct scan rate (B) to see proper response of network

Selectivity

During the logarithmic sweep, with varying instantaneous rates of scan, the selectivity is increased synchronously as the low end of

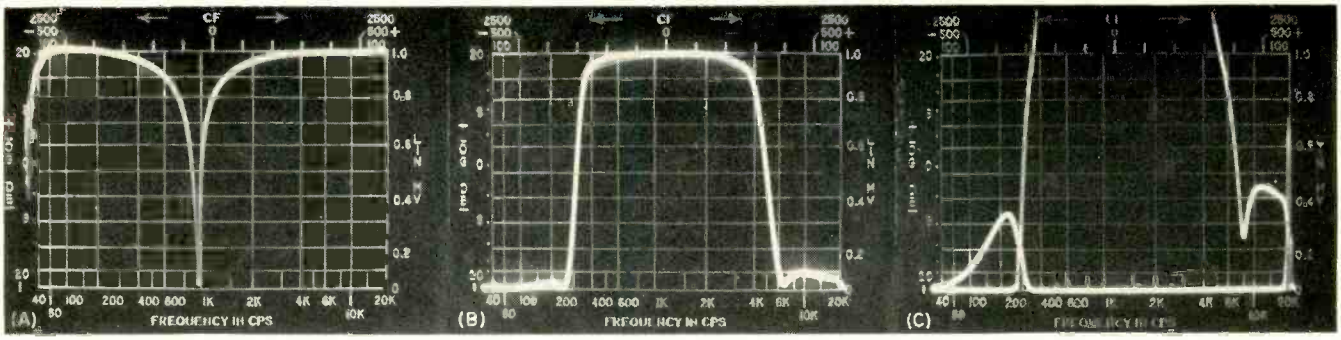


FIG. 6—Curves show log-log response of active R-C filter (A), f-m/f-m telemetry subcarrier filter response (B) on linear frequency and logarithmic amplitude scales and same response (C) with indicator gain 20-db higher

the audio spectrum is approached. A shaped sawtooth from the time-base generator drives the grids of the selectivity modulators V_9 and V_{10}. On linear scans, i-f bandwidths are fixed by a d-c grid potential on these tubes in accordance with the sweep width selected.

In curve tracing, the requirements for selectivity depend upon the nature of possible spurious components such as harmonics, hum, noise and upon the frequency being examined. Generally, lower frequencies should employ a narrower i-f. The bandwidths obtainable are reducible to values below 10 cps.

Excessive selectivity increases the requisite sweep period because of the greater time constant associated with a smaller i-f bandwidth.

Following the last i-f amplifier is a peak detector using a diode-connected 6SL7 to convert the variable amplitude i-f envelopes into a proportionate d-c level to drive the push-pull vertical deflection amplifiers, V_{8B} and V_{12A}. The single line presentation or response curves represents no particular problem when demodulation is effected at an r-f intermediate frequency.

Triangular-Wave Generator

The use of a variable-speed-scan symmetrical triangular waveform is almost mandatory for precise measurements at rates which are commensurable with a-f transient periods. Since the delays are always in the direction of the scan, the bidirectional linear mode shows a dual trace when the rate is excessive. Adjusting the sweep-rate frequency downward until virtual superimposition of the two responses is obtained, assures the fastest writing rate consistent with accuracy.

The triangular-wave generator shown in Fig. 4 is designed so the output amplitude is the critical parameter in switching between two stable states in a trigger circuit. Line size and sweep width are thus maintained constant with sweep rate.

Hysteresis

Operation of the 12AX7 trigger stage depends upon hysteresis effect in a multivibrator. If the plate voltage of the 12AT7 Miller integrator is rising, feedback level at the control grid of the 12AX7 will rise proportionately. At the critical level, the driven section of the 12AX7 will be turned on, lowering its plate voltage.

The second section grid voltage is lowered causing the second section to conduct less, lowering the cathode potential and causing a rapid regenerative action. The second plate level assumes the cutoff value near the supply voltage of 250 v. this tends to raise the grid voltage of the integrator. The integrator characteristic is such that the final value of plate and grid voltage is approached exponentially.

The integrator plate voltage drops therefore to approach the quiescent level determined by the impressed grid voltage. In a small fraction of the equivalent time constant the lower level on the trigger circuit reaches the cutoff point thus reversing the action. The output waveform is linear because only the initial section of the charging curve is used.

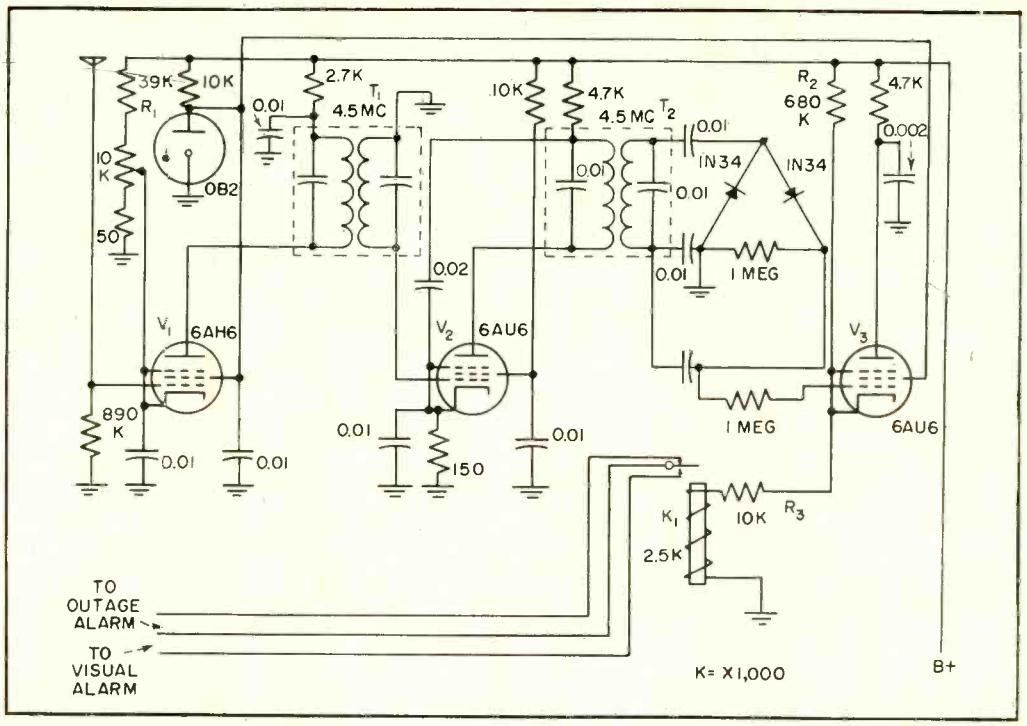
The slope equalizer control serves to set the average bias so that the two values of V_t are equidistant from their respective initial voltages. It is set visually by adjusting the 100,000 ohm potentiometer for equal forward and reverse rates as seen in Fig. 5.

With the charging capacitors indicated, the scan rates are variable between 60 a sec and one in 25 sec with no change in line size. With low-leakage capacitors the periods have been increased to 15 minutes. Measurements have been made on dynamic shaker systems in which mechanical resonances were so selective as to require several minutes of scan even at a reduced sweep width when the sweeper was used to excite the armature power amplifier. These automatic sweeping techniques are in use for setting driving-point equalization networks in the random vibration systems specified for airborne structures.

Operation

The analyzer cro presentation shown in Fig. 6A indicates that the horizontal axis contains both logarithmic and linear frequency scales. The former is read on the lower portion of the screen and is intended for rapid overall surveys of many octaves (40 cps to 20 kc).

Figure 6B and 6C show that by increasing gain so the bandpass of the tested network exceeds full-scale deflection by an amount set by front panel calibrated attenuators, band-stop regions may be precisely examined down to attenuations exceeding 100 db. This range is limited by spurious components contained within the bandpass of the analyzer i-f.



Circuit diagram of the heterodyne detector with power supply omitted for simplicity

INTERCARRIER FAILURE RINGS ALARM

SUMMARY —— Receiver detects beats between picture carrier and sound carrier displaced 4.5 mc from it. Failure of either or both carriers resulting in absence of intercarrier frequency sounds alarm and starts outage recorder

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ACCURATE records of the time and duration of carrier failure at a tv transmitter are required by the Federal Communications Commission. The device described below will obtain this information automatically. An alarm or signal light can also be actuated to warn of failure.

The carriers of picture and sound transmitters that comprise the complete tv transmitter have a separation in frequency of 4.5 mc. At KSL-TV there are two separate tv transmitters—one for standby service. Such an arrangement gives four possible combinations of picture and sound transmitters. A device was desirable that would be as simple as possible and yet work with any pair of transmitters.

Two-Signal Device

The circuit used works on the superheterodyne principle with the two transmitters acting as the two oscillators. Signals from the two carriers are applied to the grid of V_1. This tube is a remote cutoff type, so the gain of this stage is controlled by the setting of R_1, which adjusts the bias. Since V_1 has a nonlinear characteristic, especially if driven past cutoff, the two signals are mixed in it.

The output of V_1 is fed to T_1, which is tuned to the frequency difference of the two signals. This 4.5-mc signal is further amplified by V_2. Output from V_2 is fed through the tuned circuit T_2 to the detector. The detector consists of two crystal diodes connected in a voltage-doubling circuit.

The voltage-regulator tube controls the voltage applied to the screen grids of V_1 and V_2. The pentode cutoff characteristics are sharper if the screen grid is maintained at a constant value.

Tube V_3 is biased to cutoff through the voltage divider action of R_2, R_3 and the coil of K_1. A current of about 0.4 ma flows through

* Work done while author was employed at KSL-TV

K_1 when V_3 is cut off. When a signal is applied to the detector, a positive voltage is produced that raises the voltage on the grid of V_3 to a conducting state. With V_3 conducting, the current through the relay coil is increased to 2.4 ma or more, depending on the strength of 4.5-mc signal received. The relay closes.

The power supply is a conventional choke-input type to keep the B + voltage down to about 200 v.

Signal Failure

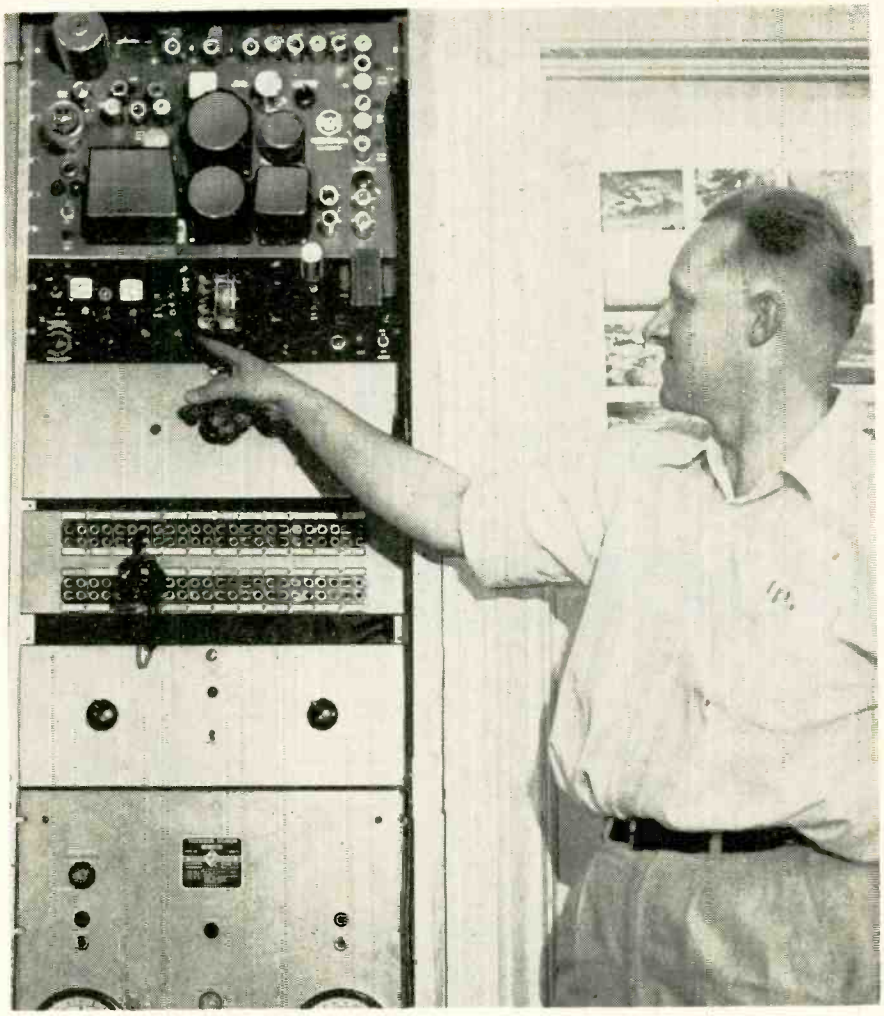
If either carrier drops out, no 4.5-mc signal is produced and V_3 is cut off. Relay K_1 opens. Loss of a tube or a blown fuse will also allow the relay to open. The circuit will thus give an alarm if part of the circuit itself fails. An outage clock unit is available that gives the time outage occurred and the duration of the outage. This unit must be actuated through the relay contacts by an outside source. The relay is also used to actuate a light circuit or an aural signal such as a bell.

Since the monitor unit is used at the transmitter site a strong signal is available to feed it. A simple half-wave antenna tuned to the tv carrier picks up plenty of voltage to actuate the circuit. An inside antenna was tried first, but in the steel building where this transmitter is located, a great variation of signal strength was found as the antenna was moved.

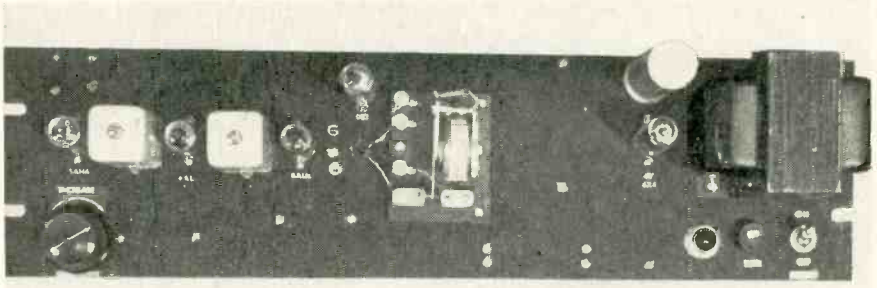
The strength at any one place was found to vary with sound modulation or with the movement of a person near the antenna. This effect was undoubtedly caused by changes of the standing-wave pattern with changes of the sound frequency or the placement of obstacles to the waves.

When an outside antenna was used, a good strong signal was available. Input impedance to the unit is high and a great mismatch to the antenna will result. This mismatch need not be bothersome if the transmission line is cut to a length such that maximum voltage is observed at the input to the unit.

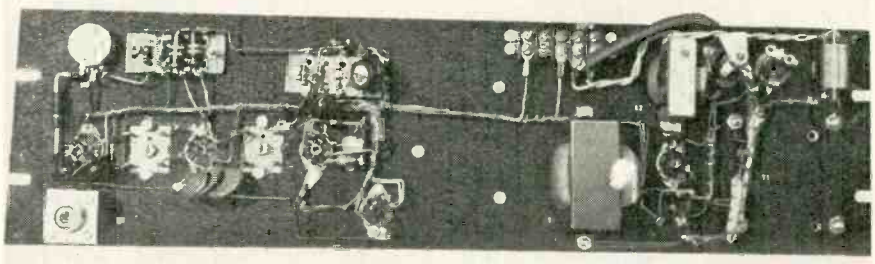
Tuning the circuit can be accomplished by placing a vacuum-tube voltmeter across the detector and tuning for maximum direct voltage out with both transmitters on.



Failure of picture or sound carrier is detected by unit mounted in cabinet with other tv transmitter monitoring equipment



Sensitivity control (left) adjusts operation of relay device (center). Power supply is at right



Reverse of panel shows mounting of r-f components (left). Remainder of power supply components (right)

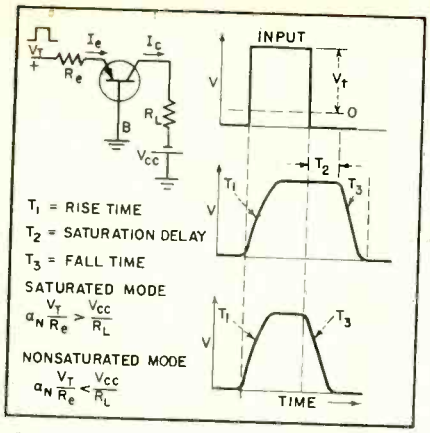


FIG. 1—Response time with storage delay (middle curve) and no delay (lower curve)

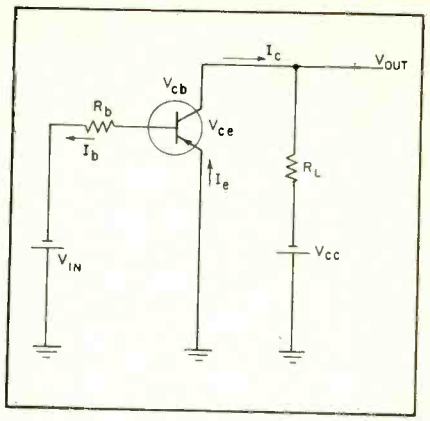


FIG. 2—Back-clamping technique giving voltage gain along with good efficiency

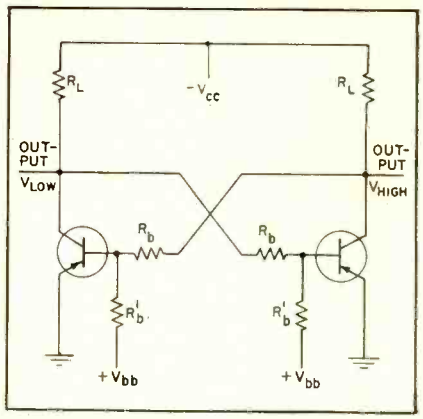


FIG. 3—Bistable saturated circuit is less efficient at low output power

BOOSTING TRANSISTOR

By RICHARD H. BAKER

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Lincoln Laboratory, Cambridge, Mass.

SUMMARY — Transistor properties affecting response time in switching circuits are summarized and basic circuits given for obtaining maximum energy conversion efficiency. Combined use of pnp and npn transistors gives circuit symmetry that utilizes inherent advantages of transistors. Other circuits include saturated and nonsaturated current-demand flip-flops with single or double triggering, designed for maximum reliability despite normal variations in circuit constants and input pulses

THE NORMAL three-region junction transistor (excluding graded-base or drift types) is a slow device when compared to a vacuum-tube triode. In a tube, the movement of electrons from cathode to plate is aided by strong electric fields, whereas in a transistor the transport of carriers (electrons or holes) is only by diffusion.

In designing transistor circuits for high-speed switching, the designer must consider normal integrative effects due to shunt capacitances as well as the delay or carrier transit time between emitter and collector. When the transistor is operated in the saturated mode, there exists an additional effect, that of hole storage or saturation delay.

Response Times

There may be as many as three separate response times, depending upon the mode of operation, associated with a single-stage transistor network. These are rise time, storage or saturation delay and fall time, all shown in Fig. 1. If R_L, R_e, V_{cc} and V_T are chosen so that the voltage polarity across the collector junction maintains the collector junction under reverse bias at the peak of the output pulse, the saturation delay vanishes.

The magnitudes of response times T_1, T_2 and T_3 are different for each of the three basic connections. In all modes of operation, however, the transistor switching time is dependent on the constants of the device and the amount of overdrive supplied at the input.

The single most important factor affecting the switching time is the frequency response of the device itself. Also, minimum response time occurs when current gain α_N is 1.

There is promise of obtaining high-frequency transistors by using graded-base structures and other configurations. However, the interim solution of transistor manufacturers has been to build transistors with very narrow base widths to increase the frequency response. This approach is fruitful to a degree, but there is an op-

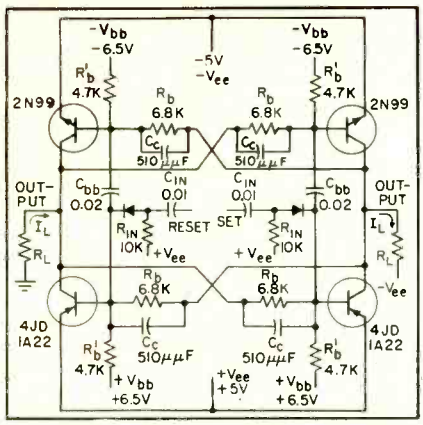


FIG. 4—Saturated current-demand single-triggering circuit with 1-mc transistors

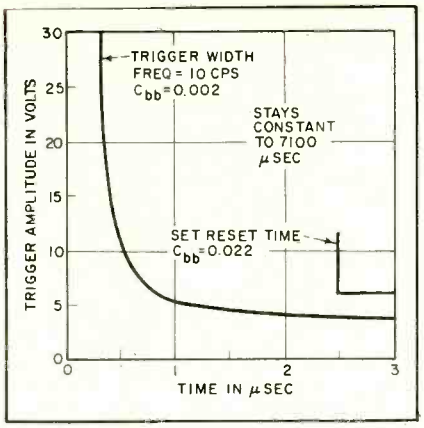


FIG. 5—Characteristics of single-triggering circuit of Fig. 4

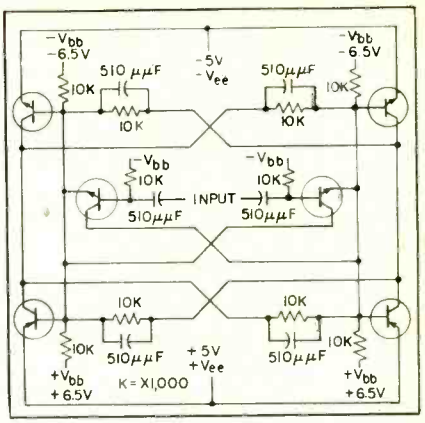


FIG. 6—Saturated current-demand flip-flop double-triggering with 1-mc transistors

SWITCHING SPEED

timum base width that yields minimum switching time for practical switching circuits. This optimum base width is generally different for each of the three basic connections.

In transistor circuits the transit time of the carrier across the base region imposes an absolute minimum input pulse width. This in turn sets rather large minimum capacitance values in a given circuit, creating recovery time problems that may be more serious than actual rise time considerations.

Signal Levels

Because transistors are extremely efficient voltagewise, the system levels are usually set by a combination of system and transistor considerations.

The low voltage limit is automatically set if the transistors are allowed to saturate, this being primarily determined by speed considerations.

The upper voltage limit is set by the total power consumption of the system and by the punch-through and avalanche phenomena in the transistor.

The signal voltage swing in an all-transistor system is usually chosen as a compromise between two inherent opposing effects. As the signal level increases (total swing), the amount of energy dissipated in charging and discharging capacitance increases. This effect indicates that the signal level should be low. On the other hand, for convenience of circuit design the signal level should be large compared with the transistor off-on uncertainty region, which is about 0.2 volt for germanium transistors and about 1 volt for silicon transistors.

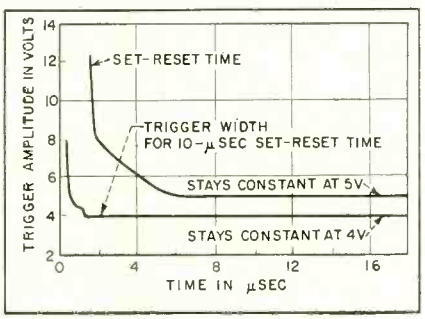


FIG. 7—Characteristics of double-triggering circuit of Fig. 6

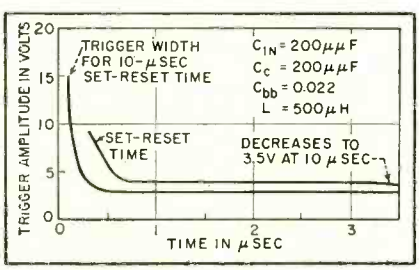


FIG. 8—Characteristics of double-triggering circuit using 5-mc transistors

Energy Conversion Efficiency

Fundamentally the transistor, like the vacuum tube, has gain by virtue of dissipation changes. Unlike the vacuum tube, the input impedance is much lower than the output impedance. In the design of realistic transistor systems, then, a serious problem arises in the available power to drive succeeding stages. This situation is aggravated still further in the design of high-speed systems, since it is necessary in the transient state to overdrive the stages to obtain fast switching. This fact, more than any other, accounts for the large number of transistors required to build transistor systems compared with equivalent vacuum-tube systems.

These considerations indicate that circuitry should be designed to deliver maximum output power and that a high percentage of the available output power should be available to drive other transistors. Further, since currently available high-frequency transistors are ex-

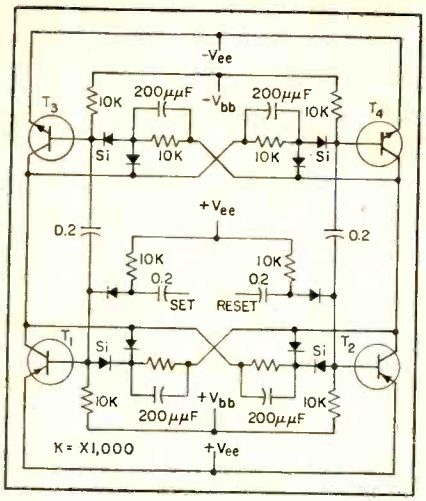


FIG. 9—Nonsaturated current-demand single-triggering flip-flop

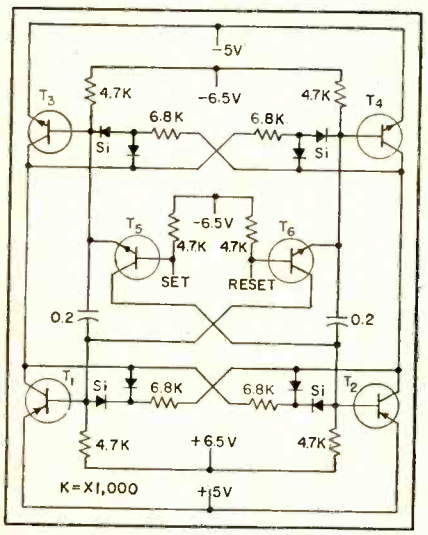


FIG. 10—High-speed nonsaturated current-demand double-triggering flip-flop

tremely low-power devices (on the order of 0.5 mc-watt as a figure of merit for SBT-100 at 50 mc and 10 mw), circuitry should be designed to give highest possible energy conversion efficiency. The ratio n_1 of useful signal output power to transistor dissipation should therefore approach infinity.

For optimum circuit design of a minimum-power-drain system, the ratio n_2 of useful signal output power to power supply drain should approach 1.

The product of n_1 and n_2 should be made as large as possible. The ratio represented by n_1 can be made large by allowing the transistor to saturate or by controlling the voltage from collector to base through the use of clamping diodes. However, minimum-power systems can be built only by making n_2 close to unity (this must be true if there exists a minimum power level to process intelligence).

In most present transistor circuit designs, a high percentage of useful output power from the transistor is dissipated in the load resistors. This is especially true for direct-coupled logic. Therefore, the value of n_2 may be increased significantly by removing the standby power dissipated in this area.

The circuit design techniques in the following sections show how the values of n_1 and n_2 may be increased to give minimum power dissipation, maximum speed and minimum sensitivity to component and transistor drift circuits.

Maximum-Efficiency Circuits

Aside from eliminating the power dissipated in load resistors, an additional gain in system power efficiency may be obtained by using circuits that draw power from the supplies according to the power and demand at the output. This process always involves feedback. Cathode-follower and emitter-follower (grounded-collector) circuits do this, but unfortunately have no voltage gain.

A transistor circuit involving voltage gain, along with an ability to convert d-c power into signal power as required by the load, is shown in Fig. 2. The transistor dissipation is low and the output power is high for collector currents less than the maximum output current. The major portion of the power drawn from the supplies is available at the output for dissipation in the load resistor, so that n_2 approaches 1 and the circuit draws from the supplies only the power dissipated in R_L and R_b (neglecting transistor dissipation). The only transistor parameter of importance in the conducting state is the minimum base-to-collector current gain β_N.

To illustrate the design of this circuit, assume that β_N is 20, input d-c voltage V_{in} is 5 volts, transistor saturated base resistance r_b is 50 ohms, V_{cc} is 10 volts, R_b is 10,000 ohms and R_L is 1,000 ohms. Then I_b is about 0.5 ma, $I_{c\,max}$ is 10 ma and I_e is the sum of these or 10.5 ma. Useful signal output power is $\frac{1}{2} V_{cc} I_e$ or 50 mw and transistor dissipation is 10.5×0.2 mw, so that n_1 is about 24. Power supply drain is 50 mw + 2.5 mw, so that n_2 is about 0.95.

Two of the circuits of Fig. 2 may be coupled together, with only slight modification, to form the bistable circuit of Fig. 3. This has several drawbacks, however. The low-voltage level is not fixed, being dependent on I_{co} and other factors. The power dissipated in internal load resistor R_L (in shunt with the actual load) may be an appreciable percentage, particularly at low output power levels. For fast fall time (when the transistor is turned off), R_L must be made small.

Current-Demand Circuit

A circuit that circumvents these disadvantages is shown in Fig. 4. Here essentially all of the output current (collector current) is available to drive load R_L.

Standby power is low; when there is no load, the power taken from the supplies is approximately equal to the dissipation $2 I_b^2 R_b$ in the base resistors. Both the high and low voltages are clamped (the transistors saturate). The

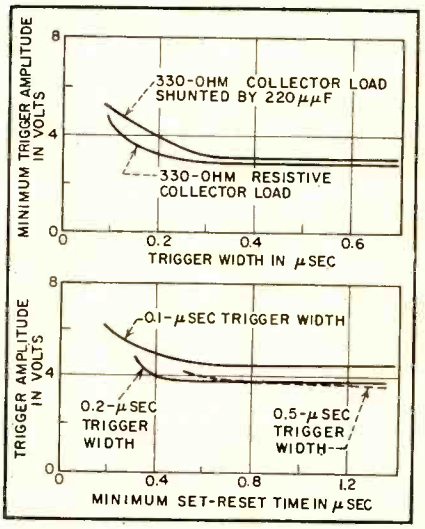


FIG. 11—Triggering characteristics of flip-flop of Fig. 10

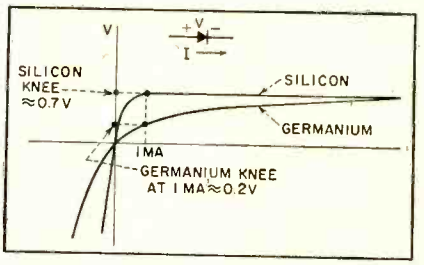


FIG. 12—Diode characteristic curves

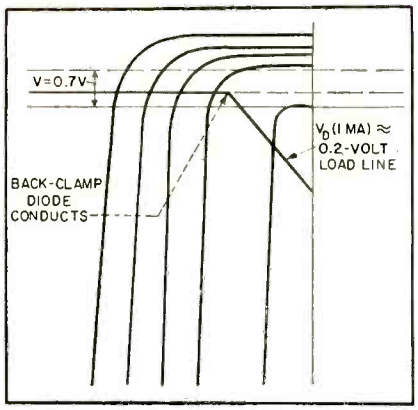


FIG. 13—Family of collector curves for silicon transistor

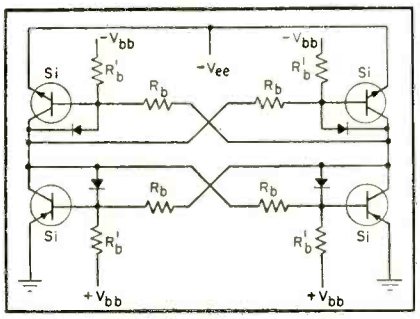


FIG. 14—Basic silicon transistor circuit for nonsaturated current-demand flip-flop

tolerance on all resistors may be large (on the order of 50 percent).

Circuit operation is substantially independent of transistor parameters. The stability of the configuration is insensitive to supply voltages. The configuration leads to fast rise and fall time since large transistor overdrive is inherent. The last three advantages accrue because the configuration allows the transistors to set their own levels. Some of the operating characteristics of the circuit are shown in Fig. 5.

One difficulty with the circuit of Fig. 4 is that there is an appreciable delay around the loop because the conducting transistors are saturated. This difficulty may be minimized by double triggering (triggering all four transistors simultaneously). The current-demand flip-flop circuit of Fig. 6, employing this feature, gives the characteristics shown in Fig. 7. By using 5-mc transistors in this circuit and changing all 510-$\mu\mu$f capacitors to 200 $\mu\mu$f, the characteristics of Fig. 8 can be obtained.

The circuit techniques described may be extended to nonsaturating circuits. The primary gain in designing the circuits to operate in the nonsaturating mode is decreased switching time. Figure 9 shows a typical design using the nonsaturated configuration with single triggering. Figure 10 shows a higher-speed version using double triggering, and Fig. 11 gives triggering conditions for the circuit. The diode characteristics in Fig. 12 show why these back-clamped circuits do not allow the transistors to be saturated.

If silicon transistors are used, the nonsaturated circuits do not require the four silicon diodes. This may be seen from the silicon collector curves in Fig. 13. The basic circuit using silicon transistors is shown in Fig. 14.

The salient features of the saturated back-clamping current-demand technique are low transistor dissipation, high conversion efficiency, insensitivity to component and transistor parameters (standby load resistors not needed), insensitivity to voltage supply drift, maximum system efficiency (power drawn from supplies according to needs of load), fast rise and fall time (inherent overdrive) and loop delay (caused by saturation time). Nonsaturated circuits give increased operating speed because they have no saturation delay, but are otherwise identical.

Gating Circuits

The design of maximum-reliability switching systems depends heavily upon the reliability of the voltage-pulse voltage-level gate. To assure maximum system reliability (assure positive action and suppress superfluous triggering), the gate circuits should be independent of pulse width, pulse amplitude, pulse repetition frequency and pulse level (within given limits), and should have fast response to pulse and level changes. The circuit design should also be insensitive to component values and transistor parameters, require minimum standby power, have high output power, present a constant load to the pulse source (driver) and deliver standardized output pulse and level amplitudes.

A circuit configuration that fulfills to a high degree the above reliability characteristics is shown in Fig. 15 along with its gating waveforms.

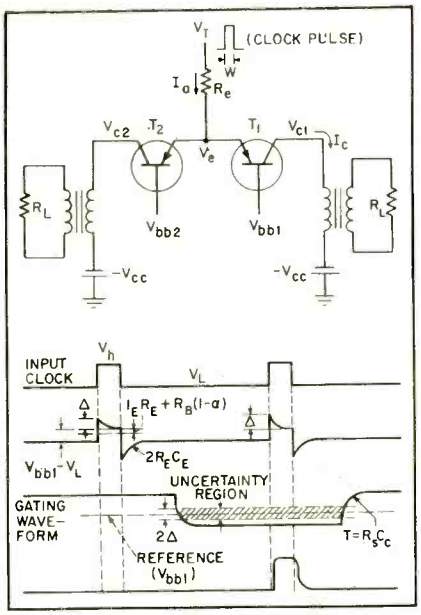


FIG. 15—Circuit and waveforms of pulse-level gating circuit

Conclusions

The reliability of transistor switching systems is closely related to the design of circuits. The circuit designer must consider the drift of operating points caused by aging and ambient self-generated temperature changes. For high-speed networks, due to the lack of high-speed transistors, overdrive must be used to speed up the circuit response.

Transistors are inherently efficient devices (both voltagewise and powerwise). This, along with the fact that two types of transistors are available (*npn* and *pnp*), allows circuit design that is extremely efficient in terms of power supply drain for a given signal power output.

The transistor, being an efficient, reliable and small device, may be soldered into systems much as are ordinary resistors and capacitors. This, plus the fact that it is basically a three-terminal passive device which can produce power gain, makes its use attractive in networks where feedback techniques are widely employed.

The research work herein described was supported jointly by the Army, Navy and Air Force under contract with Massachusetts Institute of Technology.

Dual-Triode Tester

By RONALD L. IVES

Palo Alto, Calif.

SUMMARY —— Zero-balance meter indicates the static and dynamic characteristics of any dual-triode, simplifying tube selection for critical requirements. Circuit uses difference-amplifier bridge with complex-wiring connections from pin-terminals of four tube sockets to a nine-deck selector switch. Meter is protected against overcurrent and alarm rejects bad tubes

INCREASING use of dual-triodes in modern equipment has made necessary use of tubes in which the two triodes are closely matched, statically, dynamically, or both. Selecting a dual-triode which is balanced within usable limits may be done quickly with the balance tester to be described.

Balance Requirements

Commercial equipment using balanced dual-triodes requires static and dynamic performance of the two triodes within a few percent. Allowable deviation depends upon a number of factors which may include the range and effectiveness of the compensating adjustments and the tolerance of the circuit components.

For many applications, only the static characteristics of the two triodes need be in balance. When the same plate and grid voltages are applied to both, the plate currents must be equal, plus or minus the predetermined allowable deviation.

For other applications, the dynamic characteristics of the two triodes must be in balance. When the same plate and grid voltages are applied to both, the plate currents must be equal, plus or minus the predetermined allowable deviation, when an a-c signal is applied to both grids. For most uses, the frequency of this signal is unimportant and the amplitude is not critical, so long as it does not drive the grids positive on the positive half cycle, or cut the tube off on the negative half cycle.

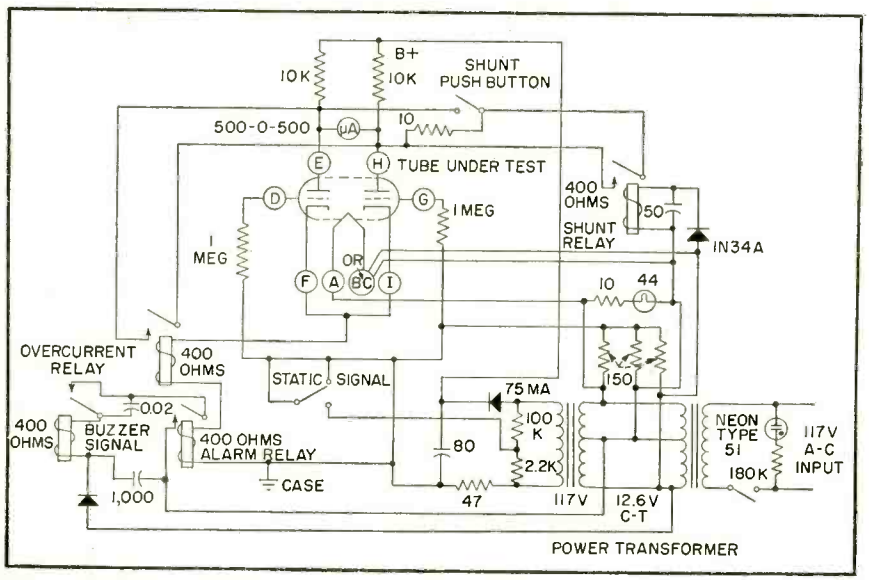


FIG. 1—Dual-triode test-balance circuit. Letters *A* through *I* designate connections to each level of q nine-deck selector switch. Pin-terminal connections for each tube are given in Table I. Relays protect the meter

Difference Amplifier

The ideal circuit for determining the degree of unbalance of the two halves of a dual-triode is the well-known difference-amplifier, the thermionic element being the tube under test. If the two triodes are identical in performance, the meter will read zero. If they are not identical, the meter reading will give a measure of the unbalance.

Because this is effectively a bridge circuit, null position, which corresponds to perfect balance of the two triodes, is uneffected by changes in line voltage or in supply-current waveform.

Conversion Circuit

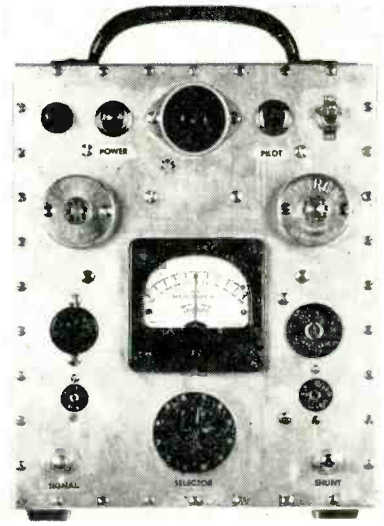
Conversion of the basic difference-amplifier circuit into an effective dual-triode balance-checker requires a power supply, a switching system to accommodate the fifty or more dual-triodes now in use, and safety devices to protect the meter against the effects of possible defective tubes. The circuit used, minus the switching sequence, comprises Fig. 1.

The switching system consists of a nine-deck selector switch wired to the terminals of the tube sockets-connections. The internal wiring, from each of the nine decks of the selector-switch, to the pin-

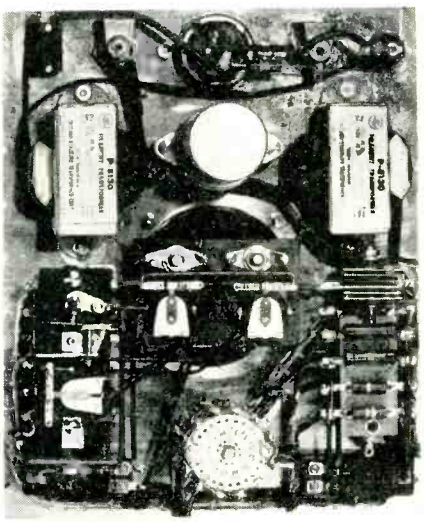
Measures Tube Balance

Table I—Switching Sequence of Balance Tester

	FILAMENT VOLTS	6	12	6	6	12	6	6	12	6	12	12	12
	RETMA SOCKET DIAGRAM	8 BD	8 BD	8B	8S	8S	7 BF	8 AC	8 AC	8 BW	8 BW	9 AJ	9A
	SELECTOR SWITCH POSITION	1	2	3	4	5	6	7	8	9	10	11	12
SWITCH LEVEL	FUNCTION												
A	H COM	7	7	7	7	7	3	1	1	2	2	4	4
B	6V H	8	-	2	8	-	4	8	-	7	-	5	-
C	12V H	-	8	-	-	8	-	-	8	-	7	-	5
D	GRID 1	1	1	4	3	3	6	4	4	1	1	2	2
E	PLATE 1	2	2	3	2	2	1	3	3	3	3	1	1
F	CATH 1	3	3	8	6	6	7	2	2	4	4	3	3
G	GRID 2	4	4	5	4	4	5	5	5	8	8	7	7
H	PLATE 2	5	5	6	5	5	2	6	6	6	6	6	6
I	CATH 2	6	6	8	6	6	7	7	7	5	5	8	8
SOCKET →		OCTAL					7	LOKTAL				NOVAL	



Sockets are on both sides of the meter and selector switch and under a pair of pin-straighteners



Wiring-connections are made to the nine-deck selector switch, shown at bottom center. Construction is relatively simple

terminals of the four tube-sockets is shown in Table I.

The RETMA socket designation for each dual-triode that may be tested indicates the selector-switch position and the numbers in the main column designate connections to sockets named at the bottom of the column. With this arrangement, all sockets except the one in use are electrically dead.

The power transformer consists of two 12.6-volt transformers connected back-to-back. This arrangement effectively isolates the B supply from the line while also supplying 6.3 and 12.6 volts for filament heating, as well as auxiliary voltages for other uses.

A signal of slightly less than 3 volts a-c is available from a resistive tapeoff from the B supply transformer winding. Plate and grid resistors for the difference-amplifier are matched within 0.1 percent.

Relays used in the safety devices are Price radiosonde relays, with a nominal resistance of 400 ohms and a sensitivity of about 8 milliamperes.

Meter Protection

So that vibration and jarring incident to moving will have a minimum effect on the meter, it is shorted by relay contacts when the power is turned off.

To protect the meter against the sometimes extreme warm-up surges occurring in some dual-triodes, even though they may be balanced when fully warmed up, a shunt resistance is connected across the meter movement through a push button.

Gassy tubes and those with one triode shorted sometimes produce heavy cathode currents on one side only. These may damage the meter and indicate that the tube should be discarded immediately. Meter protection and indication of heavy cathode currents, is provided by a pair of 400-ohm relays connected in series in the common-cathode circuit. The overcurrent relay in Fig. 1 shorts the meter, effectively protecting it against any asymmetrical overcurrent likely to occur in the system. The alarm relay actuates a small high-frequency buzzer, which is fed from a rectifier-filter supply powered by the filament circuit. This prevents confusing a bad tube from one with perfect symmetry. As the meter reading for a perfectly balanced tube is the same as the reading when the meter is shorted, a bad-tube alarm is necessary.

After power connections have been made, the tube to be tested is inserted in the appropriate socket on the front panel. The selector switch is then dialed to switch position determined by the RETMA socket designation of the tube.

After a two minute warm-up, the shunt button is pressed and the meter reading is noted. If this is within allowable limits for the projected use, the signal button is pressed and the reading is again noted. If the tube is within allowable limits, it is used, if not it is returned to stock for use in a non-critical position.

Performance

Use of this instrument in a laboratory devoted to research and servicing of critical equipment discloses that its performance is satisfactory, electrically and economically. Balanced dual-triodes for use in d-c and a-f equipment can be selected by its use with substantially 100-percent assurance that they will operate in the equipment.

At 10 megacycles, approximately 90 percent of the tubes that test good for balance will work in the equipment. At 100 megacycles, the percentage falls to 80, due in large part to capacitance unbalance which are not disclosed by the balance testing method.

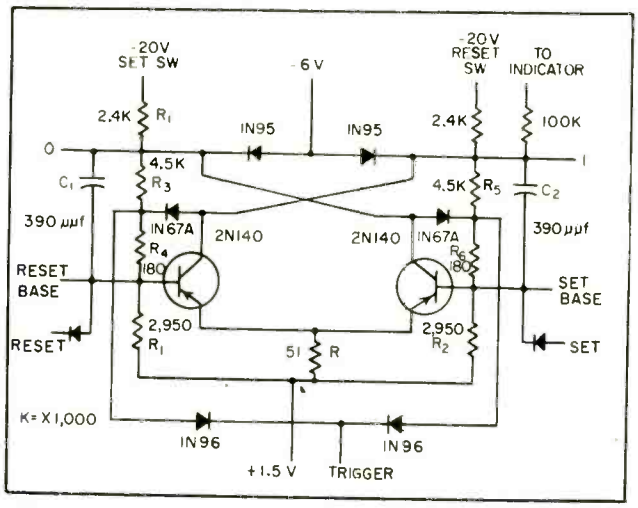


FIG. 1—Flip-flop stage has saturation operation of transistors

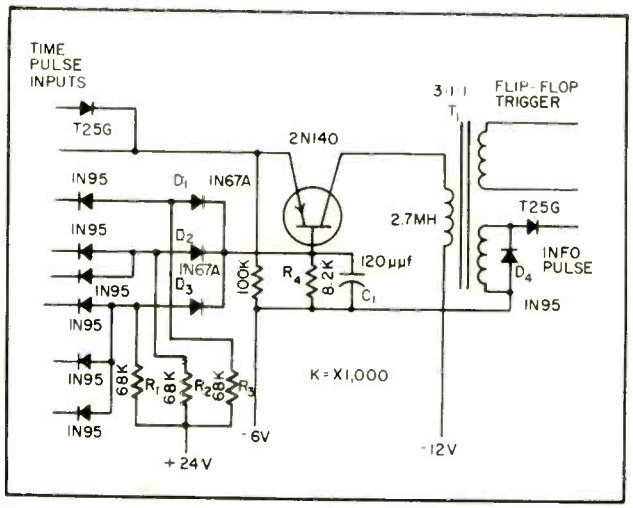


FIG. 2—Gated pulse amplifier has 250-kc repetition frequency

Basic Logic Circuits for

SUMMARY —— Digital computer circuits, including flip-flop, gated pulse amplifier, d-c amplifier, power amplifier and indicator, use high-frequency junction transistors to obtain high reliability and performance characteristics. Circuits operate over temperature range of —30 to +60 C; their low dissipation imposes minimum requirements on power supplies and cooling

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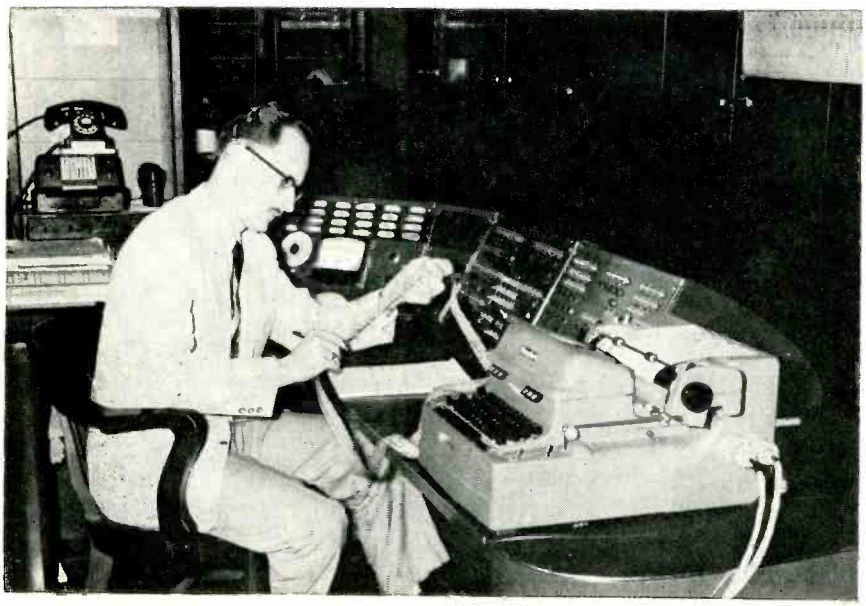
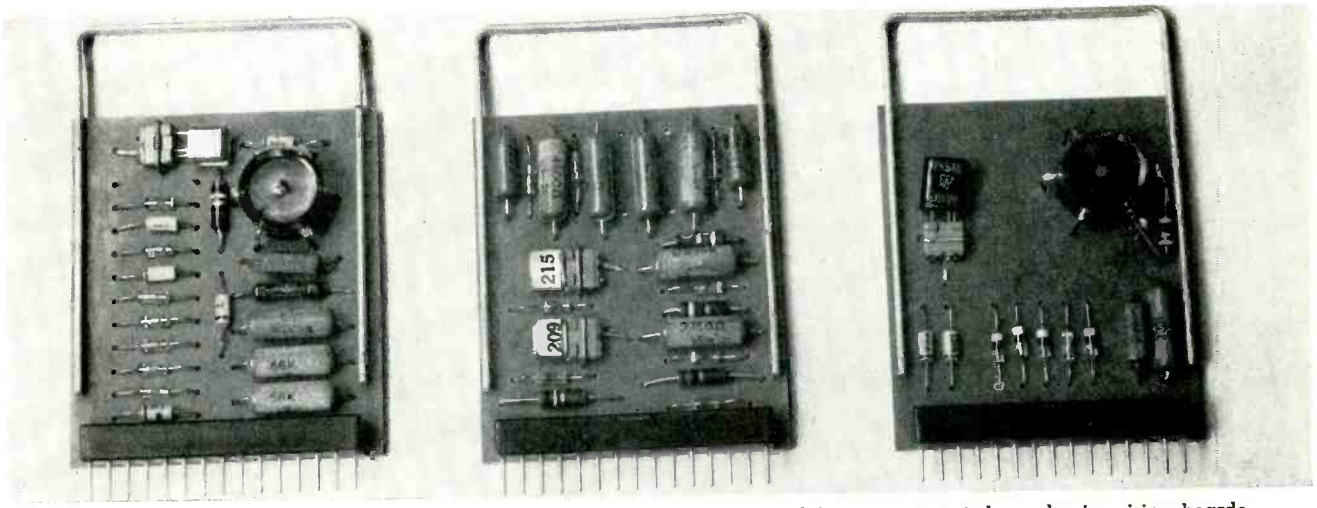


Operator reads out punched tape from NIFTE computer console. Transistor circuits are in rack seen in back of operator's head

ONE of the important properties of a digital computer is that it may be assembled simply and easily from a few well-chosen functional circuits. Each of these circuits represents a logical building block that is useful to the system or logic designer in planning a computer.

This article presents a group of transistor circuits for a general digital computer application.[1-4] The circuits described are the result of a conservative design approach which takes advantage of the high switching efficiencies obtainable with the alloy junction transistor. Precision resistors are used throughout, and are treated as five-percent resistors in the design. Power dissipation, current, and voltage levels are kept low in



Gated pulse amplifier, flip-flop and power pulse amplifier circuits (left to right) are constructed on plug-in wiring boards

Computer Applications

diodes and transistors, yet are large enough to avoid serious problems resulting from noise pickup. Circuit dependence on individual parameters of the transistors is minimized. Commercially available high-frequency alloy-junction transistors are used and a considerable slump of transistor gain from specified values can be tolerated without sacrificing performance.

The two basic circuits are a flip-flop and a gated pulse amplifier. All information flows in the form of 0.5-μsec pulses through chains of one or more gated pulse amplifiers and is ultimately stored in a flip-flop. Gate control information is in the form of d-c levels from flip-flops, in most cases without intermediate amplification being necessary.

Flip-Flop

The first of the basic circuits is a flip-flop. The Eccles-Jordan circuit shown in Fig. 1 was chosen for complementary outputs, its designability and the efficiency obtained by saturation operation of the transistors.

The limited frequency response available in alloy junction transistors requires clamping of the turn-off transient for fast rise times under load. Collector current in the flip-flop transistors is limited to 10 ma. A collector output swing of six volts was chosen as large compared to diode forward voltage drops, yet small compared to breakdown voltages of diodes and transistors.

A d-c stability analysis determined the circuit parameters to assure a two-ma load specification, stability under conditions of large I_{co} and discrimination against small noise pulses that would tend to trigger the circuit.[5] Reverse bias on the base-emitter diode of the nonconducting transistor is guaranteed with allowances for I_{co} and leakage in diodes of at least 120 μa, which corresponds to the I_{co} that might be encountered at +60 C. Since this figure is based on tolerance extremes of all components, a considerably greater I_{co} can generally be tolerated.

The design assures saturation in the on transistor for worst cases of all resistor and supply voltage tolerances for transistors with large-signal current gains greater than 15 at the 10-ma collector current required for flip-flop operation. No maximum gain figure need be specified.

Switching Speed

At the instant the conducting transistor turns off, its collector rises toward some potential which is less than the supply voltage. In a flip-flop of this type, the aiming potential should be at least as large as the clamp voltage since the d-c stability analysis is based on a collector voltage equal to the clamp voltage.

Aiming Potential

The aiming potential is defined as the resultant potential at the cut off collector due to the divider action of the collector resistor, the feedback resistor and the load resistor when the clamp diode is disconnected. However, to assure that worthwhile advantage in speed is obtained, the aiming potential-to-clamp voltage ratio must be somewhat greater than unity. For Fig. 1, with a two-ma load current, this ratio is 1:5.

Feedback capacitors C_1 and C_2 were chosen empirically to perform speedup and memory functions for a typical pair of transistors. Too large a capacitance results in slow

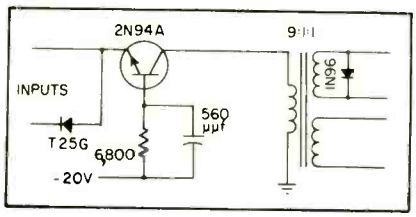


FIG. 3—Power pulse amplifier provides 180-mw output for 30-mw input

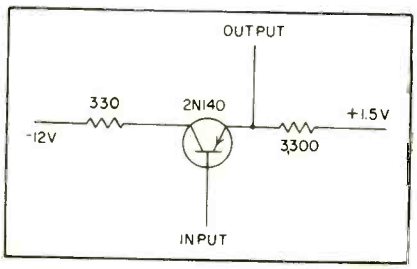


FIG. 4—Emitter follower provides current gain with nearly unity voltage gain

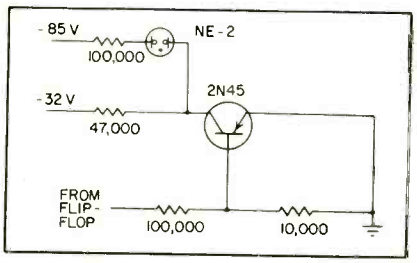


FIG. 5—Biased neon-lamp indicator

switching at the cut-off collector. Too small a capacitance results in tight frequency response requirements on the transistors for a satisfactory range of trigger pulse voltage and width. A compromise in the vicinity of 400 $\mu\mu$f provides a feedback coupling which is relatively independent of transistor characteristics.

To achieve a high repetition rate for the flip-flop, the discharge time constant τ of the feedback capacitors should be as small as possible. This time constant is given by

$$\tau = C_f[R_bR_f/(R_b + R_f)]$$

where C_f is C_1 or C_2, R_b is R_1 or R_2, and R_f is $(R_3 + R_1)$ $(R_5 + R_6)$.

Capacitor C_f must be increased as R_f is reduced; R_f is largely determined by current levels in the circuit. Thus, for minimum resolution time, it is desirable to have R_b as small as practicable.

Common emitter resistor R_e is included to obviate the need for a small bias supply voltage. With R_b small, the bias potential to which R_b is returned must be small to maintain an adequate current in the base of the conducting transistor. Such small bias voltages are both difficult and inconvenient to generate and regulate.

For this purpose, a bias is generated by the saturation current of the on transistor through R_e. The emitter return is set at + 1.5 v so the collector of the conducting transistor is assured to be positive with respect to ground, providing a reverse bias on ground-returned loads.

Saturation Effects

Pulse steering is incorporated into the circuit to reduce saturation effects of the turn-on trigger pulse at large trigger amplitudes. A feedback diode from each collector to a tap on the feedback resistor provides a shunt path from this base tap to the collector of the conducting transistor.[6] Hence, a large amplitude trigger does not cause a high degree of saturation in the conducting transistor.

On the cutoff transistor, the feedback diode is reverse biased by six volts and has no effect on circuit operation. This feedback diode does not assure nonsaturating operation of the transistor, since some fixed current will flow through the resistor between feedback diode and base for the essentially constant forward bias drop of the diode.

For a high-gain transistor, this fixed current may represent saturation; for a low gain transistor, it may not. However, if the gain of the conducting transistor is sufficiently low as to cause it to be out of saturation by more than a few tenths of a volt, the feedback diode cuts off, providing maximum base current to the conducting transistor. In any case, d-c stability is not sacrificed by the use of the feedback diodes in the circuit.

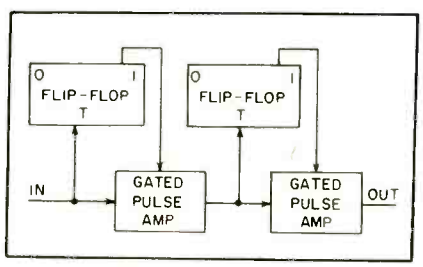


FIG. 6—Two stages of binary counter with high-speed carry

Table I—Output Specifications

Circuit	Output Form	Output Maximum Load
Gated Pulse Amp	2.6-v pulse 1/2 μsec (10 ma)	2—F-F or 3—GPA or 1—PPA
Power Pulse Amp	2.6-v pulse 1/2 μsec (55 ma)	11 F-F or 17 GPA or 7 PPA
Flip-Flop	6-v level (2 ma)	4 GPA or 2 EF + 1 Ind
Emitter Follower	6-v level (18 ma)	36 GPA

For the circuit of Fig. 1, a trigger-amplitude range of 2.1 to 4.5 v was obtained for a resolution time of 1.2 μsec. Operation with a trigger pulse width from 0.4 to 0.9 μsec at the 2.6-v nominal pulse amplitude was achieved.

Gated Pulse Amplifier

The second basic logic circuit is the gated pulse amplifier shown in Fig. 2. The gating function of the circuit is controlled by the or-and diode gate in the base lead of the transistor.

Each or input of this gate is derived from a flip-flop whose output is 0 or − 6 v. A 2.6-v positive pulse, biased at −6 v, is applied at the emitter. A pulse output will appear only if the base potential is more negative than − 3.4 v since, if this condition is not met, the base emitter diode will never be forward biased. This condition can only exist when all and inputs have at least one or input at − 6 v.

If one and input is at ground, the voltage division between its associated resistor R_1, R_2 or R_3, and R_4 will raise the base to − 3 v. More than one and input at ground will make the base even more positive.

When the gated pulse amplifier is primed D_1, D_2 and D_3 are cut off. Hence the diode gate may be neglected and the pulse amplifying qualities of the transistor amplifier alone considered. The transistor is driven from zero bias to saturation by the 0.5-μsec pulse applied at the emitter.

Capacitor C_1 offers an increase in effective frequency response by

allowing the circuit to operate as grounded base during the 0.1 μsec turn-on and turn-off periods of the transistor. During the rise of the pulse, the transient current in the base lead is determined by the size of C_1 and the low pulse source impedance in series with the transistor base and emitter resistances. During the fall, the capacitor provides a low impedance in the base lead to diminish the effects of storage.

Each of these transient effects are settled in approximately 0.1 μsec and have little effect on the circuit during the flat-top portion of the pulse. When the transistor is operating in saturation the voltage drop from emitter to collector is negligible and $\beta I_B > I_c$. In this condition, a constant voltage appears across the load and the magnetizing current in the output transformer increases linearly.

The pulse output will collapse if βI_B becomes less than I_c or if the pulse falls at the input. The primary inductance of T_1 is chosen to assure that the second of these two conditions determines pulse width. Either case will cause a high collector impedance to be presented to the load.

Diode D_4 provides a low resistance path to damp the overshoot of the transformer at the end of the pulse.

The circuit design allows for a 250-kc pulse repetition frequency.

Amplifiers

Two amplifiers complete the system, one a power pulse amplifier and the other type is a d-c amplifier.

The power pulse amplifier is basically similar to the gated pulse amplifier, with the exception that no gating bias is provided and a 2N94A *npn* transistor is used to obtain a high power output. For a given emitter current, power output is proportional to collector voltage and maximum collector voltage on the available *npn* was higher than on the available *pnp*'s. This amplifier, shown in Fig. 3 is capable of providing a 180-mw pulse output for a 30-mw pulse input.

The d-c amplifier, shown in Fig. 4, is an emitter follower, providing current gain with nearly unity voltage gain. To prevent excessive dissipation and to avoid saturation in the transistor, a collector load resistor was introduced. Maximum transistor dissipation was calculated to be 40 mw and maximum load current 18 ma.

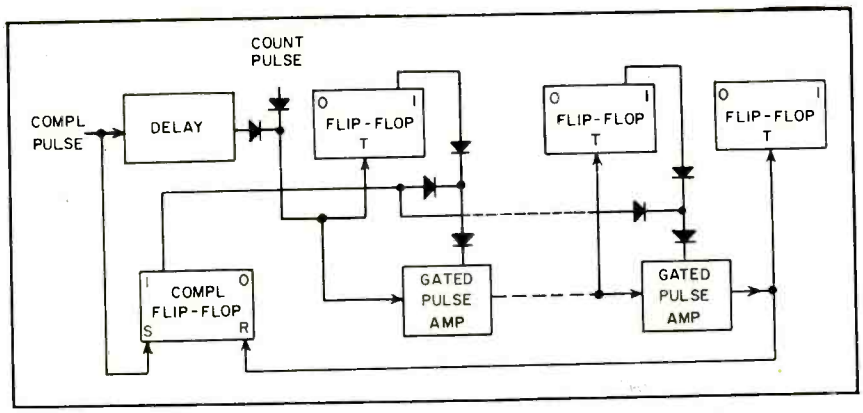


FIG. 7—Binary counter modification allows complementation and reversible counting

Indicator

Although not necessary to the logic, an indicator is desirable for any test of the system and for trouble shooting. The indicator shown in Fig. 5 employs a biased neon tube which is switched off and on by an a-f transistor. The transistor requirements are modest—collector breakdown greater than 35 v and current gain greater than 10.

Dissipation in the transistors is negligible since only the on current of the neon lamp need be supplied. Neon tube requirements are more strict because extinguishing potential is about 55 v and firing potential about 85 v.

Transistor requirements for flip-flop and gated pulse amplifier circuits are modest enough that 85 percent of the high-frequency transistors purchased in 1955 from one manufacturer were acceptable in all respects.

Rejects were primarily due to high leakage current at 20 v. Although the transistors were operable in the circuits, the low output impedance was taken as an indication of a poor junction, with adverse implications on long-term transistor life.

A suitable, currently available *pnp* is the 2N140; a *npn* is the 2N94A.

Complete specifications, formulated along with the test circuits to determine the specifications, are too lengthy to cover here. Three basic requirements are: 1) grounded-base frequency response > 4 mc; 2) large signal current gain (β) > 20 at I_c = 10 ma for flip-flops, > 30 at I_c = 10 ma for gated pulse amplifiers; 3) collector leakage and saturation currents (grounded base) I_{co} at 6 v $\leq$ 3 μa, I_{co} at 20 v $\leq$ 6 μa.

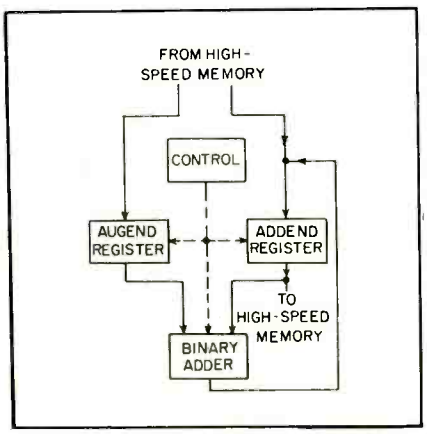


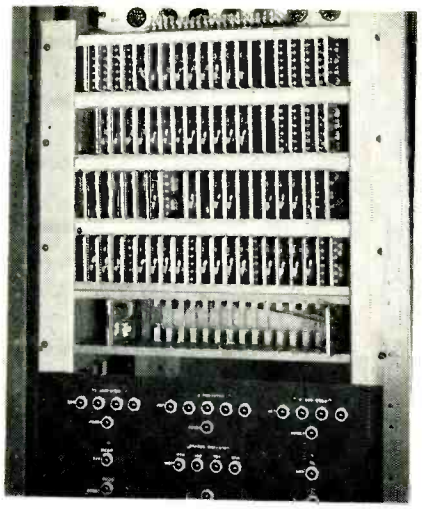
FIG. 8—Adder, excess-three-converter

Application Rules

Table 1 summarizes the minimum output specifications for the circuits described.

Note that the gated pulse amplifier has two types of input, one requiring a 2.6-v, 3-ma, 0.5-μsec pulse and the other requiring a 6-v, 0.5-ma level. Hence, the outputs of the gated pulse amplifier and power pulse amplifier can drive only the pulse inputs of a gated pulse amplifier.

The outputs of the flip-flop and emitter follower can drive only the level (diode gate) inputs of the gated pulse amplifier. The emitter



Rack-mounted transistor adder-excess three converter uses plug-in boards

follower was designed to drive a maximum of 36 gated pulse amplifier inputs. This restriction is a matter of design convenience and not fundamental to the circuit.

Maximum pulse repetition frequency for the gated pulse amplifier is 250 kc. The flip-flop may be set and reset at a 500-kc rate; maximum triggering rate is 400 kilocycles.

Logic Techniques

The binary counter shown in Fig. 6 illustrates the type of logical structure to which the circuitry lends itself.

When a count is added to a binary counter, each bit is complemented according to the following two rules. Complement if: 1) the next least significant bit was one before addition of the count and 2) all less significant bits have been complemented under rule 1. The least significant bit is always complemented.

Hence, all bits of a counter are complemented starting from the least significant bit and continuing through the first bit in which a zero is found to be stored. This function is performed by the chain of gated pulse amplifiers in Fig. 6. The trigger pulse will pass from the first to the second stage and complement the second flip-flop only if the first flip-flop is in the one state before the trigger occurs.

Although the state of the flip-flop may change as a consequence of the pulse, the gated pulse amplifier acts on its initial state. This results from the relatively slow rise of the flip-flop to the -3-v level required to affect the output of the diode gate.

Carry Time

Since the carry propagation of the counter is independent of the switching time of the flip-flop, fast carry ripple can be achieved. The circuit described here results in a 30-mμsec carry-ripple time per stage. Hence in a 12-bit counter, the longest carry time will be 0.36 μsec. Time required for the result to be available is longer than this by the settling time of the flip-flop stages.

With very little additional equipment, the counter of Fig. 6 becomes a reversible counter. Figure 7 shows the logic for a simple version. Here the chain-gate logic performs both complementation and binary count. When subtraction from the original count is desired, the counter is complemented by the complement pulse and flip-flop, triggered with the count pulse, and recomplemented to be read.

Three characteristics of the counters shown might be highlighted for general computer logic applications: the pulse delay encountered through the gated pulse amplifier is small enough to allow a rather lengthy chain of amplifiers to be used with a minimum delay in passage through them; the gated pulse amplifier allows a wide variety of logic because of the or-and cascade and the ability to use these circuits in an interative connection; the relationship between the flip-flop resolution time and the pulse width allows the flip-flop to be sensed and changed in state with the same pulse.

Operating Experience

The proper test of circuits for digital computer use is their actual operation in a computer. There is available at RCA a general purpose computer specifically designed as a test facility. It has a high-speed random-access magnetic-core memory with a capacity of 1,024 seven-bit characters and uses a Flexowriter for input-output.

Using these transistor circuits, two components have been constructed for test in this machine. The first of these was a reversible counter and associated logic for keeping track of iterations during the multiply instruction and was built with a simple breadboard construction. Twenty-three transistors and 81 diodes were used.

Marriage between machine and transistor circuits was performed by a group of vacuum tube amplifiers, pulse shorteners, etc. The unit has operated without error for over 200 hours of computer operation. Routine testing of transistors during shutdown did indicate progressive deterioration of a group of transistors, all of one manufacturer. Since these have been replaced with another type no further deterioration has been encountered so far.

Adder Converter

An adder, excess-three-converter unit for the test computer was constructed as the second test component. Figure 8 is a block diagram of the adder converter. This equipment was paralleled with the existing vacuum tube arithmetic unit. Results computed by the transistor equipment are substituted for those computed by the vacuum tube adder and a parity check is made between the two results.

The basic circuits for this equipment were laid out on five types of individual plug-in units. A total of 81 such plug-ins are used, containing 110 logical and 20 indicator transistors and 450 diodes.

To date more than 300 hours of operation (39,000 transistor hours) have been logged on this unit since debugging, with no transistor or diode failures.

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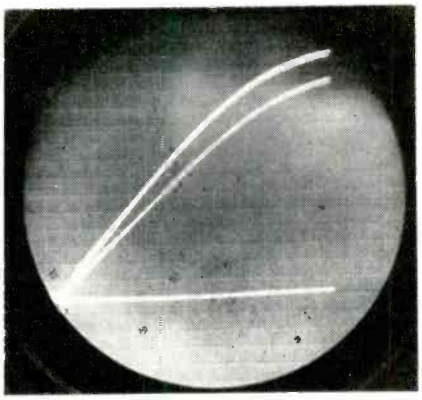


Face of crt shows sweeps just before they are superimposed to indicate correct adjustment of system

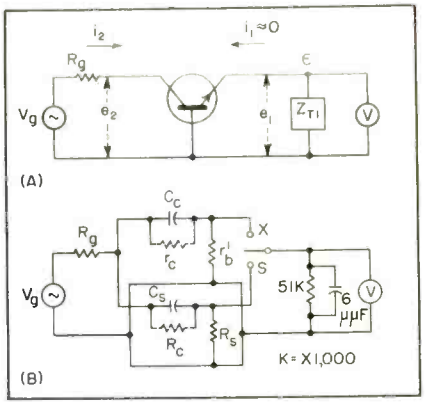


FIG. 1—Basic circuit for measuring h_{12b} (A) and comparison circuit for measuring r'_bC_c product (B)

Sweeper Determines Power-Gain Parameter

SUMMARY —— Transistor $r'_b C_c$ product that detrmines power gain is evaluated by a variable-frequency sweep generator in conjunction with cro and standard network using comparison technique. Two-channel system compares transistor output over range of 2 kc to 2 mc and provides direct dial reading of $r'_b C_c$ product

ONE OF THE MORE useful quantities in evaluating the high-frequency performance of a junction transistor is the available power gain. This gain may be measured directly at frequencies of interest[1] or may be calculated from the measured circuit parameters at those frequencies.[2, 3, 4, 5]

The h-f power gain may be found from the inherent alpha-cutoff frequency, the ohmic base resistance r'_b and the collector-base junction capacitance C_c all of which can be measured at low or medium frequencies.

Moreover, the gain is determined from the alpha-cutoff frequency and r'_bC_c. This article describes a rapid and accurate means of measuring r'_bC_c product to evaluate quickly the high-frequency capabilities of junction transistors.

The r'_bC_c product is related to the common-base h_{12} parameter by[6] $h_{12b} = h_{120} + j\omega r'_bC_c$, where h_{12b} is the common base voltage feedback parameter, h_{120} is the low frequency value of h_{12b}, ω is the frequency in radians per sec, r'_b is the ohmic base resistance and C_c is the inherent collector-base capacitance.

The quantity h_{120} is the sum of the Early feedback voltage μ_{ec} and the product of r'_b and the collector-base conductance.[7]

The parameter h_{12} can be measured in a circuit as shown in Fig. 1A. The impedance Z_{t1} consists of the impedance of the voltmeter and the impedance of the circuit used to supply d-c emitter current to the transistor.

Since the emitter-base terminating impedance Z_{t1} is many times the short-circuit input impedance h_{10b}, then $h_{12b} \cong e_1/e_2$.

The first and second equations result in $e_1/e_2 = h_{120} + j\omega r'_bC_c$. At the higher frequencies where $\omega r'_bC_c >> h_{120}$, $e_1/e_2 = \omega r'_bC_c$ so that if e_2 is constant with frequency the measured voltage e_1 will be proportional to frequency.

In the sweeper, the output voltage of the transistor e_1 is compared with the output voltage of a simple R-C high-pass network as shown in Fig. 1B.

An exact equivalent circuit for the transistor is not shown here but rather an exact circuit to represent the measurement of h_{12b}. If the transistor and the comparison network R_cC_c are driven from a common a-c voltage generator, then a

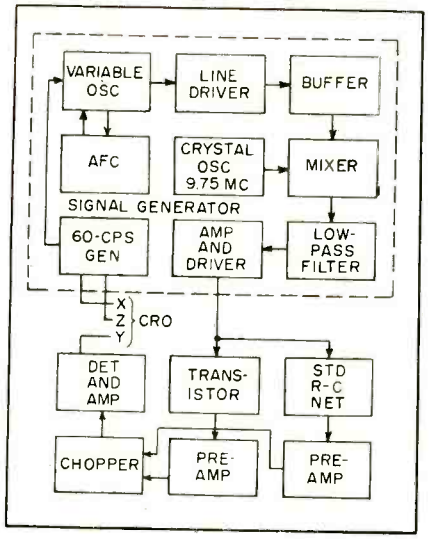


FIG. 2—Complete system required to measure power gain parameter

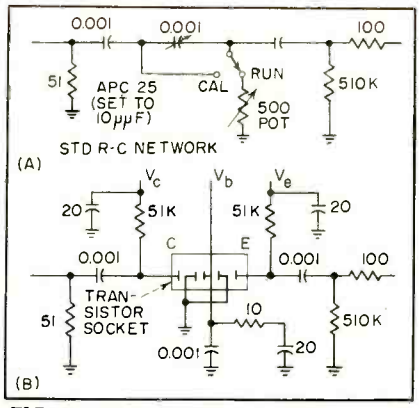


FIG. 3—Input circuit to standard preamplifier (A) and transistor preamplifier (B) used in sweeper system

voltmeter connected at the output terminals of either the transistor channel or the comparison channel will indicate the same voltage if $R_sC_s = r'_sC_c$.

If these two voltages remain equal as the frequency of V_g is changed over an interval Δf, and if R_s and C_s are independent of frequency over this interval, then r'_sC_s must be independent of frequency over the interval.

Resistor R_s is a 500-ohm variable resistance and C_s is a fixed element of 10 $\mu\mu$f. The maximum value of the r'_sC_s product, which can be measured is thus 5,000 ohm-$\mu\mu$f. Accuracy of the measurement decreases as the frequency increases. This occurs when the reactance of the parasitic capacitance shunting R_s is no longer negligible compared with R_s and when the reactance of the parasitic inductance in series with R_s is no longer small when compared with R_s. The first condition occurs at high values of R_s, the second at low values. Using R-C high-pass networks with parameters known to 1 percent as sample transistors the sweeper determined the R-C products within 5 percent of the calculated value.

Circuit Description

A block diagram of the sweeper is shown in Fig. 2. The variable oscillator is swept from 9.752 mc to 11.75 mc at a 60-cps rate by applying a quasisawtooth current to the control winding of the oscillator tank coil. An integrating network in the sweep circuit portion of the 60-cps timing generator provides a control current for the sweep oscillator that will give a linear rate of change of frequency versus time. A linear sawtooth is generated for X-axis deflection. The 60-cps multivibrator in this circuit is synchronized by 6.3 v a-c heater voltage. The output voltage of the sweep oscillator is maintained flat over the frequency range by an avc circuit.

To heterodyne the 9.752-mc to 11.75-mc interval down to 2 kc to 2 mc the variable-oscillator signal mixes with a 9.75-mc signal from a third-overtone crystal oscillator. The lower side band is selected from the plate circuit of a pentagrid-mixer stage by a low-pass filter consisting of two constant-k pi sections with a cutoff frequency of 7.8 mc and terminating half sections of the m-derived type that provide nearly infinite attenuation at 9.75 mc.

The filter is followed by a gain-controlled video-amplifier stage and a line driver working into an a-c load of 25 ohms. This stage supplies the nominal 0.2-volt peak-to-peak signal, impressed across the collector-base terminals and input to the R_sC_s network. The signal generator portion of the circuit is now a packaged unit.

Direct current bias is delivered to the transistor in the shunt-feed arrangement of Fig. 3. The comparison network consists of an APC-25 variable capacitor set to 10 $\mu\mu$f and a 500-ohm carbon po-

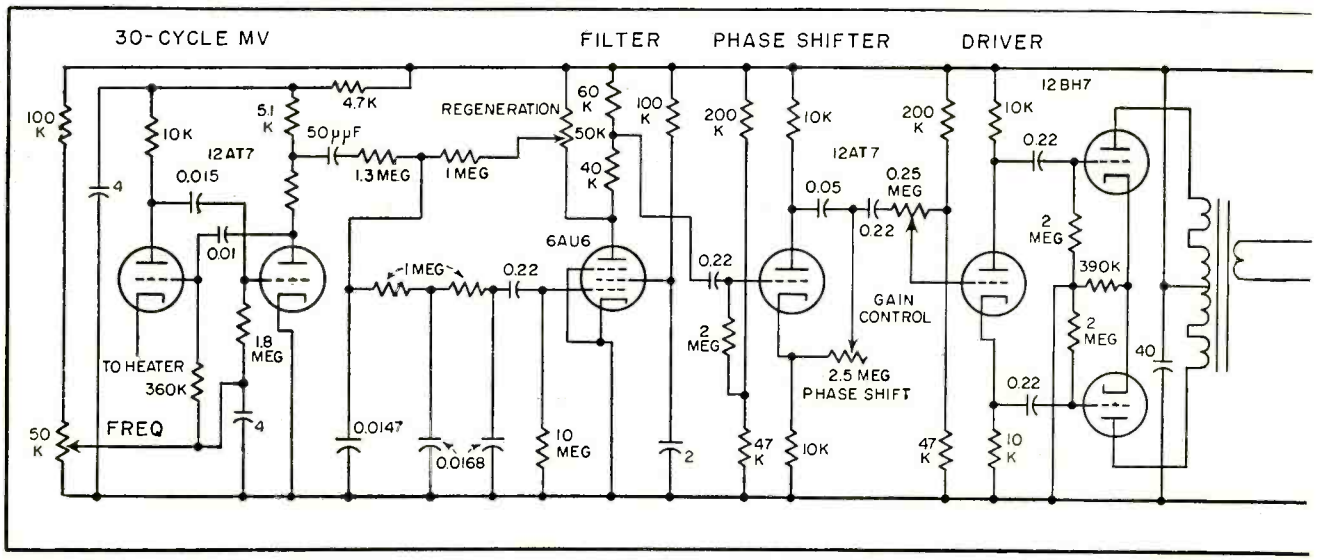


FIG. 4—Chopper driver uses filament as source of 30-cycle synchronization. Filter removes high-frequency components from multi

tentiometer with a dial calibrated in ohms. The R-C product is thus ten times the dial reading.

The comparison network and the transistor are followed by video preamplifiers with voltage gains of about 100 and bandwidth from about 1 kc to 4 mc. In addition, the comparison channel provides a gain control to allow the amplification of the two channels to be equalized.

The output from the two channels is coupled to a chopper. Each channel is alternately connected to the main video amplifier shown in Fig. 4 for 1/60 second. This amplifier has a voltage gain of about 100, bandwidth of approximately 1 kc to 3 mc and is equipped with the master gain control. The amplifier is followed by a diode envelope detector with a load impedance time constant of about 330 μsec, which is a compromise between adequate filtering for the carrier signal and fast response to the 60-cps fundamental modulation frequency and its harmonics.

The chopper is driven by a 26 volt, 30 cps sine wave obtained from a 30-cps multivibrator also shown in Fig. 4. It is synchronized from the 6.3 v a-c heater voltage.

The following stage is an electronic filter that transmits only the fundamental sinusoidal component of the rectangular wave. A phase shift network allows the chopper to commutate at the proper time with respect to the sweep period.

The envelope-detector output is applied to the vertical axis input terminals of an oscilloscope with a response down to d-c and equipped with a long-persistence phosphor screen to eliminate 30-cps flicker. The complete sweeper requires 300 v d-c at 390 ma for the plate power.

Calibration

Initial calibration of the sweeper requires strapping through both the comparison channel (set switch to calibrate) and the transistor channel (place jumper wire between *e* and *c*). The gain in both channels is equalized over the entire swept spectrum. If it is impossible at first to make the two traces coincide perfectly, small 0.5 to 5.0 $\mu\mu$f trimmer capacitors can be added between plate and ground of one of the preamplifier stages to compensate for small variations in tube and wiring capacities.

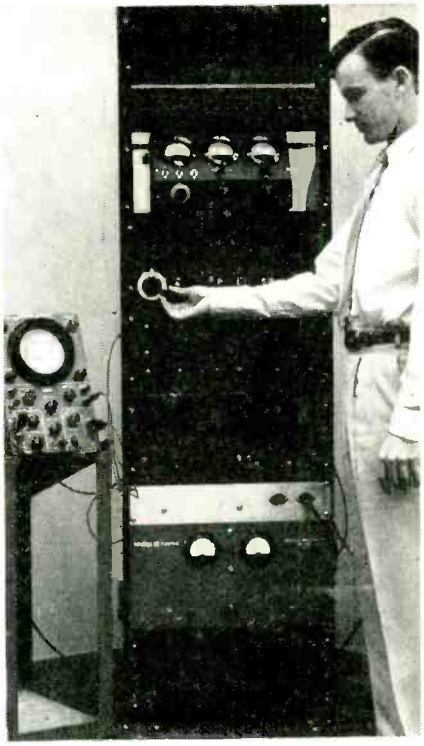
To measure an unknown R-C product, adjust the calibrated potentiometer until the two traces on the display tube coincide. The value of the product can then be found from the reading on the dial.

Compensation

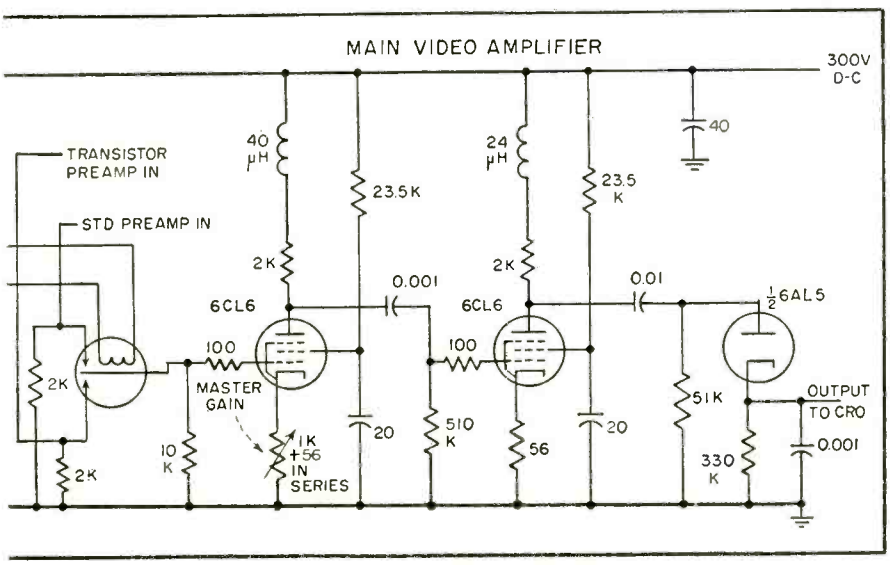
It may be difficult to match the trace generated by a transistor of moderate h_{12o} with the trace from the comparison network. For precision the two traces should coincide and to accomplish this it is necessary to add the proper value of resistance R_e across the capacitance C_s. Small $\frac{1}{2}$-watt composition resistors that can be plugged into the circuit will be satisfactory if it is remembered that their shunt capacitance of about 0.8 $\mu\mu$f must be added to the value of C_s. The value of h_{12o} can be determined approximately by $h_{12o} \simeq R_s/R_e$ since in most cases $R_e >> R_s$.

The value of R_s is available on the calibrated potentiometer dial.

The author thanks R. L. Pritchard for many helpful discussions and H. W. Griffin, Jr. for his assistance in the design and testing of the sweeper.



Potentiometer in standard network is adjusted to produce sweeps that are superimposed on face of cro.



vibrator output to provide sinusoidal drive to chopper in main video amplifier

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(4) L. J. Giacoletto, Study of *p-n-p* Alloy Junction Transistors from D-C Through Medium Frequencies, *RCA Rev*, **15**, p 555, Dec. 1954.
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(6) R. L. Pritchard, Frequency Variations of Junction Transistor Parameters, *Proc IRE*, **42**, p 792, May 1954.
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(8) R. L. Pritchard and W. N. Coffey, Small Signal Parameters of Grown Junction Transistors at High Frequencies, *IRE, Conv Rec*, **2**, Part 3, p 90, 1954.

Transistor Transformer Design Nomographs

SUMMARY — Critical parameters of volts per turn and magnetizing inductance for transistor-driven audio coupling transformers are conveniently given by individual nomographs. Final chart gives wire size

By C. J. SAVANT
and
C. A. SAVANT
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Western Division
Hawthorne, California

TRANSISTORS operate with lower input impedance and higher output impedance than tubes, hence transformer coupling often becomes more expedient than R-C coupling for audio circuits.

The transformers required are only a fraction of a cubic inch in volume and weigh only a fraction of an ounce. The accompanying nomographs simplify the design of these subminiature a-f transformers for use in transistor circuits.

Turns and Core Area

For sinusoidal flux changes the basic transformer equation is

$$e = N\,K\,A\,B\,f\,/\,3{,}490 \qquad (1)$$

where e is rms primary volts, N is number of primary turns, K is stacking factor, A is core cross-sectional area in sq in., B is peak flux density in kilogauss and f is frequency in cps.

Having selected the core material and the maximum value of flux density allowable from physical considerations, the designer must determine the number of turns and the core area from the operating voltage and frequency. The stacking factor is usually specified by the core lamination manufacturer and is essentially constant.

The volts-per-turn design nomograph in Fig. 1 is readily constructed by rearranging Eq. 1 in the form

$$(e/N)\,(3{,}490) = (KAB)\,(f) \qquad (2)$$

The operating frequency is known from the circuit application of the transformer. To get KAB, the maximum flux density is taken from the B-H characteristics for the particular iron, K is obtained from the iron specifications and the approximate area is taken from the known size requirement. From these values of f and KAB, the volts per turn can be read directly on the nomograph. Division of primary volts by the value of e/N gives the number of primary turns.

Magnetizing Inductance

In a transformer-coupled amplifier, the loading effect of the transformer working through the high output impedance of a grounded-emitter transistor may be serious. For low-power transformers at audio frequencies the most significant parameter in the determination of this load-

(Continued on p 206)

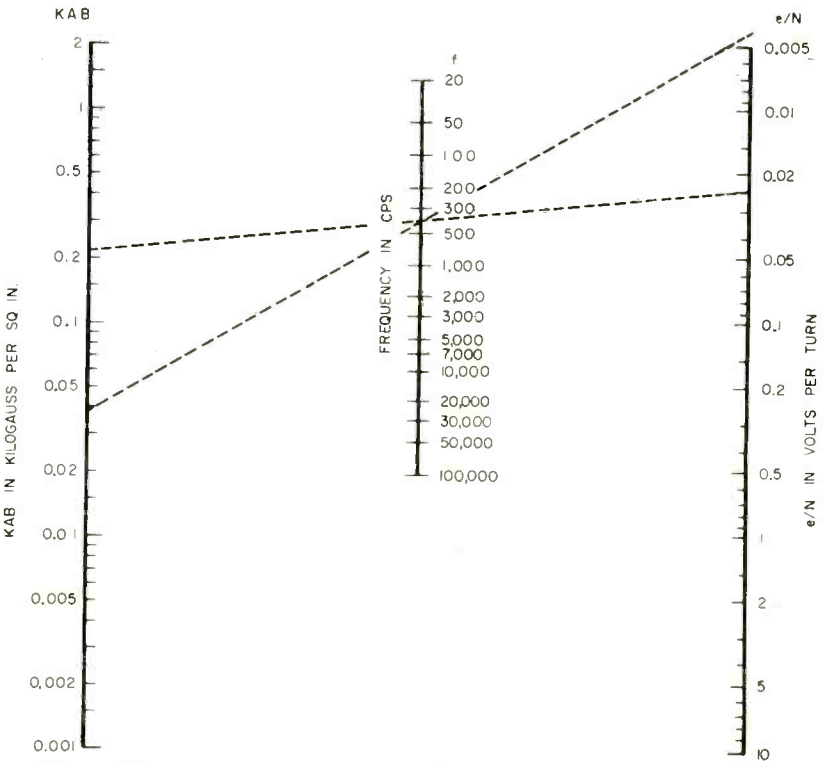


FIG. 1—Volts-per-turn nomograph for subminiature iron-core coupling transformers used in transistor circuits. Dashed lines correspond to design problem worked out as example

NEW DEVELOPMENTS IN PRINTED CIRCUIT SOCKETS BY CINCH

No. 22920

No. 22920—7 contact miniature molded vertically mounted socket with JAN type shield base. Mica insulation. Silver plated phosphor bronze contacts drop through .062" dia. clearance holes arranged on a .1" X and Y axis.

EXP-9553 — 8 contact button base subminiature molded, vertically mounted socket. Mica insulation. Silver plated beryllium copper contacts drop through .070" dia. clearance holes arranged on a .1" X and Y axis.

EXP-9553A—Same as above except insulation to withstand temperatures above 200° Centigrade.

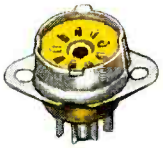
EXP-9553

No. 22024—7 contact flat press subminiature molded, vertically mounted socket for conventional wiring. Assembled with a special shield base to accept a subminiature shield with the "J" lock. Flat sided retaining nuts and screws are provided for mounting. Mica insulation. Silver plated beryllium copper contacts.

No. 22024

No. 22023—Same as above except insulation to withstand temperatures above 200° Centigrade.

No. 22022 — 8 contact button base subminiature molded vertically mounted socket for conventional wiring. Assembled with special shield base to accept a subminiature shield with the "J" lock. Mica insulation. Silver plated beryllium copper contacts.



No. 22022

No. 22021—Same as above except insulation to withstand temperatures above 200° Centigrade.

EXP-9542—7 contact miniature molded right angle mounted socket with JAN shield base. Mica insulation. Silver plated beryllium copper contacts drop through .062" dia. clearance holes arranged on a .1" X and Y axis.

EXP-9542

EXP-9561 — 7 contact flat press subminiature molded right angle socket. Mica insulation. Silver plated beryllium copper contacts drop through .046" dia. clearance holes arranged on a .1" X and Y axis.

EXP-9561A—Same as above except insulation to withstand temperatures above 200° Centigrade.

EXP-9561

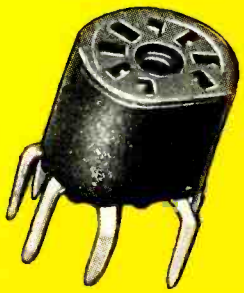
EXP-9562—8 contact button base subminiature molded, right angle mounted socket. Mica insulation. Silver plated beryllium copper contacts drop through .046" dia. clearance holes arranged on .1" X and Y axis.

EXP-9562A — Same as above except insulation to withstand temperatures above 200° Centigrade.

EXP-9562

These latest developments in printed circuit sockets offer the highest quality in material and workmanship to meet the most rigid government specifications. They insure positive contact and hold tubes securely in place. Maintenance and replacement easily made. They provide maximum insulation resistance and minimum high frequency loss. Adapted to printed circuit boards up to and including 1/8" thick.

Sockets shown enlarged.

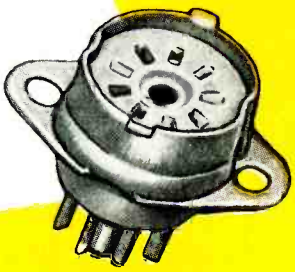


EXP-9553

No. 22024

These sockets will take care of the three types of receiving tubes in use today: Miniature, Flat Press and Button.

The contacts are so spaced that they can be mounted in an incremental drill pattern as stated. This fact together with the exact precision and uniformity of Cinch sockets make them ideal for automatic assembly.



No. 22022

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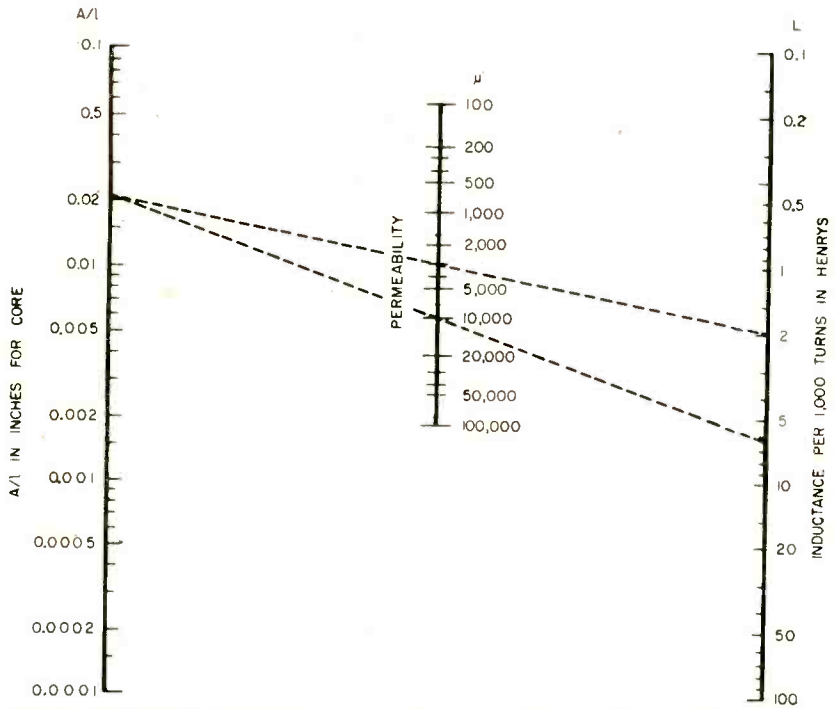

FIG. 2—Magnetizing inductance nomograph for transistor coupling transformers

ing is the shunt magnetizing inductance, L_m, across the primary. A practical equation for this is

$$L_m = K\,3.2\,N^2\,A\,10^8\,\mu\,/\,l \quad (3)$$

where L_m is magnetizing inductance in henrys, μ is incremental permeability for the core material and l is magnetic path length.

It is again possible to construct a nomograph to facilitate design calculation, if Eq. 3 is rewritten as

$$L_m' = (A/l)\,(\mu)\,(K \times 320) \quad (4)$$

where L_m' is inductance per thousand turns. The nomograph is given in Fig. 2. The minimum allowable inductance per thousand turns is determined from the circuit application of the transformer. Transformer dimensions, the turns ratio and the initial permeability are then chosen to satisfy the nomograph, and wire size to fit the available window area is found from Fig. 3.

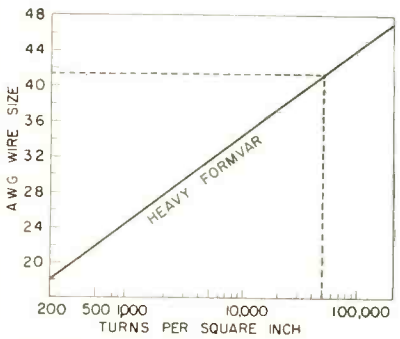

FIG. 3—Wire size chart for transformers using heavy Formvar insulation on windings. For single Formvar or plain enamel, increase turns per sq in. by six percent

Example of Use

A transistor transformer is to be designed for matching a 5,000-ohm source to a 500,000-ohm load, using a 10-v, 400-cps primary and a 6.6-v secondary. Maximum phase shift is 10 deg.

When the transformer is operated from the specified source impedance, neglecting transformer losses, the magnetizing inductance required for 10-deg phase shift at 400 cps is

$$L = \frac{5{,}000}{(2\pi)\ 400 \tan 10^\circ} = 11.3 \text{ h}$$

The core type is selected next, largely from experience, as a laminated core, 187 E-I, in standard 14-mil audio A. For this material, A/l is 0.0216 in., KA is 0.0309 sq in. and permeability is 10,000 at 7 kilogauss. The value of KAB is then 0.0309 × 7 or 0.216. Using this and a frequency of 400 cps in Fig. 1 gives 0.023 volts per turn for e/N.

With a primary voltage of 10 v, primary turns are 435 and must produce an inductance of 11.3 h. The inductance per 1,000 turns is 11.3 $(1{,}000/435)^2$ or 59.7 h.

To check the design, use 0.0216 for A/l and 10,000 for permeability in Fig. 2. This gives 6.3 h for inductance per 1,000 turns instead of 59.7 h, hence more turns will be necesary. After one or two trials, 2,400 turns were decided upon for the primary. From Fig. 2, with 11.3 h per 2,400 turns or 1.96 h per 1,000 turns, at A/l of 0.0216 the permeability can be as low as 3,000. From Fig. 1, with e/N at 10/2,400 or 0.00417 and frequency at 400 cps, KAB is 0.037. Flux density B then is 0.037/0.0309 or 1.19 kilogauss. At this flux density, the material characteristics indicate that the permeability is actually 4,000, hence the magnetizing inductance of at least 11.3 h can easily be achieved.

The secondary turns will now be 0.66 × 2,400 or 1,580. Total turns are then 3,980. The window area for 187 E-I is 0.0822 sq in., hence the turns per square inch are 48,400. From Fig. 3, the allowable wire size is No. 42 heavy Formvar.

Thus, the final design is a primary of 2,400 turns and a secondary of 1,580 turns, both of No. 42 heavy Formvar, with core of 14-mil 187 E-I audio A.

The nomographs in themselves accomplish a simple multiplication. This fact alone would make them of little value. However, the designer of these transformers must manipulate between the circuit requirements, core type and size and wire size until all equations and requirements are satisfied. Actual experience indicates that this trial-and-error process is greatly speeded and simplified by using these nomographs.

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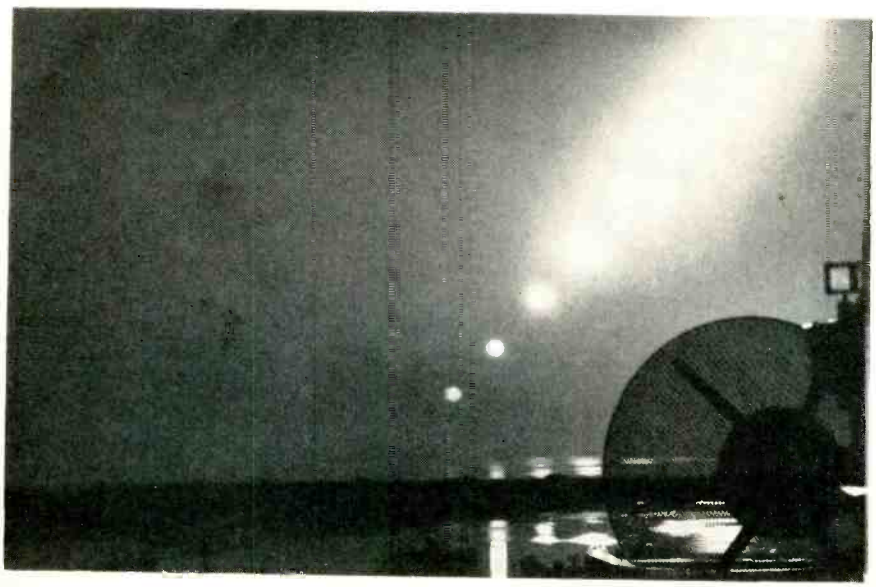
Electrons At Work

Edited by ALEXANDER A. McKENZIE

Atmospheric Effects on Propagation



Rising sun photographed at five-minute intervals appears to travel in arc

TRACKING and radio guidance of long-range missiles require precise knowledge of the refractive effects of the atmosphere. Equally important accurate vectoring information for antimissile devices must also take into account these effects. Thus the characteristics of the atmospheric effects are of great importance to the Air Force.

Using the sun as the source of radio-frequency energy, the Electronics Research Directorate of the Air Force Cambridge Research Center is studying the effect of the atmosphere on microwaves and meter wavelength radiation. Both the ionosphere and the troposphere produce refractive effects and scintillations on solar radio-frequency radiation.

► **Rising Arc**—The accompanying photo, a multiple exposure of the rising sun taken at five-minute intervals, visually demonstrates the atmospheric effects in that the sun as it rises appears to travel along an arc rather than along a straight line.

The technique used for measuring the atmospheric refraction consists of a single mount for both optical and radio-frequency measurements. A small telescope is used for sighting the position of the sun as it rises through fixed positions of the antenna. Two small parabolic dishes feed stable receivers in the 3-cm and 8-cm region. The sun essentially traces out the antenna pattern. The time difference between the sun's crossing the pattern as recorded on the radio equipment and the time it should cross according to spherical astronomy determines the amount of refraction.

Along with the measurement of the apparent change in position of the sun, the absorption of the atmosphere as a function of angle of elevation and meteorological conditions is determined. Fluctuations in signal are also seen at the lower angles indicating the irregularity in the troposphere. These scintillations are produced by variations in the lower atmosphere and are not apparent at higher angles of elevation.

Sleeve Radiator for TV Reception

By GEORGE P. KEARSE
Senior Engineer
Radiation Laboratory
Temco Aircraft Corp.
Garland, Texas

THIN DIPOLE antennas are not well suited to broadband operation owing to large variations in impedance and radiation patterns. Impedance variations can usually be compensated by well-designed matching transformers but the radiation patterns are entirely dependent upon the geometry of the dipole and its proximity to ground and other objects.

These pattern changes are not minimized unless its construction is appreciably changed. At higher frequencies increasing the cross-

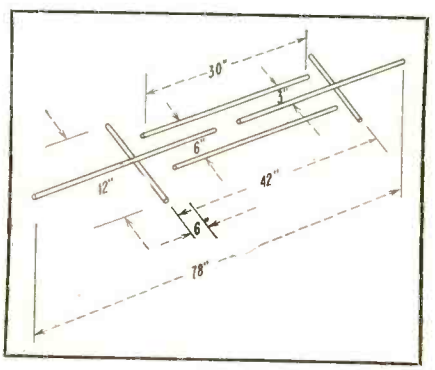


FIG. 1—Configuration of 54 to 220-mc sleeve dipole

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MODEL	Volts	Current	Regulation Line 105-125	Regulation Load 0-Max.	Ripple	Recovery Time*	Stability For 8 Hours	Output Impedance DC-20 ~	Output Impedance 20 ~ —100 KC	Dimensions W	Dimensions H	Dimensions D	Price
2600	0-60	0-2 Amp.	5 Mv.	5 Mv.	1 Mv.	50 μ sec.	10 Mv.	0.002 Ω	0.0005Ω	19"	10½"	17"	$690
2650	0-60	0-5 Amp.	5 Mv.	5 Mv.	1 Mv.	50 μ sec.	10 Mv.	0.001 Ω	0.0002Ω	22½"	28"	19"	$1190

***Good** stability*
***Fast** recovery time*
***Low** output impedance*
***Excellent** regulation*
***Low** ripple*

POWER REQUIREMENTS: 105-125 volts, 60 cycles.
FUSE PROTECTION: Input and output fuses on front panel. Time delay relay is included to prevent unregulated voltage from appearing at the output terminations.

OUTPUT TERMINATIONS: DC terminals are clearly marked on the front panel. Either positive or negative terminal of the supply may be grounded. DC terminals are isolated from the chassis. A binding post is available for connecting to the chassis. All terminals are also brought out at the rear of the unit. Two terminals are mounted at the rear of the chassis to provide for picking up the error signal directly at the load. This connection compensates for the voltage drop in the wires (and ammeter) connecting the power supply to the load.

METERS: Ammeter: 0-2 amperes, 4" rectangular for Model 2600
0-5 amperes, 4" rectangular for Model 2650
Voltmeter: 0-60 volts. 4" rectangular

CONTROLS: Power on-off switch, DC on-off switch, remote error signal on-off switch, coarse and fine voltage controls. The coarse voltage control is a ten turn potentiometer which varies the voltage from 0-60 volts. The fine voltage control is a ten turn potentiometer which varies the voltage 1 volt. The voltage divider network allows a 61 volt variation in output voltage.

*Recovery time is less than 50 microseconds. The excursion in the output voltage during the recovery period is less than 50 millivolts for line fluctuations from 105-125 volts or load variations from 0-to maximum current.

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section area by means of large conductors, either actual or simulated, reduces pattern and impedance changes with frequency. The conical configuration represents a design widely used to minimize these variations. On the lower frequencies, however, even the conical dipole passes a point of diminishing returns.

The coaxial construction of the sleeve dipole[1] involves mechanical difficulties that also prevent its use in the vhf television channels. However, use of the sleeve principle where overall length of the antenna resonates at one frequency and the length of the sleeve section resonates at a higher frequency results in an excellent dipole element for television applications provided that a different construction be found for the sleeve section.

Since the sleeve section of the dipole is essentially a short length of coaxial transmission line connected in series with short antenna elements, it was believed that another type of transmission line could be used equally well and retain the broadband performance desired.

The three-wire transmission line with the two outer conductors grounded[2], seemed applicable to the sleeve dipole principle. A sample

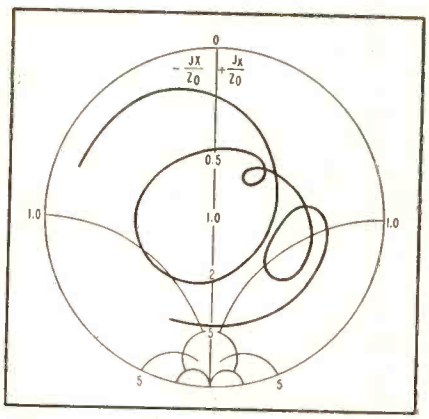


FIG. 2—Impedance plot of sleeve dipole over range from 54 to 220 mc

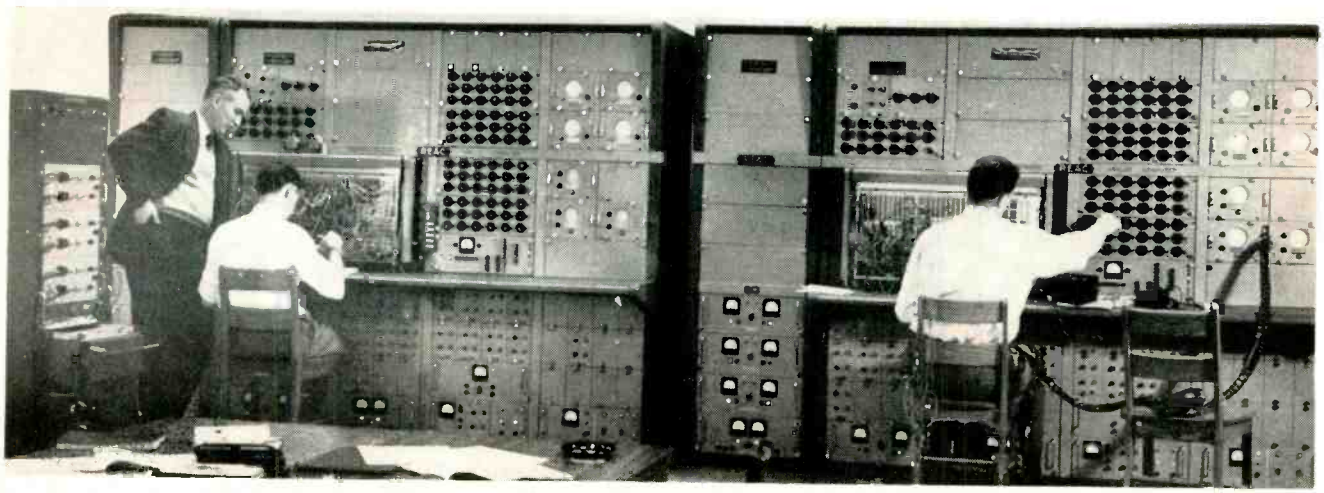
was constructed and measured. The data indicated that the three-wire transmission line section produced a broadband element that would hold its bi-directional patterns, over a frequency range up to 4 to 1.

Further tests indicated that this range could be increased by changing the current distribution on the end sections of the dipole. This was accomplished by mounting short conductors on the dipole close to each end of the transmission-line section. The upper frequency limit is reached when the length of both the transmission-line section and the short conductors approach one-half wavelength. Above this frequency, the pattern changes to one that is normal for a harmonically operated antenna.

Since this dipole is the outgrowth of a television antenna investigation the dimensions and data are shown for the vhf television bands. It is believed, however, that essentially the same performance could be duplicated on much lower frequencies. Figure 1 shows a sketch of this dipole designed to operate in the frequency range of 54 to 216 mc. Figure 2 shows impedance variations from 50 to 220 mc that appear normal for a dipole operating over such a wide frequency range. Figure 3 shows the measured radiation patterns. The bidirectional patterns remain essentially constant.

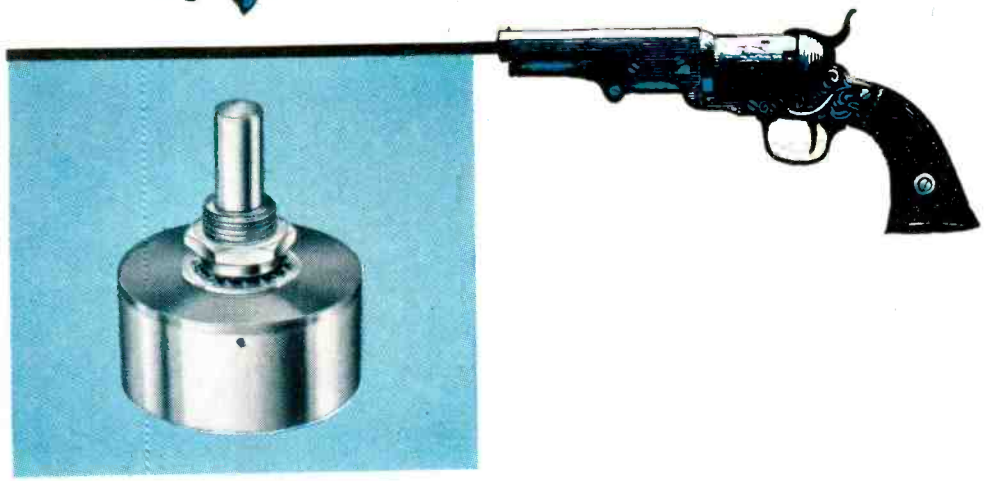
The first application of this dipole was to an antenna for vhf television reception. In this application, it was necessary to substitute a folded dipole for the driven element to raise impedance. The short conductors were also found to be unnecessary. The folded dipole was cut to a half wavelength at the low-frequency end of the lower tv channels, while the transmission line section was cut to a half wavelength in the low-frequency end of the upper tv channels. Separate reflectors, spaced approximately a quarter wave-

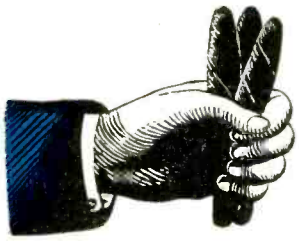
Canada Gains Computing Center



Two identical analog computers that can be used independently or connected together have been installed in the new computing center of Computing Devices of Canada, Ltd. The machines are Reeves Reacs built to CDC specifications and are for use by engineering organizations on a rental basis. The instrument on the left is a recording voltmeter used to make permanent records

Another product surprise from Helipot!





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Tooting a symbolic clarion and passing out imaginary cigars, Helipot introduces one of its new-born offspring . . . the series 5300 precision potentiometer.

A single-turn unit, it's 1-1/4 inches in diameter . . . designed for bushing mounting. With its innards comfortably ensconced in an accurately drawn one-piece aluminum cup, the 5300 gives you ruggedness, compactness and long life. We proud papas direct your attention to such salient features as the range of total resistance . . . from 25 to 49,000 ohms . . . linearity as close as ±0.25% . . . and considerable improvement in torque, noise and mechanical runout.

For vital statistics on this prodigy of a progeny, write for data file 321.

Helipot makes precision potentiometers . . . linear and non-linear . . . in the widest choice of sizes, mounting styles and resistances. Many models are stocked for immediate shipment. Our engineers will gladly adapt standard models to your requirements or design entirely new HELIPOT* precision potentiometers for you.

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length at their respective frequencies, were first tried. It was found that side lobes were produced by radiation from the extremities of the long folded dipole when the antenna was operated on the upper frequencies. A three-section reflector was found necessary to produce the desired patterns.

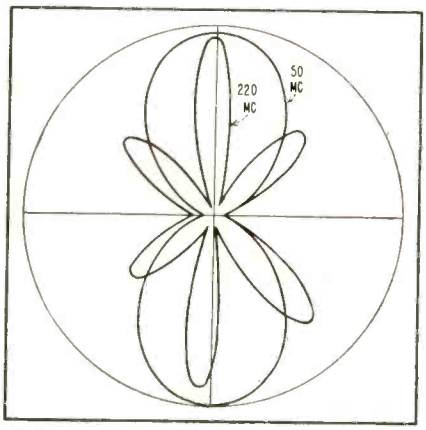


FIG. 3—Radiation pattern of sleeve radiator at extremes of frequency range

The author wishes to thank Norbert Sladek and Allan Crites who built the samples, took the data and otherwise assisted in the development of this dipole and R. M. Soria for his guidance and constructive criticism. The work was done while the author was with Amphenol Electronic Corp.

REFERENCES

(1) "Very High Frequency Techniques," Vol. I, Radio Research Laboratory, Harvard University, McGraw-Hill Book Co., Inc., New York.
(2) E. A. Laport, "Radio Antenna Engineering," McGraw-Hill Book Co., Inc., New York.

Light Actuated Transistorized Counter

By JOHN GRANT
Applications Department
Electronics Division
Sylvania Electric Products
Woburn, Mass.

Many circuits and devices have been used for controlling a relay or other actuating mechanism by the light falling on a photocell. This article will describe a simple circuit using semiconductor devices. It incorporates a 1N77A photodiode and two 2N35 germanium junction transistors.

The light-actuated section of the circuit is a bridge in which the 1N77A photodiode is one leg. The diode's reverse resistance is approximately balanced by the 100,000-ohm resistor. The opposite side of the bridge is a 50,000-ohm potentiometer. The potentiometer is used to vary the no-signal current through the relay and to set the overall circuit gain by biasing the transistors into a higher gain region.

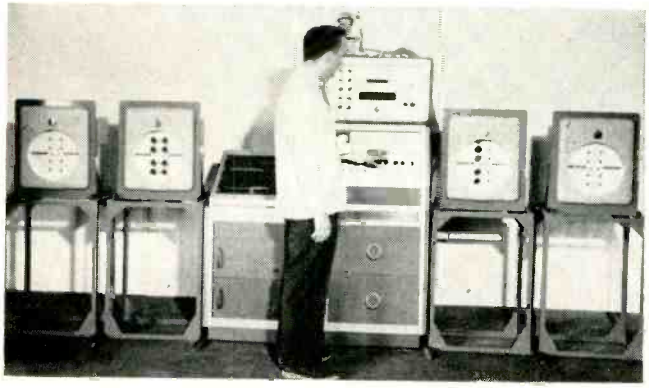
The two-stage transistor amplifier is connected in the common-collector configuration to take advantage of the maximum available current gain. The 10,000-ohm resistor increases somewhat the second stage transistor stability and keeps the amplifier input impedance at approximately 100,000 ohms for maximum power gain.

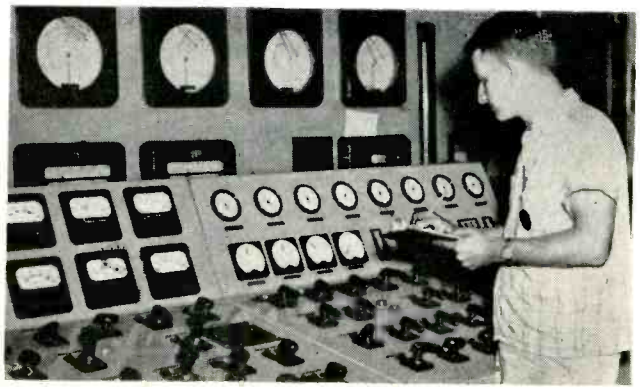
When a light beam strikes the light-sensitive junction of the photodiode, the reverse resistance of the diode decreases, thereby increasing the voltage at the base of the first transistor. The increased voltage allows emitter current to flow from the first transistor into the base of the second transistor. The increased base current of the second transistor increases the emitter current through the relay coil and actuates the relay armature.

If the 50,000-ohm potentiometer is not adjusted correctly, the voltage at the base of the first transistor will be too negative with respect to its emitter for the change in bridge voltage to turn the transistor on. On the other hand, if the potentiometer is set too far in the opposite direction both transistors will stay on. A small amount of experimentation will give the potentiometer setting for the best operation of the amplifier.

The relay used in this setup was

Boiler Analysis By Remote Control





Designed to analyze operation of a giant steam generating unit in a few hours, a system developed jointly by Babcock & Wilcox and Bailey Meter can make use of a central computer in New York City over teleprinter circuits. After the information has been evaluated, the resulting figures are returned to the boiler site for application by technicians. Data indicated at the boiler room control point (right) is likewise picked up by equipment (left) that transforms signals to digits and punches out tape on a perforator

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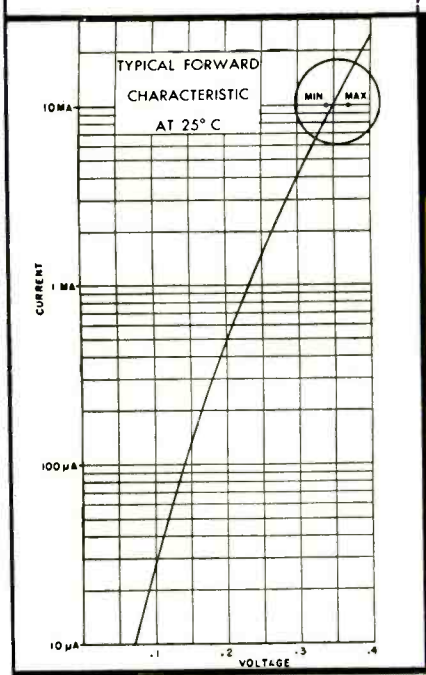

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Characteristics at 25° C

Forward voltage drop @ 10MA	
Minimum	0.34V
Maximum	0.37V
Maximum reverse current at −10V	10UA
Peak inverse voltage	60V

Maximum Ratings at 25° C

Maximum inverse operating voltage	50V
Continuous DC forward current	100MA
Surge current for 1 second	500MA
Average power dissipation	80MW
Derating above 25° C	10MW/10° C

DR 385 exhibits fast transient response and similar diodes can be offered fully tested to your recovery conditions.

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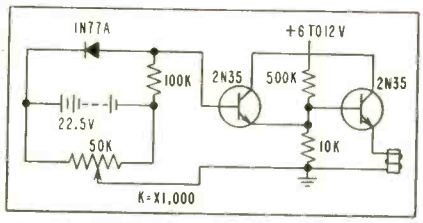
a Sigma 5F-1000-G. It was set to close at 4 ma and open at 2 ma. Approximately 5 to 6 ma can be drawn through the relay for positive switching action.



Light operated relay will trigger counter tube at rates better than 60 counts per sec

With a miniature 22.5-v battery and a 6-v battery, the entire device can be built in a box smaller than 6 in. x 2 in. x 2 in. The output of the relay has been used to control a mechanical counter up to 200 counts per minute. If used in conjunction with a glow transfer counter tube, rates better than 60 counts per second could be easily handled. The photodiode frequency response is about 15 kc and the transistors can handle 600 kc.

Applications are as a headlight controlled garage door opener and a production-line controller for counting and material detection. Clear glass rod of ¼ in. diameter has enough diffusion effect on a small light beam to actuate the counter. An automobile headlight will trigger the amplifier at distances of the order of 10 feet or more depending on whether an optical system is used to concentrate the light beam.

The battery drains are small with no-signal drains of the order of 0.5 ma. Either delayed relay pull-in or drop-out may be obtained by placing a 10 μf capacitor either from the first transistor base to ground or across the 10,000-ohm resistor. Varying the capacitor will allow delays of 10 seconds or less.

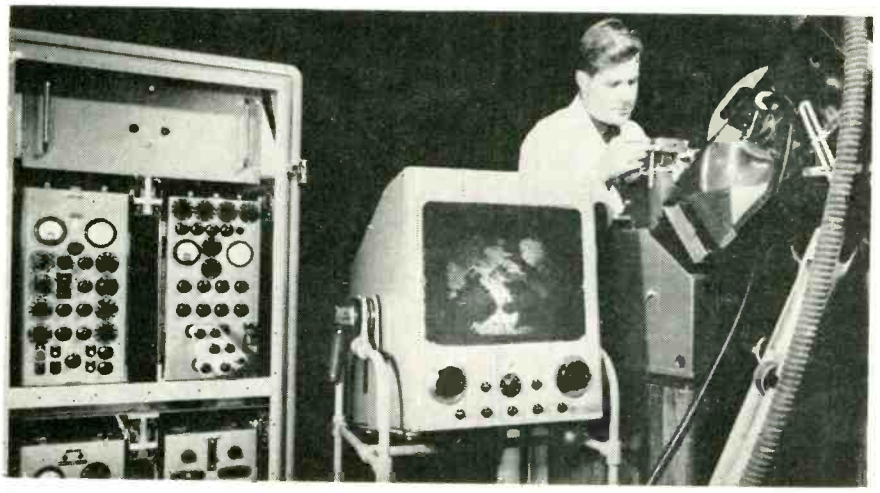
Grid-Operated Thyratron

By L. L. BOYARSKY
Dept. of Anatomy and Physiology
University of Kentucky
Lexington, Kentucky

BIOLOGICAL INVESTIGATIONS require the use of a relay activated when contact is made through an animal. In measuring the drinking rate, for example, the animal's tongue touches a drinking tube and contact is established. The current through the tongue is of the order of microamperes, so that a current amplifying device is needed.

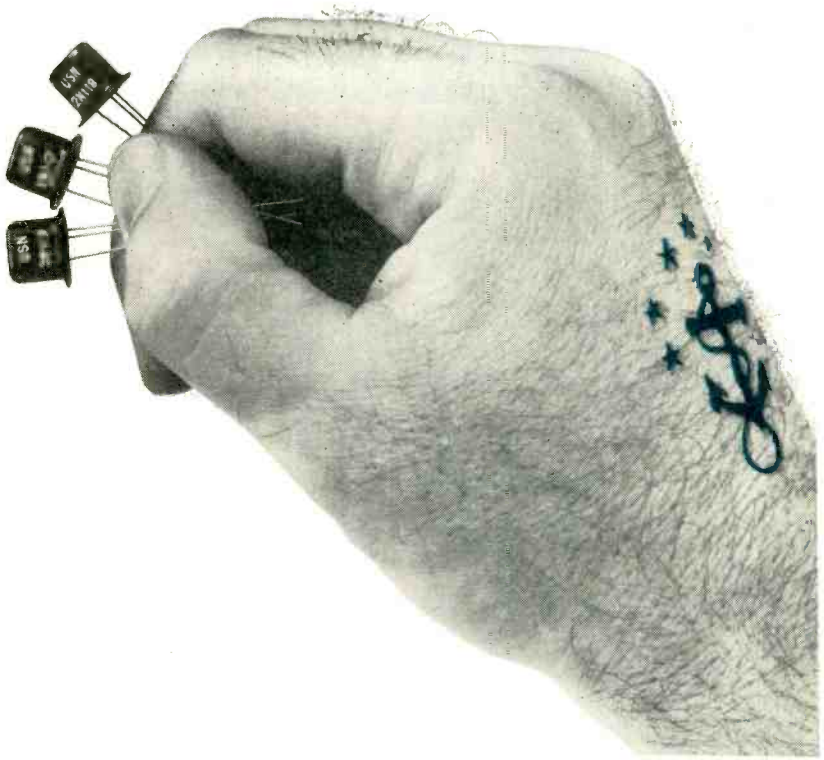
The circuit shown here is designed on the basis of a rarely used property of gas-discharge tubes. Usually, the plate voltage must be

British Atomic Research Uses TV



Experimental television microscope used at Britain's Atomic Energy Research Establishment, Harwell. A demonstration image is shown on the 15-inch screen. Purpose of the equipment is to enlarge highly radioactive metal specimens without damage to the eye of the researcher

FIRST silicon transistors meeting NAVY SPECS



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All 20 Texas Instruments silicon transistor types have proved themselves in military use. First and largest producer of silicon transistors, TI is the country's major supplier of high temperature transistors to industry for use in military and commercial equipment.

degradation rate tests for TI's USN-2N117, USN-2N118, and USN-2N119

test	condition	duration	end point at 25°C
lead fatigue	three 90-degree arcs	—	no broken leads
vibration	100 to 1000 cps at 10 G	3 cycles, each x, y, and z plane	I_{CO} = 2 μA maximum at 5V
vibration fatigue	60 cps at 10 G	32 hours, each x, y, and z plane	h_{ob} = 2 μmhos maximum
shock	40 G, 11 milliseconds	3 shocks, each x, y, and z plane	h_{fb} = −0.88 minimum (USN-2N117)
temperature cycle	−55°C to +150°C	10 cycles	h_{fb} = −0.94 minimum (USN-2N118)
moisture resistance	MIL-STD-202	240 hours	h_{fb} = −0.97 minimum (USN-2N119)
life, intermittent operation	P_c = 150 mW, V_c = 30V	1000 hours, accumulated operating time	
life, storage	150° C, ambient	1000 hours	
salt spray	MIL-STD-202	50 hours	no mechanical defects interfering with operation

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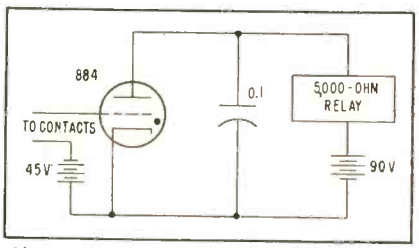
lowered if the grid of a thyratron is to regain control of the tube. If, however, the plate supply voltage is maintained at a lower level so that the plate current is low, a high negative grid voltage will turn off the tube.[1]

Using this principle, the plate voltage is lowered to 90 v and the grid voltage is placed at −45 v by conventional means. When the contact circuit is closed the tube is extinguished by the high negative grid voltage. The circuit will operate without the capacitor shown; but, if a high resistance, such as that of a body, is present in the grid circuit the capacitor must be included. Short circuit grid current is less than one microampere.

Two such circuits have performed continually for a year. The circuit also performs adequately as a drop indicator.



Closing contacts through high resistances extinguishes thyratron to operate relay

REFERENCE

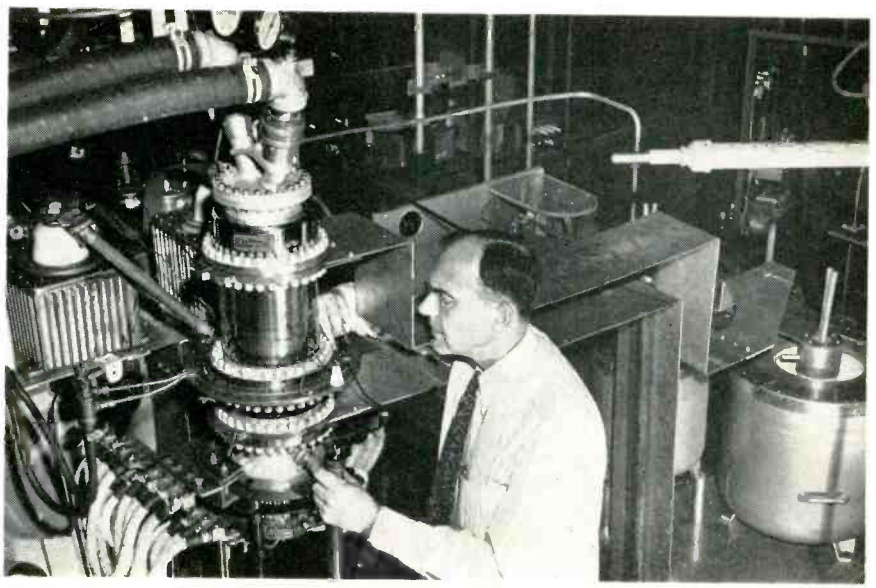
(1) I. S. Gray, "Applied Electronics", John Wiley & Co., New York, 1954.

Printed Circuit Microwave Attenuator

By JOHN W. FALLON
Sanders Associates, Inc.
Nashua, N. H.

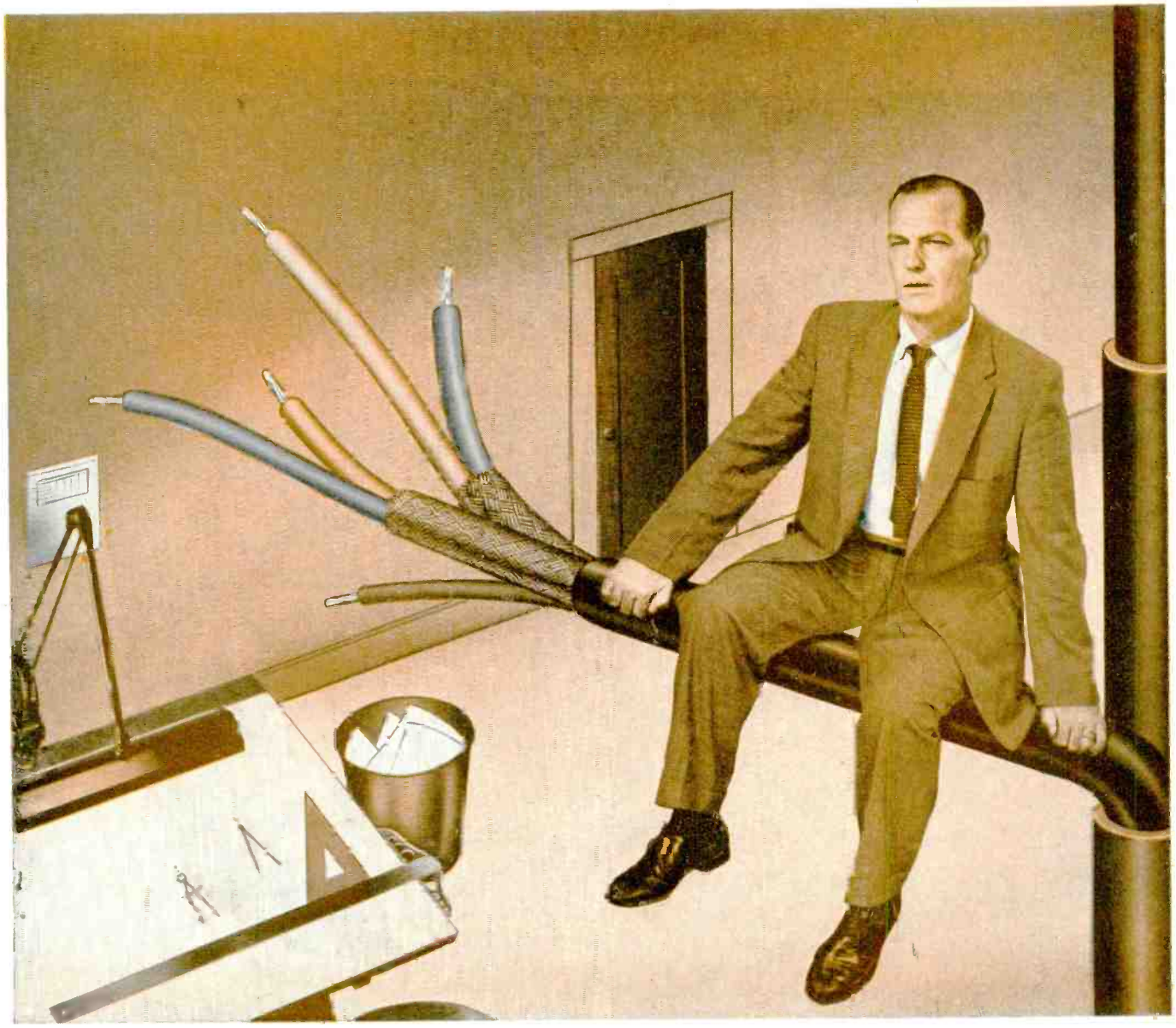
THREE basic types of attenuating devices are available for varying continuously the attenuation of a microwave signal. These are (1) coaxial, (2) waveguide and (3) cut-off, the last being essentially a combination of (1) and (2). Each of these has its own inherent limitations with respect to one or more of the following: frequency range,

Megawatt Broadcast Beam Triode



A new developmental tube undergoing test is RCA's type 5831 said to operate at a magawatt of power input through the standard broadcast band and even higher without reducing plate voltage

Up A Custom Cable Tree, Engineer ?



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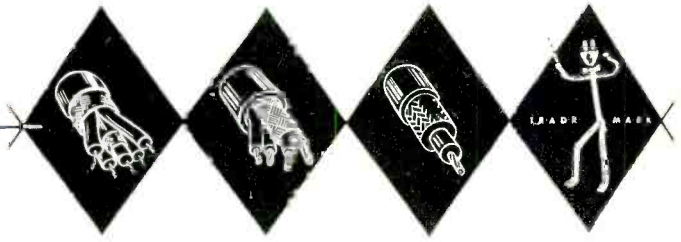
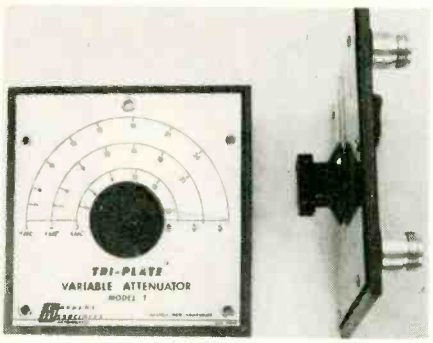


insertion loss, radiation leakage, vswr, simplicity of construction and operation, size, weight and form factor. By rotating a resistive card between the two center conductors of a strip-type transmission line, these limitations have been appreciably reduced.

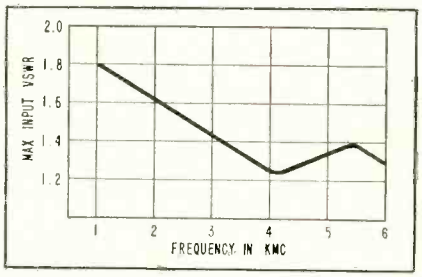


Front and side views of the attenuator

The transmission line used in the device described consists of a sandwich of metal foil and dielectric filling. It is formed from two thin sheets of dielectric, each of which has a copper film bonded to both its faces. Identical circuitry is etched on one face of each sheet, and the etched faces are placed together. Screws and eyelets that give mechanical support to the sandwich also act as shorting bars to force the two outer faces to remain at equal potential, thereby minimizing radiation leakage.

In the Tri-Plate variable attenuator, the two center conductors of the transmission line are separated by a dielectric spacer to permit insertion of the resistive card. By rotating this card, varying degrees of attenuation are obtained.

The attenuator is designed for optimum performance at 4,000 mc where the vswr is a maximum of 1.25 and attenuation is 20 db but the dial is also calibrated to indicate approximate attenuation at 3, 4 and 5 kmc.



Characteristic of the attenuator in terms of vswr vs frequency

▶**Maximum VSWR**—As shown in the curve, maximum vswr over the operating range between 1,000 and 6,000 mc is 1.8 or less. Leakage is —70 db and insertion loss is less than 1.5 db over the frequency range. The attenuator has a characteristic impedance of 50 ohms and its power rating is two watts.

Certain concessions must be made to provide a simple, reasonable accurate attenuator, variable over a wide range of microwave frequencies, capable of being matched to a low vswr, and having small insertion loss. Coaxial construction will give broadband operation, but it is too complex; the waveguide type is simple enough, but its range is restricted. A combination of the two, such as the loop-type cutoff attenuator, presents high insertion loss and an innately poor match as the price for its extreme accuracy.

Incompatible characteristics of simplicity and broadband performance are combined in this device without sacrificing other vital features. Mechanically this results

C-D Alarm

Warning device shown plugs into any convenience outlet and is activated by signal transmitted through power lines. Developed by Midwest Research Institute of Kansas City, Mo., for mass production and sale at $5, the unit might be used in 96 percent of homes wired for electricity

Design Manufacture Inspection

The Result is Reliable Choppers

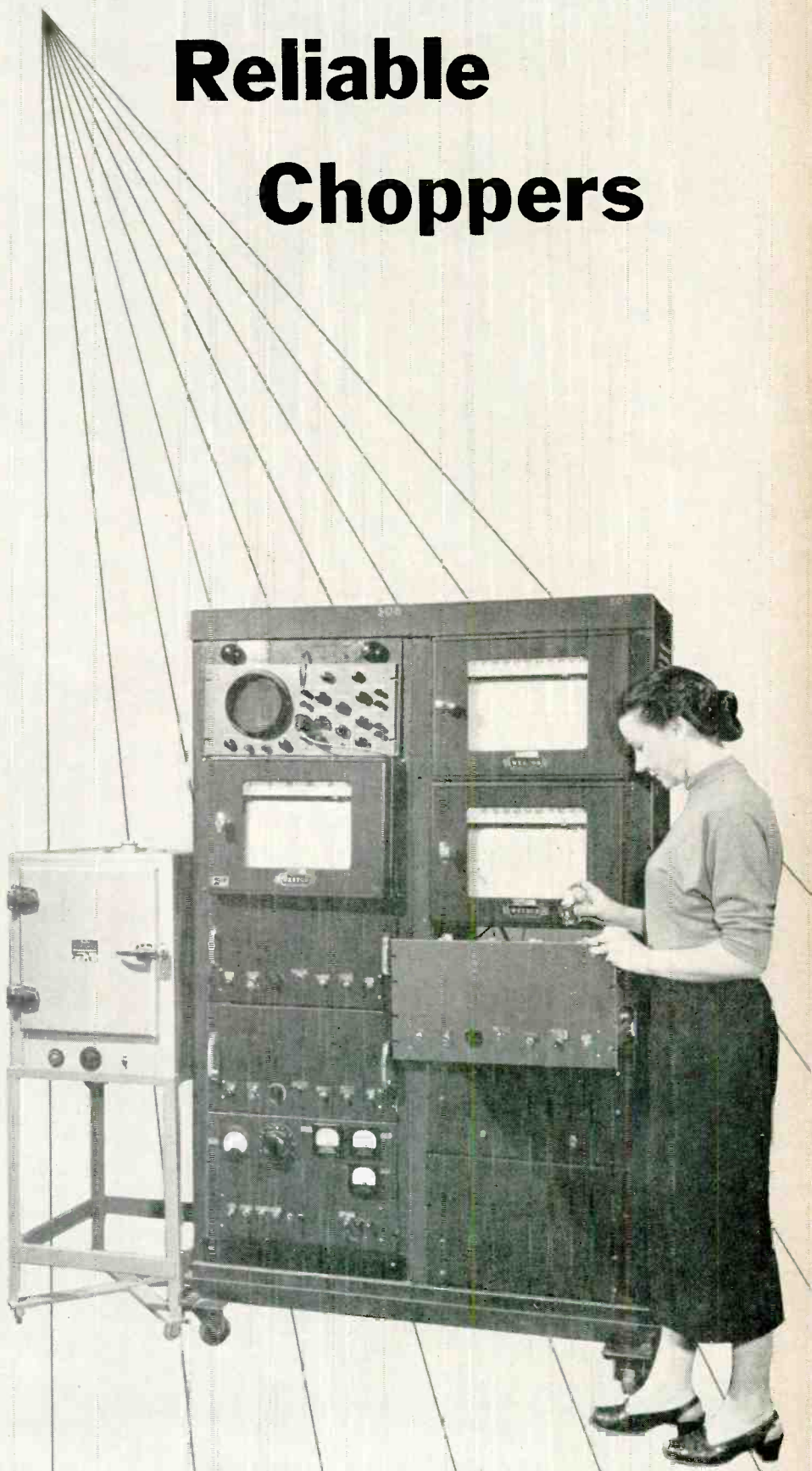
It takes all three: design, manufacture, and inspection to produce reliable choppers. Airpax chopper design is the result of years of experience with magnetic-mechanical devices. A resonant reed gives Airpax choppers positive contact action. Materials and their shapes are thoroughly considered in the design of these choppers.

Full potentialities of the design are retained in the finished choppers by careful manufacture. Skilled workers using precision machines assemble Airpax choppers in a completely air-conditioned factory.

And to be certain that Airpax choppers are actually as good as they can be, the materials that go into them are inspected before assembly and the completed choppers are inspected after assembly.

For example, the young lady to the right is placing a chopper in a special Airpax life-test rack where the chopper will be operated for at least its rated life. This rack automatically records the performance of this and other choppers at regular intervals. Any irregular behavior or signs of possible incipient failure will be amplified and plotted on the strip chart along with the life lines of other choppers sampled from production.

This record shows, in terms of hour to hour performance, how effective the design and manufacture are. The result is a reliable chopper.



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from the ease with which it can be made; electronically it is primarily a result of the fact that the *TEM* mode is the dominant mode in both this type and in coaxial lines.

Rectifier Locomotive

By J. E. WALLACE
General Electric Co.
Erie, Pa.
and
J. L. ZEHNER
General Electric Co.
Schenectady, N. Y.

SUCCESSFUL APPLICATION of standard d-c traction motors on rectified single-phase, 25-cycle power revolves about the need of smoothing the ripple resulting from rectification.

Rectified a-c has been used in industry for many years as a source of power for d-c motors. In these cases, it has been largely derived from multiphase rectifiers operating on 3-phase systems, so that the resulting current is essentially pure direct current with an

New locomotive using ignitron rectifiers to supply d-c to traction motors

insignificant amount of ripple. The ripple in the output of a rectifier operating on single-phase a-c, on the other hand, is of considerable magnitude and has a bad effect on both motor performance and maintenance. Fortunately, this ripple can be reduced by filters of a practical size to a point where it is tolerable.

When a d-c series motor is operated on rectified single-phase a-c, the adverse effect of ripple current appears in three ways: poor com-

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Military applications and equipment (radar, aircraft, missles) will benefit from the following features of HOFFMAN Silicon Diffused Junction Full-Wave Rectifiers:

COMPARISON OF CHARACTERISTICS

	Peak Inverse Plate Voltage	Max. Average Output Current	Note 2	Typical Rectifier Efficiency*
Hoffman HFWR-1	2100 V	400 ma @ 2100V (Note 1)	430 V 220 ma	98.3%
5R4-GY	2100 V	250 ma	400 V 200 ma	79.5%
5U4-G	1550 V	270 ma	400 V 200 ma	75.5%

Note 1—At 2100 V peak inverse plate voltage, 25°C ambient, with choke input to filter. Max. Avg. output current of 300 ma at 2100 V peak inverse with 12 mfd max. capacitor input to filter.

Note 2—DC output voltage and current when indicated type is substituted in a typical rectifier circuit with choke input to filter. *Operated at 1414PIV into a 1650 ohm Load

★ *High efficiency (see chart)*
★ *Long life*
★ *Maximum reliability*
★ *Long time stability*
★ *No energy loss in a hot filament*
★ *Small size—for compact design needs*
★ *No maintenance required in critical military circuits*

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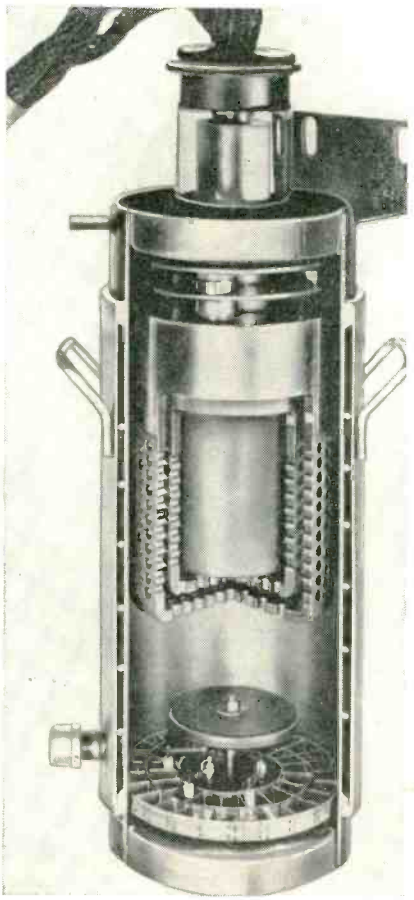
mutation, heating and torque pulsations.

The 50-cycle ripple results from rectifying single-phase 25-cycle a-c can impair commutation. The greatest difficulty is encountered when the pulsating component of the commutating flux produced by the ripple current is not proportional at every instant to the ripple



Internal view of locomotive type ignitron rectifier

current flowing in the armature. This condition results when eddy currents are present in the magnet frame and commutating pole bodies. The end result is destructive sparking at the brushes.

It is essential that this ripple current be limited sufficiently to insure acceptable commutation throughout the load range over which the motor is to operate. The obvious means of doing this is to use a smoothing reactor in the motor circuit.

The smoothing reactor is designed to complement the commutating ability of the motor. The

characteristics of the locomotive traction motor are such that the value of the allowable ripple current is constant regardless of the magnitude of the d-c component. This characteristic permits the use of a reactor which saturates with load. The impedance characteristic curve of the smoothing reactor is shown in Fig. 1.

Eddy currents produced by the ripple in the rectified 25-cycle power cause a core loss in the frame which increases the operating temperature and causes added heating of field windings. The operating temperature of the laminated armature is not noticeably affected by the presence of the ripple current. However, the continuous rating of the fields must be reduced or their allowable operating temperature raised to compensate for the additional motor heating resulting from the additional core loss caused by the ripple current.

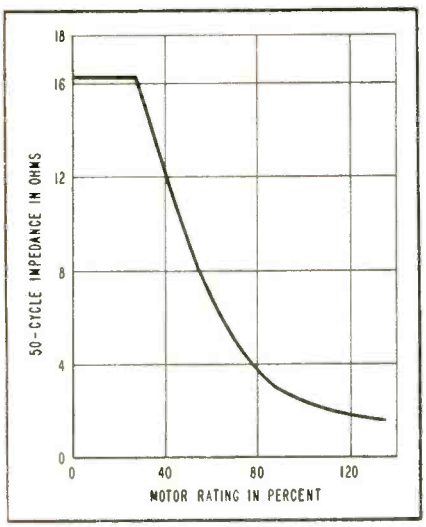


FIG. 1—Impedance characteristics of smoothing reactor used in rectifier locomotives

Tests indicate that a 50-cycle torque pulsation exists in the shaft of a motor operating on rectified single-phase, 25-cycle power. With solid gears, this torque pulsation is 9 percent of steady-state full-load torque. The substitution of resilient gears will reduce it to 4 percent. The magnitude of the pulsation with solid gears, however, is not great enough to cause mechanical failure, so the additional

expense of resilient gears is not justified.

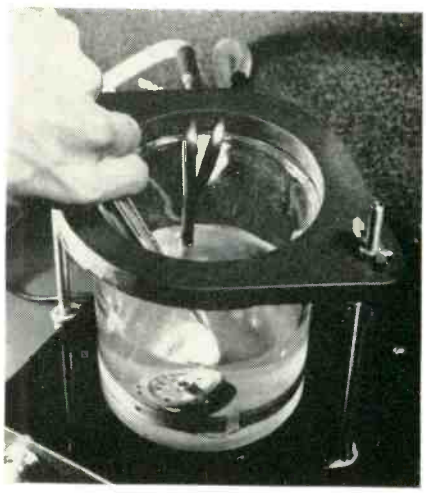
Smoothing the current supplied to the traction motors tends to cause severe distortion of the primary current wave supplied from the trolley. This distortion sets up conditions of possible telephone influence.

A number of field tests have been made to determine the amount of interference rectifier locomotives generate in adjacent telephone lines. The results indicate that telephone interference is much less than had been anticipated. It has proved of minor importance, especially where telephone lines are run in cable. Moreover, a small R-C filter circuit connected across the input to the rectifier tubes produces a substantial reduction in the noise level.

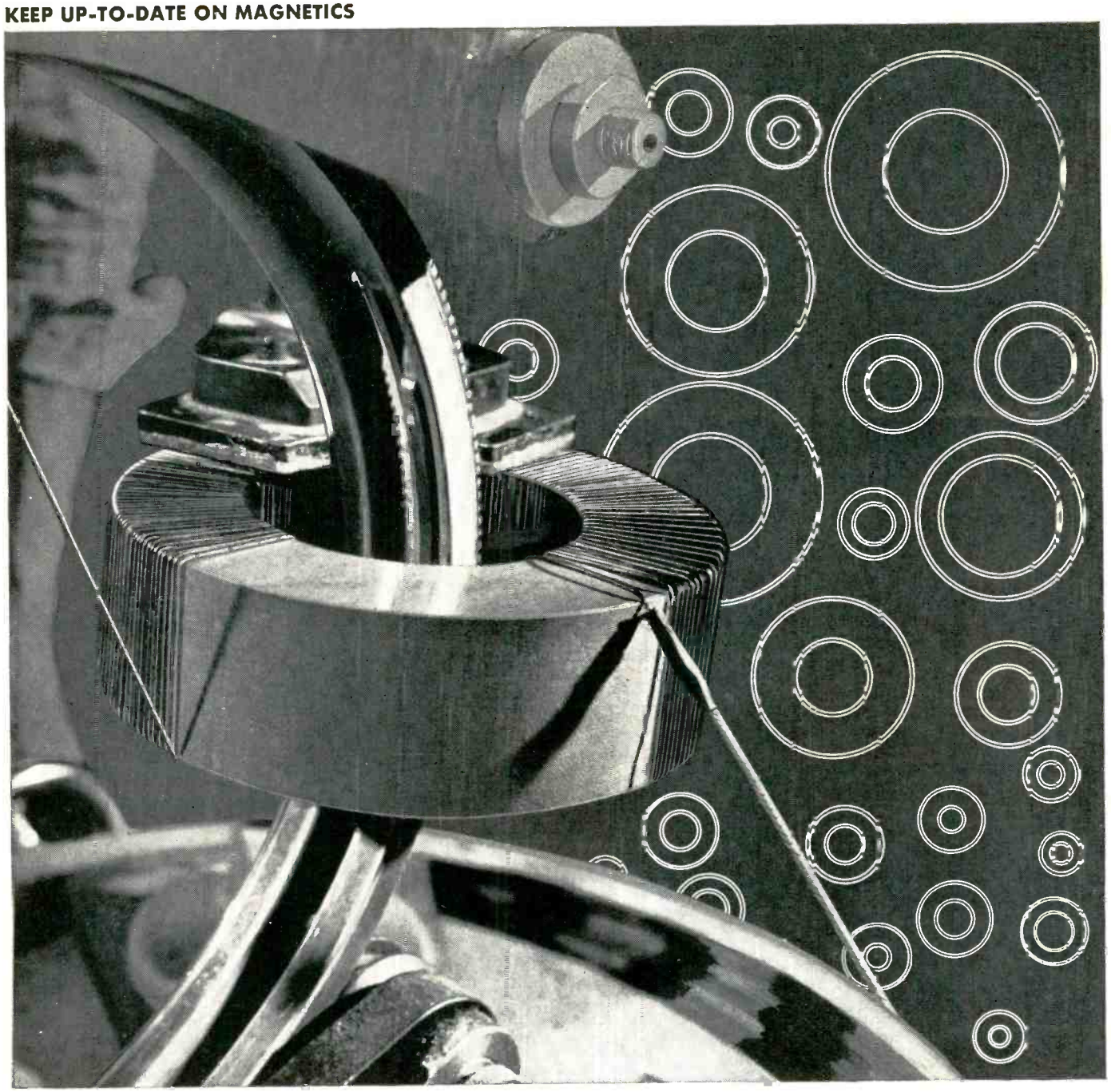
Rectifiers on locomotives are subjected to very severe operating conditions. The load may vary from zero to maximum almost instantaneously, and large blocks of power, peak outputs of approximately 1500 horsepower per motor for short periods must be handled. To assure proper operation of the tubes under conditions of wide trolley voltage variation, a flexible yet reliable control is required.

It took several years to develop a rectifier tube which meets these

Ultrasonic Cleaner



Magnetostriction oscillator produces high-frequency vibrations in cleaning solution. Resultant cavitation or effective scrubbing action removes dirt and foreign particles from gyro assembly at Kearfott plant



How will tape wound core users be affected by new size standards?

If toroidal core winding is a familiar sight in your plant, you'll welcome news that standard sizes for tape wound cores have been proposed by the A.I.E.E.* You are going to benefit from a high in consistency of core performance, brought about by our being able to concentrate on your most important sizes.

Magnetics, Inc. is now stocking all of the proposed standard core sizes in both aluminum and phenolic core boxes for immediate delivery. Consistency of core performance is increased because each size is made in large lots taken from the same alloy batch and dry hydrogen anneal. They all bear our exclusive Performance-Guarantee.

You can find all specifications for these AIEE-standardized tape wound cores in Catalog TWC-102, a new publication which, incidentally, is the most comprehensive tape wound core text published anywhere by anybody. Your copy of this Catalog-Design Manual may be obtained by writing on your letterhead to *Magnetics, Inc., Dept. E-34, Butler, Pa.*

MAGNETICS inc.

**Paper 57-206, Proposed Size Standards for Toroidal Magnetic Tape Wound Cores. Report of the Magnetic Amplifiers Material Sub-Committee, at the 1957 Winter General Meeting, A.I.E.E.*

requirements. The tube used in the New Haven locomotives and shown in the photograph is a GE type GL-6504 locomotive ignitron. It has two grids to ensure high commutating ability at high currents and high voltages. A special baffle was designed for use in the mercury pool cathode to ensure reliable ignition of the arc in spite of vibration.

The cathode connection is made at the top of the enclosing cylinder so that the cylinder forms a concentric conductor of current to the

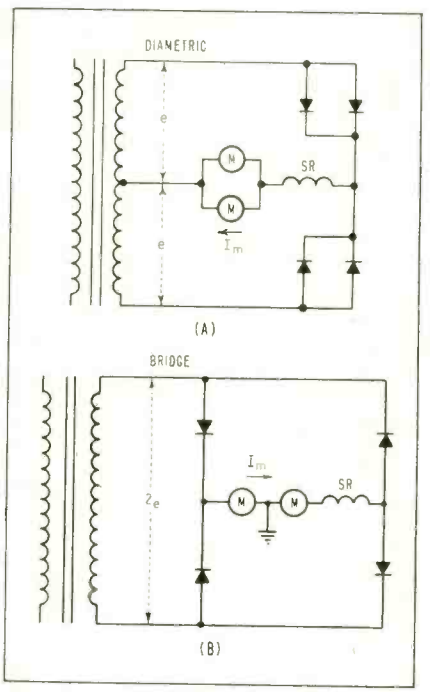
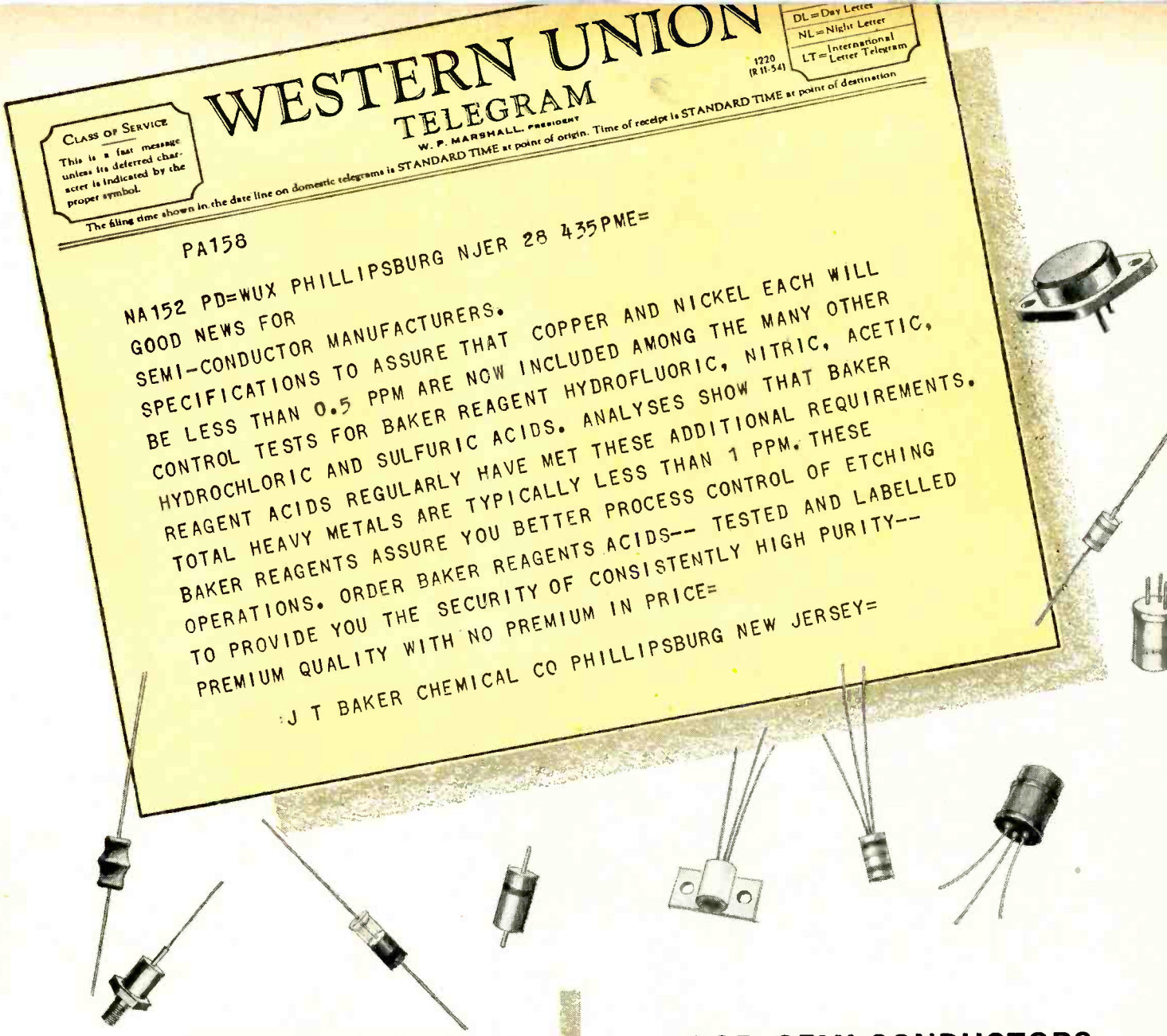


FIG. 2—Diametric (A) and bridge (B) type connections for locomotive drive motors

cathode pool, thereby reducing the magnetic fields set up inside the tube by this current. Reduction of the effect of magnetic fields on the arc stream in high-power rectifier tubes is an important factor contributing to their long life expectancy.

There are two types of rectifier connections which could be used for converting alternating to direct current. The first is the diametric connection, and the second is the bridge or 2-way connection. The principal elements of these types are shown in Fig. 2.

The diametric connection is economical of rectifier tubes at the expense of transformer weight and cost. The transformer must be



SEMI-CONDUCTOR CHEMICALS

Acetic Acid, Glacial	Hydrogen Peroxide 30% Solution
Acetone	Methanol
Ammonium Hydroxide	Nitric Acid
Carbon Tetrachloride	iso-Propyl Alcohol
Chloroform	Sodium Carbonate
Ether, Anhydrous	Sodium Hydroxide
Hydrochloric Acid	Sulfuric Acid
Hydrofluoric Acid	Xylene

OTHER ELECTRONIC CHEMICALS

Acetic Acid	Lithium Carbonate
Aluminum Nitrate	Lithium Nitrate
Aluminum Sulfate	Lithium Sulfate
Ammonium Carbonate	Magnesium Carbonate
Ammonium Chloride	Magnesium Chloride
Ammonium Phosphate	Magnesium Oxide
Antimony Trioxide	Manganous Carbonate
Barium Acetate	Methanol
Barium Carbonate	Nickelous Chloride
Barium Fluoride	Nickelous Nitrate
Barium Nitrate	Nickelous Sulfate
Benzene	Nitrate & Oxide
Boric Acid	Nitric Acid
Cadmium Chloride	Potass. Dichromate
Cadmium Nitrate	Potass. Hydroxide
Cadmium Sulfate	Radio Mixtures
Calcium Carbonate	Silicic Acid
Calcium Chloride	Sodium Chloride
Calcium Fluoride	Sod. Phos. Dibasic
Calcium Nitrate	Strontium Nitrate
Calcium Phosphate	Sulfuric Acid
Ether, Petroleum	Toluene
Hydrochloric Acid	Triple Carbonate
Lithium Chloride	Zinc Chloride

FOR SEMI-CONDUCTORS

These new control tests for copper and nickel have a double significance for the manufacturers of electronic components. They prove that:

1. Baker reagent purity regularly offers the quality-plus needed for semi-conductor manufacture.

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wound for twice the voltage of the output circuit, since the current flows alternately in the two halves of the secondary winding as first one and then the other set of tubes conducts.

During the commutating period of the rectifier, current flows in all tubes and the entire secondary of the transformer is short circuited When the nonconducting tubes start to conduct, the short-circuit current begins to build up. When it reaches half the value of the output current, the currents in the two sets of tubes are equal. Hence, the currents flowing in the two halves of the transformer secondary, being in opposite directions, result in zero net secondary ampere turns, and hence zero primary current.

The build-up continues until the current in the second set of tubes equals the output current and commutation is complete. The algebraic sum of the short-circuit current and the current originally flowing in the first set of tubes is then zero, since these currents flow in opposite directions, and current ceases to flow in the first set of tubes.

In the bridge connection, the

Small Missile Recorder

Tiny tape recorder solves problem of collecting areodynamic data from missiles too small for telemetering equipment. Developed by North American Instruments, Inc., the unit has been used to obtain skin temperatures during high-speed, high-altitude flights of a hypersonic test vehicle that reached 5,000 mph at approximately 50,000 feet. In tests at Holloman Air Development Center, N. M., one recorder was recovered and reused eight times. Other uses included testing missiles and free-flying models in wind tunnels

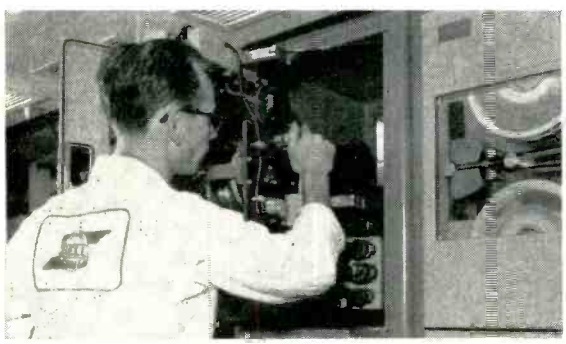
How to use a Wave Analyzer on an Ocean Wave

(or any low frequencies from 1/10th to 5 cycles per second)

A head-on attack on this problem will soon uncover the disconcerting fact that wave analyzers just don't come this big. Those of a more comfortable size generally operate on frequencies of five cycles per second and more.

But frequencies as low as 1/10th cycle per second – like earthquake waves, ship motion, and low-frequency vibrations of large machines and structures can be fed to conventional wave analyzers with completely satisfactory results. Magnetic tape recording provides an essential conversion step between.

Bell Aircraft Corporation's magnetic-recorder installation aboard the SS Mariposa for study of ship motion.



Speed change on the Ampex FR-100 is accomplished quickly and easily by a selector knob and switch.

Two Ampex FR-100 magnetic recorders were purchased and installed aboard the SS Mariposa for Bell Aircraft Corporation's study of ship motion at sea. The frequencies encountered were far below one cycle per second. These were recorded at the lowest tape speed on the recorder (1⅞ in/sec.). Reproducing the tape at the highest tape speed (60 in/sec.) multiplied the frequencies by 32. Recopying onto the second recorder and speeding up again increased the total speedup to 32 x 32 or a total of 1024. As an example, a frequency of 1/10th cycle per second became approximately 100 cycles per second and was easily separated and measured by wave-analysis equipment.

The Ampex FR-100 recorder has six standard speeds from 1⅞ to 60 in/sec. in the ratio of 1, 2, 4, 8, 16 and 32. Recopying accomplishes further multiplication by powers of two. Even a second recopying is perfectly feasible just in case you are interested in a frequency multiplication of 32,768.

Putting low frequencies onto magnetic tape requires an FM-carrier recording. On the Ampex FR-100 this is conveniently provided by plug-in amplifiers. Frequency response at 1⅞ in/sec. tape speed is 0 to 312 cycles/sec. At 60 in/sec. it is 0 to 20,000 cycles/sec. Besides its ability to record very low frequencies, FM carrier recording has the very desirable attribute of high instantaneous amplitude accuracy. Thus, the reproduced waves retain their original form very accurately through any amount of speedup.

If you have a problem that might be solved by data speedup, we would be pleased to furnish further information. Others of magnetic tape's remarkable capabilities will be the subjects of a continuing series of these bulletins. Would you like copies mailed direct? Write Dept. E-3134.

MAGNETIC TAPE APPLICATIONS BY AMPEX

1 ONE OF A SERIES

Series FR-100

Series 800 Mobile and Airborne

Model FR-200 Digital

Tape Loop Recorder

Series FR-1100

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tube action and currents flowing during commutation are much the same as for the diametric connection, except that the secondary winding of the transformer has the same voltage as the output circuit, and the current in the winding flows alternately in the two directions. Since the secondary winding of the transformer carries current during the entire cycle, the transformer is utilized to the fullest extent.

On the other hand, when using the diametric connection, two secondary windings are required, and each carries current for only half of the time. This means that there must be 40 percent more copper in the secondary winding of a diametric-connected transformer than for a bridge-connected transformer. As a result, the transformer as a whole has approximately 20 percent more kva and 10 percent more weight.

▶ **Duty Time**—Per rectifier tube it is the same for either of the two connections, provided the motor circuits are connected so that the output voltage of the diametric circuit is one-half that of the bridge circuit. This does not consider fault currents. When a tube arcs back, the arc-back current will be one-third greater for the diametric connection than for the bridge.

The bridge connection provides advantages desirable for locomotive design to insure maximum performance with minimum weight and cost.

One of the most important control considerations of a rectifier locomotive is to insure that the tubes will fire over a wide range of trolley voltage. Ignitron rectifiers require pulsed firing voltages to start tube conduction at the beginning of each half cycle. The firing circuits which provide this voltage are supplied from the same source as the power to the rectifier tubes. Because unusual conditions may result in low trolley voltage, it is essential that the firing circuit be designed to provide for locomotive operation over a relatively wide range of voltage. Firing circuit operation is complicated by the fact that rectifier commutation involves a system short circuit

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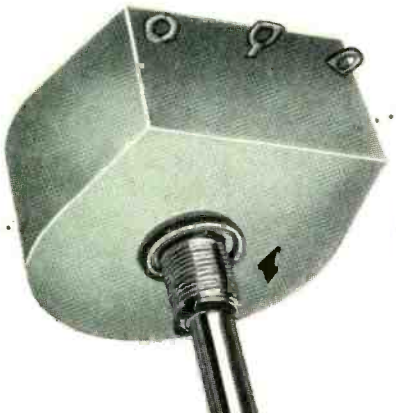

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Select that Clarostat standard wire-wound or composition-element potentiometer (Series 10, 48M, 49M, 43, 37, 51 or 58) for superlative electrical and mechanical characteristics.

Then, if you wish a water- and vapor-tight housing, have it **encapsulated.** That's the Clarostat POTPOT encapsulated control. Completely sealed with exception of external shaft assembly and terminal ends. Special water-tight provision for shaft. Meets MIL-STD-202 Test Specification. Also necessary salt-spray, humidity and temperature cycling requirements of MIL-E-5272.

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during the commutation period. The result is that a notch is cut into the applied voltage wave as supplied to all rectifiers on the line at any given time. This commutating notch becomes worse as the supply voltage falls and with any increase in trolley circuit reactance as the locomotive traverses the line.

To insure that the rectifiers will continue to operate under all reasonable low-voltage conditions, the excitation circuits are designed to provide a firing pulse of long duration. This insures firing circuit stability and makes them capable of operating over the desired voltage range.

Ignition of the rectifier may be prevented by short-circuiting the firing circuit output by a high-speed relay. By connecting the relay to suppress ignition in the event of a tube arcing back, the normally conducting tubes may be prevented from feeding current into the faulty tube for more than one-half cycle. Arc suppression thus provides rapid interruption of arcback current and reduces the duty-time on tubes, transformer and contactors during faults.

Movable-Anode Tube

BLOOD pressure measurements and a correct reproduction of pressure variations are of importance in biology and medicine. The principle of the manometer described here is a transmission of the pressure variations acting on the membrane into variations of an electric current. This is accomplished by means of a mechanoelectronic transducer tube, RCA type 5734.

This subminiature triode has a movable anode with a small extension shaft protruding through the center of a thin air-tight metal diaphragm. An angular displacement of the anode shaft will change the distance between the anode and cathode causing a change of anode current.

The transducer tube housing is directly joined with the membrane housing as shown in Fig. 1. The housing consists of a cone shaped hydrodynamic chamber and the

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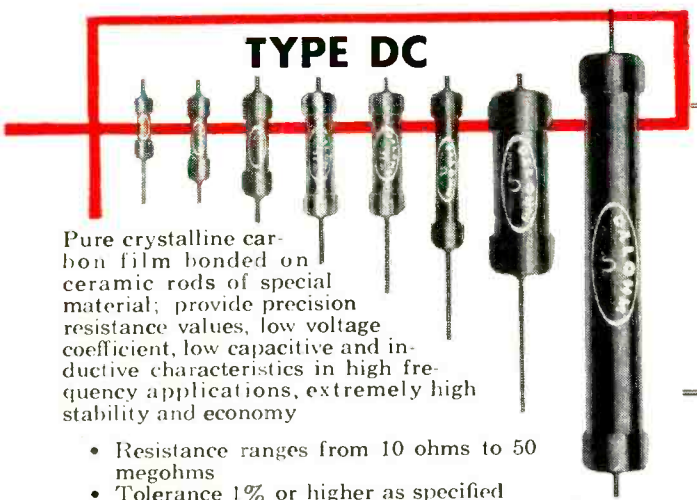
TYPE DC

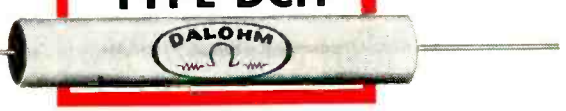


Pure crystalline carbon film bonded on ceramic rods of special material; provide precision resistance values, low voltage coefficient, low capacitive and inductive characteristics in high frequency applications, extremely high stability and economy

- Resistance ranges from 10 ohms to 50 megohms
- Tolerance 1% or higher as specified
- Five wattages—⅛, ¼, ½, 1 and 2; eight physical sizes

Write for Bulletin R-24A

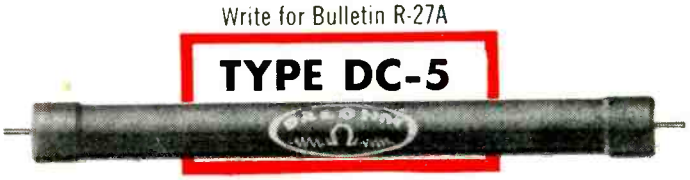
TYPE DCH



Essentially the same as type DC except hermetically sealed in a non-hydroscopic ceramic envelope to provide absolute protection against thermal shock, salt water immersion and humidity.

Write for Bulletin R-27A

TYPE DC-5



For extremely high resistance where maximum stability is a prime factor in high voltage applications. Powered at 5 watts; high voltage up to 20,000 VDC; resistance range 1 megohm to 200 megohms; tolerance 1% or up to 10% on request.

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See It At The I.R.E. Show

You can see the complete line of DALOHM precision resistors, potentiometers and collet-fitting knobs, including the products depicted above, at the I. R. E. Show in New York, March 18-21.

You are cordially invited to stop at the Dale Products, Inc. booth, Number 2742-2744. We'll be looking for you.

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connection tube. This tube is connected to the artery or vein under observation by a hollow needle.

The movable-anode tube is placed somewhat off-center in relation to the membrane to enable the pin to rest in the center of the membrane. The pin and the membrane are adjusted to impart to the anode shaft a degree of deviation from its neutral position.

Maximal angular displacement from that position when in operation is 0.15 deg in either positive or negative direction. Through its strong tendency to return to its neutral position the anode therefore always presses the pin firmly against the membrane and will correctly follow the movements.

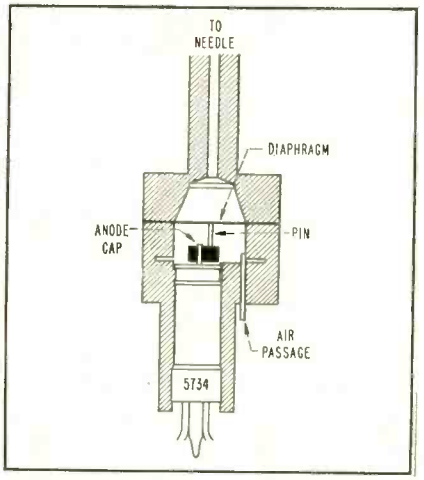


FIG. 1—Cross-section of pressure chamber. Tube anode is connected to diaphragm by pin

The membrane is made of platinum and has a free diameter of 12 mm and a thickness of 0.2 mm. The sensitivity of the system is so high that a deflection of the membrane of only 10^{-5} mm will be recorded.

The output voltage of the transducer tube is large enough to simplify amplification. The working properties of the transducer tube, however, make an amplification necessary to get complete linearity of the response curve. With an anode voltage of 250 v and an anode load resistance of 75,000 ohms this is attained, but the relatively large anode dissipation causes overheating, owing to the thermal insulation of the tube housing. Lowering anode load

MICROWAVE PROGRESS

Frequency Measurement Devices

A couple of years back, it seemed to us that there were almost as many frequency measuring devices as frequencies. Anticipating that, sooner or later, some sort of definitive material would be needed, our engineer, Bob Lebowitz, consolidated the scattered, available information into his excellent report, "Frequency Measurement Devices"

This report provides a valuable summary of the various equipment types for measuring frequencies in the 300 to 40,000 mc/s range, and a succinct reference source for their respective design considerations and applications. It covers coaxial and cylindrical cavity wavemeters; crystal oscillator frequency standards; and use of stable reference spectral lines.

Most of the commercial requirements for precision are met by open circuited coaxial and right cylindrical waveguide cavities. Since the $\lambda/4$ and $3/4\ \lambda$ coaxial cavities can be made smaller than right cylindrical waveguide cavities, they are generally preferred for lower microwave frequency measurements. To overcome the critical design problem of contacting the movable plunger without introducing contact resistance in coaxial frequency meters, it has been found more satisfactory to use a non-contacting choke system rather than shorting fingers.

Broadband cavity frequency meters have accuracies that vary between .01 and 1%. For accuracies greater than .001%, low frequency quartz crystal standards are utilized. For microwave applications, multiplying and heterodyning means are required to compare the l.f. frequency oscillator signal with the signal of unknown frequency.

Although we've tried to cover most of the aspects of Bob Lebowitz' report in the preceding paragraphs, space has forced us to omit many of the important details. But, the full report on frequency measurement devices is available to you for the asking. Just request on your company letterhead, "PRD Report Vol. 2 No. 2C".

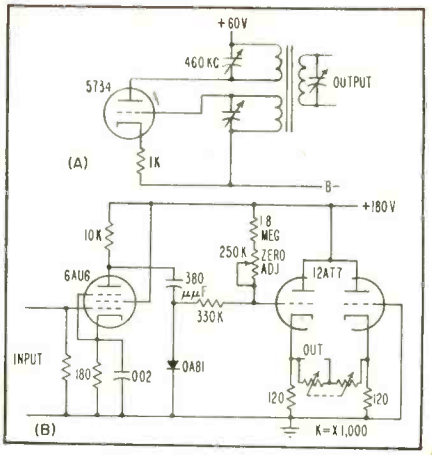


FIG. 2—Oscillator (A) and amplifier (B) used with blood pressure recorder

resistance, on the other hand, would cause nonlinearity.

Originally, direct-coupled amplifiers were used. In addition to the operating temperature problem, some difficulties were experienced in obtaining complete zero stability. Successful operation was finally obtained by having the transducer tube working as an oscillator. The oscillator circuit is shown in Fig. 2A.

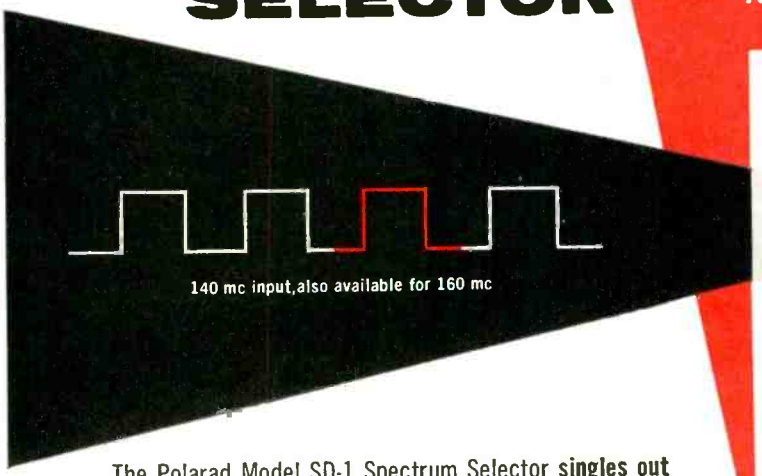
Experiments with a number of different oscillating frequencies have shown that a frequency in

Voltage Multiplier

Used to simulate high voltage created on aircraft by clouds, which are composed of microscopic ice crystals, the leaning r-f type voltage multiplier built by Stanford Research Institute can attain as much as 200,000 volts

MULTI-PULSE SPECTRUM SELECTOR

Permits spectrum analysis of individual microwave pulses in a pulse group in the fields of IFF, beacons, interference coding, radio telemetering and radar.



Model SD-1

The Polarad Model SD-1 Spectrum Selector **singles out** a particular microwave pulse from a coded pulse chain so that it can be examined individually on a Spectrum Analyzer or Microwave Receiver.

Operation is simple. A pulse group is displayed on the CRT of the Selector. The pulse to be analyzed is intensified on the scope, and at the same time an automatic electronic gate allows only this pulse to pass through to the Spectrum Analyzer.

The Model SD-1 has been designed for use with Polarad Models TSA and LSA Spectrum Analyzers as well as microwave receivers within the frequency range of the instrument. Its operation does not affect the performance or restrict the frequency of the Spectrum Analyzer to which it is connected.

Write to Polarad or your nearest representative for complete information.

FEATURES:

- Makes possible the spectrum analysis of individual pulses in a pulse group.
- CRT display of a pulse group.
- Sweep expansion provided for inspection of closely grouped pulses.
- Pulse intensification to facilitate pulse selection.
- Automatic gating of spectrum analyzer, during the interval of pulse analysis.
- Continuously variable sweep width.
- Continuously variable gate width and gate position for pulse selection.
- Triggered sweep on first pulse in any pulse train.
- Provision for external sync and gate.
- Completely self-contained portable unit.

SPECIFICATIONS:

Gate Width
Continuously variable from 0.4 to to 10 μsec.

Gate Delay
For the Model SD-1
Continuously variable from 0.3 to 180 μsec.
For the Model SD-1X
Continuously variable from 1 μsec to 350 μsec.

Maximum Pulse Train Time
For the Model SD-1 ..... 180 μsec.
For the Model SD-1X ..... 350 μsec.

Minimum Pulse Rise Time.....0.05 μsec.

Minimum Pulse Separation
0.5 microsecond between first and second pulses; 0.2 microsecond between any two following pulses.

Pulse Repetition Rate....10 to 10,000 pps.

Minimum Pulse Width.....0.1 μsec.

R-f Input Frequency
160 mc input also available for 140 mc input

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Reliable maintenance service throughout the country is an important part of the Polarad instrument.

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the range from 400 to 500 kc is the most suitable. Used in this way, the transducer-tube anode voltage needed will be only about 60 v and the anode current is about 200 μa. Anode dissipation is too small to cause any serious rise in the operating temperature.

Using the amplifier shown in Fig. 2B, the oscillator output voltage is adjusted to about 2 v. A pressure change in the manometer from 0 to 300 mm of mercury will cause a variation of the output alternating voltage of about 5 percent.

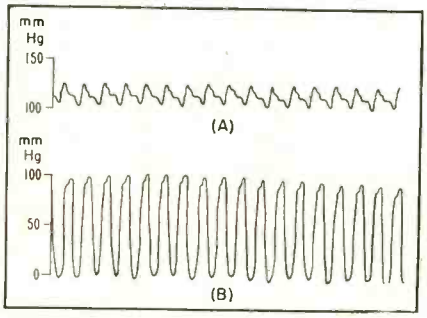


FIG. 3—Blood pressure recordings made in right carotid artery (A) and in left heart ventricle (B) of rabbit

Typical blood pressure recordings from the heart of a rabbit are shown in Fig. 3.

This material was abstracted from a paper entitled Research on Mechano-Electronic Transducer Blood Pressure Manometers by Hjalmar Pettersson and Carl-Johan Clemedson at the 1956 ISA Conference.

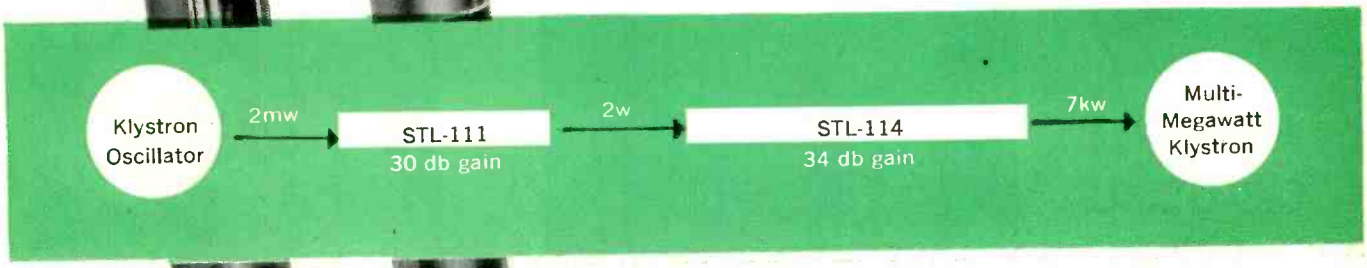
Tester Checks Grid Emission

By E. A. Bramsen
President
Seco Mfg. Co.
Minneapolis, Minn.

Grid emission in vacuum tubes can cause unstable or improper operation of circuits. Tubes that check out on conventional tube testers as satisfactory may fail to operate properly owing to grid emission.

This phenomenon is most often encountered with high gain tubes such as the 6AK5. After the tube has reached operating temperature, the grid may emit electrons that

New Driver Chain for Pulsed High-Power Radar



STL-111

STL-114

Sperry's New Metal Traveling Wave Amplifiers Cover 1100-1600 mc Range in L-Band

NOW IN PRODUCTION, these Sperry high-power traveling wave amplifiers bring new flexibility to pulsed high-power radar systems, and offer special advantages as wide-band repeaters and swept frequency amplifiers.

AS THE DRIVING POWER for multi-megawatt klystrons, the STL-111 and STL-114 feature a high duty cycle and fast—even instantaneous—frequency change *with no need for tuning or voltage modification.* In cascade they amplify a signal from 2 mw to 7 kw, with a gain of over 60 db.

RESISTANCE to thermal and mechanical shock is extremely high, due to sturdy metal envelope and ceramic rods supporting the helix. RF connectors are integral parts of the tube structure.

Write our Electronic Tube Division for data sheets on these new amplifiers (as well as other driver chains in other high frequencies).

CHARACTERISTICS:	STL-111	STL-114
Frequency Range	1100-1600 mc	1100-1600 mc
Saturation Power Output	4w.	7kw
Gain at Saturation Power	30 db	34 db
Small Signal Gain	36 db	40 db
Beam Voltage	900 v	14 kv
Duty Cycle	Continuous	.005
Magnetic Field	450 gauss	700 gauss

ELECTRONIC TUBE DIVISION

SPERRY GYROSCOPE COMPANY

Great Neck, New York

DIVISION OF SPERRY RAND CORPORATION

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VISIT SPERRY AT THE RADIO ENGINEERING SHOW, NEW YORK COLISEUM, MARCH 18-21, BOOTHS 1416-1422

will permit the flow of grid current in a reverse direction. Where biasing circuits are fed through a common bus, grid emission in one tube may change the value of bias on other tubes.

Effective tube life and equipment availability has been increased by checking tubes for grid emission. It was also found that 90 percent of the tubes that had grid emission could not be checked on a trans-

Checker finds grid-emission defects that do not show up under conventional tube tests

conductance-type tester. Gas tests provided on most tube testers do not have sufficient sensitivity.

One method for checking grid emission uses a capacitor charged by the reverse grid current. By measuring the time required for the voltage across the capacitor to reach a steady state, the grid current can be computed as

$$\Delta e = \frac{i}{RC}(dt), i = CR\frac{\Delta e}{\Delta t}$$

When a 1 μf capacitor and a 1-megohm resistor are used,

$$i = \left(\frac{\Delta e}{\Delta t}\right)$$

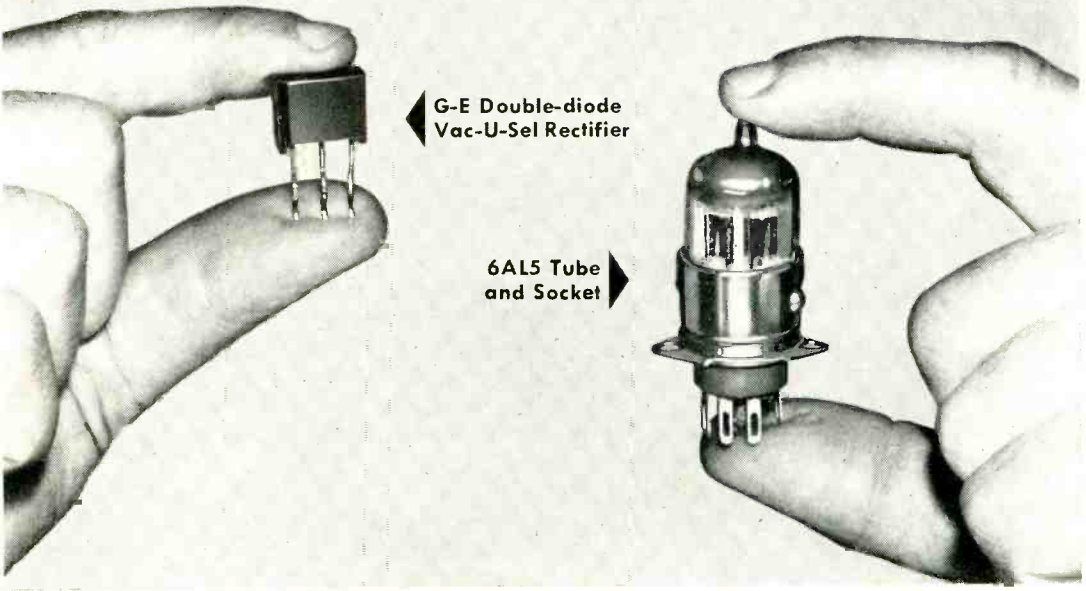
A tube tester developed for laboratory and field use checks control-grid emission in addition to checking for grid-to-cathode shorts, gaseous conditions and cathode-to-heater shorts.

The tester is provided with eight tube sockets, a zero-adjust knob and a filament voltage selector switch. To check a tube, the filament voltage selector switch is set to the right value and the zero-adjust control is set so that the

NEW...

General Electric Double-diode Vac-u-Sel* Rectifier Cuts Costs as Much as 35%

THIS REPLACES THIS



With a few minor modifications in most basic circuits General Electric's new double-diode Vac-U-Sel rectifier can replace the heavier, larger, 6AL5 tube and socket. Cost of the new Vac-U-Sel rectifier to you may be only about 65% that of a tube and socket.

Although designed for a wide range of uses, the new General Electric Vac-U-Sel double-diode rectifier is ideally suited for use as a TV horizontal-phase-detector diode. Other outstanding features include:

- longer life
- breakage-resistant
- low cell capacitance
- no filament power required

Sealed firmly in a durable, moisture-resistant housing the new General Electric Vac-U-Sel selenium rectifier is designed to be automatically assembled by machine. Longer leads are available for hand assembly in conventional chassis. Units consist of two single cells which may be either common cathode or plate-to-cathode connected.

SEE THIS GENERAL ELECTRIC VAC-U-SEL DOUBLE-DIODE RECTIFIER . . . INSTALL IT . . . OBSERVE FIRST HAND ITS HIGH PERFORMANCE . . . WRITE TODAY FOR A FREE PRODUCT SAMPLE.

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tester's electronic eye indicator just closes. The tube is then plugged into the appropriate socket. If the eye opens beyond the indicated limits, after a warm-up period, the tube is defective. By doubling the filament voltage for a few seconds and then testing at rated filament voltage, borderline tubes will show up as defective.

The instrument contains a simple d-c amplifier circuit with an electronic-eye tube as an indicator. The circuit is shown in Fig. 1. Resistors R_1, R_2 and R_4 form a voltage divider network that biases the tube under test to cutoff or beyond cutoff. Potentiometer R_4 is adjusted so that the eye tube is closed. At this setting the d-c amplifier is biased

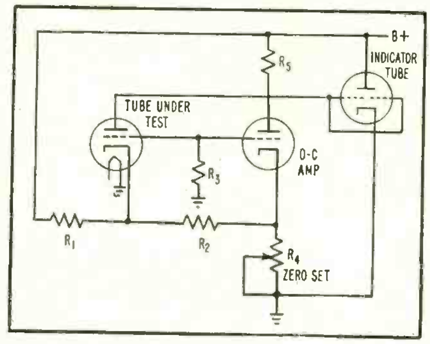


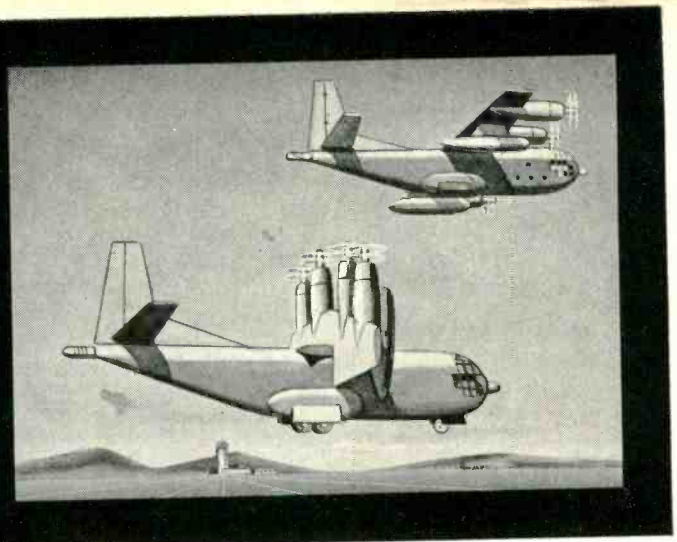
FIG. 1—Simple circuit uses electron-eye tube to check grid emission

Rapid Missile Tester

Automation of missile testing in tactical combat areas is possible with RACE (Rapid Automatic Checkout Equipment) produced by Sperry Gyroscope. If a faulty component is detected, its location and replacement time is flashed on the console screen (top left) and a punch card spotting the plug-in replacement for technicians is delivered (below)

tomorrow is here today!

Rising like a 'copter, this tilt-wing transport will cruise at 350 m.p.h. Originally thought of as an impossibility, this unusual plane is in the design stage today. The versatility of flight direction is accomplished by tilting the wings 90 degrees for vertical takeoffs and landings. Tilting with the wing are four six-blade, contrarotating propellors and their high powered turboprop engines. Today's airports with their extensive runways may soon be facing obsolescense.



Z821A

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Z820A	1.0	33	33	1,000	.001	0.5/2000 2.5/400	1/190-250	6x2x3	1400	4J50, QK-349 RK-6249
Z821A	14.0	90	160	560	.001	2.0/200-500	3/440-550	7x4x7	6800	QK-338
Z822A	0.2	20	10	3,330	.018	10/1200-1800	3/440	6x3x4	3330	SAL 39 (GL-6625)
Z823A	0.042	12.7	3.3	3,330	.064	coded/300	3/440	6x4x4	3200	SAL 39
Z824A	0.625	25	25	1,000	.001 at 0.5/2000	1.0/1000 2.0/250 5.0/100	1/190-250	6x2x3	2500	QK-349 at reduced power
Z825A	1.6	40	40	1,000	.001 at 0.5/2000	1.0/1000 2.5/400	1/190-250	6x2x3	2500	WE-5780

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to cutoff and no current flows through R_5.

If reverse grid current flows in the tube under test owing to grid emission or other cause, the input of the d-c amplifier becomes less negative causing the d-c amplifier tube to conduct and produce eye-tube deflection. Any appreciable leakage between the cathode and heater of the tube under test will also lower its bias as well as the bias on the amplifier, resulting in eye-tube deflection. Gas and grid-to-cathode shorts will also actuate the amplifier.

A spare tube socket on the front panel is used for preheating tubes.

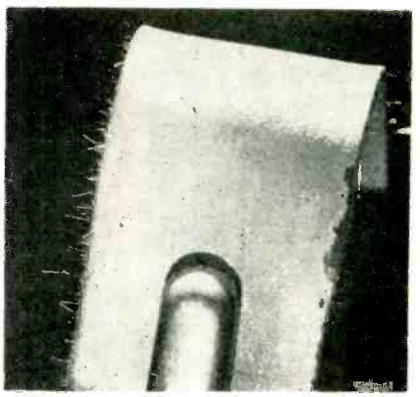
To prevent damage to tubes under test, grid-to-cathode potential difference is limited to 45 volts.

Effects of Radiation

TESTS of electronic components under reactor radiation indicate that most components will function under extended irradiation. Exceptions are phototubes, germanium and copper-oxide rectifiers, resistance-wire strain gages and some types of resistors and capacitors. Presence of boron, ionizable gases or definite crystal structure make components likely to fail.

In most of the tests, components

Radiation Whiskers



The phenomenon whereby growth of hair-like metallic whiskers occurs on certain metals has recently been enhanced by exposure to atomic radiation. Samples of tin placed in the Brookhaven reactor for a month and allowed to stand for a year exhibit greater whisker growth, probably resulting from damage to crystal structure by neutron bombardment

FENWAL'S THERMOSTATS NOW CIGARETTE SIZE

Some Units Smaller Still
Take Little More Room Than Sugar Lump

ASHLAND, MASS. — If you want to control temperatures in tight spots, you should see Fenwal. Fenwal has cut the size of thermostats way down.

You can fit one of their Midget THERMOSWITCH units anywhere a cigarette will fit. And, if you're working with even less space, one of their Miniature THERMOSWITCH units is what you're looking for. The Miniatures are little bigger than a lump of sugar, and some are even smaller.

The Midgets and Miniatures use the same unique principle used in Fenwal's bigger THERMOSWITCH controls. They use it with the same high degree of success.

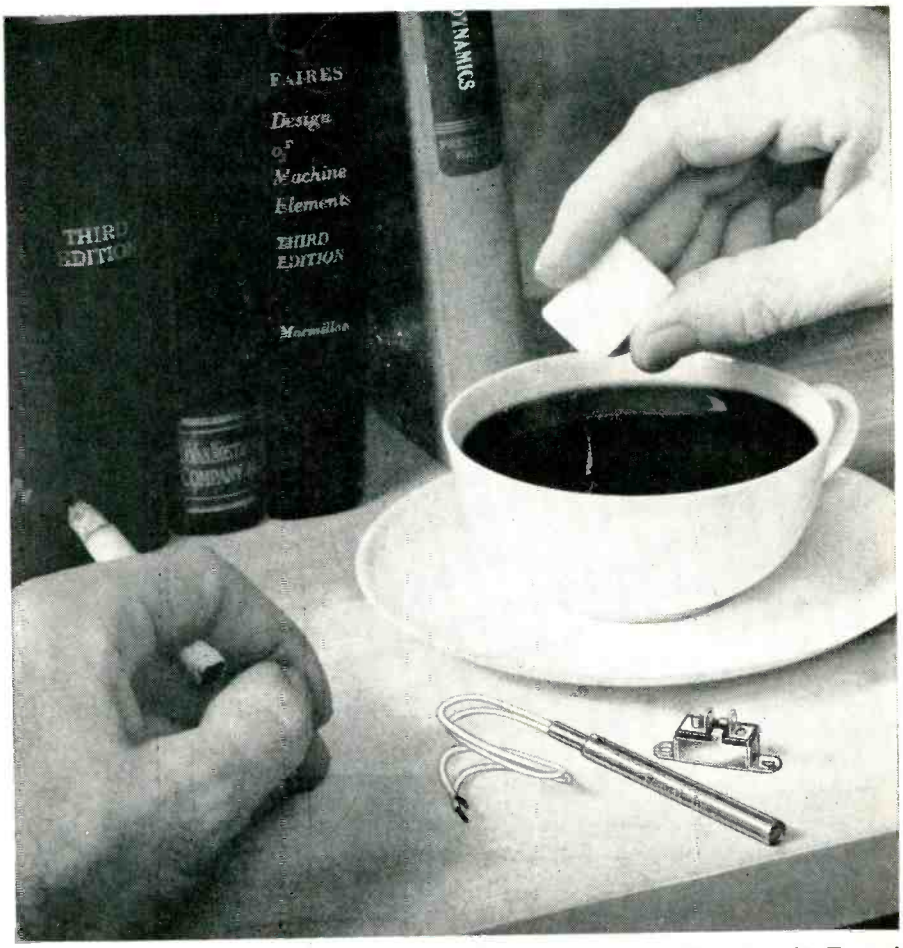
The principle of all Differential Expansion THERMOSWITCH units, large or small, is this: a single metal shell expands or contracts with temperature changes, making or breaking totally enclosed electrical contacts.

The smallness of the Midget and Miniature units does not deprive them of any of the performance characteristics that have made larger THERMOSWITCH units famous. They have THERMOSWITCH ruggedness, THERMOSWITCH accuracy, and reasonable THERMOSWITCH prices.

Temperature range of the Midget series: −50°F to 500°F. Range of the still smaller Miniature series: −20°F to 275°F.

Midgets and Miniatures, all in stainless steel, come in a variety of mountings. Hermetic sealing is also available.

These Fenwal THERMOSWITCH units are precision-engineered to give optimum temperature control with minimum-sized devices. They remain accurate under the most severe operating conditions.



THERMOSTATS FOR TIGHT SPOTS — A Fenwal Midget THERMOSWITCH® unit and a Fenwal Miniature THERMOSWITCH unit — two good answers to the question, "How can you install an accurate, reliable thermostat where there's almost no room?" Actual sizes of these particular models — ¼" x 2 25/32" for the Midget; 1" x ½" for the Miniature.

You should have details on this advance in temperature control at your fingertips. Write for information to **Fenwal Incorporated, 203 Pleasant Street, Ashland, Massachusetts.**

Fenwal

CONTROLS TEMPERATURE
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were connected in circuits typical of their usual functions and data were taken during irradiation.

As a detailed test of circuit operation a composite multiplier-phototube assembly excited by an argon lamp was operated during irradiation. The argon exciter lamp required increased d-c bias for operation under irradiation. The phototube gave a reduced signal. This was probably caused by an increase in dark current under irradiation.

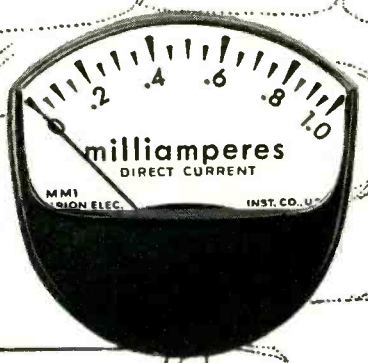
▶ **Results**—Except for exciter lamp and phototube, no changes were observed in 145 equivalent hours of irradiation. Signal modulation, output, temperature and all power-supply voltages were observed in addition to the bias voltage of the argon lamp.

Five tubes (6AG7, 6SN7, 6B4G, 6L6 and 6L6G) showed no changes in their dynamic characteristics. More extensive tests with five others for controls showed no radiation effects on either gas pressure or plate resistance. The same type of test was performed on types 6SJ7 and 6H6 with similar results. No effect was observed in either extinction or ignition voltages of irradiated VR75's

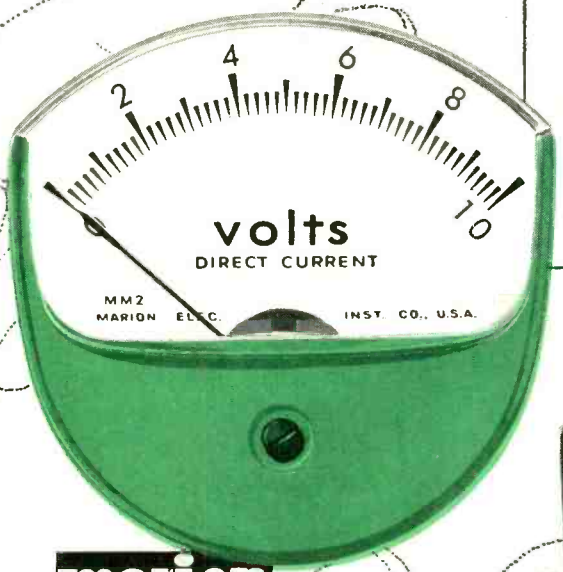
Irradiated Polyethylene

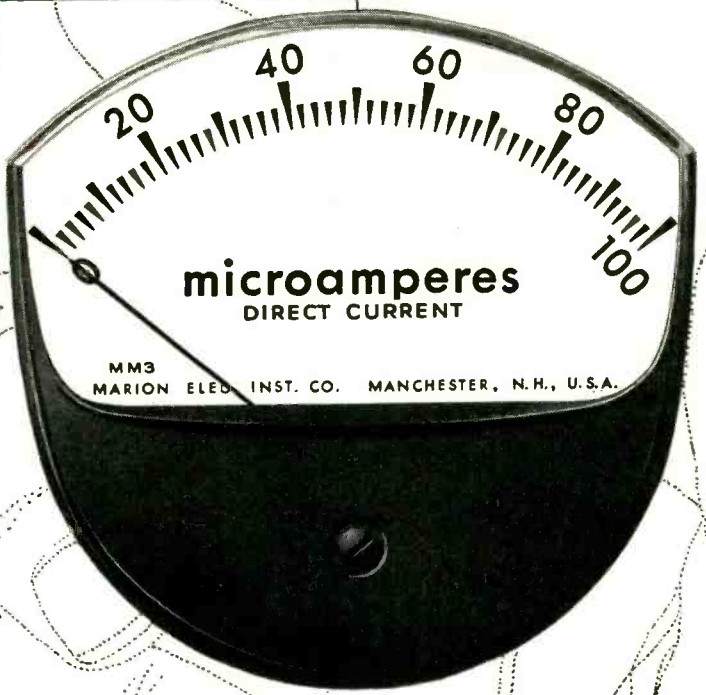
First commercial product of GE research in electron radiation, Irrathene irradiated polyethylene tape is used here to wrap coils for Sonotone's sintered-plate, nickel-cadmium batteries. Conventional polyethylene is bombarded with high-velocity electrons to give it improved high temperature qualities (ELECTRONICS, p 146, May 1956)

WHERE ELECTRONICS MEETS THE EYE



marion MEDALIST meters





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Three things set Medalists apart from other panel instruments: style, color and readability. Their distinctive shape enhances whatever equipment they become a part of; standard or custom-matched case and dial colors further improve equipment appearance. Longer scale length, larger numerals and better over-all dial illumination vastly increase their readability.

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argon and neon glow tubes.

▶ **Ballast**—Tests on ballast tubes and gage tubes especially designed to measure performance of platinum and tungsten filaments showed that neither was affected by radiation.

Tests indicate that capacitors containing boron should not be used in nuclear radiation fields. Other types displayed satisfactory performance, in general, although some decreased in capacitance value.

With the exception of one type, resistors showed only small radiation effects. Wire-wound types are among the most stable of resistors tested.

Fission-produced radiation has negligible effect on thermal and current-induced noise in resistors. This conclusion comes from two hours of measurements with both carbon and wire-wound resistors in a flux of 10^{11} n per sq cm per sec.

Different types of dry rectifiers behave differently in radiation fields. Particularly stable in high fluxes are silicon types 1N21 and 1N23 and the selenium type 403-D2625.

▶ **Piezo Devices**—Quartz crystals were used in oscillators that operated in the reactor for 46 days with no changes in frequency.

Strong radiation fields cause some deterioration in all dry cell

Two Megawatt Klystron

Smallest and largest klystrons produced by Litton Industries at San Carlos, Calif. are described by vice-president Norman H. Moore to guest at recent West Coast open house

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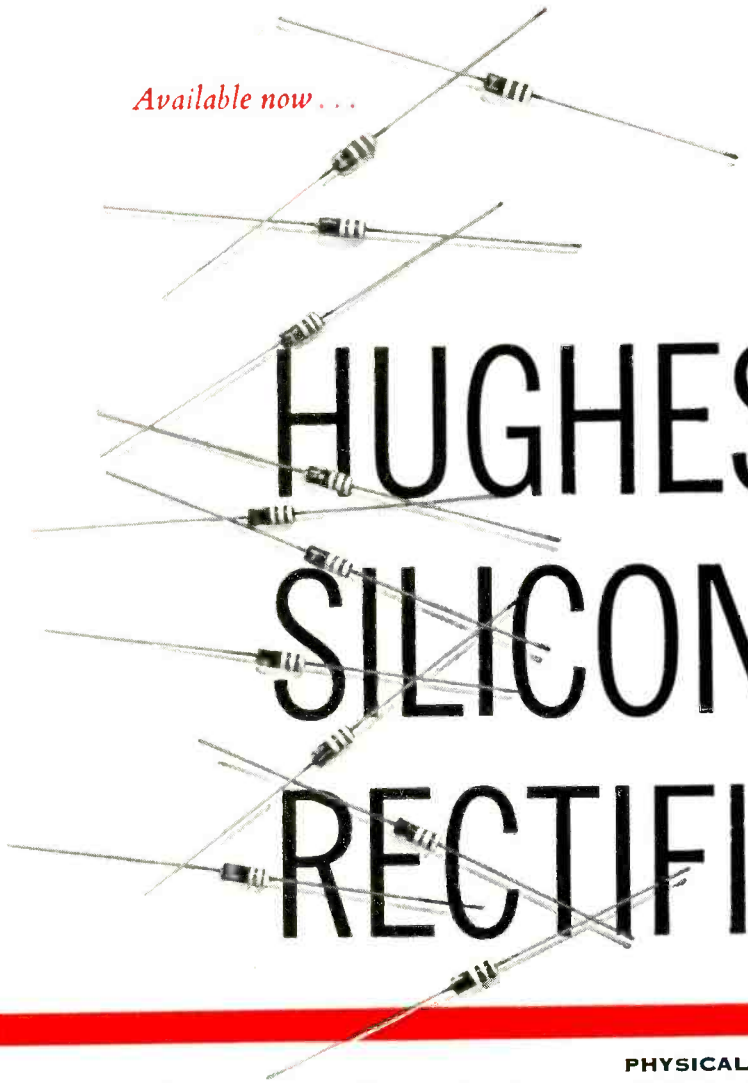
HUGHES SILICON RECTIFIERS



Hughes introduces a new series of high-quality silicon rectifiers, especially designed for use in miniaturized circuitry. These new low-power rectifiers are characterized by low forward voltage drop, together with low back leakage. They are exceptionally efficient units in electronic power supplies and, in such applications, can be used in place of many conventional vacuum tubes.

The new Hughes Rectifiers feature: maximum AC input voltages up to 275 volts RMS; maximum reverse DC working voltages up to 375 volts; maximum average rectified forward current up to 200mA; maximum power dissipation (at 25°C) up to 200mW. Operating temperature range for all types: −75°C to +150°C.

PHYSICAL CHARACTERISTICS

All Hughes Rectifiers are packaged in a one-piece, fusion-sealed glass body. This famous construction is impervious to moisture penetration, ensures stable operation under severe operating conditions. Maximum dimensions, rectifier glass body: length, 0.265-inch; diameter, 0.105-inch.

Our sales engineers will welcome the opportunity to discuss applications of these new rectifiers with you. For the address of our sales office nearest you, or for more complete specifications concerning the new Hughes Rectifiers, visit Booths 2801, 2803, 2805 at the I.R.E. Show, or write:

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batteries. In general-purpose applications this would cause only a slightly shortened useful life. However, the single type of bias cell tested showed such changes of terminal voltage as to be unusable in strong fields.

In three experiments flashlight and hearing-aid type batteries were divided into four groups: test on open circuit, test under load, control on open circuit and control under load. Daily readings of terminal voltages were made with 100 and 10,000-ohm loads.

In the bias-cell experiment, heat caused no appreciable change in the voltage of test cells but radiation caused unreliability.

➤**Strain Gages**—Also unreliable were resistance-wire strain gages. These were strained by energizing relays to which they were bonded for testing. Differences between strained and unstrained output voltages were used as the gage readings. The results showed that radiation has a significant effect.

This material was abstracted from an article "What are Effects of Radiation on Electronic Components" appearing in *Nucleonics*, p 33, July 1956.

Iron Dust Magnet

Ordinary iron in the form of submicroscopic elongated particles has been used by GE engineers to make magnets equal in strength to available commercial types. Unit shown has wire coil soldered to one end. Other end is tapped

BEGIN YOUR RADIO ENGINEERING YEAR

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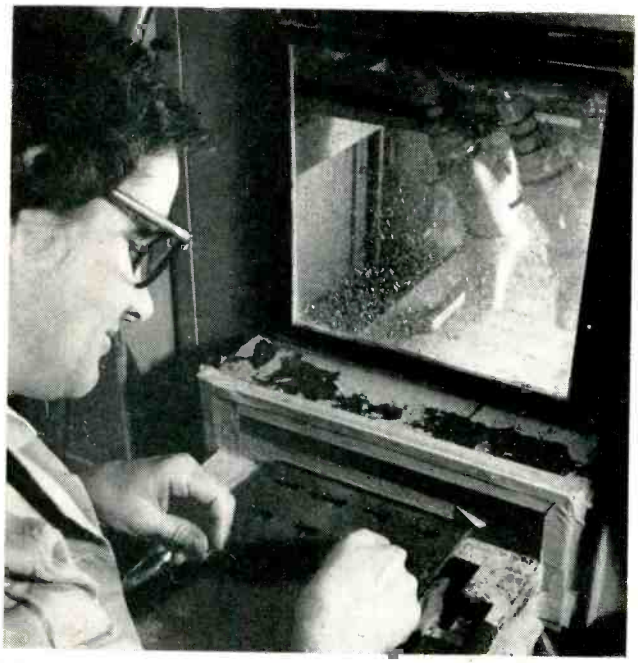
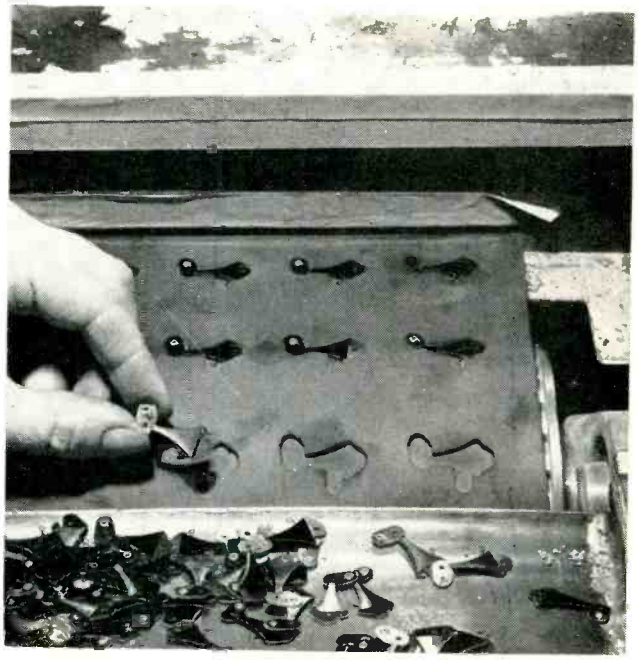
Production Techniques

Edited by JOHN MARKUS

Pecan-Shell Blast Removes Enamel From Coils on Conveyor



Behind strong glass, four blasts of cracked shells knock enamel off fine wire on one side of flat coil in each recess of conveyor belt



Method of loading coil on belt. Coil serves as compensating heater for thermostat in electronic temperature-control system

TO REMOVE ENAMEL from hair-thin wires used in shaped flat nonlinear coils, Minneapolis-Honeywell bombards the coils with finely ground pecan shells and apricot pits. The flying grit does the job at a fraction of the cost of chemicals or other more conventional burnishing methods. For still more sensitive wire coils, powdered corn cobs are used as the abrasive in the machine.

Production of the elements now runs at a rate of 1,000 an hour. The best previous rate, by routine enamel-removing operations, was 1,000 a day.

The operator loads the coils into four rows of masking slots on an endless conveyor belt that travels through the cleaning chamber. Inside, each row of coils passes under one of the four shell-blast nozzles, for removal of enamel on the side over which a wiping contact arm is to travel. Cleaned coils travel out the rear of the chamber and drop into a container as the belt comes down over its rear roller.

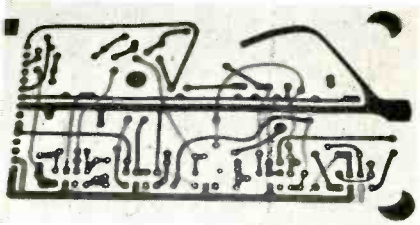
The shell particles fly around inside the cleaning chamber and eventually drop off the sides of the belt into a hopper below. Shells can be used over again if screened occasionally to remove pieces that have broken up during use. Shells are loaded into an overhead hopper, from which they enter the air blasts of the individual nozzles.

New Materials Cut Drafting Costs for Printed Circuits

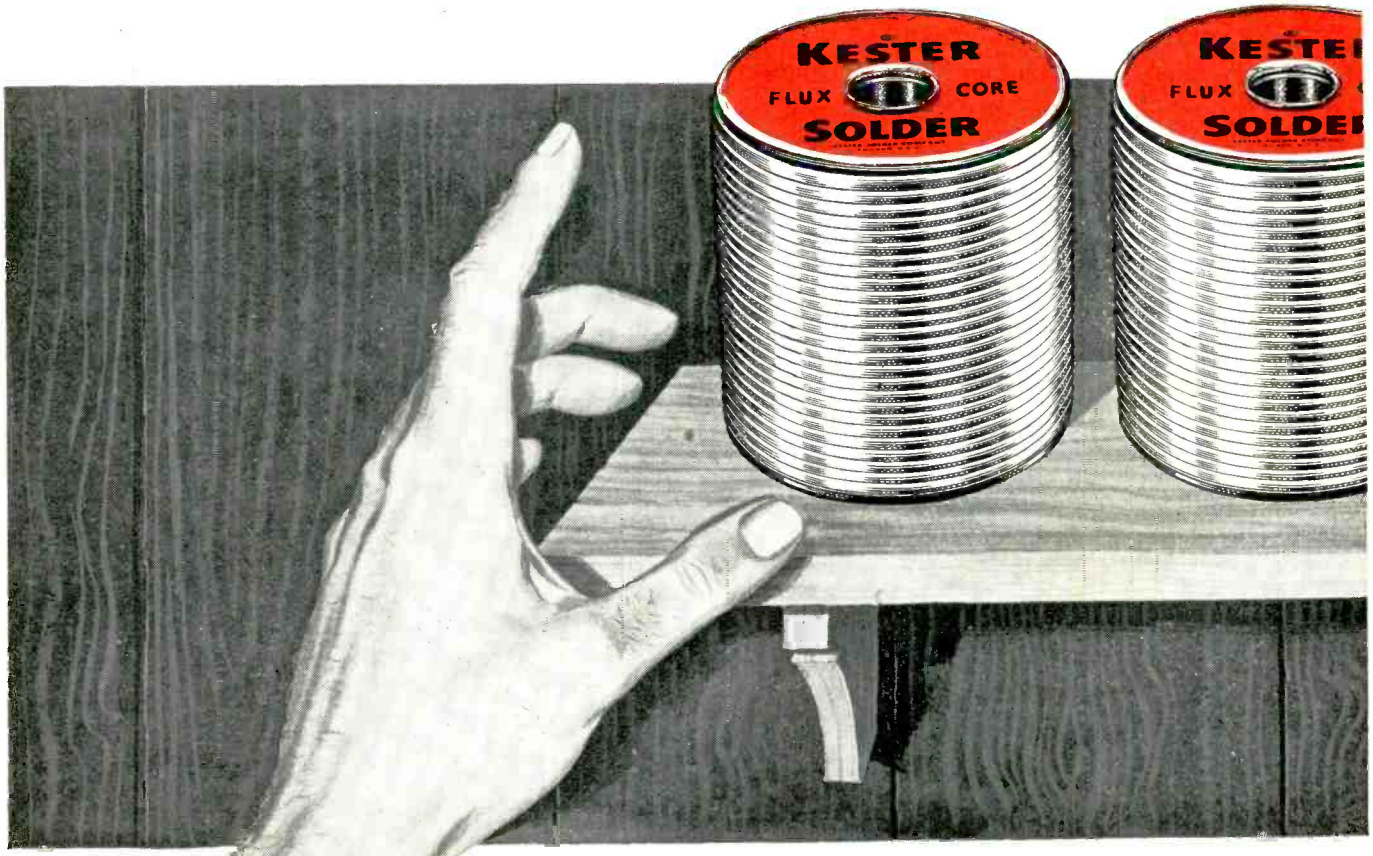
By N. J. SCHUSTER

Electronics Development Department
Lockheed Aircraft Corp.
Research Branch
Missile Systems Division
Van Nuys, California

THE CHANGING NATURE of data requirements in a missile testing program made it necessary to seek an improved procedure for preparing reproducible copy for printed circuits and to find a method of eliminating costly and time-consuming art revisions. After experimenting with various techniques, it was found that B-150 pressure-sensitive self-sealing black tape manufactured by W. H. Brady Co., Milwaukee, Wisc. and Stabilene plastic film manufactured by Keuffel and Esser Co. could be substituted for the usual India ink and opaque illustration board. The use of these new tools permitted a lower degree of skill, saved a skilled draftman's time for other tasks, eliminated the dimensional instability inherent in



Checking master copy registration. Two-sided circuit is aligned back-to-back, greatly simplifying art changes. All wiring lines are made with easily changed pressure-sensitive tape. Curves are inked in on other side of film



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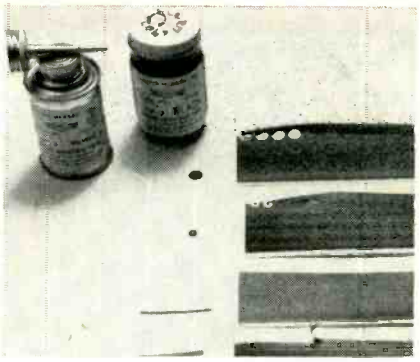
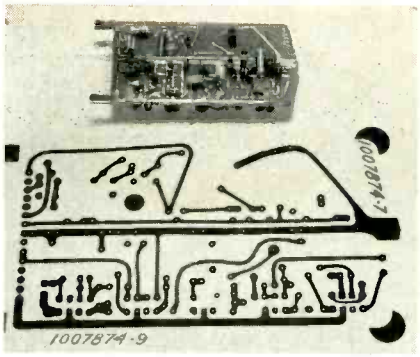
art board and resulted in more accurate registration of a two-sided circuit. Total time for preparing original art masters was cut approximately in half.

▶**Drafting Technique**—The printed-circuit pattern is first roughed out on vellum, enlarged two or four times if the circuit is very small. The plastic film is placed over the pattern, matte side up, and the circuit is taped on the plastic film using the appropriate pressure-sensitive circles and lines. The drawing is now turned over and a special type 1001S black ink and solvent 1052S supplied by Pannier Corp., Pittsburgh, Pa. is used on the glossy side of the film to add odd shapes and tight curves.



New art materials for designing printed circuits include special plastic film, ink, solvent and pressure-sensitive tape

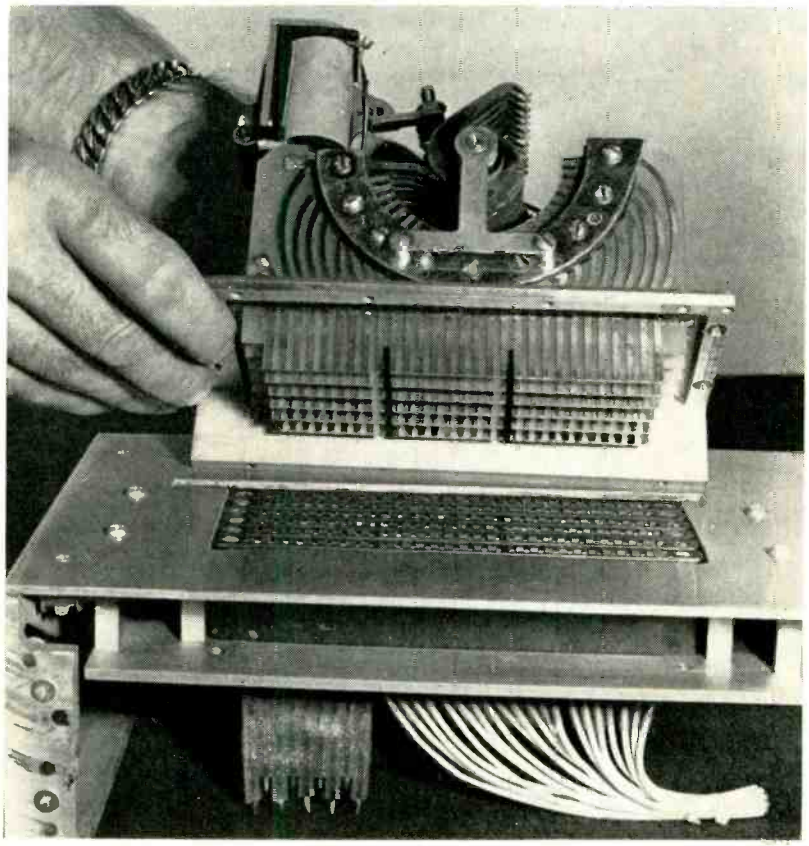
When a two-sided circuit is to be reproduced, the pattern of the second side is drawn on a separate piece of film. The two sides are then placed back-to-back. The transparent film allows exact corrections to be made with the special ink for more perfect registration. Changes are made simply by moving the tape or retaping. The ink wipes off easily from the glossy side of the film, using a rag moistened with the 1052S solvent.



Assembled circuit, with example of art master revised many times without showing evidence of change

The wrinkled finish of the black tape may produce highlights on the negative due to the intense lights used in photography. This can be eliminated completely by spraying Crescent Matton, manufactured by Crescent Portrait and Frame Co., East Cleveland, Ohio, over the finished master. The spray will not affect the ease of making changes in the master copy.

Design of the Month: STEPPER SWITCH

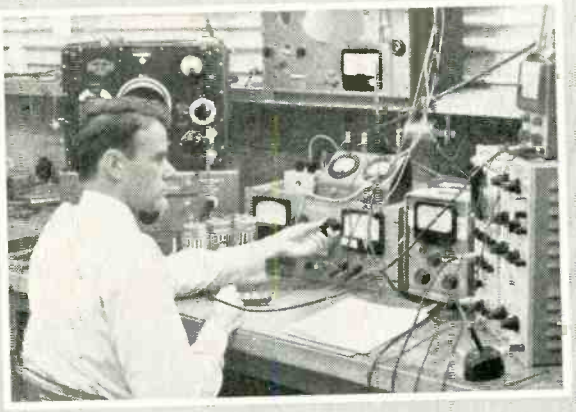


Six etched wiring boards provide all contacts, wiring and terminals for 12-deck, 26-position stepper switch developed at Northrop Aircraft for use in ground equipment of Snark intercontinental missile. Copper-clad epoxy-glass-fiber laminate is gold-plated to prevent oxidation of the plug-in contacts on one end of each strip, and rhodium-plated at the other end for improved mechanical strength of wiper contacts. Use of boards simplifies assembly and permits plugging complete switch into 348-contact socket. A malfunctioning switch can thus be replaced in a few seconds. Switch is currently being manufactured by Electrodynamic Division of United Geophysical Corp., Pasadena, Calif.

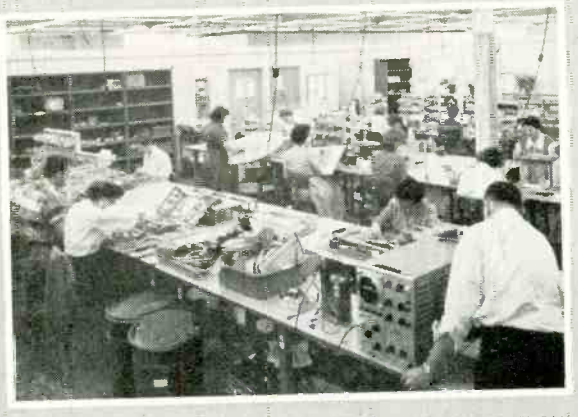
Rollers in Viewer Hold Large Circuit Diagrams

QUICK ACCESS TO any of up to 80 different circuit diagrams is achieved with a simple arrangement of two rollers and a frame in the missile development laboratory of Northrop Aircraft's Hawthorne, Calif. plant. The blueprints are pasted together end to end and rolled up on the hand-cranked rollers. Diagrams pertaining to a particular job can be run back and forth across the viewing area as required during assembly or testing of a complex airborne electronic system. A strip of Scotch tape anchors each end of the print strip to a roller.

On the model that holds 80 prints, an index card on the front of the stand identifies each print. An operator thus knows how far, how fast and in what direction to

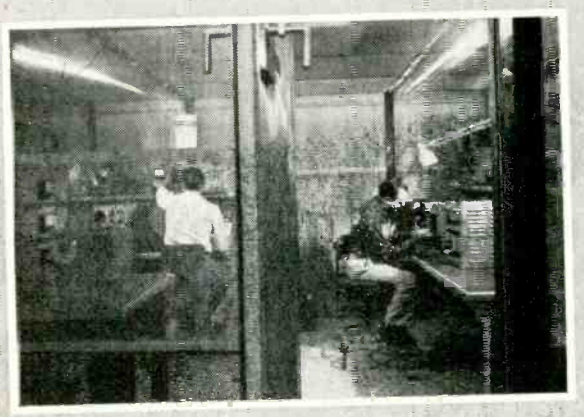


RESEARCH AND DEVELOPMENT



PILOT LINE PRODUCTION

FINAL ASSEMBLY



TESTING IN SCREEN ROOM

COMMUNICATIONS at Ramo-Wooldridge

Communications activities at The Ramo-Wooldridge Corporation include research, development, and manufacture of advanced types of radio communication systems, ground-reference navigation systems, and electronic countermeasure systems. Major programs are in progress in each of these fields.

New and unusual techniques have been employed to provide systems having a high order of security in the transmission of information, broad flexibility in combating unfavorable signal propagation conditions, and substantially greater information capacity per operating channel.

Some of the techniques used have made possible an increased range for given levels of transmitter power and reliability of communications. Others have provided specific advantages in very long distance communications or in operational situations requiring unique signaling capabilities. Developments in navigation systems have resulted in new equipment that is suitable for the guidance of aircraft at long ranges from their bases.

In the work currently under way, some systems are in the laboratory development stage, some in the flight test stage, some are in production. Several types of systems developed and manufactured by Ramo-Wooldridge are in extensive operational use.

Openings exist for engineers and scientists in these fields of communications activities:

- Systems study and analysis
- Airborne transmitters
- Transistorized video and pulse circuitry
- Airborne receivers
- Reconnaisance systems
- Digital communications systems

The Ramo-Wooldridge Corporation

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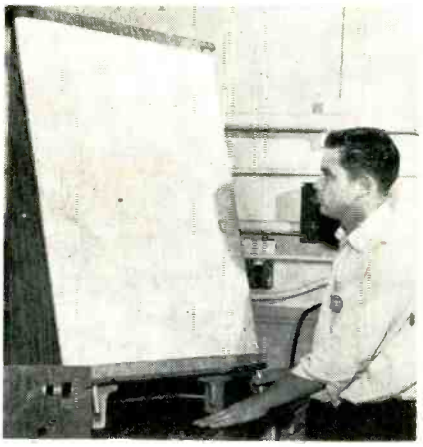
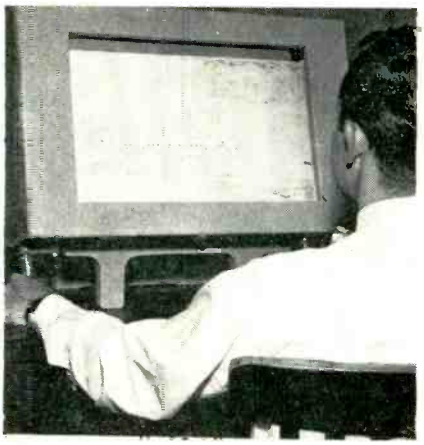


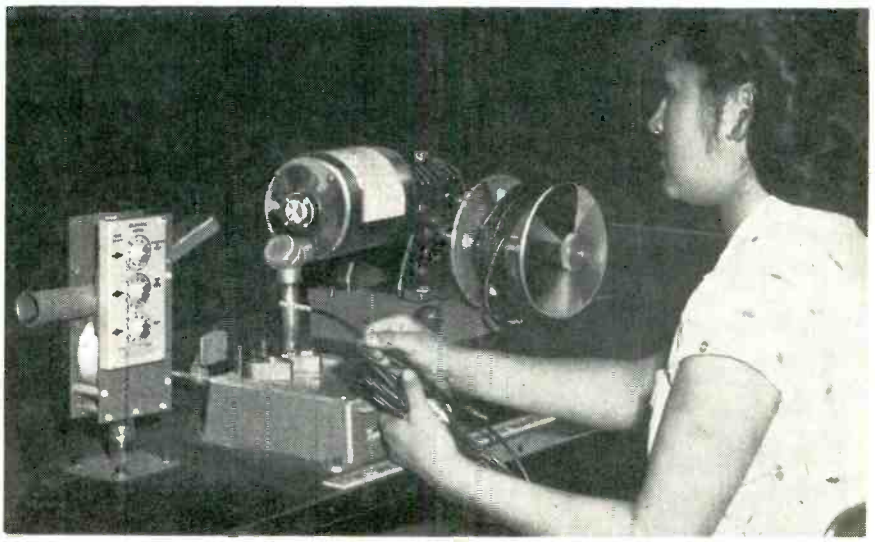
Simplest version of viewer. Crank at right moves print to right; for opposite direction, crank on left-hand roller is used



More elaborate desk-top viewer with back illumination is 26 inches wide, 12 inches deep and 18 inches high

turn for access to a desired print. Another model in a simpler frame holds up to 30 feet of prints. In addition to speeding access to the desired print in a large set, the device keeps prints clean and smooth, and reduces the space needed for viewing large prints.

Cutting And Stripping Long Coaxial Cables

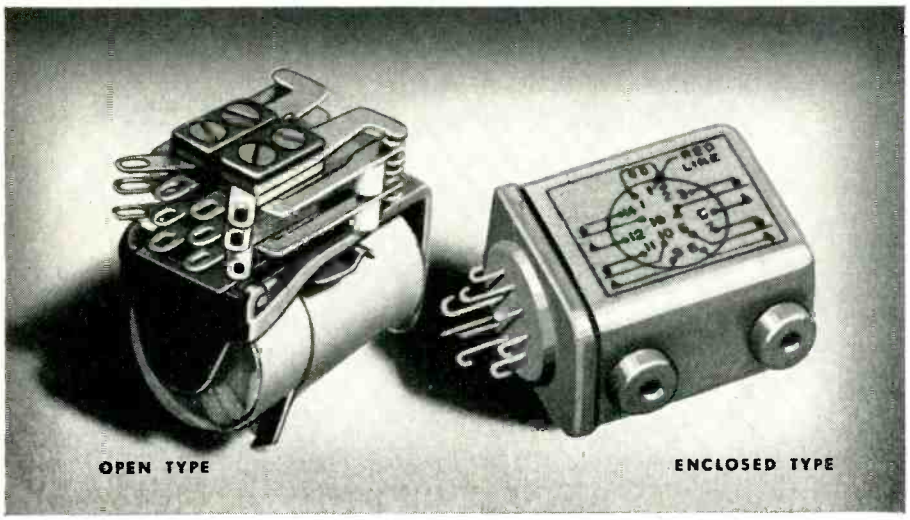


Former Navajo rug weaver now prepares coaxial cable at work position that combines measuring (left), coiling (right) and stripping (center)

LONG RUNS OF coaxial and multiconductor cables are measured at high speed, cut, stripped and coiled at a single work position in the new Flagstaff, Arizona plant of Lear Inc. This plant taps a large labor pool of Navajo Indians, who possess above-average manual dexterity. It is expected that over 100 Navajos will be at work by this spring, performing electronic subassembly operations having a high labor content. This includes the assembly of wiring harness, preparation of cables with and without connectors, and carefully controlled tinning of critical leads for airborne electronic units.

▶**Preparing Coax** — For long lengths, a large spool of cable is placed on a shaft supported by brackets mounted on the end of the assembly bench. The cable comes up over a free-turning roller mounted at the top end of the bench, then runs through a measuring device mounted at the left of the work position. This is made by Olympic Instrument Laboratories, Cove, Washington and has three dials, reading in feet with quarter-

R-B-M Miniature Multipole Relays of Proven Reliability



Light weight, Small Size Open and Hermetically Sealed Types for Electronic and Communication Application

APPLICATION: R-B-M Miniature Multipole Relays are used where the prime factors in switching electronic circuits are small size, light weight and reliability. These proven designs are produced for switching low power circuits, low capacitance circuits and power circuits. 125° C insulation now available on some versions. Coils can also be designed for plate circuit.

CONSTRUCTION:

Magnet Frame—Four sizes available on open type relays and three sizes on hermetically sealed type.

Contacts—Cross-bar palladium welded to nickel silver springs or button contacts on Beryllium copper springs.

Terminals and Mountings—Glass headers provided with either solder or plug-in type terminals with many various types of mountings available. Octal type plug-in headers can be provided on the HL enclosure. Plug-in terminals to fit either 9 or 14 pin standard sockets. Maximum of 14 pins for solder connections.

TYPICAL SPECIFICATIONS*

Open	Maximum Coil Resistance (OHMS)	Minimum Power Requirements Per pole at 25°C(WATTS)	Maximum Contact Form With rated current at 32 V.D.C. or 115 V.A.C. (non-inductive load)	Maximum Coil Watts	Enclosed
SM	9,000	.2	4 PDT 5 Amps. or 3 Amps. 6 PST 3 Amps.	3.75	HSM
SMD-2	9,000	1.0	SPNO Parallel Contacts Make 80 Amps. Break 20 Amps. at 32 V.D.C.	3.75	HSMD-2
SC	18,500	.16	4 PDT 5 Amps. or 3 Amps. 6 PST 3 Amps.	4.5	HPSC
SA	18,500	.14	4 PDT 5 Amps. or 3 Amps. 6 PST 3 Amps.	4.5	HLSA
SM-RF	9,000	.2	SPNO, SPDT, DPNC, SPNC, DPNO	3.75	HSM-RF HLSM-RF
SAD-2	18,500	1.0	SPNO Parallel Contacts. Make 80 Amps. Break 20 Amps. at 32 V.D.C.	4.5	HLSAD-2

*Other ratings and specifications available.

For additional information write for Bulletin No. 1050

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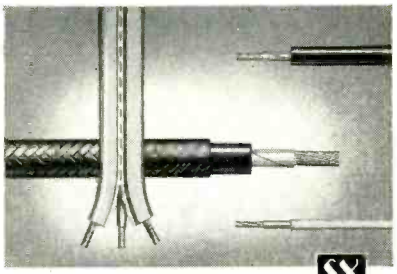
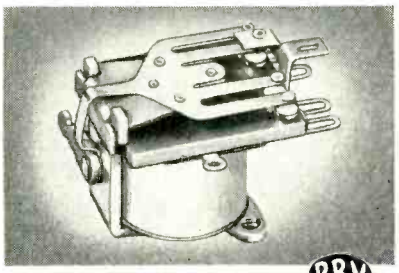


WIRE AND CABLE

A full "Extra Test" line of lead, test lead, appliance, automotive and refrigeration wires, plus submersible pump cable and 200° C. Sil-X insulations are examples of the versatility of "Essex Engineering".

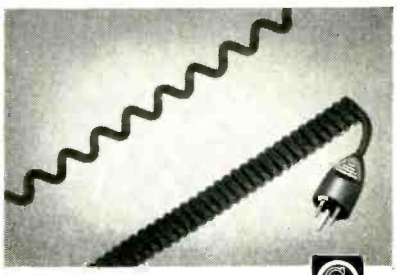
Wire and Cable Division



MINIATURE RELAYS

The Type MS Miniature Sensitive Relay is ideal for any application requiring a compact, highly reliable single pole D. C. device, where a low cost solution is required because of volume usage and competitive problems. Request Bulletin No. MS-1.

R-B-M "Control" Division

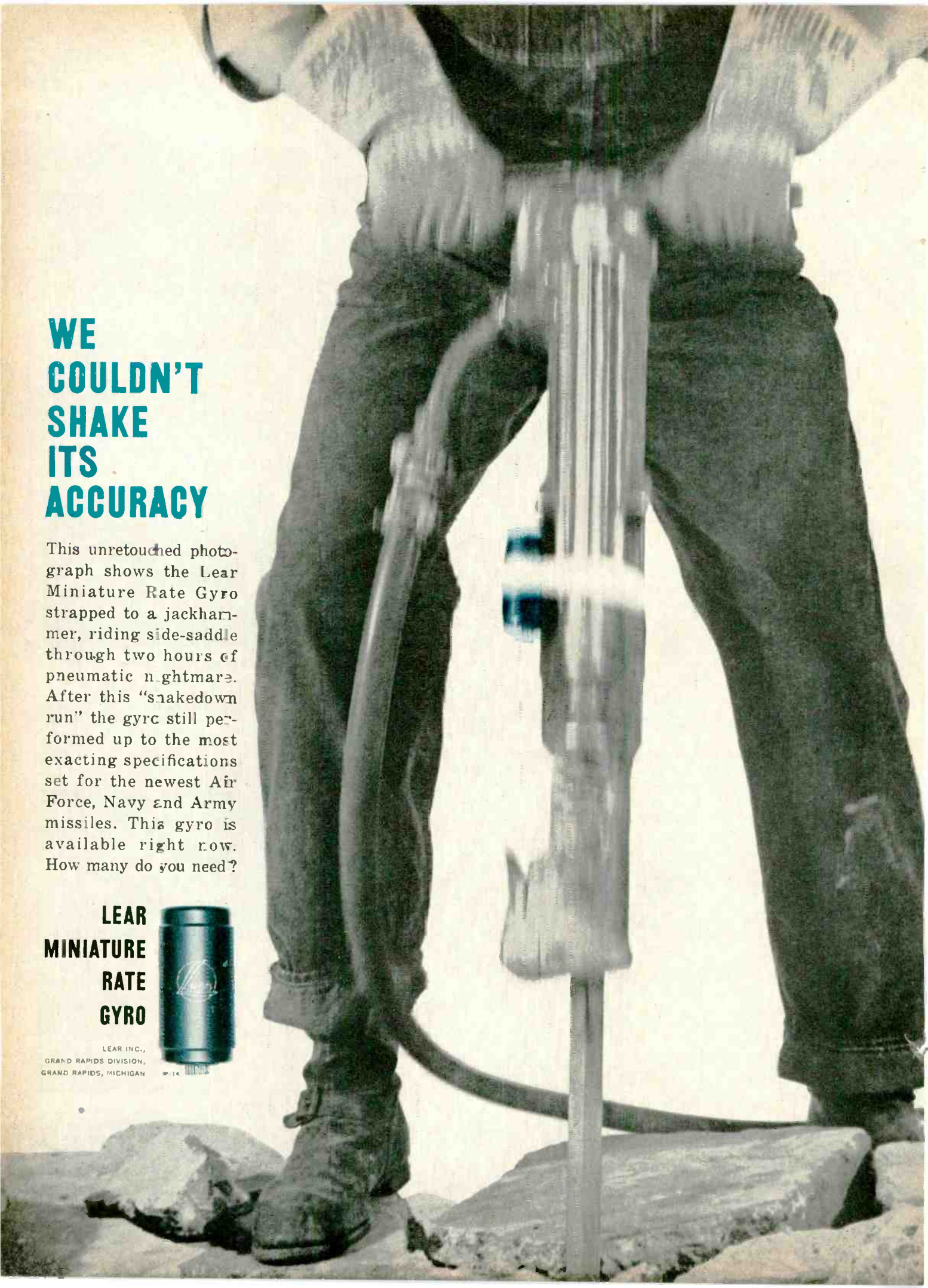


COILED CORDS

The "spring" in Coiled Cords automatically synchronizes with moving components that are electrically powered. There are no looping, tangling cords in the way . . . because Coiled Cords extend and retract as needed. Write for new literature.

Cords Limited Division

ESSEX WIRE CORPORATION

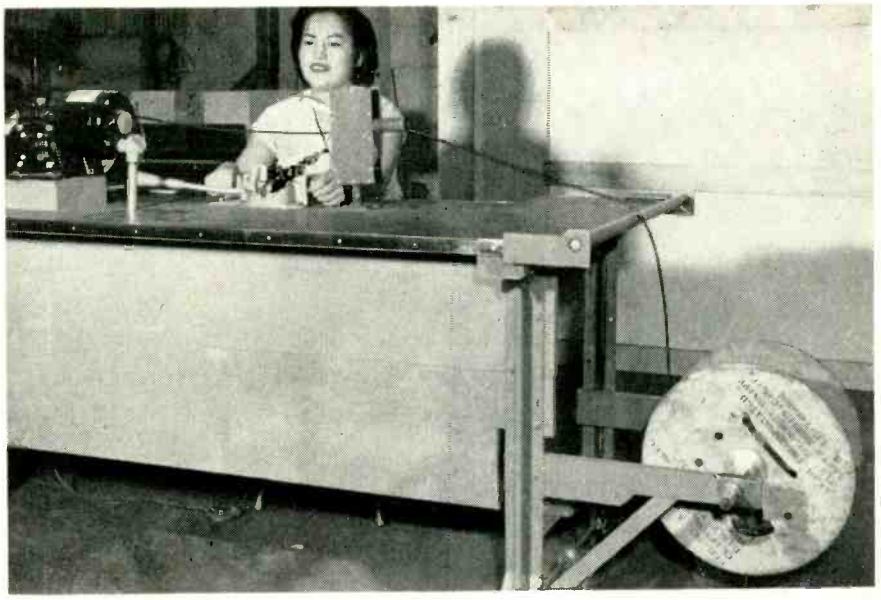


WE COULDN'T SHAKE ITS ACCURACY

This unretouched photograph shows the Lear Miniature Rate Gyro strapped to a jackhammer, riding side-saddle through two hours of pneumatic nightmare. After this "shakedown run" the gyro still performed up to the most exacting specifications set for the newest Air Force, Navy and Army missiles. This gyro is available right now. How many do you need?

LEAR MINIATURE RATE GYRO

LEAR INC.,
GRAND RAPIDS DIVISION,
GRAND RAPIDS, MICHIGAN



Method of mounting spool of coaxial cable at end of bench

foot divisions, in tens of feet and in hundreds of feet respectively.

A hand-operated lever cuts the cable at the correct point when the dials read the desired length. Operating the cutter resets the indicator dials to zero.

To run off a length of cable, the operator pulls the projecting end across from the cable meter to a motor-driven coiling reel at the right, and anchors the end in a spring clip on the reel. She then starts the reel motor by pressing a foot-operated rheostat, to wind on the desired footage as indicated on the dials. Use of the rheostat with the motor and gear box permits starting and stopping slowly while winding long lengths at high speed. A hand-operated braking system prevents overrun and backlash when slowing down.

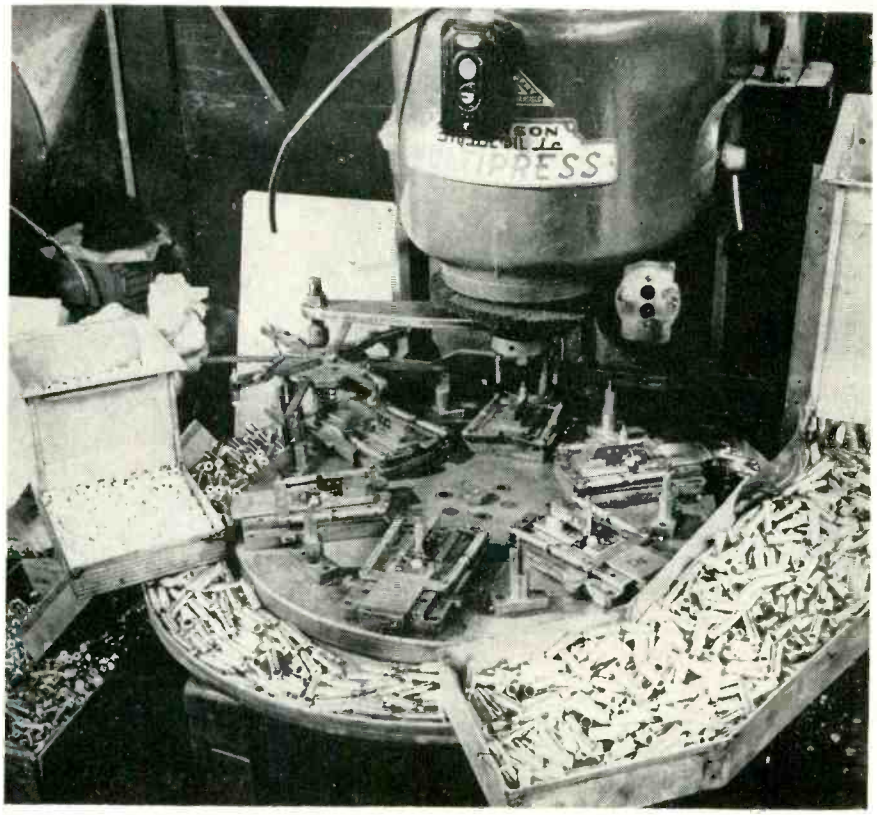
After the cable length is coiled and cut, the operator pushes the end through the jaws of an Ideal Industries stripper to a preset stop, then pulls back the cable to strip the outer jacket off the metal-braid shield. With the cable completed, the operator loosens a knurled knob and takes the flange off the motor-driven reel, then slips off the coil of cable.

Press Crimps Metal Electrode Over Ceramic

PRIOR TO INSTALLING hydraulic equipment, crimping of thin-metal electrode tubes to ceramic insulators presented a critical problem in the Los Angeles plant of Electrical Products Corp. Through trial and error, an operator had to learn to apply the exact pressure necessary to crimp pieces together without fracturing the ceramic insulator. This proved to be a costly, time-consuming procedure.

To cut costs, speed up production and insure product uniformity, the production setup was converted to use of a hydraulic Multipress manufactured by Denison Engineering Co., Columbus, Ohio. An unskilled operator with a six-station index table on the new press now turns out 15,000 pieces per day, as compared to 6,000 pieces using the old manual pressing method. Labor fatigue is also greatly reduced because tube parts are hopper-fed to the operator, who places the ceramic insulator on the tube and fits it into the holder at each station of the index table.

▶**How It Works**—The crimping press consists of a spider ejection mechanism, six cam-operated sliding split-type crimping dies and a die-closing cam. As completed electrodes are ejected by the spider mechanism, new tubes and ceramic inserts are placed in their respec-



Metal tubes and ceramic insulators, transferred by operator from hoppers to holders on revolving table, are indexed to press station where sliding die closes and descending ram crimps metal tube. Assembled unit is picked up by spider mechanism at left rear and dropped into tray. Extension arm on press ram actuates spider

tive holders and are automatically indexed to the pressing station. At this point, a cam brings the crimping dies together around the ceramic insert. The ram then descends, pressing the tube downward into the die and crimping it to the insert.

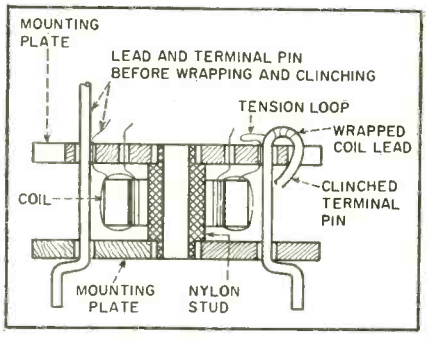
The spider ejection mechanism is attached to the ram banjo. When the ram descends the mechanism is pushed downward against spring tension to a pick-up position where the clamp arm grasps the completed electrode. As the cam rises, the mechanism is raised by the spring, lifting the electrode.

When the ram cycle is ended the table indexes, causing the spider-actuating pin to strike the spider arm. In doing this it revolves the arm in synchronization with the motion of the table until the next index station is reached. The completed electrode is dropped into a tray located at the side of the table.

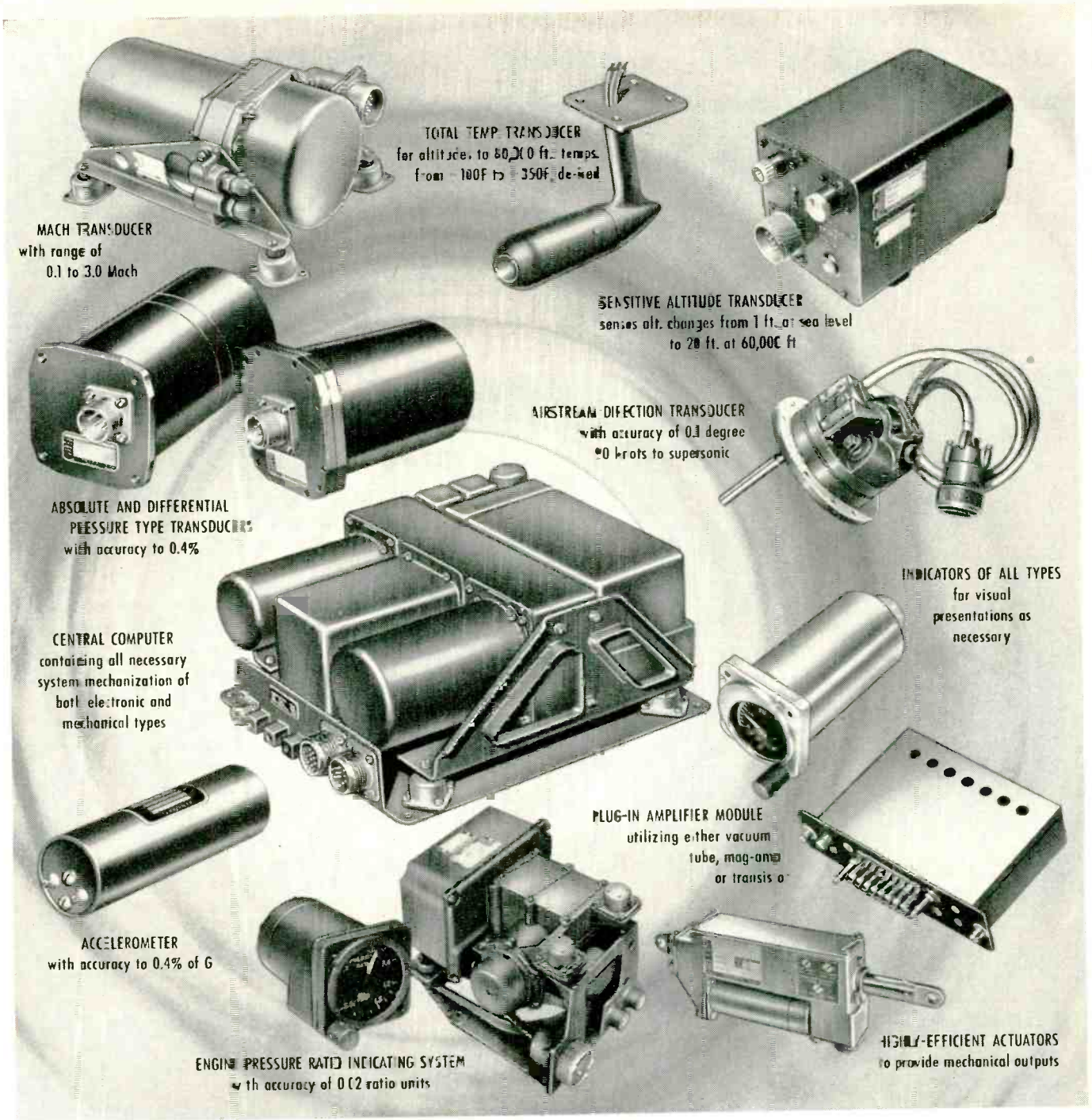
Plug-In Toroid Assembly Techniques

By Arthur J. Rose
Chief Engineer
Magnetics Research Co.
White Plains, N. Y.

An inexpensive and rapid method of producing an assembly that includes a five-winding toroidal core and a selenium rectifier involves foolproof identification of the coil leads and their connection to precisely positioned pins for insertion in printed wiring boards. The assemblies are used in great quantities as elements of shift-register



Cutaway section of coil assembly. Clinching terminal pins over through slots in coil mounting plates provides a rugged yet inexpensive assembly



Finer components mean better air data systems

AiResearch makes transducers, computers and indicators of superior sensitivity and accuracy in *all* required parameters. These can be combined into systems that provide the air data you require and convert it into any desired type of information or impulse. The products shown in the above illustration indicate some of the areas in which we are thoroughly experienced. If desired, we will take complete system responsibility. We invite inquiries to meet the most rigid specifications.

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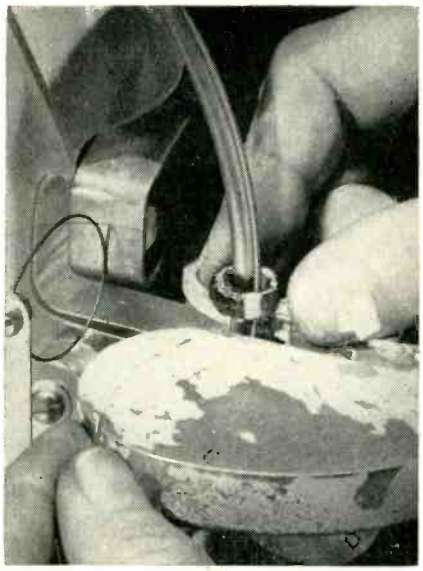
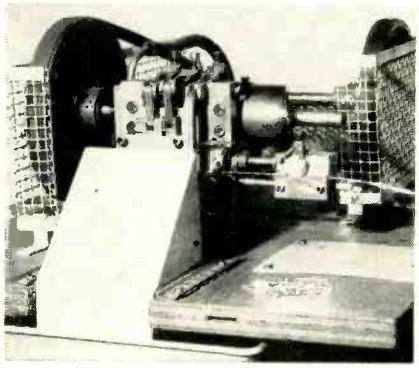


Winding of toroidal coil. Self-adhesive color tabs identify each loop brought out for connections

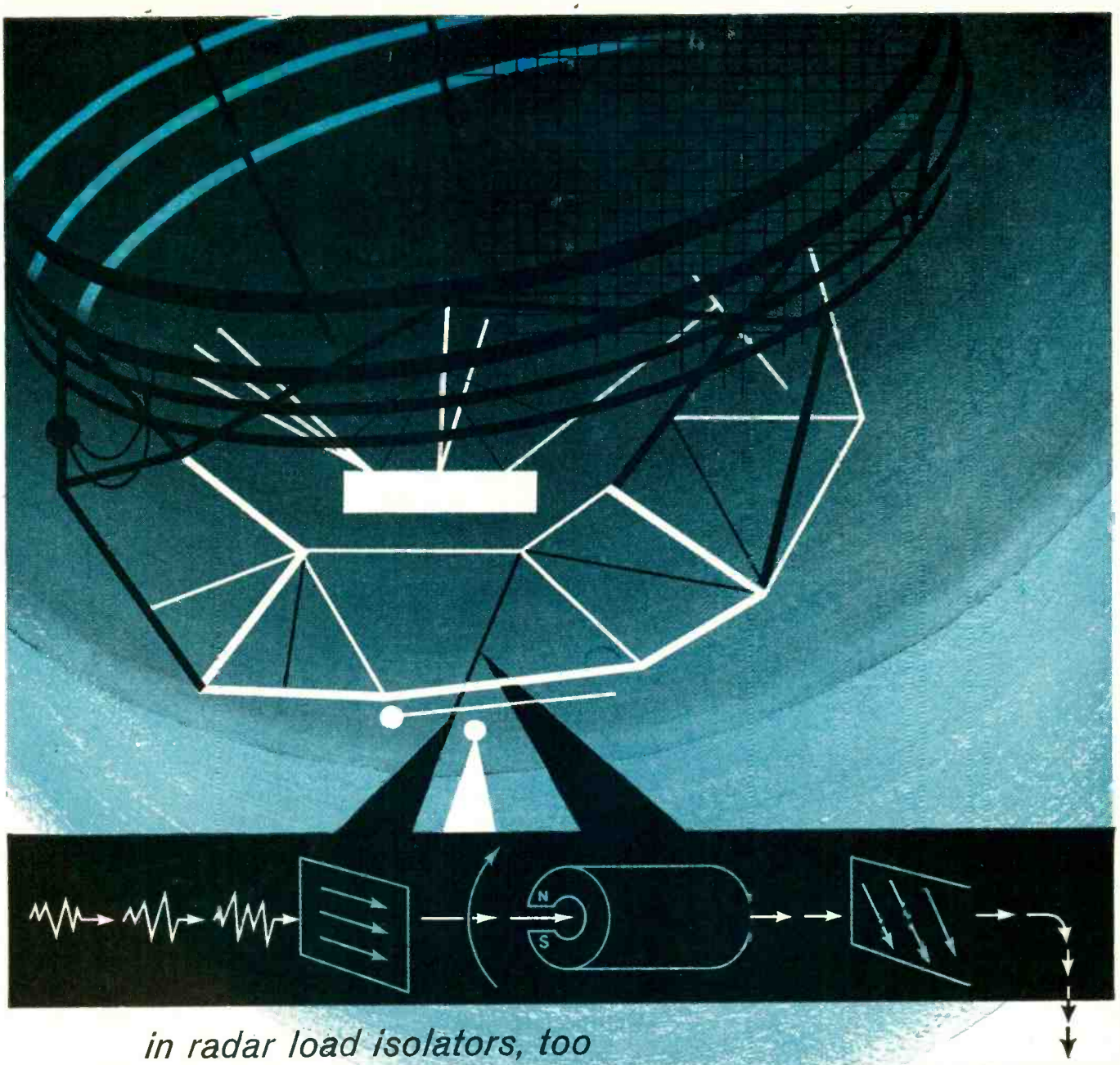
types of magnetic storage and data handling systems. The cores themselves are quite sensitive to pressure of any sort. They quickly depart from their rectangular hysteresis loop property if subject to strain or pressure, hence handling and mounting techniques are of prime importance.

▶ **Lead Identification**—The large number of windings (five) on a core diameter of ½ inch presents a problem in the identification of the various leads. Color coding at the winding machines is practical and necessary, but somewhere in the production process, stripping of insulation and trimming of leads is necessary. This problem has been met by an extremely simple technique that lends itself well to high production.

To avoid the use of expensive headers that employ delicate pins



Automatic wire pin forming machine cuts and forms terminal pins for coil assembly at rate of 10,000 per hour



in radar load isolators, too

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Special applications, such as radar load isolators, demand compact but powerful magnet assemblies. And this is but one of the many places where the *consistently* higher energy product provided in Crucible Alnico magnets pays off.

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The design and production of permanent magnets has been a Crucible specialty ever since Alnico alloys were discovered. It's one of the good reasons why so many people bring their magnet applications to Crucible. Why don't you? *Crucible Steel Company of America, The Oliver Building, Mellon Square, Pittsburgh 22, Pa.*

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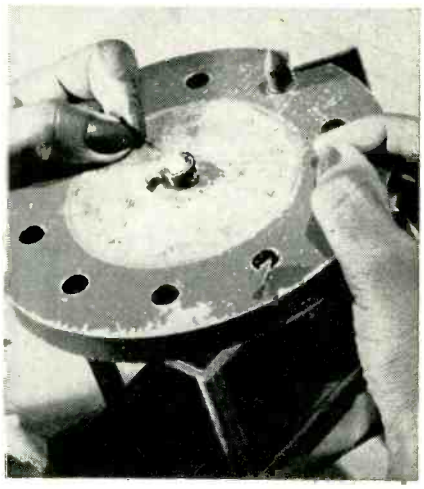
swaged into position, a rugged cage assembly was developed that uses phenolic stampings and pins made from ordinary tinned copper wire. An automatic machine of the type used in the watch industry for making small wire springs is used for forming and cutting the pins at a rate of 10,000 per hour.

Using standard toroidal winding machines, the cores are wound by skilled operators who pull out loops of wire at the end of each set of windings. A five-winding coil has four loops and two end wires. Each loop is identified by a piece of colored pressure-sensitive tape. Special tape with bands



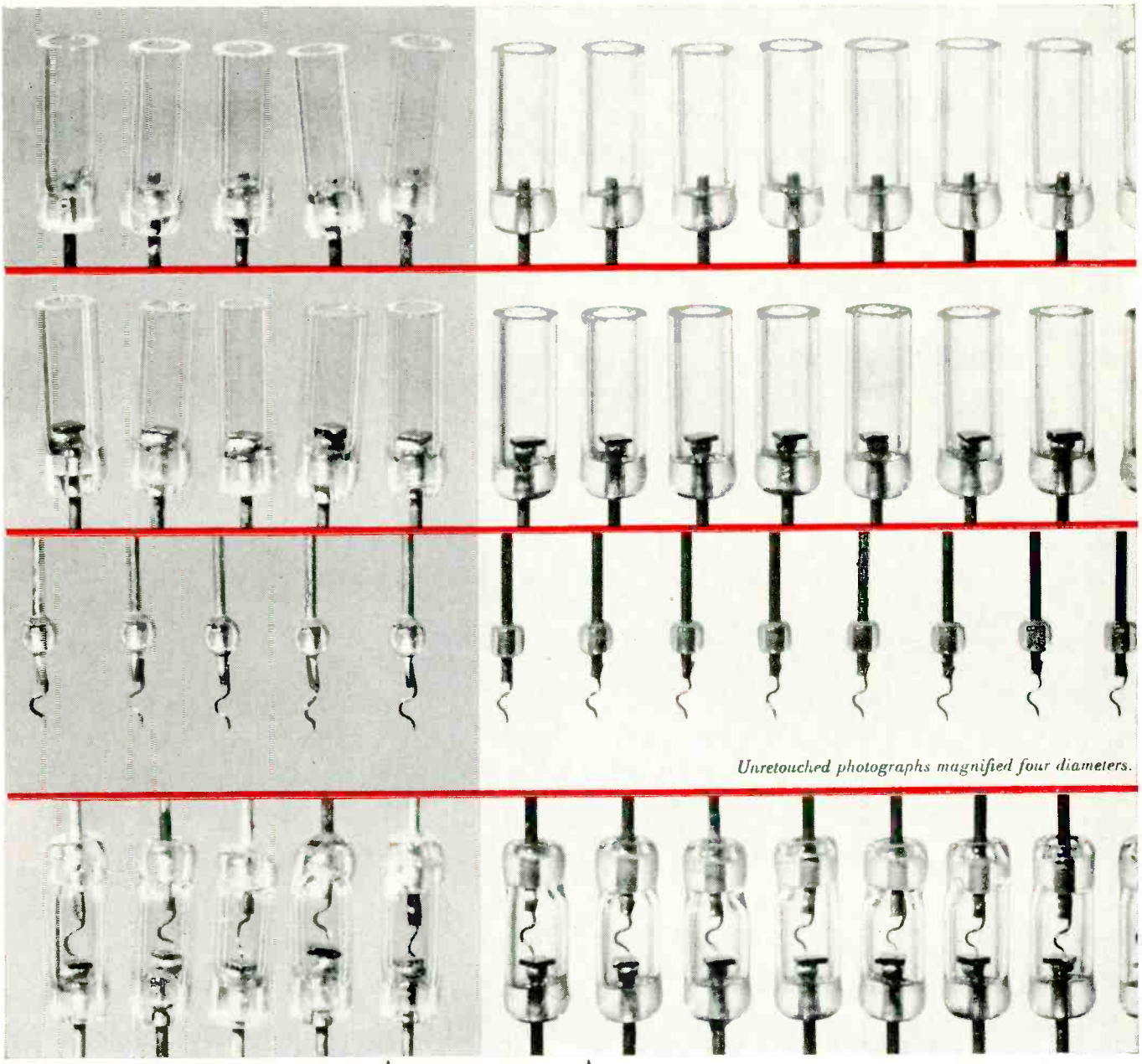
Coil-mounting fixture assures positive identification of lead connections by stringing coil leads through radial holes in coil-mounting plate

of color in sequence is dispensed one color at a time.

Leads are then identified as either top or bottom and of a particular color. Each loop is comprised of a top and a bottom wire. The end wires are either top or bottom.

▶ **Mounting Fixture**—As a step in the assembly process that virtually eliminates wrong lead connections, a special mounting fixture is used. It strings each lead through the upper mounting plate in a relationship to the terminal pins so that there is no question as to where each lead is to be soldered.

Because the pin connections must be in two linear rows of five and the leads from the coils are radial, conversion of these two



Unretouched photographs magnified four diameters.

Hand assembled diodes ↑ **COMPARE** ↑ *Automatically assembled CBS diodes*

UNIFORMITY

by and for automation

The increasingly automatic assembly of electronic equipment is placing serious limitations upon component manufacturers. Rigid, tight tolerances must be maintained to avoid jamming the automatic machines. This spells automation for components, too.

CBS has done something about it. On seven integrated machines, CBS glass diodes are automatically assembled, packaged, tested. The picture tells the story . . . compares the results of this automatic assembly with that of ordinary hand assembly. The controlled uniform quality is apparent. As you would expect, the uniformity is both mechanical and electrical.

Take advantage of CBS Advanced-Engineering. Specify CBS glass diodes for uniformity . . . for dependability . . . for automatically controlled quality.

CBS semiconductors

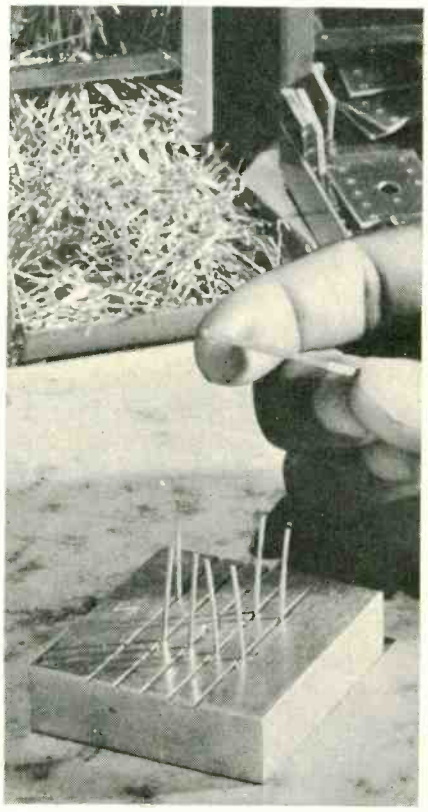
Reliable products through Advanced-Engineering

CBS-HYTRON
Semiconductor Operations, Lowell, Mass.
A Division of Columbia Broadcasting System, Inc.

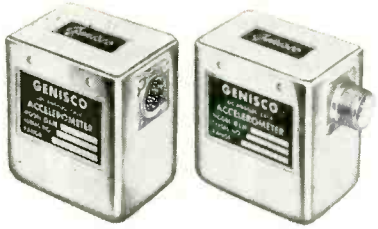
geometric factors has to be made. A mounting plate was designed that provides a circular row of holes for each of the coil leads and two linear rows of holes for the terminal pins. The small space available necessitated using a common hole that appeared in the midposition of the linear rows.

At each position of the hand-operated turntable of the fixture, a hooked needle is brought up and down through one of the holes in the coil-mounting plate by a foot pedal. After setting the coil on a nylon stud pressed into the coil mounting plate, the operator stops at each turntable position, hooks the appropriate lead under the hook and draws it through the plate. Wire loops are cut as required. The numbering sequence is marked T for top and B for bottom in five colors. A skilled operator can mount as many as forty coils per hour on this fixture.

▶**Stripping**—After all coil leads have been drawn through their holes in the mounting plate, a chemical stripping solution is



First operation on final assembly line. Operator is placing lower terminal plate over upright terminal pins in jig

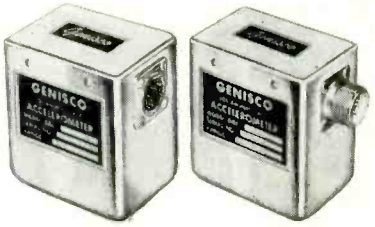


Model GLH

A rugged magnetically damped instrument with low natural frequencies for low range. High-quantity production assures good price and delivery schedules. Available in ranges from ±1 G to ±30 G.

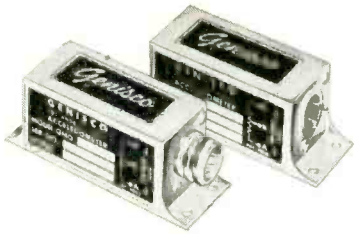
Model DDL

Magnetically damped low-range instrument available in ranges from ±1 G to ±30 G. Ultra-sensitive models supplied as low as ±0.1 G. Certified to MIL-E-5400 and MIL-E-5272A. Especially good in severe shock and vibration applications. An acceleration-sensitive switch version of the DDL is designated as the Model DDS.



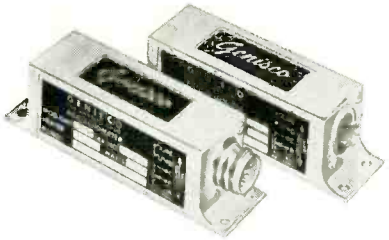
Model GAL

Incorporates a variable transformer a-c output with the magnetically damped sensory mechanism of the proven Models DDL and GLH. Superior reliability, life, resolution, and sensitivity. Available in ranges from ±1 G to ±30 G. Range as low as ±0.1 G also obtainable.



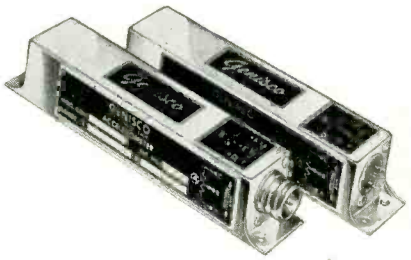
Model GMO

A rugged, miniature, viscous-damped instrument with ranges from ±2 G to ±30 G. Unbalanced-range instruments also available. Medium high natural frequencies.



Model GMT

Basically a Model GMO with internal thermostat-operated heater, assuring maximum environmental stability within the instrument. Damping remains constant with change in ambient temperature.



Model GDM

Miniature double-potentiometer instrument capable of sensing lateral acceleration in two mutually perpendicular planes (e.g., pitch and yaw). Ideally suited for missile and high-speed aircraft flight control systems.

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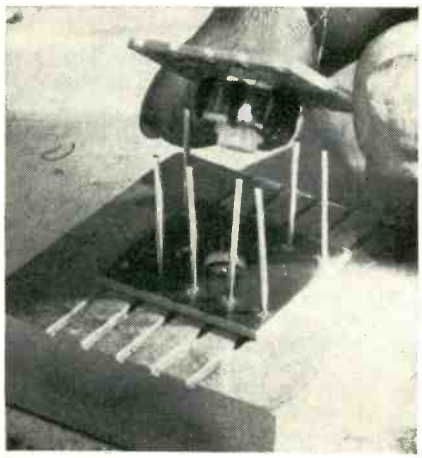
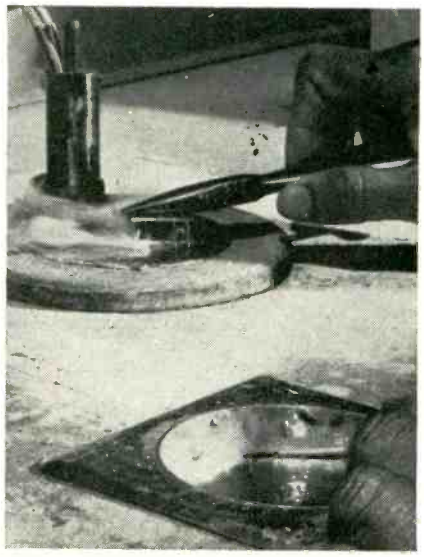


Second operator places mounted coil over terminal pins. Nylon spacer stud snaps into bottom hole and squares assembly

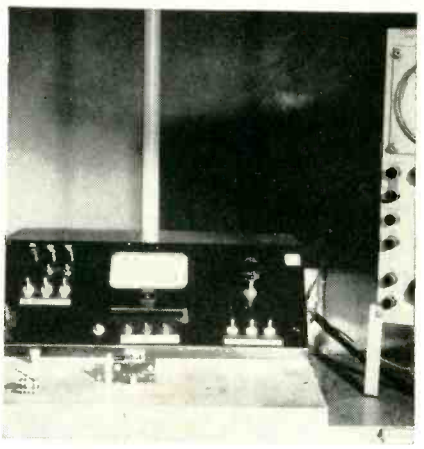
used to remove insulation and foreign matter from the leads. The advantage of having the coil on a mounting plate is obvious here. Should stripping solution get on the coil itself, the damage is final. However, the barrier of the mounting plate assures freedom from this source of production shrinkage.

▶**Terminal Pins**—A cage assembly provides a flexible yet rugged means of fastening terminal pins. The bottom bends are accurately made by the forming machine. The upper part of the pin is bent over and down through the slots on the coil mounting plate by operators on the final assembly line.

Simple jigs with accurately laid-out holes and slots are used in assembly until the cage be-



All connections are soldered in one dip-soldering operation



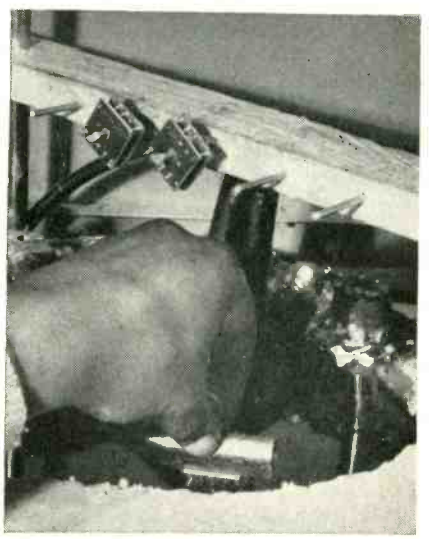
Completed cage assemblies on test fixture

comes self-supporting. In the first position, the operator inserts pins into the jig and places a bottom or terminal plate over the pins. One pin is left out for a later operation.

In the second operation the coil plate is set over the pins and pressed into place. Shoulders on the center stud position the plate and lock it in place.

At subsequent positions, each operator bends certain terminal pins over, clinches them, and/or wraps coil leads around the pins. The pins are wrapped while they are in a right-angle position, then clinched. A loop is left between the coil lead and the terminal pin to prevent lead breakage.

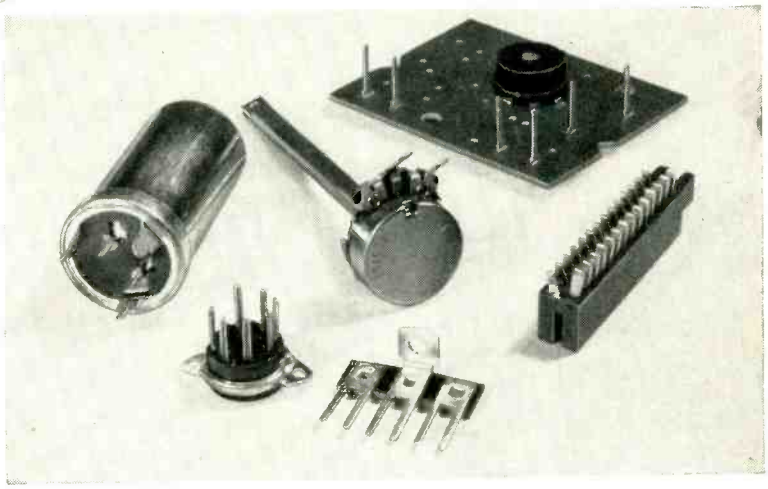
In a following line position the assembly is lifted from the jig, fluxed and dip-soldered. Mounting



Assembly is moisture-proofed by dipping in a pliable wax while gripping terminals with large paper clip. Cores used in these assemblies are sensitive to strain, hence hard-setting compounds cannot be used for the incapsulating operation

If you use . . .

to interconnect . . .



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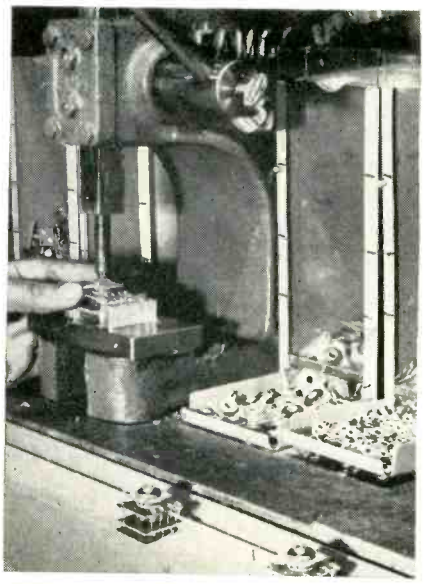
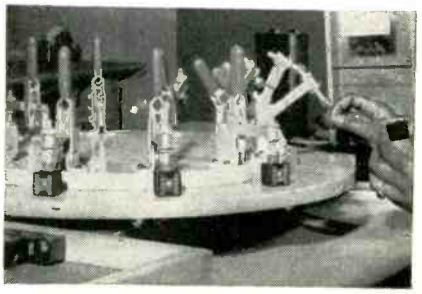

Arbor press setup on work center for swaging rectifiers to coil assembly


Last step in assembly involves applying bonding cement to edges of halves of plastic cases, putting package together over coil assembly, then placing under spring clamp on turntable for drying under pressure

jigs are returned to the first position on the lower portion of the conveyor belt.

▶ **Testing**—In-line testing for continuity and dynamic operating properties follows the soldering operation. This is conveniently done since the assemblies will plug into a test socket made for the purpose. Salvageable rejects are routed off the line to a repair line and then back again for completion.

For moistureproofing, the assemblies are dipped in a special wax compound and then hung diagonally to drain. The setting process is rapid enough to allow flow through the line.

▶ **Final Assembly**—Pretested rectifiers are mounted and riveted onto the assembly. As the rectifiers are somewhat pressure-sensitive, some operator skill is

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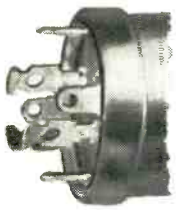

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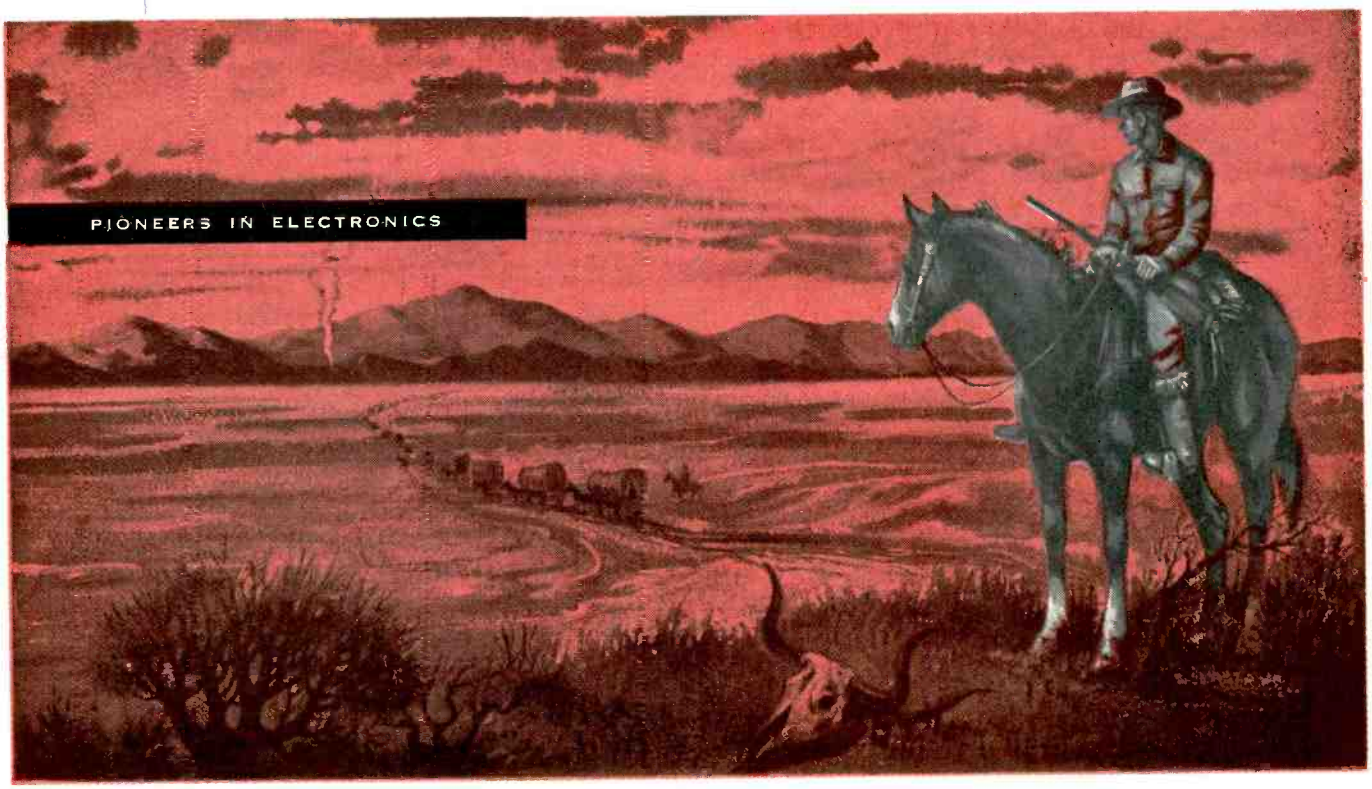

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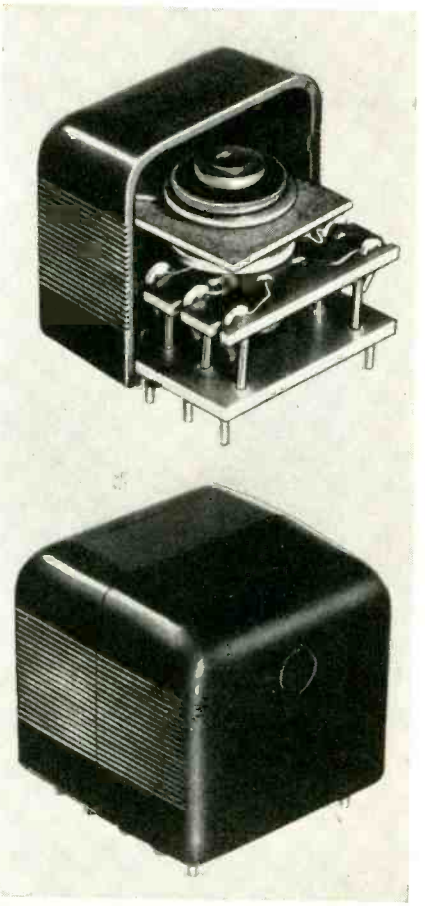

Finished coil assembly before and after sealing in plastic case

required in judging swaging pressure. The coil assembly itself receives no pressure from the swaging tool as it is mechanically isolated by the center mounting stud. Compactness and efficiency is afforded here by Alden Systems work positions and parts dispensers. All positions on the main assembly line involve finger motions of only a few inches.

At the final position, an operator inserts the assembly into plastic case-halves and cements them together. A turntable using toggle clamps gives a 5 to 10-minute drying cycle under pressure.

Welder Locks Turns on Tape Core Winder

MULTIPLE-CORE winders used by Magnetics, Inc. of Butler, Pa. allow winding of tape on five or more ceramic cores in one loading. The cores are placed on the shaft and a nut is hand-tightened to lock them in place. The magnetic tape core is

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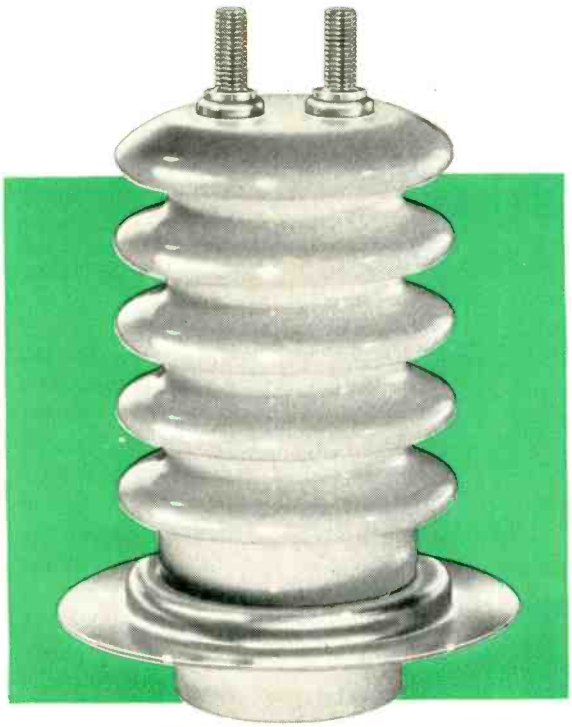

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Dielectric Constant @ 10,000 mc	8.4
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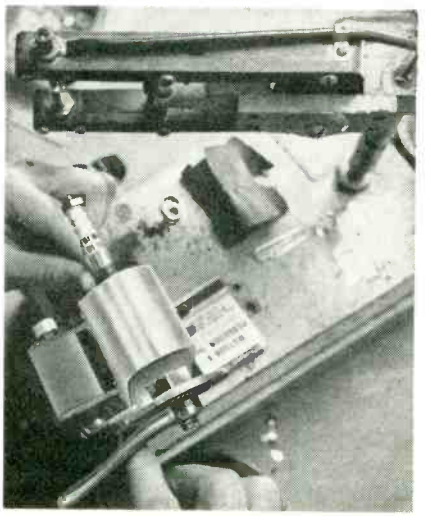
then wound on each bobbin by guiding the tape with the left hand while turning the shaft with the right hand. A disk and handle arrangement on the other end of the shaft facilitates rotation. A pin on the disk, next to the handle,



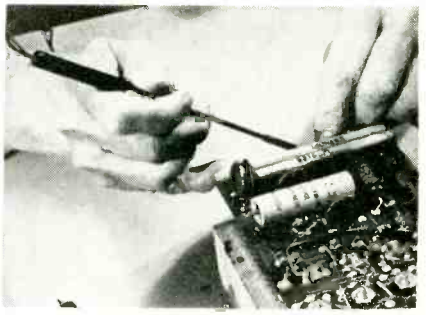
Straight arm pushed around by forefinger rotates winding shaft while left hand guides tape. Pivoted welder is swung over each finished core in turn

flicks the counter arm once in each revolution to give a turns count.

When the proper count is reached for a core a pivoted spot welder head is swung over the core to tack the last turn of tape. The welder timing is set to fuse only the outer two turns together. The winding process is then repeated for each other core.

Miniature Soldering Iron

ESPECIALLY SUITABLE for soldering to transistors and diodes, a new miniature low-voltage soldering iron greatly expedites production



Pin-point soldering iron weighing no more than ordinary lead pencil simplifies production of etched wiring circuits for transistorized Geiger counters in plant of UM & F Mfg. Corp., North Hollywood, Calif.

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Sprague 2N240 transistors with their fast response time—in the millimicrosecond range—give reliable operation in switching circuits up to 20 megacycles. The ideal electrical characteristics of these surface barrier transistors permit direct coupling for faster operation than any alloy junction type.

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- availability

Among these features, the most important to you may well be availability. Sprague is manufacturing 2N240 transistors NOW in production volumes. You can answer today's transistor needs *today* by specifying Sprague surface barrier transistors!

Write for complete data sheets on Sprague 2N240 germanium surface barrier transistors and on Sprague general purpose high-frequency surface barrier types SB 101 and SB 102. All are available on letterhead request to the Technical Literature Section, Sprague Electric Co., 35 Marshall Street, North Adams, Mass.

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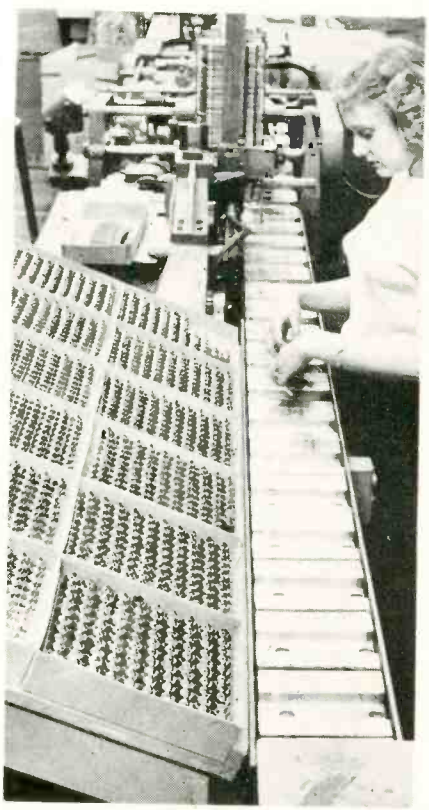
wiring of all fine subassemblies. The pencil-size precision tool, weighing only ¼ ounce, supplies rapid pin-point heat in 30 seconds from interchangeable nickel-plated tips as fine as 1/16 inch in diameter. The light weight permits continuous use all day without hand fatigue.

The iron is available from Oryx Company, 9015 Wilshire Blvd., Beverly Hills, Calif. in models with voltage ratings from 6 to 50 volts and wattage ratings from 6 to 12 watts.

Machine Inserts Tubes in Cartons

AN AUTOMATIC tube-packaging machine in the Elmira, N. Y. plant of Westinghouse Electric Corp. automatically opens a carton, inserts a tube, closes the carton and prints the tube type designation on the end of the carton. The individually packaged tube is then delivered by conveyor to the packing operator.

After production and initial test, the receiving tubes are stored in cell partitions in open trays like



Packaging starts here. Operator places tubes in built-in channels on conveyor of machine

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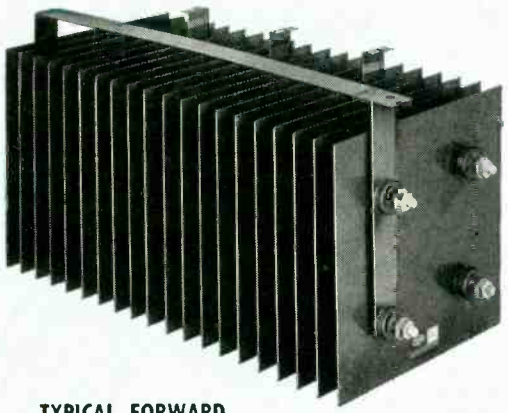
** High Current Density*

Industrial type SELENIUM RECTIFIERS

Developed by the famous Siemens Organization of West Germany and now manufactured by Radio Receptor Co. in the U. S. A.



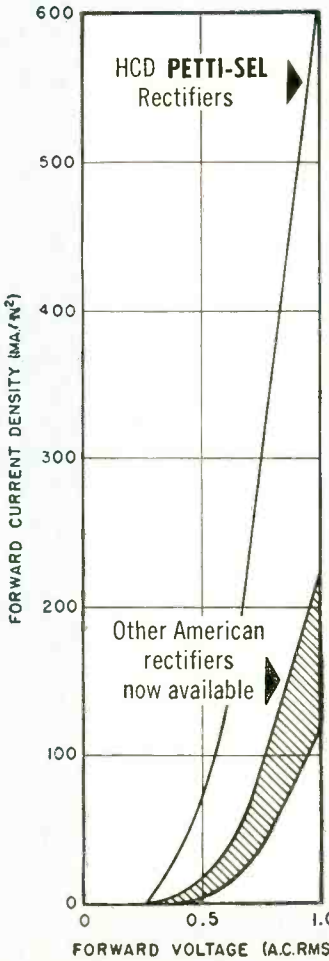
Estimated life 100,000 hours

Much smaller cell sizes than conventional units of the same ratings

Lower forward voltage drop

Suitable for high temperature applications

TYPICAL FORWARD CHARACTERISTICS



Far smaller in size than other rectifiers of the same current ratings, the new Radio Receptor HCD Petti-Sel units are manufactured under laboratory controlled conditions with fully automatic machinery, assuring new standards of product uniformity.

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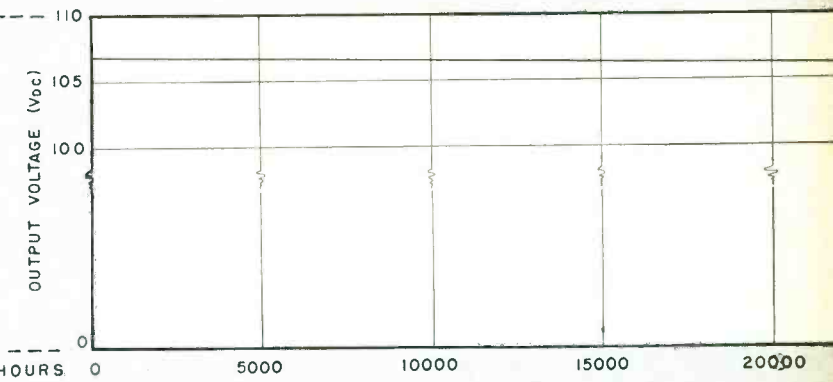

Watch for further announcements of unique developments on these history-making rectifiers. If you would like our new bulletin as soon as it is available, write today to Section E-3R.

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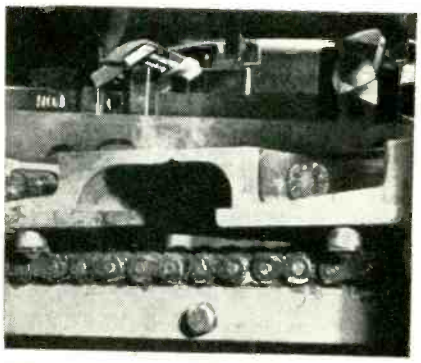
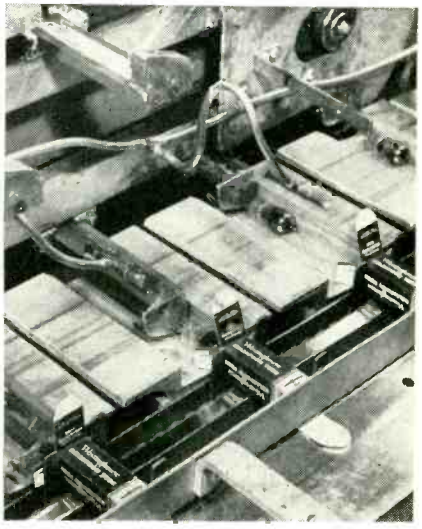


After cartons are delivered to conveyor, machine automatically opens carton prior to tube insertion

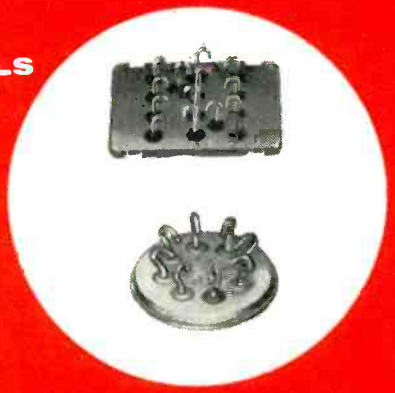


Tube insertion, shown here with slide bar removed from unit. Tube is conveyed in rigid channels while being pushed into open carton. Air blows into channel to keep tube from twisting or jamming in box during insertion

egg crates. When an order comes in, each tube is electrically tested and mechanically inspected in an area adjacent to the packaging machine. The tube is next branded with the manufacturer's code, customer's brand and date code. The pre-shipment tested tube is then moved in the bulk handling trays directly to the input end of the packaging machine. This procedure reduces excess handling and minimizes the chance that a defective tube can reach the customer.

▶ **Loading**—An operator removes the tubes from their cells in the tray and places them in buckets built into the packaging machine conveyor. Simultaneously, the cartons are hopper-fed to another packaging-machine conveyor belt traveling parallel to the tube conveyor line. The packaging machine opens the cartons automatically in

Constantin GLASS-TO-METAL SEALS



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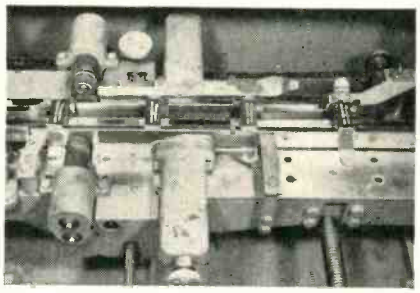


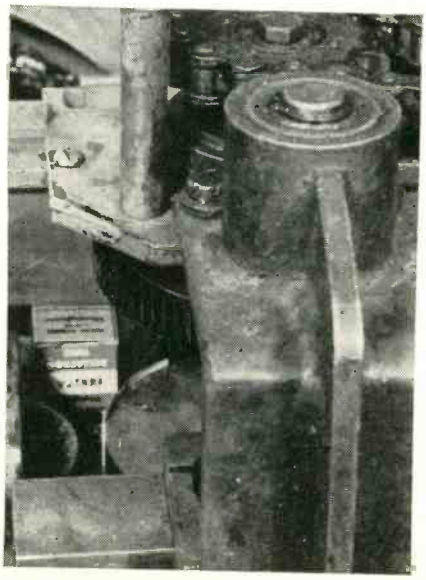
Closing of carton begins at this step of operation. Flaps are folded and tucked into carton

preparation for loading. The tube conveyor lines up a tube with an empty carton and the machine feeds the tube into the waiting carton. Next the flaps are automatically closed and locked on both ends of the carton.

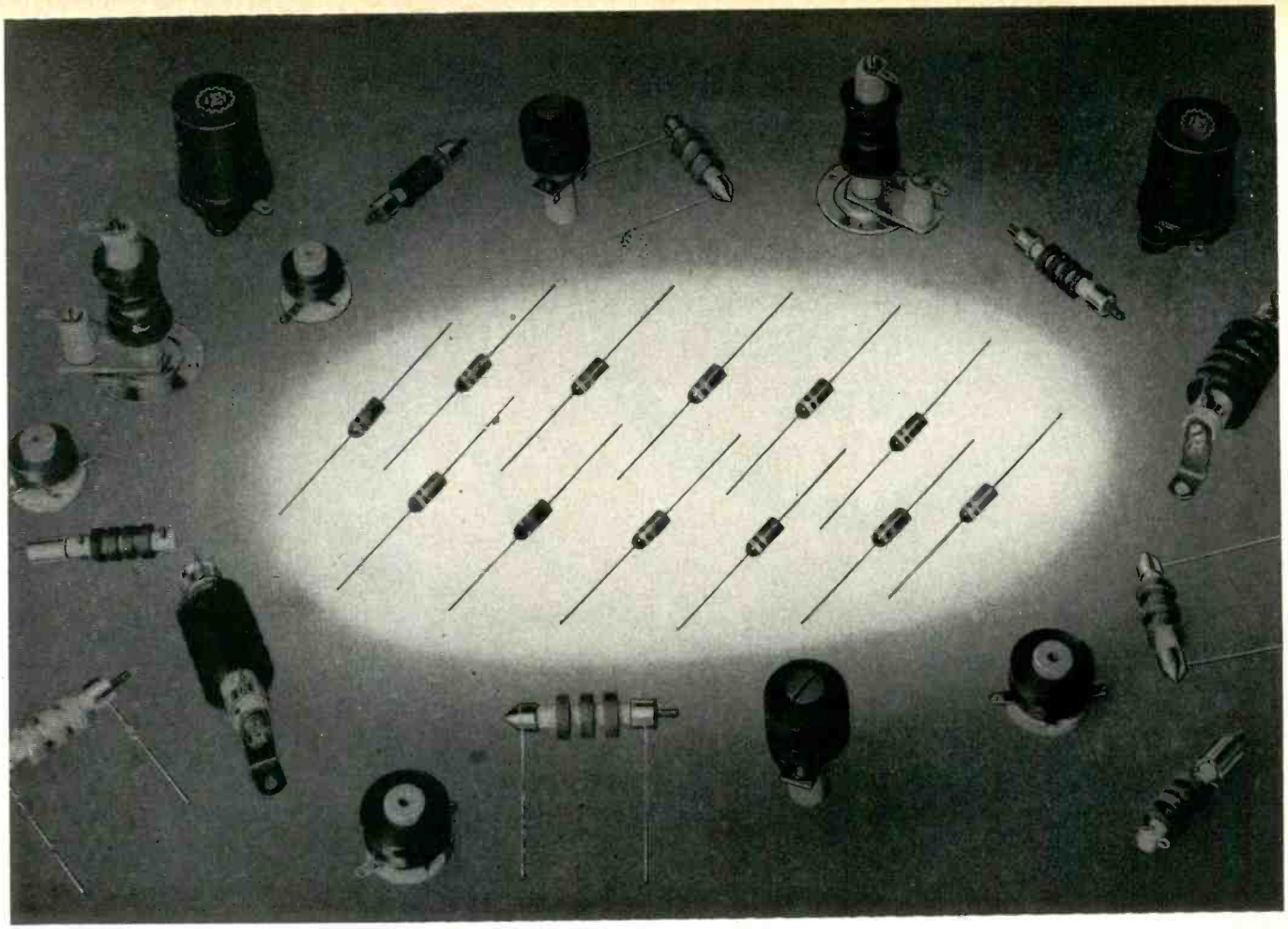
At this stage the tube type designation is imprinted on one end of the carton. The conveyor line then moves the cartons to packers for loading into 5-pack sleeves and shipping containers.

The machine has several snap-action switches to prevent malfunctioning. It is comparatively easy to change the marking stamp to accommodate a production run of another type of tube.

An interlocking device called a no-carton detector is adjusted to stop the machine if one carton is missing or improperly positioned for insertion of the tube. A similar device reacts to missing tubes. The machine has been designed to handle tubes gently, without shock



After flaps are tucked in, printer applies tube type designation to carton in space provided



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Millen DESIGNED for APPLICATION encapsulated coils provide another advance in the r-f inductor field. Modern application requires miniature, heat and cold resistant, hermetically sealed, and abrasion resistant r-f inductor assemblies. The James Millen Manufacturing Company has pioneered many advances in the r-f inductor field including the now standard 4 pi r-f choke, the axial lead r-f choke, and the miniature r-f choke. Developments have now made possible another advance, the No. 34301 and No. J301 encapsulated inductors—hermetically sealed—miniature size. Ambient temperature minus 55 degrees to plus 100 degrees C.

NO. J-01 MINIATURE ENCAPSULATED INDUCTANCES

DESIGNED for APPLICATION miniature inductances are: extremely small (see table at right)—hermetically sealed—wound on axial lead Carbonyl cores—color coded. Coils are available in RETMA standard values plus 25, 50, 150, 250, 350, 500, and 2500 microhenries. Coils are three layer solenoids up to 350 microhenries. From 360 to 2500 microhenries coils are pi-wound. Current rating 50 to 600 milliamperes depending on coil size. Inductance ± 5%. Special coils on order.

NO. 34301 STANDARD ENCAPSULATED INDUCTANCES

Encapsulated DESIGNED for APPLICATION axial lead phenolic form r-f inductances. Hermetically sealed—heat resistant—abrasion proof—color coded. 1 to 350 microhenries available in RETMA standard values plus 25, 50, 150, 250, and 350 microhenries. Inductance ± 5%. Values available in same progression as J301 coils listed in the table at the right. Solenoid winding for 1 to 15 microhenries. Universal pi winding from 20 microhenries to 350 microhenries. Current rating 250 to 1500 milliamperes, depending on coil size. Ambient temperature range—minus 55 degrees to plus 100 degrees Centigrade. Size: ⅜ inches diameter × ⅞ inches long. Special coils on order.

COIL NUMBER	INDUCTANCE MICROHENRIES	DIAMETER INCHES	LENGTH INCHES
J301-25	25	3/16	9/16
J301-33	33	3/16	9/16
J301-47	47	3/16	9/16
J301-50	50	3/16	9/16
J301-82	82	3/16	9/16
J301-100	100	3/16	9/16
J301-120	120	3/16	9/16
J301-150	150	3/16	9/16
J301-200	200	3/16	9/16
J301-220	220	3/16	9/16
J301-250	250	3/16	9/16
J301-300	300	3/16	9/16
J301-330	330	3/16	9/16
J301-350	350	3/16	9/16
J301-360	360	7/32	5/8
J301-390	390	7/32	5/8
J301-430	430	7/32	5/8
J301-470	470	1/4	11/16
J301-500	500	1/4	11/16
J301-510	510	1/4	11/16
J301-560	560	1/4	11/16
J301-620	620	1/4	11/16
J301-680	680	9/32	3/4
J301-750	750	9/32	3/4
J301-820	820	9/32	3/4
J301-910	910	9/32	3/4
J301-1000	1000	9/32	3/4
J301-1200	1200	5/16	13/16
J301-1300	1300	5/16	13/16
J301-1500	1500	5/16	13/16
J301-1800	1800	5/16	13/16
J301-2000	2000	3/8	7/8
J301-2200	2200	3/8	7/8
J301-2400	2400	3/8	7/8
J301-2500	2500	3/8	7/8

Tubes in single cartons are placed in the handy five-pack sleeve, and sleeves in turn are packed in standard shipping cartons

and vibration which might cause internal breakage.

▶**Output**—The new machine is capable of packaging 200 receiving tubes per minute, or 96,000 tubes in an 8-hour period. By way of contrast, an operator can package only 3,000 tubes in an 8-hour day.

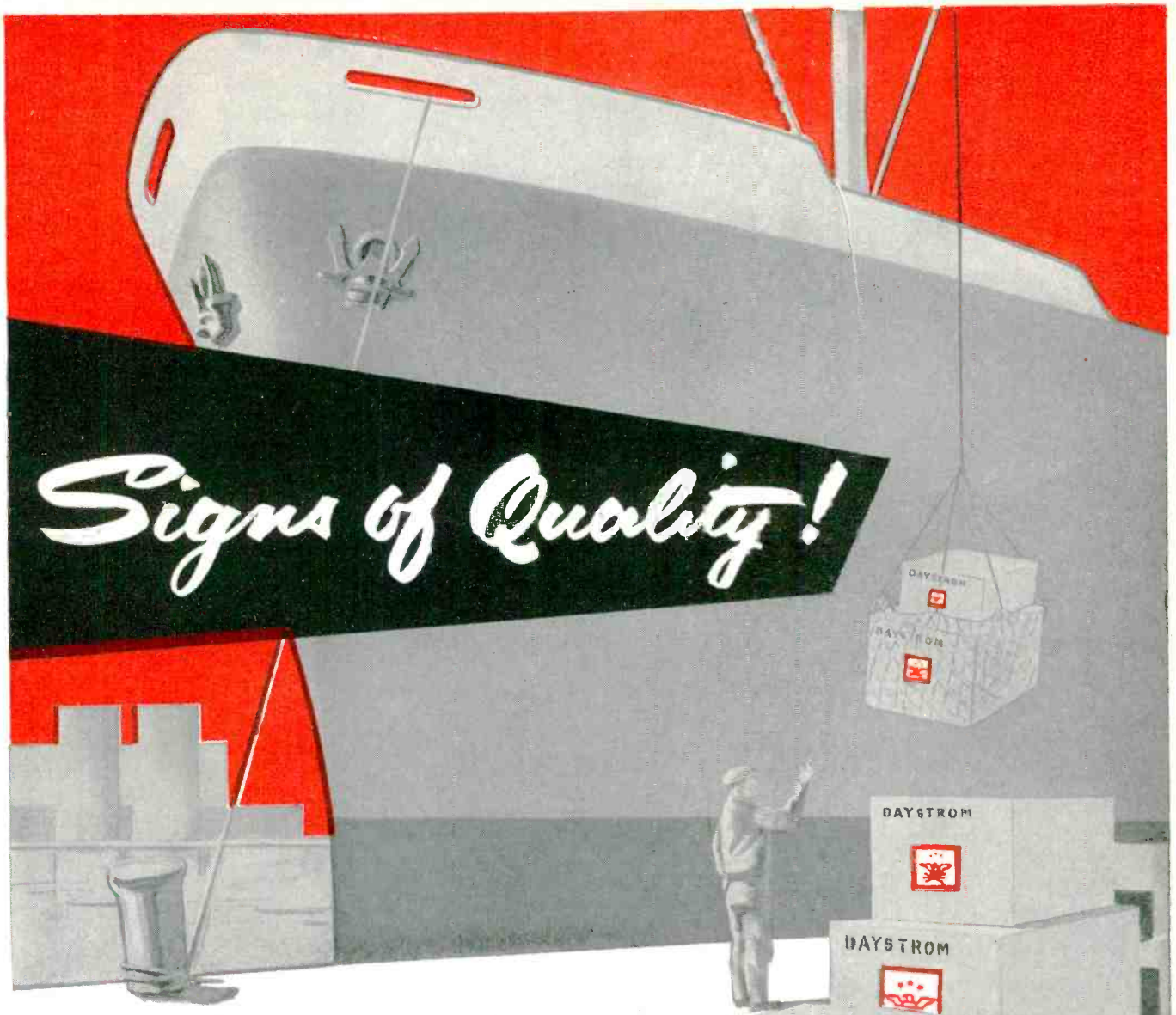
Leak Detector for Hermetic Seals

BY B. W. SCHUMACHER
Research Fellow
Ontario Research Foundation
Toronto, Canada

RAPID NONDESTRUCTIVE testing of hermetically sealed components for leakage through seals is now being achieved with a carrousel-like pumping turntable setup having a sensitivity comparable to that of the mass spectrometer. No special test gas is required, however.

Though designed for rapid 100-percent testing at the end of a production line, the apparatus serves equally well for sampling inspection and for following changes that occur in a component during storage or when subjected to various atmospheric conditions or acceptance tests. The latter tests served to reveal correlations between shelf-life leaks and certain electrical failures arising during storage.

Where the units are filled with helium gas, the mass spectrometer type of leak detector may be used



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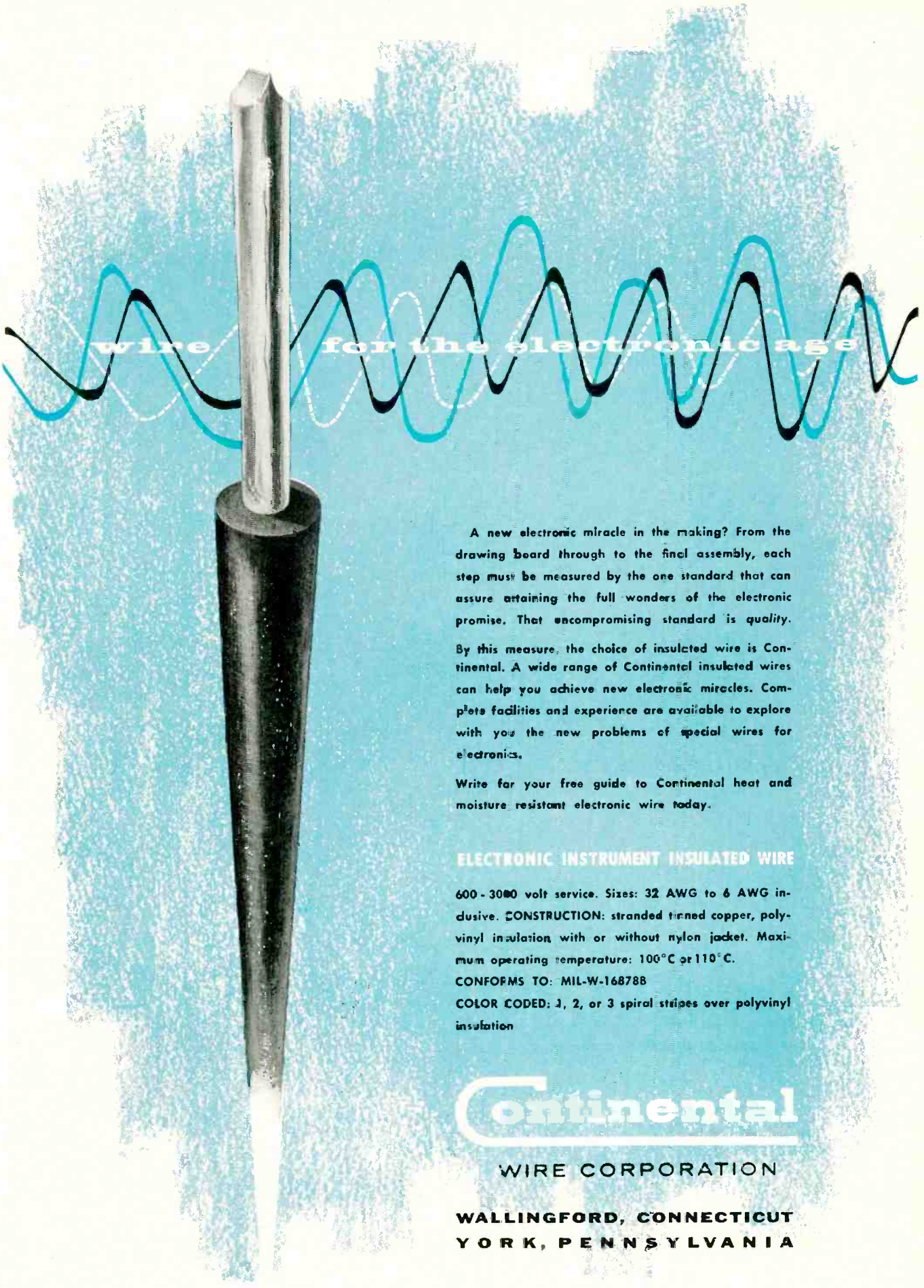
in connection with a sampling probe (which reduces sensitivity) or in connection with some kind of a test chamber into which the units are inserted. The instrument is costly, however; besides, the cans are usually filled with dry nitrogen rather than with helium.

▶ **Problems**—Several problems had to be overcome. For mass production tests, the units have to be locked in and locked out of the high vacuum testing chamber continuously. During this process, the pressure in the test chamber should never become higher than about 10^{-3} mm Hg whether small or big leaks are present because the gas may be absorbed on the walls, requiring either an undue time for pumping off again or limiting the sensitivity by virtual leaking. Absorbed gas and volatile materials on the outside of the samples to be tested had to be removed by a proper method of cleaning. No spurious leaking along any moving parts of the leak tester could be tolerated. Pumping or gettering

Operator loads quartz crystal unit into pouch of carrousel with left hand. Right hand is on lever that indexes turntable to next position



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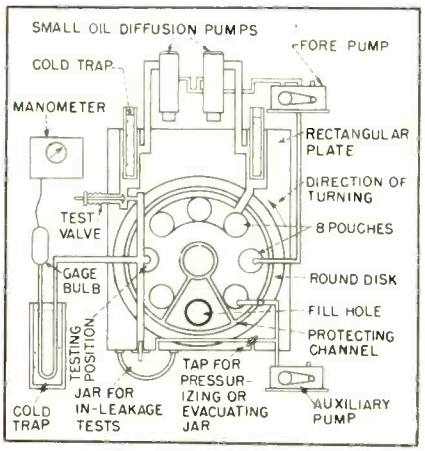
YORK, PENNSYLVANIA

effects by the manometer had to be avoided. All these requirements were met by the apparatus as built and described here.

▶ **Carrousel Construction** — The carrousel lock consists of an upper stationary steel plate and a lower rotatable steel disk 8½ inch in diameter and 1½ inch thick. The disk has eight pouches each 1¼ inch deep, into which the specimens may be fed through a hole cut in the stationary plate. This disk turns around a pivot in close contact with a round area of the stationary rectangular steel plate, also 1½ inch thick, into which a number of channels are bored to connect the



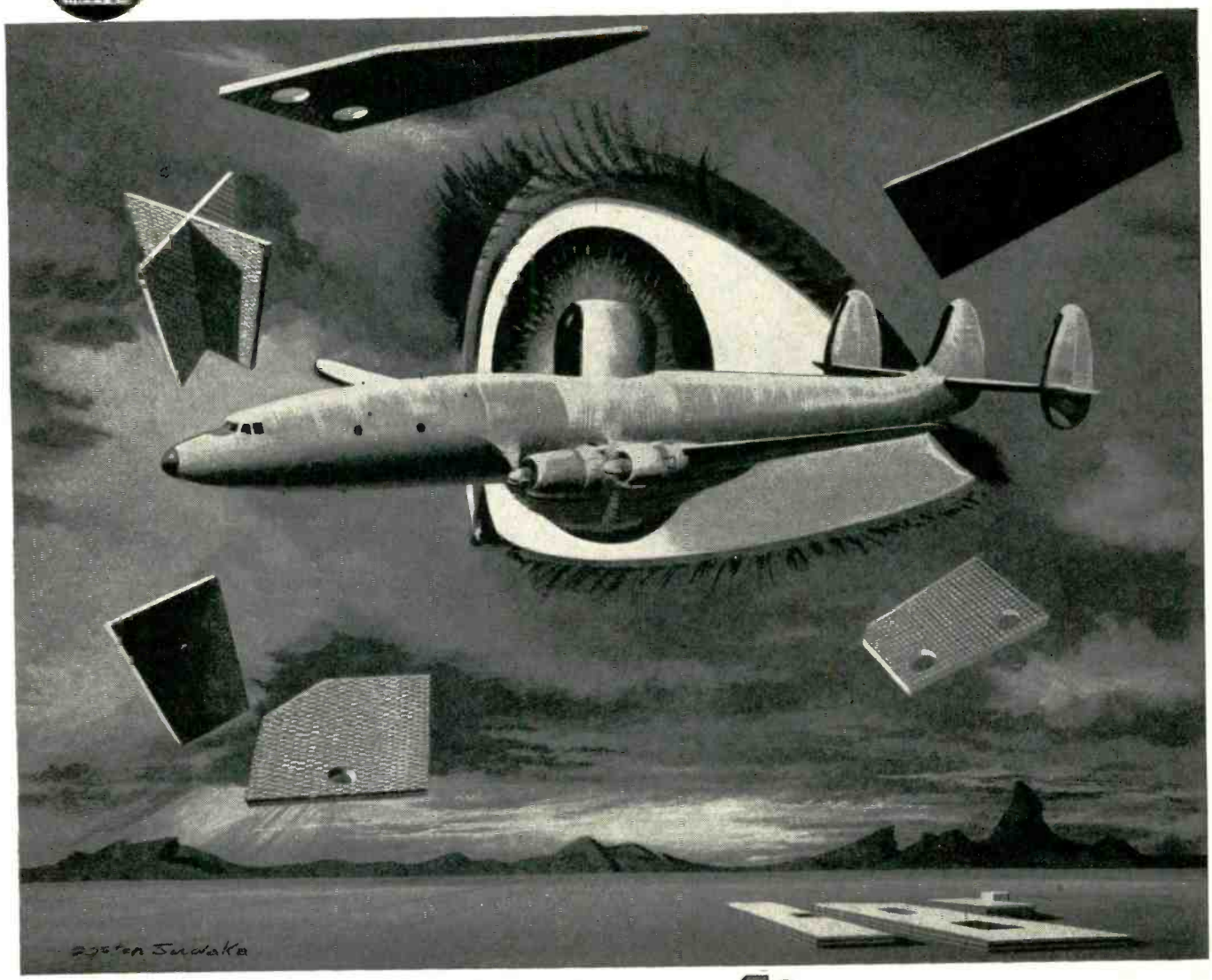
Arrangement of leak detector units

pouches with different vacuum pumps when the disk is turned around. The lock was manufactured to specifications by Extrusion Machine Co. Ltd., Toronto.

The two contacting surfaces of this carrousel are ground one against the other as for grinding optical lenses. Two annular grooves divide each possible leaking path from the atmosphere to the high-vacuum chamber into two parts. These grooves, forming a protecting channel, are connected with a small auxiliary pump which keeps the pressure below 0.7 mm Hg. Thus, any possible leaking path to the high-vacuum chamber has only 1/1,000th of the atmospheric pressure at its inlet, reducing spurious leaking more than 1/1,000th. As a lubricant having a vapor pressure below 10^{-7} mm Hg, Apiezon oil C is applied.

▶ **Manometer**—For the manometer, a model 3 thermionic ionization

US-KON CONDUCTIVE CARDS



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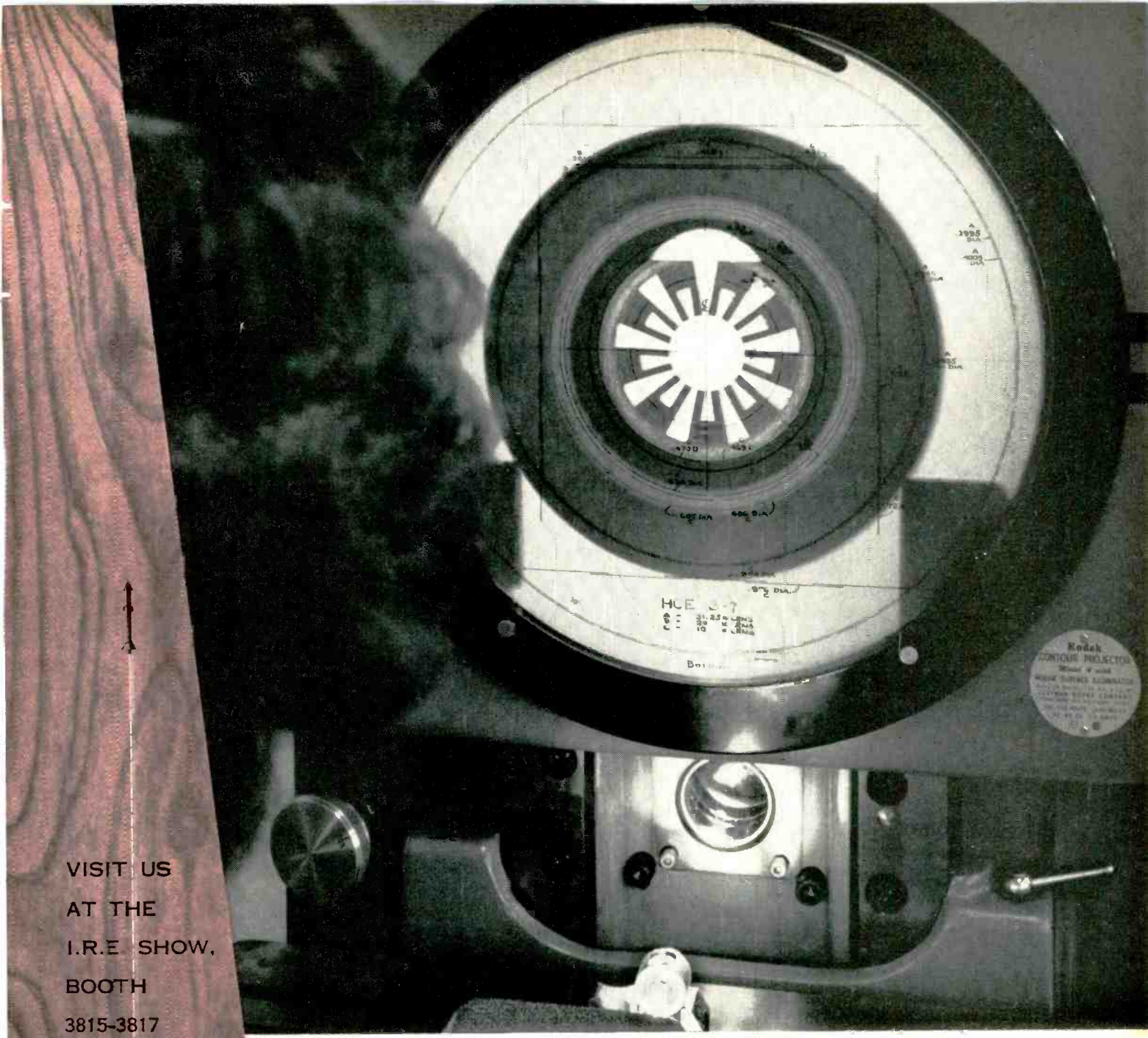
gage made by Edwards High Vacuum Ltd. is used in series with a cold trap filled with liquid air. All the parts are assembled using O-rings and loose flanges. The cold traps in the pumping lines are filled only if the highest sensitivity and speed is required. In this case, the gage can also be operated with a lower current than usual, reducing any possible gettering effects to a negligible amount.

▶**Operation** — The samples are cleaned by washing them in trichlorethylene, then warmed on a hot plate to 80-110 C to remove moisture. To increase the speed and sensitivity of the test, the hot plate may be put under a vacuum jar connected with the auxiliary pump. The cleaned units are put into the pouches through a filling hole in the upper stationary plate. As the carrousel rotates, a connection with the auxiliary pump is made first, followed by the forepump of two small oil diffusion pumps, then by the first of the oil diffusion pumps which brings the pressure in the pouch down to about 1×10^{-5} mm Hg. The pouch is then at the testing position, where it is connected with the second of the oil diffusion pumps and the manometer.

If in the testing position a pressure of 2 to 5 x 10^{-6} mm Hg is reached, usually after 15 to 20 seconds, a test valve is pressed down to close the pump line. The manometer and pouch with the specimen now form one closed chamber and the manometer is watched for a pressure increase.

Usually, a small amount of gas is given off by the walls of chamber and specimen, causing a pressure rise of 0.5 to 2 x 10^{-6} mm Hg within the first few seconds, depending upon how long the pouch was cleaned by pumping at 10^{-6} mm Hg. After 15 seconds it can usually be decided whether a small leak is present or not. Larger leaks cause an immediate pressure increase to 10^{-5} or 10^{-4} mm Hg; as soon as such a rapid rise is seen, the test valve in the pump line is opened immediately in order not to contaminate the test chamber. Due to the test valve, there is no danger that even very big leaks will con-



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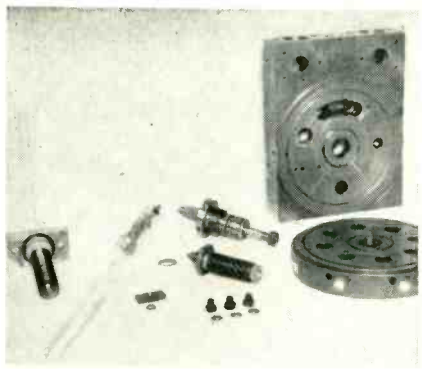


Components of carrousel

taminate the apparatus or cause a burn-out of the gage.

As long as the test valve is open the pressure in the test chamber will be determined by the equilibrium between leak rate and pumping rate. For leaks which show up in a bubble test, the equilibrium pressure is in the order of 10^{-4} to 10^{-8} mm Hg. If that sample is left in long enough, it would be emptied by the pumping. Calculations show, however, that more than an hour would be required to empty it so far that it would no longer be seen in the test. The apparatus can thus be used for big leaks as well. Most of the leaks found were 100 to 1,000 times larger than the minimum detectable size.

For tests in a manufacturing line, sensitivity often can be sacrificed for higher testing speed. The apparatus can then be equipped with a simpler manometer and the cold trap omitted. Nevertheless, the tests will still be much more sensitive and reliable than bubble tests, and also nondestructive.

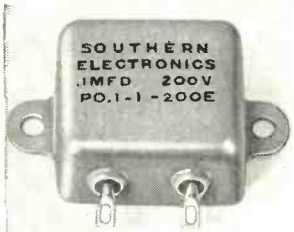
► **Test Procedure** — The test set should be put into operation by an experienced technician. For the tests themselves, no special knowledge is required. A test series would proceed in the following manner.

A group of units is cleaned, generally in trichlorethylene, to remove soldering flux residues and other contamination, then dried on a hot plate. The first unit is picked up with tweezers and put into pouch No. 1. The carrousel disk is turned one position with a key, the second unit is put in pouch No. 2 and the carrousel is turned again. The other pouches are similarly filled until pouch No. 1 reaches the

where precision counts—it's S.E.C. first!

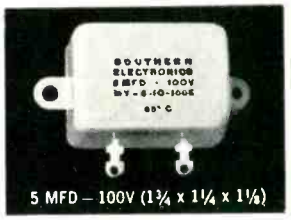
PLASTIC PRECISION CAPACITORS

Tubular .1 MFD—200V

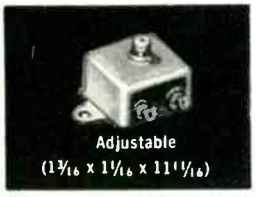


.1 MFD—200V


10 MFD ± 1% 200V
(4 7/16 x 3 1/16 x 2 1/8)


5 MFD—100V (1¾ x 1¼ x 1⅛)


1 MFD—200V


Adjustable
(1 3/16 x 1 1/16 x 11 11/16)


Plug in (1 MFD—150V)

1. POLYSTYRENE

with these outstanding properties:

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- Insulation Resistance as HIGH as 1 x 10^{12}
- Dielectric Absorption as LOW as .0001
- Dissipation Factor as LOW as .0002
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- Stability as close as .05% drift in 1 yr.
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- **Hermetically sealed for enduring accuracy!**

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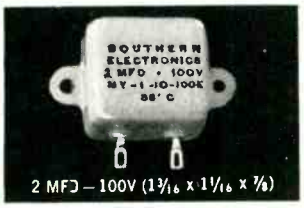
- Any capacitance from .001 to 50 MFD (incl. special values)
- Voltages from 50 to 5000

2. POLYESTER

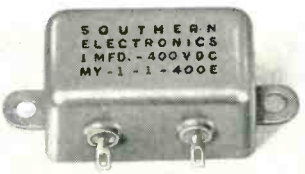
with these outstanding properties:

- Tolerances as close as 1%
- Insulation Resistance as HIGH as 1 x 10^{11}
- Dielectric Absorption as LOW as .001
- Dissipation Factor as LOW as .003
- Temperature Coefficient...800 PPM per°C
- Temperature range.....to 150°C.
- **Hermetically sealed for enduring accuracy!**

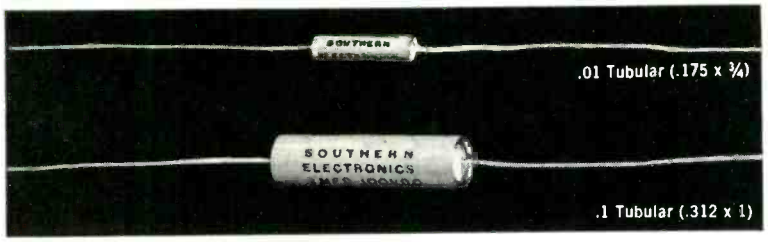

4 MFD—300V (2 x 2 x 1)


2 MFD—100V (1 3/16 x 1 1/16 x ⅞)

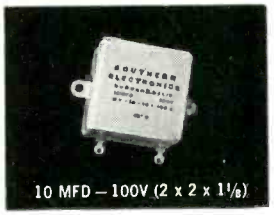

120 MFD ± 10% 50V


1 MFD—400V (1¾ x 1¼ x 1)


Plug in (4 MFD—150V)




Printed Circuit Small .11 MFD—50V


10 MFD—100V (2 x 2 x 1⅛)

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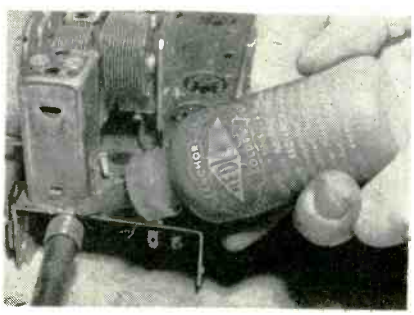
testing position. Here the operator watches the pressure for about 15 seconds, then presses the test-valve control and watches the pressure again. If a pressure rise indicates a leak in the specimen, he puts a marker on that pouch, releases the valve and turns the carrousel to the next position. After another step the first unit, designated by a marker if leaking, comes to the filling position. Here it is taken out, set aside and the pouch filled with a new unit.

The author is indebted to Dr. A. E. R. Westman, Director, Department of Chemistry, and to his colleagues, Drs. D. B. DeLury and M. H. Jones, for their interest and help. Valuable support was given by the Project Officer, W. R. Prendergast. The work was performed under Defense Research Board ECDC Project C19 (PCC No. D48-55-60-22 Contract No. P69-10-116).

Solder-Flux Dispenser

SQUEEZE-BOTTLE DISPENSERS for a new solder-flux paste make it possible to clean, flux and solder joints in one quick operation. The new Redi-Mix product, manufactured by Anchor Metal Co., Inc., Brooklyn, N. Y., is a special combination of high-strength tin-lead solder and chemically active corrosive flux suspended in an agent that assures free flow regardless of how long it remains in the bottle. The paste joins, tins and solders practically all housing and chassis metals except aluminum and magnesium. Being corrosive, it is not intended for electrical connections. As yet, it has not been possible to achieve a rosin-flux solder paste in which the rosin stays intimately mixed with the solder.



Squeeze-bottle dispenser expedites soldering to steel chassis by applying solder and flux simultaneously

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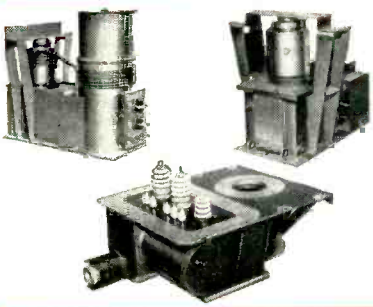

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New Products

Edited by WILLIAM P. O'BRIEN

100 New Products and 55 Manufacturers' Bulletins Are Reviewed . . . Control, Testing and Measuring Equipment Described and Illustrated . . . Recent Tubes and Components Are Covered

AUDIO LEVEL INDICATOR

for r-f square law detector

WEINSCHEL ENGINEERING, 10503 Metropolitan Ave., Kensington, Md. Model IN-1 audio level indicator consists of a variable gain amplifier broadly tuned to 1,000 cps driving a rectifier type a-c indicating instrument which responds to the average level. The time constant of the indicating meter is adjustable to increase the accuracy of the observation of the small signals in the presence of noise.

This unit makes an ideal companion instrument to the bolometer preamplifier, BA-1A, and the a-f substitution attenuator, CF-1, allowing the maximum use to be made of these instruments for r-f insertion loss measurement. At maximum gain a 100-μa signal gives full-scale indication. **Circle P1 inside back cover.**

DIGITAL OHMMETERS

two new types offered

NON-LINEAR SYSTEMS INC., Del Mar Airport, Del Mar, Calif. Fast, automatic and precise measurement of a wide range of resistance values, with very small currents passed through the test resistance, is provided in models 758 and 759 digital ohmmeters. To assure maximum, trouble-free life, each model features the NLS oil-sealed stepping switch system.

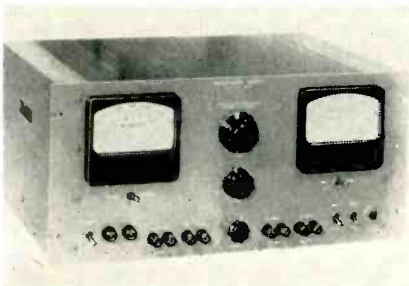
Resistance values are displayed in a horizontal line of inch-high luminous numerals, with the decimal point and resistance symbol shifting automatically. Connection of accessory NLS digital recording systems provides permanent records.

Model 758 displays four digits with a range of 0.0001 K to 9999 K. Accuracy is $\pm$0.1 percent of value read or one digit, whichever is greater.

Model 759 displays five digits and has a range of 0.0001 K to 9999.9 K. Accuracy is $\pm$(0.01 percent of value measured + 1 digit) in the lowest range and decreases to $\pm$(0.1 percent of value measured + 1 digit) at the upper end of the highest range. **Circle P2 inside back cover.**

H-C POWER SUPPLY

for transistor work



DRESSEN-BARNES CORP., 250 N. Vinedo Ave., Pasadena, Calif., announces a low-voltage, high-current power supply developed for transistor work and other uses requiring excellent regulation and microsecond response.

Output is 0 to 50 v d-c, continuously variable without switching; current 0 to 1,000 ma maximum. Full output current is available, without derating, throughout the entire range. A second output supplies 6.3 v a-c at 10 amperes. Recovery time from 0 to full load is 0.5 millisecond; from full load to removal, 0.25 millisecond.

Regulation for 50-v, 1,000-ma output is 80-mv change, no-load to full-load. For line voltages of 105 to 125 v, regulation is 0.1 percent change in output voltage. Outputs may be pulsed with square-wave

our leadership protects yours...

It takes a lot of doing to produce the exact same thing over and over again hundreds of thousands of times—without slipping up on a thousandth of an inch, watt, or milligram. This insistence on *uniformity* has helped build our reputation as the world's most Consistently Dependable producer of CAPACITORS. Continuously uniform production is a science —one that we've painstakingly pursued since 1910.

Typical of the "countless" C-D electrolytics used by major equipment manufacturers the world over are:

"EC" MINIATURIZED CERAMIC CASED TUBULARS For cramped-space applications in hearing aids, transistorized devices, and remote control assemblies. Less than ¼" D., only ¾" L.

"NL" ULTRA-SMALL Hermetically sealed aluminum cased electrolytics, built for compactness, ruggedness, low leakage, long shelf and in-use life.

TANTALUM 3 tubular types, all with low power-factor, moisture-impervious hermetic seal, long service and especially long shelf life. "TX" with sintered anode; "TAN" miniature foil type; sub-miniature, low-voltage wire anode type "NT".

TYPE "UP" Made in the smallest tubular aluminum cans possible for any given capacity and voltage combination. In single, dual, triple and quadruple capacity combinations.

Write for catalog to Cornell-Dubilier Electric Corporation, South Plainfield, New Jersey.

CONSISTENT HI-EPENDABILITY
CORNELL-DUBILIER CAPACITORS

SOUTH PLAINFIELD, N. J.; NEW BEDFORD, WORCESTER & CAMBRIDGE, MASS.; PROVIDENCE & HOPE VALLEY, R. I.; INDIANAPOLIS, IND.; SANFORD, FUQUAY SPRINGS & VARINA, N. C.; VENICE, CALIF.; & SUB.: THE RADIART CORP., CLEVELAND, OHIO; CORNELL-DUBILIER ELECTRIC INTERNATIONAL, N. Y.

Want more information? Use post card on last page.

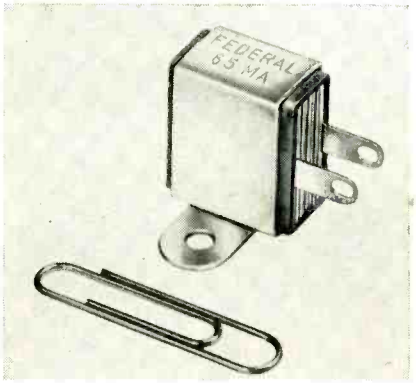
load without affecting normal regulation. Ripple and internal noise for 50-v, 1,000-ma output is below three mv rms. Accurate setting of output voltage is provided by a three-turn Helipot.

Designated model .5-1MB, the unit is of standard 7 in. by 19 in. relay rack construction, with a depth of 15 in. Literature is available on request. **Circle P3 inside back cover.**

SELENIUM RECTIFIER

with wrap-around design

FEDERAL TELEPHONE AND RADIO CO., 100 Kingsland Road, Clifton, N. J., has announced a new type of 65-mil selenium rectifier with a metal wrap-around design. It has its individual cells placed flat against each other like pages in a book instead of being placed on a center shaft with an air space between cells.

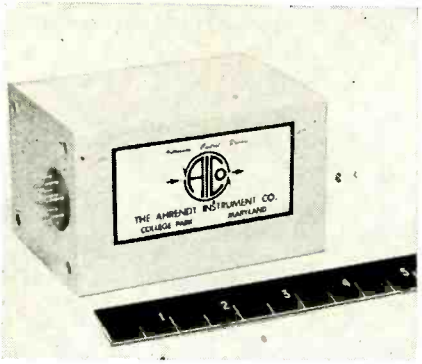


▶ **Advantages** — Center mounting shafts, with associated nuts and washers, are eliminated, giving more rugged construction and greater protection against contamination by moisture. The metal wrap-around provides thermal coupling to the chassis which acts as a heat sink, so that air cooling is not necessary. This permits flexibility of mounting, an important consideration in portable equipment where space is at a premium and where conventional rectifiers often have to be mounted to allow cooling by air convection. The wrap-around also protects the rectifier from physical damage and permits it to be easily screw mounted, riveted or eyeleted.

Elimination of the center hole gives each cell a larger effective area and a greater current safety factor. Addition of a seventh cell provides another safety factor, voltagewise, over six-cell rectifiers. **Circle P4 inside back cover.**

MAGNETIC AMPLIFIER

designed for servo systems



THE AHRENDT INSTRUMENT CO., 4910 Calvert Road, College Park, Md. Designed for self-contained 400-cps input signals, this magnetic amplifier is adaptable to input signals from d-c to 1,000 cps with the addition of a reference transformer. It is suitable for driving a Bu Ord Mk 7 or Mk 8 servo motor or equivalent. It does not require any vacuum tube or transistor driving stage in a normal servo loop.

Magnetic amplifier C-150-223 is a rugged, reliable amplifier designed for use in instrument and computing servo systems. It is potted and hermetically sealed in a MIL-T-27A size HA can. Circuit is of full-wave design. External circuitry is reduced to a minimum through built-in servo motor reference and anti-stickoff voltage for double speed data systems. It meets shock and vibration requirements of MIL-STD-202. **Circle P5 inside back cover.**

ANTENNA

for use with marker beacon receiver

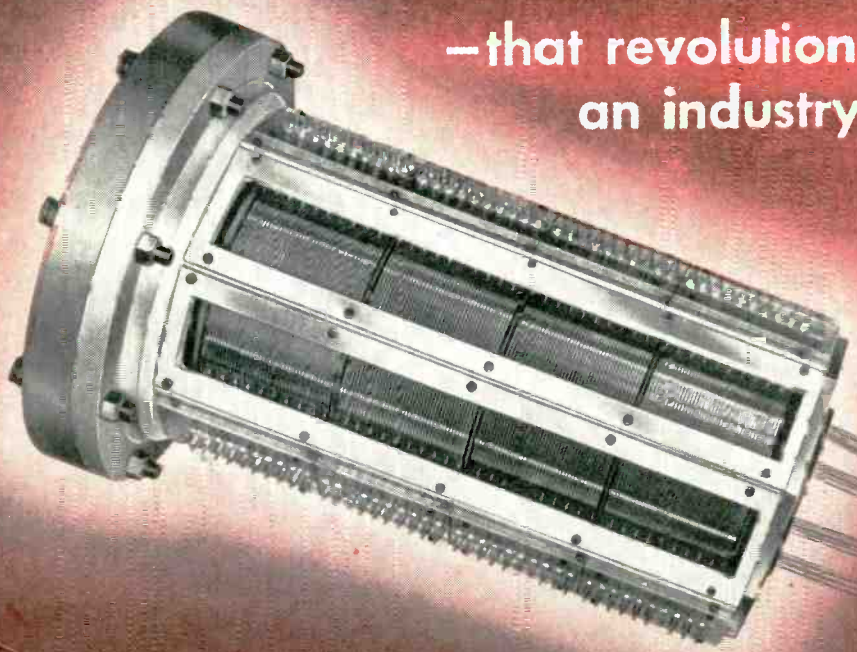
TELECTRO INDUSTRIES CORP., 35-16 37th St., Long Island City 1, N. Y. Model AT-134 is a 75-mc marker-beacon antenna designed specifically for use with aircraft type marker beacon receivers. It is installed by flush mounting it on the bottom of an airplane fuselage.

The external arrangement is a flanged deep drawn aluminum alloy case forming the antenna cavity, with the slotted shaft of the variable loading capacitor extending through the closed top of the case to permit screwdriver adjustment and tuning. The flanged bottom or airplane surface side of the antenna, as furnished, is open. On the short sides of the cavity are the receptacle for the connection of the lead-in and an 18-mm threaded hole. The hole may be closed by a plug, but it is intended to be used for antenna dehydration. This may be accomplished either by screwing into the hole an 18-mm spark-plug type dehydrator, or by connecting to a remote dehydrator.

The internal arrangement includes a shunt-fed bent-channel receiving element, top loaded by a small variable capacitor in parallel with a 25-$\mu\mu$f temperature-

A DESIGN CONCEPT*

—that revolutionized an industry!



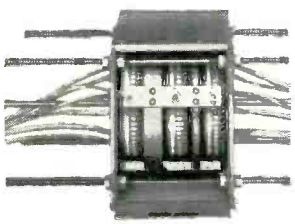
ELECTRO TEC

PRECISION MACHINED ONE-PIECE CONSTRUCTION

SLIP RING & COMMUTATOR ASSEMBLIES

Diameters of multi-ring assemblies from .035" to 36"

Individual components or complete assemblies to precise electrical, mechanical, and environmental specifications.



Uniformly hard rings, low noise, minimum friction and dimensional stability.

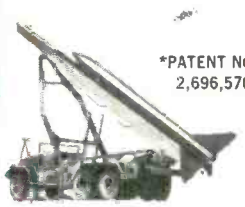
An Unmatched Record of Performance

Today, Electro Tec Slip Ring and Commutator Assemblies are the choice of leading aircraft, instrument, and component manufacturers throughout the world. Our units are selected for Gyro and Servo applications, for Telemetering and Radar devices, for Guidance systems, and Automation equipment... where sustained and reliable performance is a requisite.

Facilities Available to Serve You

Plants in South Hackensack, N. J., Blacksburg, Va., and Ormond Beach, Fla., are currently producing a wide variety of Slip Ring, Commutator, and Brush Block Assemblies, Precision Selector Switches, and Miniature Relays. Complete Engineering Facilities and Branch Sales Offices in Los Angeles, Minneapolis, Chicago, and Waltham, Mass. are geared to service your requirements.

Write for fully illustrated literature.



*PATENT No. 2,696,570

See us at the I.R.E. Show! BOOTHS 1216, 1218, 1220

ELECTRO TEC CORP.

SOUTH HACKENSACK, NEW JERSEY

PRODUCTS OF PRECISION CRAFTSMANSHIP

Research and development at Lockheed Missile Systems Division laboratories in Palo Alto is of a most advanced nature. Particular areas of interest include microwaves, telemetering, radar, guidance, reliability, data processing, electronic systems, instrumentation, servomechanisms. Inquiries are invited from those qualified by ability and experience for exploratory efforts of utmost importance.

Here members of the Electronics Division discuss systems radar problems related to measurement of missile trajectories. Left to right: K. T. Larkin, radar and command guidance; Dr. S. B. Batdorf, head of the Electronics Division; Dr. H. N. Leifer (standing), solid state, Dr. R. J. Burke, telemetering; S. Janken, product engineering.

Lockheed

MISSILE SYSTEMS DIVISION

research and engineering staff

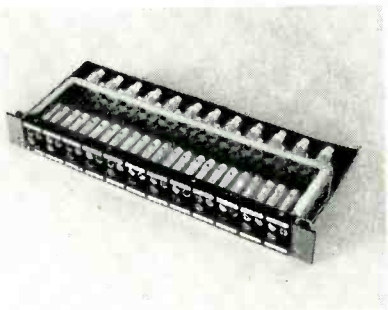
LOCKHEED AIRCRAFT CORPORATION

PALO ALTO • SUNNYVALE • VAN NUYS

CALIFORNIA

compensated fixed capacitor.

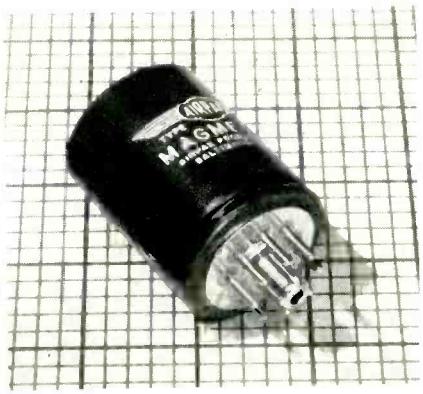
The model AT-134 measures 11¾ in. long by 7¾ in. wide by 3¼ in. high. **Circle P6 inside back cover.**



VIDEO JACK PANELS
for 70-ohm line use

NEMS-CLARKE INC., 919 Jesup-Blair Drive, Silver Spring, Md., has available video jack panels designed to provide coaxial patching facilities for tv installations or other applications where 70-ohm lines are used. These panels are available with jacks for both the RCA and the Western Electric size. Individual jacks, plugs, patchcords and looping plugs are also available.

Panels may also be obtained with 12 groups of either two, three or four jacks. A subchassis is included providing 24 Amphenol connectors and plugs to allow disconnection of long lines. The spring contacts in the jacks are of heat-treated beryllium copper to give long trouble-free life. **Circle P7 inside back cover.**



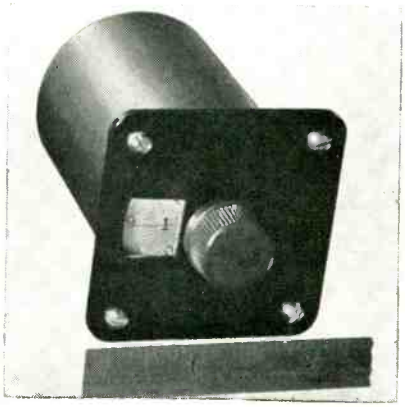
FREQUENCY DETECTOR
for automatic control

AIRPAX PRODUCTS CO., Middle River, Baltimore 20, Md. For tele-

metering, instrumentation and automatic control, type F-992 Magmeter provides an output current that is linearly proportional to frequency within the band from 375 to 425 cps. Similar detectors can be provided covering a 10-percent bandwidth at any center frequency from 30 cps to five kc. The output is suitable for operating a d'Arsonval indicating instrument, a servo-type recorder, or a control circuit.

Linearity is within ¼ percent of midband frequency. Output is zero at the low-frequency end of band providing fail-safe indication in absence of input. The Magmeter detector is hermetically sealed, operates from −55 C to +72 C; withstands 10-g vibration to 2,000 cps and shocks of 30 g in all directions.

The standard type fits an octal socket, is 1½ in. in diameter, two in. seated height and weighs six oz. **Circle P8 inside back cover**



VOLTAGE DIVIDER

one knob controls two decades

RESEARCH INSTRUMENT CO., P. O. Box 9168, Portland 16, Oregon. Single-knob control of two decades is one of several features of this vernier potentiometer-rheostat design. The unit is a four-terminal voltage divider and may be used as a potentiometer or rheostat. Only two turns of the control knob covers the full range of the device and resolution is equal to a 10-turn pot. The complete unit mounts like a panel meter and uses only 2 by 2 in. of panel space with 2½ in. projecting behind the panel.

Resistance is 10,000 ohms when

. . . for crowded panels and dashboards . . SPACE-SAVER CONTROLS

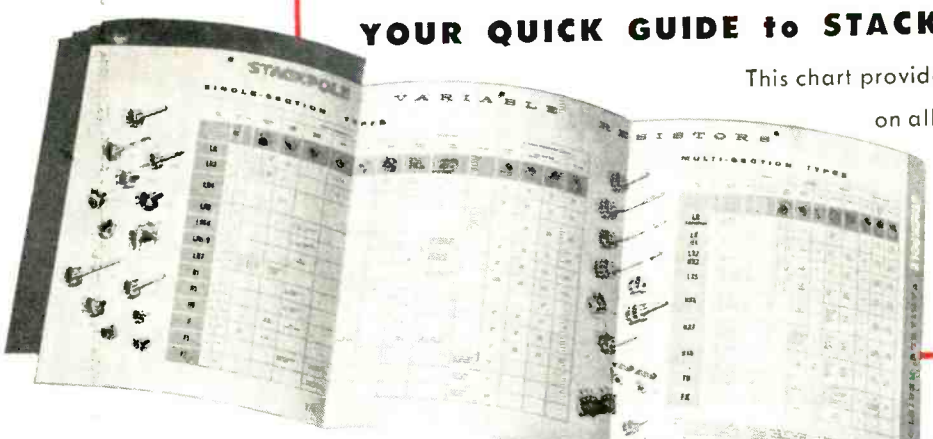
ONLY 0.637" in diameter, Stackpole "F" controls combine quiet, dependable operation with the smaller physical size needed for automotive radios and similar equipment now undergoing miniaturization.

"F" Controls are conservatively rated at 0.3-watt for values up to 10K ohms, and at 0.2-watt for higher values. Each can be equipped with new Stackpole "B"-Series line switches for practically any switching arrangement. Standard mounting types suffice in most cases—but where they don't, suitable adaptations can be produced economically for quantity users.

TYPES for TRANSISTORIZED SETS, too!

Similar to standard Stackpole miniature "F" Controls, but designed for low hop-off on the order of 2.0 ohm maximum, as compared to the higher values of conventional types. And they're electrically quiet!●

ENGINEERING SAMPLES *available to quantity users . . .*
Ask the Stackpole field engineer in your locality



YOUR QUICK GUIDE to STACKPOLE CONTROLS

This chart provides essential engineering data on all standard Stackpole Variable Resistors in handiest possible form. Designed for either wall or file use. Write today for your copy.

STACKPOLE

Electronic Components Division

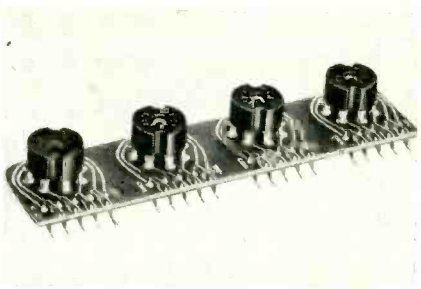
STACKPOLE CARBON COMPANY • St. Marys, Pa.

In Canada: Canadian Stackpole Limited, 550 Evans Ave., Etobicoke, Toronto 14, Ontario

Want more information? Use post card on last page.

used as a pot and 0 to 10,000 ohms when used as a rheostat. Accuracy is 0.1 percent of full scale; linearity, ±0.1 percent; resolution, 0.1 percent or better; wattage, four w when used as a pot; current rating, 25 ma when the unit is used as a rheostat.

Other resistance ranges are available using either wire wound resistors such as used in the described unit or carbon or carbon-film resistors depending on the range and accuracy desired. **Circle P9 inside back cover.**



SOCKET MOUNTING
used with printed circuits

CLEVELAND METAL SPECIALTIES CO., 1783 E. 21st St., Cleveland 14, Ohio, has designed a multiple right-angle socket mounting for use in conjunction with printed circuits. The multiple mounting can be used for two, three, four or more sockets, and can be applied for the mounting of other electronic components such as resistors and capacitors that have not previously been incorporated into the circuit.

The new mounting can incorporate either sockets of the same size or sockets of varying sizes and can be constructed to meet the combinations and specifications required. **Circle P10 inside back cover.**

RESISTOR NETWORKS
for strain gage amplifiers

EASTERN PRECISION RESISTOR CORP., 675 Barbey St., Brooklyn, N. Y., announces new precision wire-wound resistor networks especially designed to fit the front panel of strain gage amplifiers. The company can supply any number of precision resistors in one encapsulated package. Wound on

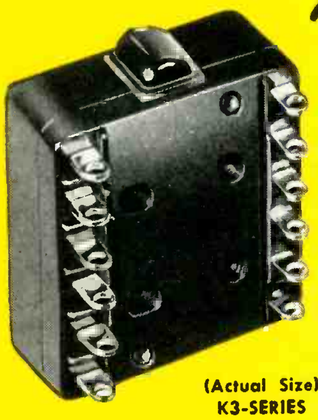
New ELECTRO SNAP SIMULTANEOUS

TRIPLE-POLE SWITCH

for interrupting 3-phase,
110 V, 400 cycle AC circuits

6-CIRCUIT CONTROL — in a small package.
Makes possible a wide variety of circuit combinations.

SIMULTANEOUS "MAKE & BREAK" ACTION
Permits unusual applications, reduces arcing, prolongs switch life and increases electrical capacity.



(Actual Size)
K3-SERIES

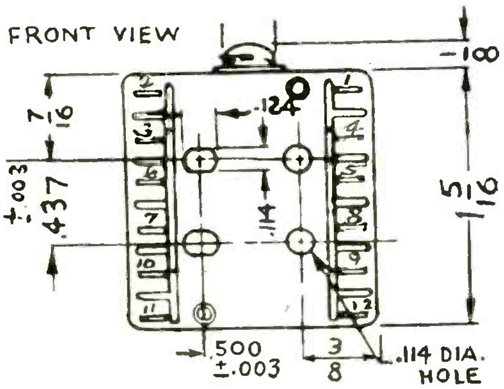
TRIPLE-POLE SWITCH

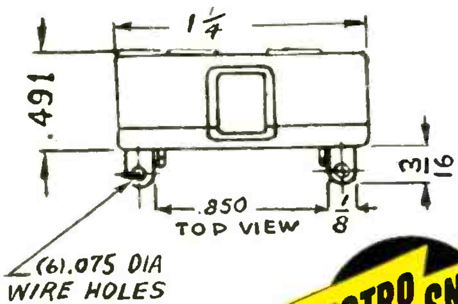
OPERATING CHARACTERISTICS

CONTACT ARRANGEMENTS:
K3-4—TRIPLE-POLE, DOUBLE THROW
K3-2—TRIPLE-POLE, NORMALLY OPEN
K3-1—TRIPLE-POLE, NORMALLY CLOSED

ELECTRICAL RATING:
15 AMP 125/250 V.A.C.
15 AMP 30 V.D.C. RESISTIVE
10 AMP 30 V.D.C. INDUCTIVE

PROBABLE MECH. LIFE.............1,000,000 OPS
PROBABLE ELEC. LIFE.............500,000 OPS
AMBIENT TEMP. RANGE.....—100° TO +275° F.*
*(—100° to +375°F. available)



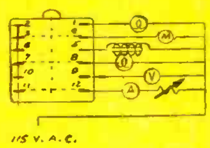


This completely new Electro-Snap triple-pole switch simultaneously reverses current flow through three windings of a 3-phase motor up to 1 H.P. and interrupts other types of multi-switching installations. Instantaneous snap-action of the three poles is independent of the speed of actuation — even extremely slow moving cams can be used.

The K3-Series offers designers a wide variety of 3-phase circuit hookups for servo-controls, to limit movement of machine members and as a start-and-stop switch which formerly were possible only with complicated relays or a number of separate switches. A large selection of standard actuators is available.

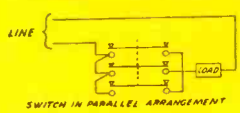
LOOK WHAT YOU CAN DO WITH IT!

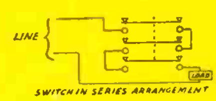
Control Six Circuits with ONE Snap



Used in motor control device switch, when actuated, turns on the red light on No. 1, the solenoid on No. 5, the voltmeter on No. 9 and turns off the motor on No. 4, the green light on No. 8 and the furnace and ammeter on No. 12.

Wire Movable Poles in Series for High Voltage or in Parallel for High Current

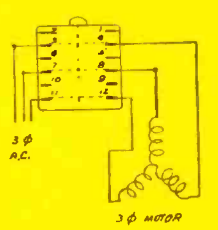




With the switch wired in parallel arrangement, the current is divided into 3 paths through the switch. This permits the switch to be used with a load rated up to 3 times the ampere rating of the switch.

With the switch wired in series arrangement, the current has only 1 path through the switch. The multiple breaks in the current path permits the switch to be used where the line voltage is rated up to 3 times the voltage rating of the switch; ampere rating not affected.

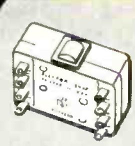
Start and Stop Three-Phase Motors
Completely disconnect all current supplied to a 3-phase motor by interrupting 3 phases simultaneously with one snap.



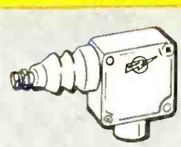
ELECTRO-SNAP
SWITCH AND MFG. CO.
4236 West Lake Street • Chicago 24, Illinois

MODERN DESIGN IN A COMPLETE LINE OF SWITCHES

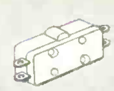
Sub-Miniature Switch



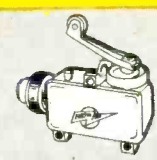
Multi-Pole Switches



One-Way Limit Switch

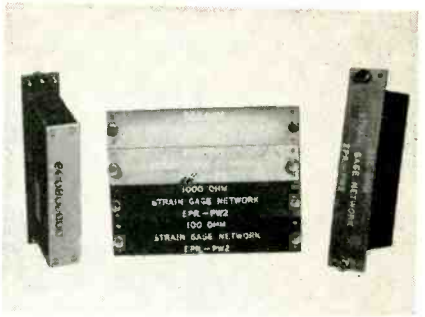


Basic Switch



Hermetically-Sealed Limit Switches

Want more information? Use post card on last page.



glass reinforced plastic forms with glass insulated wire, each resistor is capable of dissipating 10-w overload for short periods of time.

Anodized-aluminum front panels are available in 13 different colors to facilitate ease in selection of the proper resistor block. A variety of configuration and schematics are possible. **Circle P11 inside back cover.**

BETA TESTER

portable, transistorized

BAIRD-ATOMIC, INC., 33 University Road, Cambridge 38, Mass., has announced a new portable transistorized instrument for measurement of transistor parameters in quality control testing, circuit design, incoming inspection and general trouble shooting. Model KT-1 was designed specifically for measurement of Beta, h_{11} and I_{co}. It is completely self-contained with its own one-kc oscillator and mercury-cell power supply. Battery life of the mercury cell is about 1,000 hr. Printed circuitry has been used throughout, increasing the portability and ease

It's New...!

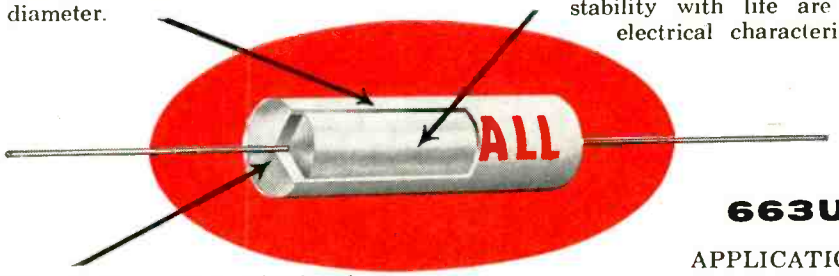
GOOD-ALL capacitors

A Space Saving capacitor WITH "SKIN-TIGHT" Case

Miniature Size • Tolerances to ±1%

This thin, tough Mylar* case provides excellent moisture and abrasion resistance — yet adds less than 1/64" to the body diameter.

Miniature size is gained through the use of space-saving mylar dielectric. High insulation resistance and real stability with life are key electrical characteristics.



663UW

A dense thermo-setting plastic that bonds securely to the lead and case. The completed assembly is rugged and durable.

APPLICATIONS:

- Instrumentation • Filter Networks
- Transistor Circuitry • Amplifiers
- Test Equipment • Computers

*DuPont's trademark for polyester film.

SPECIFICATIONS

INSULATION RESISTANCE: See curve reproduced below for typical performance

LEAD PULL TEST: Steady force of 10 lbs. applied axially for 60 seconds.

LIFE TEST: 250 hours at 85°C and 125% of rated voltage

DIELECTRIC STRENGTH: 2 times rated voltage

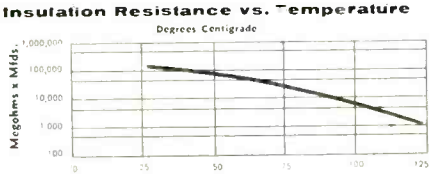
HUMIDITY RESISTANCE: Far exceeds requirements of RETMA Spec. REC-118-A

TEMPERATURE RANGE: Operation at rated voltage from −60°C to +85°C and to +125°C with 50% derating.

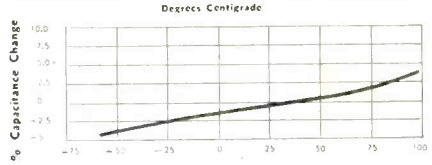
TYPICAL SIZES

Capacity	100 Volts	200 Volts	400 Volts
.001	.156 x ½	.156 x ½	.156 x ⅝
.0047	.156 x ½	.156 x ½	.186 x ⅝
.01	.156 x ½	.171 x ⅝	.250 x ⅝
.047	.234 x ¾	.296 x ¾	.343 x ⅞
.1	.281 x ⅞	.375 x ⅞	.421 x 1
.47	.468 x 1¼	.546 x 1¼	.671 x 1⅝

Insulation Resistance vs. Temperature



Capacitance Change vs. Temperature



Our engineers are ready to work with you on special applications. Write or wire for specifications and quotations.

GOOD-ALL ELECTRIC MFG. CO. • OGALLALA, NEBRASKA

A leading manufacturer of Tubular and Ceramic Disc Capacitors

of maintenance of the unit.

The tester enables adjustment in direct-reading calibrations to compensate for temperature variations. An external jack permits collector waveform observation. Positive meter overload protection is built into the instrument.

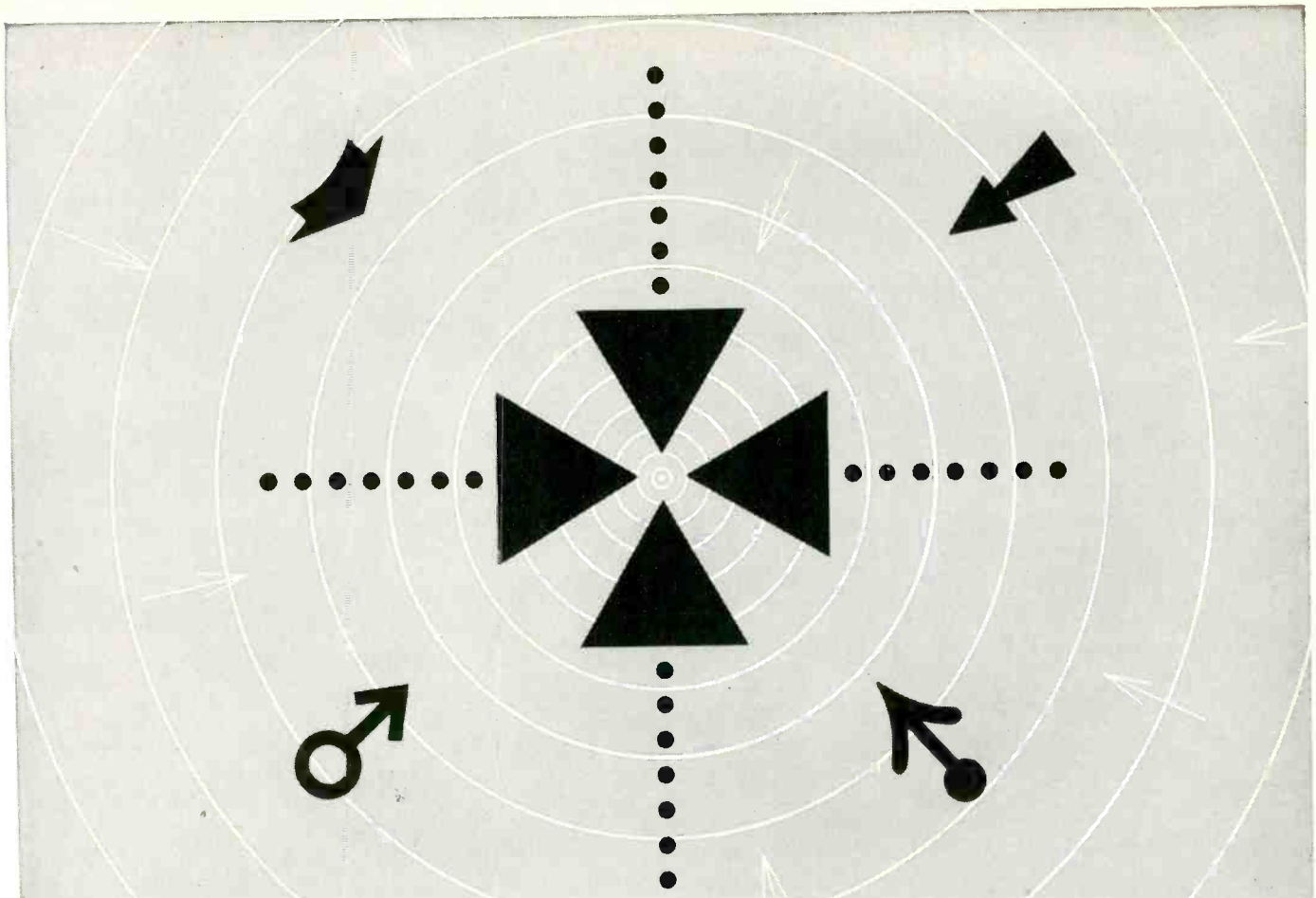
The unit measures 5$\frac{11}{16}$ in. wide, 5$\frac{1}{2}$ in. deep and 10 in. high. Weight is three lb. Further information is available from the company. **Circle P12 inside back cover.**

TRANSISTOR RELAY
actuated by 12-μa input

FISHER SCIENTIFIC CO., 717 Forbes St., Pittsburgh, Pa. Model 30 transistor relay is to be used wherever one requires a sensitive apparatus to control bath or oven temperatures, maintain liquid levels, with a monitoring photocell, or for the many chores where only a small amount of power is available to control a relatively large load in laboratory, pilot plant or industrial control. The relay will complete at least a million contacts with any resistive load up to four amperes under these conditions.

The model 30 uses three germanium junction transistors. It controls a load of as much as 1,100 w with a signal as small as five millionths of a watt—actually a power gain of 220 million times.

▶ **Features**—As little as 12-μa input actuates it. No warmup is necessary and it can't overheat. It can be used with any combination of normally closed or normally open input circuits and normally off or normally on outputs. It will handle resistive loads of up to 10 amperes for short periods. It is compact, rugged,



± 1% TOLERANCE

±1% tolerance capacitors are available from Efcon in production lots. Miniature capacitors of even greater precision will be made to your order, with either polystyrene or Mylar* film dielectric.

Efcon precision miniature capacitors have the lowest dissipation factors of any film capacitors. Both polystyrene and Mylar* film capacitors come in rigid, wax-impregnated cardboard tubes and in hermetically sealed metal cases. The hermetically sealed types feature glass-to-metal, solder-sealed terminals, and meet all applicable MIL specs.

All Efcon capacitors have extended foil construction with leads soldered directly to the foil, to minimize inductance and contact-resistance.

For analog and digital computers, communications filters, pulse-timing circuits and other equipment that demands temperature stability, precision and long-term reliability —specify Efcon capacitors!

EFCON

WHERE CLOSE TOLERANCE IS STANDARD TOLERANCE

ELECTRONIC FABRICATORS, INCORPORATED 682 BROADWAY, NEW YORK 12, N.Y.

WRITE DEPT. E2 FOR TECHNICAL DATA

*DuPont trademark for polytetrafluoroethylene

safe and convenient. **Circle P13 inside back cover.**

POWER SUPPLIES

for high-power klystrons

LEVINTHAL ELECTRONIC PRODUCTS, INC., 2760 Fair Oaks Ave., Redwood City, Calif. Model PC33 power supply provides continuously variable voltage from 0 to 30 kv at currents from 0 to two amperes d-c. Voltage ripple is less than 0.04 percent. Included are facilities to monitor output voltage and current; and for klystron operation, collector current and body current.

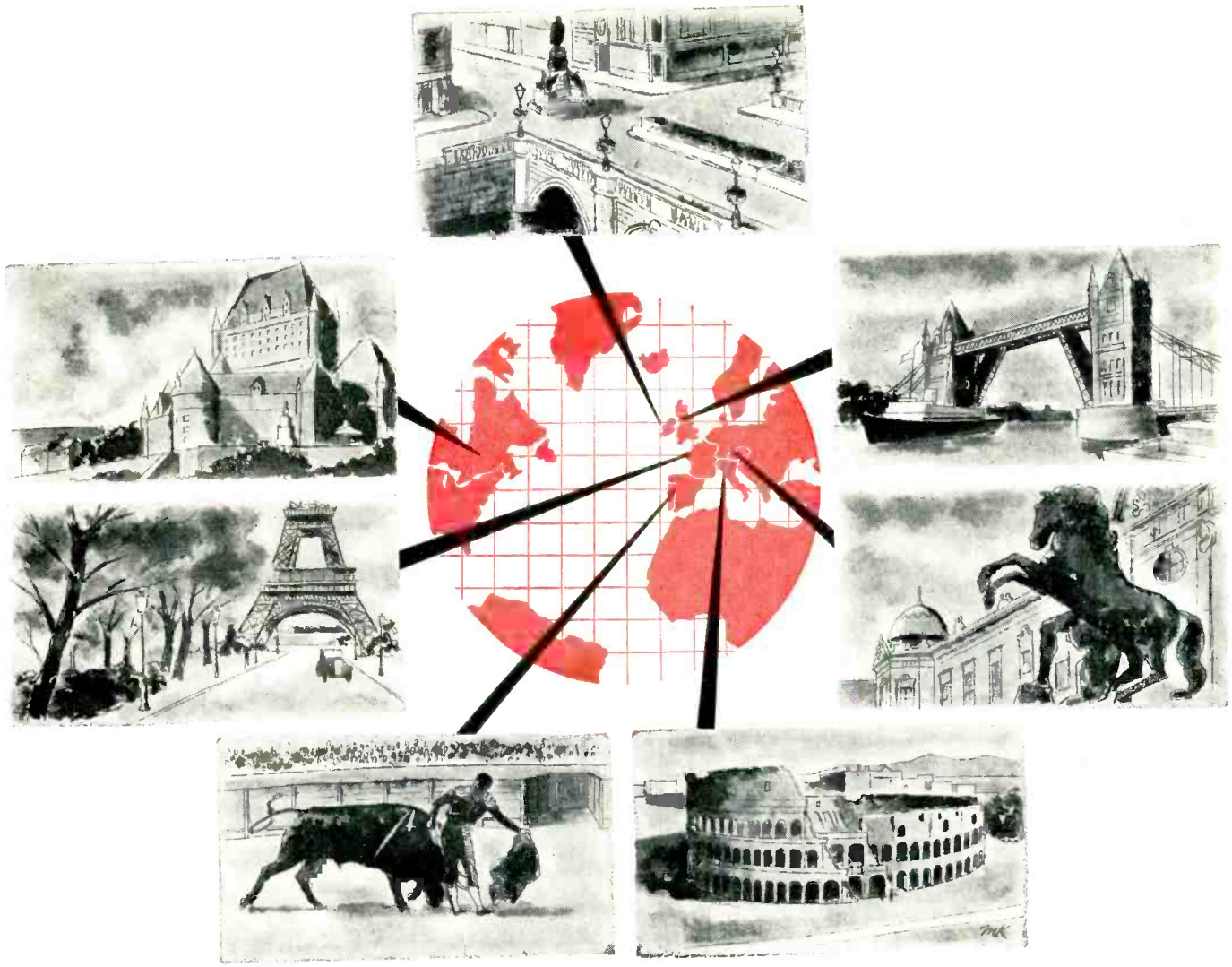
The unit is completely interlocked and overvoltage and overcurrent protection are provided. The supply can be connected to the external interlock system of associated equipment. Power input is 208 v, three phase, 60 cps.

A similar unit, the model PC44, is used for bombarded-cathode applications and provides voltages from 0 to 3 kv at currents up to six amperes with motor-driven Powerstat control. The unit utilizes air-cooled selenium rectifier stacks. Power input is 230 v, three phase, 60 cps. Internal and external interlocks are provided. **Circle P14 inside back cover.**

RECORDER

two-pen, two-zone instrument

WESTON ELECTRICAL INSTRUMENT CORP., Newark 12, N. J. A new two-pen-two-zone recording instrument, ideal for comparative measurement in both the laboratory and



Here, too, we make Nichrome*

Perhaps you didn't know that the world-famous alloy Nichrome is produced not only in The United States, but also in 6 Driver-Harris plants in England, Ireland, France, Italy, Austria, Spain, and in Canada by The B. Greening Wire Company. Also, Nichrome is a registered trade-mark in 55 nations.

At first, fifty-odd years ago, we manufactured electrical resistance alloys for furnace elements and domestic heating appliances only. Today we produce 132 different high nickel alloys in many different forms and in hundreds of sizes, for almost every kind of domestic and industrial application—of which Nichrome is the most illustrious.

Whenever you buy Nichrome, you are assured of the unsurpassed and unvarying *quality* which has made Nichrome the supreme world standard for electrical-resistance and heat-resistant alloys. This uniformly high quality, which we jealously guard as our most priceless possession, results from the technical excellence, the productive skill, and the quality controls the Driver-Harris craftsmen have gained in over 50 years of experience—and which are maintained with equal rigor in all Driver-Harris plants here and abroad. The result is a continuous benefit to the entire electrical, electronic, and heat-treating industries.

*T.M. Reg. U. S. Pat. Off.

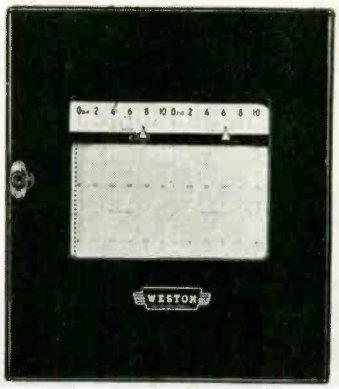
Nichrome is made only by

Driver-Harris COMPANY

HARRISON, NEW JERSEY

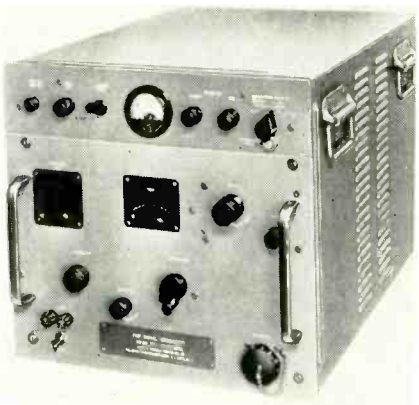
Manufacturing plants also in: ENGLAND • CANADA • IRELAND • FRANCE • ITALY • AUSTRIA • SPAIN

MAKERS OF THE MOST COMPLETE LINE OF ALLOYS FOR THE ELECTRICAL, ELECTRONIC, AND HEAT-TREATING INDUSTRIES



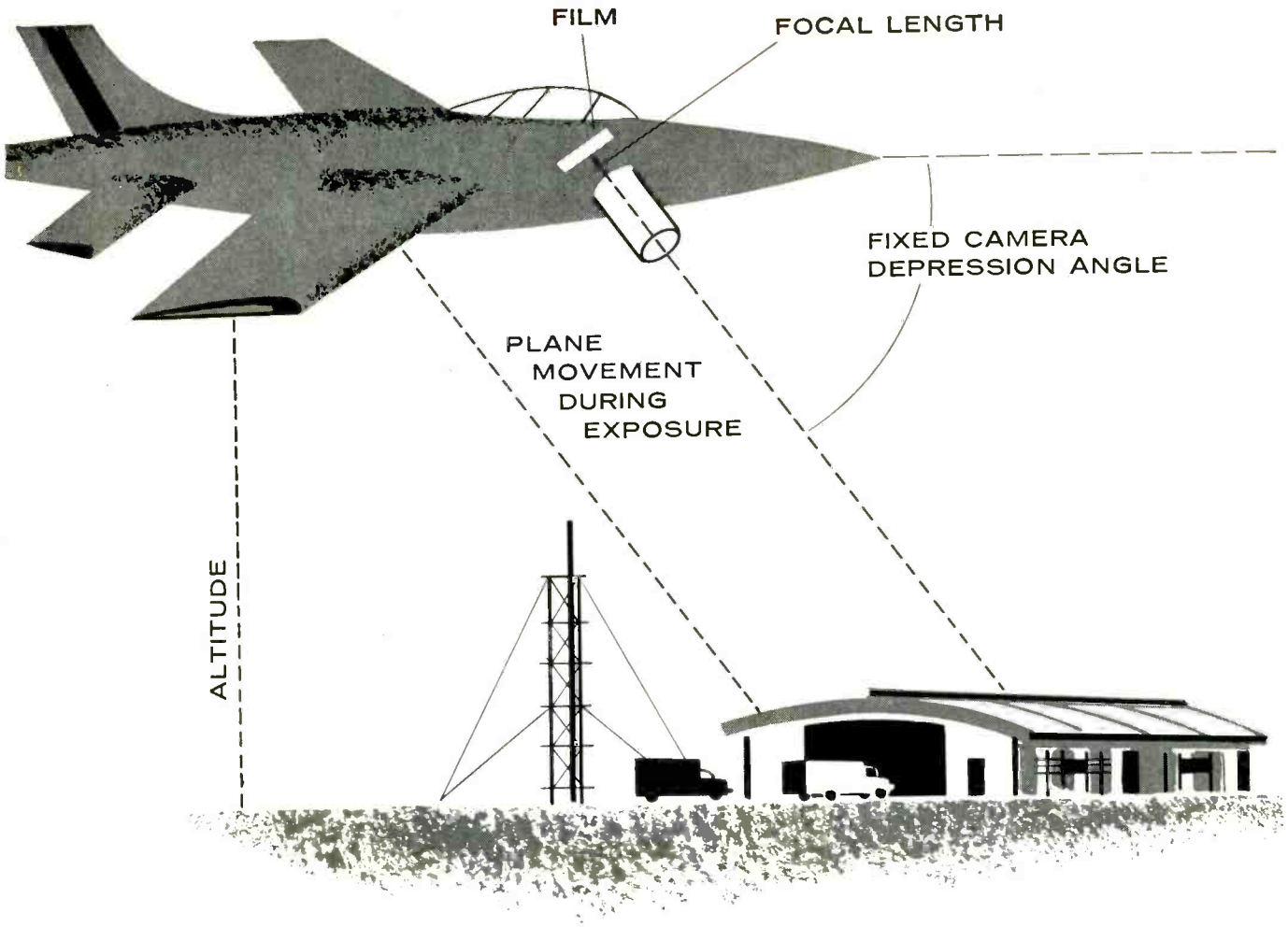
on the production line, is now included in the model 6700 line of recording-controlling instruments. While the model 6791 type 1 recorder is actually two independent instruments in one, it is housed in a case measuring only 17¾ in. wide to fit standard relay racks and is of simplified, unitized construction.

It employs two electronic amplifiers of special plug-in type for easy servicing. Two separate measuring circuits with replaceable range standards permit quick range change on either one or both zones as desired. Alarm switches are available for each zone and can be set in a matter of seconds. Slide wires are interchangeable and totally enclosed for complete protection. Chart speeds are available from one in. per hour to one in. per minute. **Circle P15 inside back cover.**



MICROWAVE GENERATORS cover 18,000 to 50,000 mc

POLARAD ELECTRONICS CORP., 43-20 34th St., Long Island City 1, N. Y., has announced a new line of microwave generators and sources, covering 18,000 to 50,000 mc, util-



How Transicoil servos help aerial camera take clear stills even from low fast planes

It's one thing to take a picture of a moving object. But it's quite another to get good clear shots of the ground from low altitude aircraft moving at today's jet speeds. Universal Camera Control System (UCCS) is the latest development in aerial reconnaissance and photography to solve this problem. Designed and engineered by the Bill Jack Scientific Instrument Co., this novel system actually moves the film through the camera to compensate for image movement during the brief exposure time.

Accuracy of the system is dependent on the airborne DC analog computer having absolute dependability and precision under all the environmental conditions of aircraft flight. Extremes of altitude, temperature and vibration cannot impair its effectiveness.

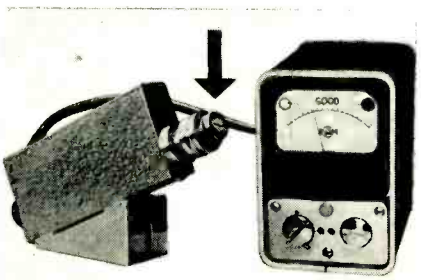
Transicoil servo assemblies are used extensively in the computer to convert inputs of altitude, ground speed, camera depression angle, and focal length into the correct "film movement" signal.

The UCCS application is typical of the way Transicoil rotating components and complete servo assemblies are achieving high orders of accuracy and dependability in countless applications. Transicoil can solve your servo problems with comparable success. A Transicoil Sales Engineer can help you to get off to a good start. A letter from you outlining your servo problem will bring him to your desk.

TRANSICOIL CORPORATION

Worcester • Montgomery County • Pennsylvania

izing interchangeable tuning units. Each of the tuning units requires no further adjustment to the basic unit after plug-in. The self-contained instruments provide c-w or modulated signals of known frequency for field, production line and laboratory testing of microwave equipment, components and systems. **Circle P16 inside back cover.**



ELECTRONIC GAGE
a high-speed inspector

INDUSTRIAL GAGES CORP., West Englewood, N. J. A new high-speed electronic inspector is shown here checking the i-d of race ring. It is the LM-1 Minitron, available with a series of attachments for high speed checking of internal or external measurements of all sizes and types. The simple plug-in console can be set up for any three selections of magnification from 0.000010 per div up to 0.0001 per div. The new principle of electronics utilized guarantees positive stability of readings without regard to temperature effects and permits lower investment cost and longer life than other types supplied for similar purposes. **Circle P17 inside back cover.**

WIRE-WOUND RESISTOR
encapsulated, card-type

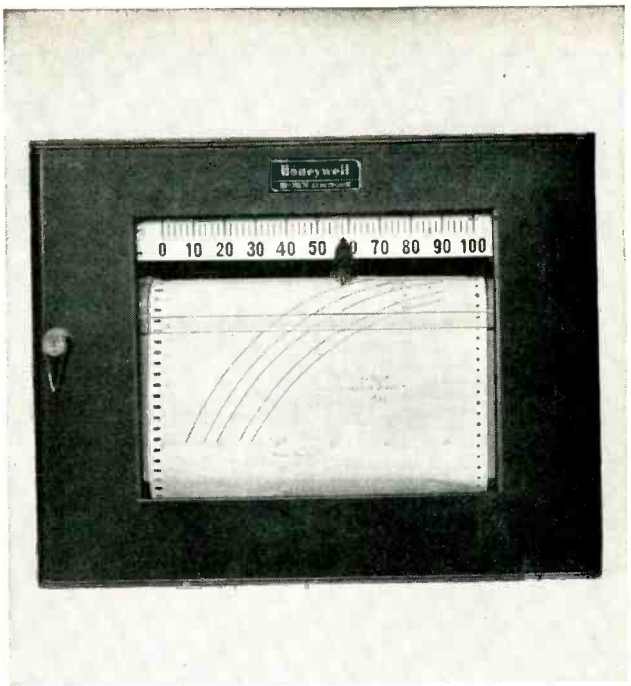
THE DAVEN CO., 530 W. Mt. Pleasant Ave., Livingston, N. J., has available a new card-type wire-wound resistor, type 1300A. The encapsulated, wafer-thin resistor is specifically designed for applications where limited space prohibits the use of the usual cylindrical bobbin types, precision wire-wound resistors. It is espe-

Measure and plot changes in variables as they occur...

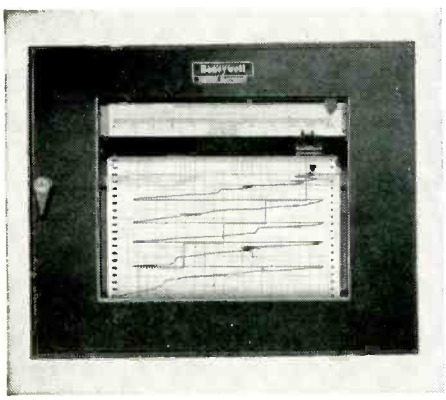
with

ElectroniK instruments for research

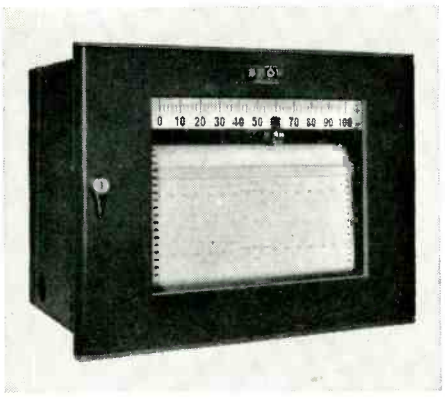
Here's an exceptional group of instruments to measure and record your research findings swiftly, surely, conveniently. These *ElectroniK* instruments for research can speed completion of your projects, by eliminating many of the tedious, time-consuming details of test work.



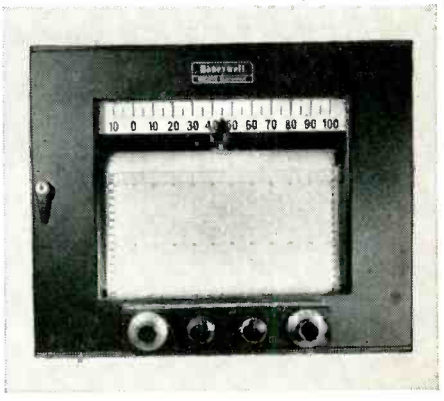
ElectroniK **FUNCTION PLOTTER** Automatically and continuously plots a curve which shows the relationship of one variable to another. Typical uses: speed versus torque, stress versus strain, temperature versus pressure, plate voltage versus plate current (and other electron tube characteristics), and many other variable relationships. *Write for Instrumentation Data Sheet 10.0-5b.*



ElectroniK **EXTENDED RANGE RECORDER** Facilitates measurement of any linear variable whose values change over a wide range, and where precise evaluation and good resolution are important. This instrument is particularly suited to the measurement of forces in conjunction with a strain gage bridge. *Write for Instrumentation Data Sheet 10.0-18.*



ElectroniK **NARROW SPAN RECORDERS** Accurately measure d-c potentials as low as 0.1 microvolt and spans as narrow as 100 microvolts. Available as a precision indicator, circular chart recorder, and strip chart recorder. Useful (with appropriate primary measuring elements) for measuring differential temperatures and slight variations in the temperatures of small objects through the use of radiation pyrometry. *Write for Instrumentation Data Sheet 10.0-8.*



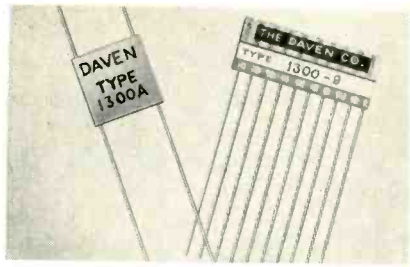
ElectroniK **ADJUSTABLE SPAN RECORDER** Measures spans and magnitudes of a variety of emf's. Instrument calibration can be in terms of any variable reducible to d-c voltage. Can be used with thermocouples, steam gages, tachometers, and other transducers. *Write for Instrumentation Data Sheet 10.0-10a.*

Your nearby Honeywell sales engineer can give you complete information about these instruments as they relate to your particular applications. Call him today . . . he's as near as your phone. MINNEAPOLIS-HONEYWELL REGULATOR CO., *Industrial Division*, Wayne and Windrim Avenues, Philadelphia 44, Pa. —in Canada, Toronto 17, Ontario.

MINNEAPOLIS **Honeywell**

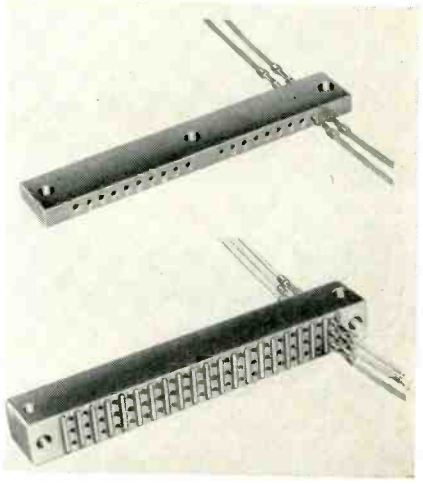
BROWN INSTRUMENTS

First in Controls



cially adaptable for circuits using transistors, in guided missiles and airborne communication and navigation equipment. Originally designed for Tinker-Toy type modules, they are also available as multisection card-type resistors. They will meet the environmental requirements of MIL-R-93A, Amendment 3.

Dimensions are $\frac{5}{8}$ in. by $\frac{5}{8}$ in. by 3/32 in. (thick). Maximum resistance is 500,000 ohms. It dissipates 0.6 w. Standard tolerance is ± 1 percent. However, resistors of this type with accuracies of ± 0.1 percent may be obtained. **Circle P18 inside back cover.**



TERMINAL BLOCKS
for solderless wiring uses

DEJUR-AMSCO CORP., 45-01 Northern Blvd., Long Island City 1, N.Y. Series 145-58 taper pin terminal blocks, designed for solderless wiring applications, are fabricated in a single row of 20 contacts, in 10 dual contacts and in 10 single contacts. These may be ordered in any pair or combination of shorted contacts. Molded or eyelet holes are provided for ease of stacking and assembly.

Series 145-48 taper pin terminal blocks are fabricated in 20 rows

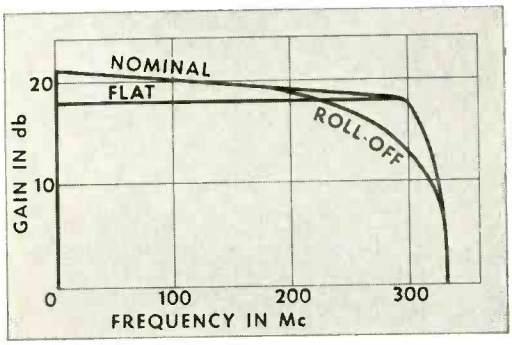
SKL *introduces*

NEW ULTRA WIDE-BAND AMPLIFIER

for fast rise pulse reproduction

320 Mc

MODEL 206



Here is another advance in the art . . . Spencer-Kennedy's new Ultra Wide Band Amplifier, Model 206. Now for the first time fast-rise-time pulses can be faithfully reproduced by providing a stable 20 db gain over a *320 Mc band!* . . . Although nominal gain for Model 206 is 20 db, sloping to 18 db at 300 Mc and 14 db at 320 Mc, flat and gradual roll-off characteristics are readily available by means of small, inexpensive plug-in accessories (see curves above). Three output modes . . . linear, pulse and high pulse . . . are selectable by means of a front panel switch. Integral regulated power supply and rack mounting are also provided. Applications include amplification of the following: short fast-rise-time pulses from pulse generators, input to wide-band vacuum tube voltmeters, output of scintillation detectors, multi-channel VHF signals, wide-band IF signals, narrow band IF signals with wide range for choice of center frequency. Model 206 also serves ideally as a distribution amplifier for wide band receiving systems feeding multiple diverse channel receivers.

SPECIFICATIONS

Bandwidth:
300 Mc at 3 db point

Gain:
18 to 20 db depending on plug-in accessory

Rise Time:
Less than .002 μ seconds

Output:
Panel switch selects
(a) Linear: 5 volts, rms
(b) Pulse: 30 volts, negative
(c) High Pulse: Greater than 100 volts, negative, open circuit

Gain Regulation:
$\pm$0.5 db for line voltage between 105 and 125 volts

Gain Control:
Panel control varies gain 6 db

Phase:
Linear to 300 Mc

Impedance:
180 ohms input, 200 ohms output

Size:
19" wide, 8 3/8" deep, 7" high

Power Requirements:
115 volts, 60 cycles

Write for Bulletin 206

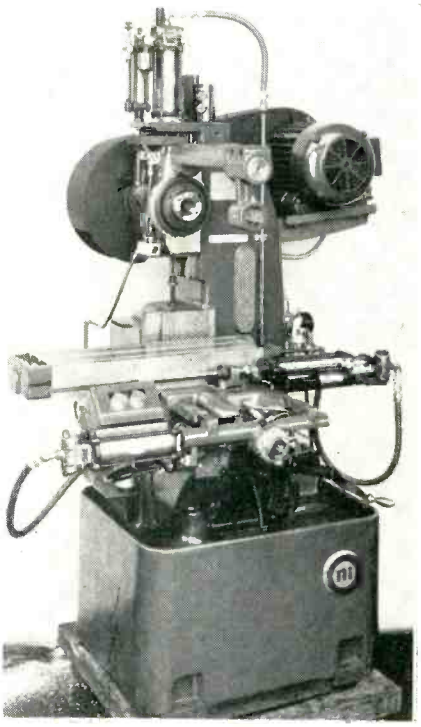
IRE Show — Booths 3502 and 3504

SKL **SPENCER - KENNEDY LABORATORIES, INC.**
1320 SOLDIERS FIELD ROAD
BOSTON 35, MASS.

Want more information? Use post card on last page.

of triple-stacked contacts arranged in any desired shorting combination. This series is supplied with perpendicular and right angle holes for mounting.

Taper receptacles are gold-plated brass over silver for low contact resistance. Bodies are molded of high-impact reinforced glass-filled Alkyd, type 440A. (Other molding materials on request). **Circle P19 inside back cover.**

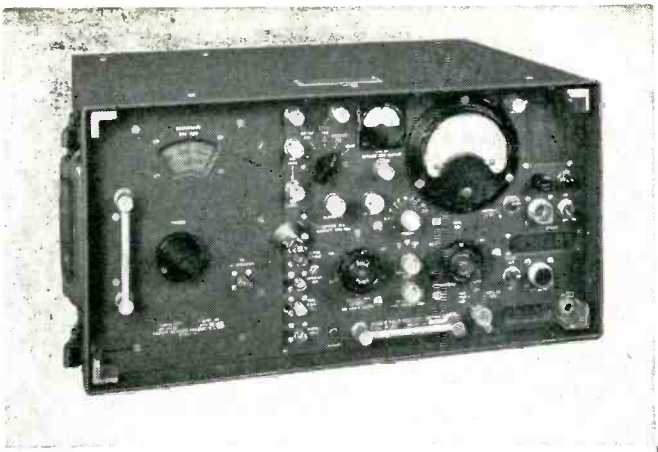


MILLING MACHINES
slice germanium ingots

THE ROBERT E. MORRIS CO., West Hartford 7, Conn. Illustrated is a high-speed automatic milling machine suitable for slicing and dicing germanium ingots for the transistor manufacturing industry. These millers are of the rise and fall spindle type with speeds up to 10,000 rpm available.

Automatic mist lubrication system is provided for spindle bearings and antifriction overarm type arbor support. Diamond impregnated sawing disks up to eight-in. diameter can be accommodated. Automatic transverse feed of six in., adjustable in increments from 0.001 in. to 0.085 in., is synchronized with automatic pneumatic feeds of spindle head and table

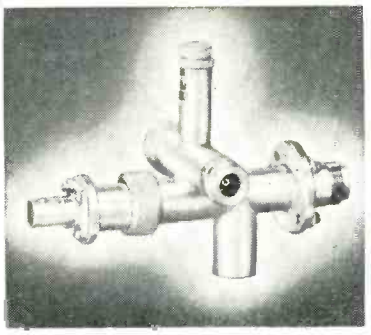
Empire's Reputation is built on Quality



NOISE AND FIELD INTENSITY METER, Model NF-105

(Commercial equivalent of AN/URM-7) **150 KC to 1000 MC**

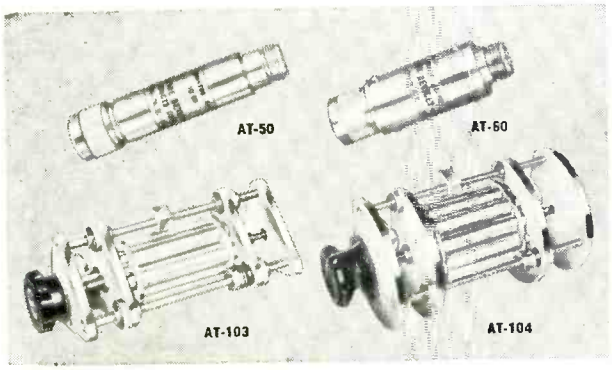
Four quick-change tuning heads • Single knob tuning for easy scanning Built-in impulse generator serves as calibrator • Carrier and peak reading VTVM • Aural slideback • Coaxial step attenuators • Regulated "A" and "B" supply.



COAXIAL CRYSTAL MIXER, Model CM-107

Broad Band, Fixed Tuned • 225 MC to 5600 MC in 8 models • Input and L.O. VSWR better than 2 to 1 • L.O. rejection at IF output better than 30 DB.

CRYSTAL DETECTOR, Model DT-123



UHF ATTENUATORS, Models AT-50, AT-60

50 ohm resistive T-networks of concentric line construction.

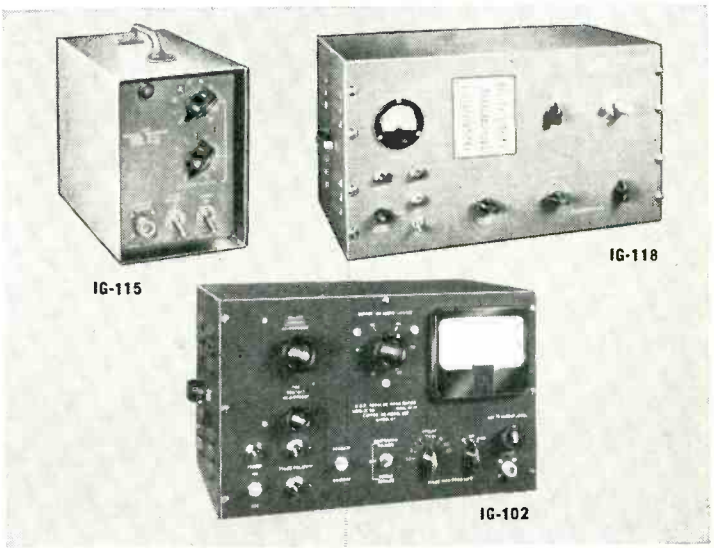
FREQUENCY RANGE:
AT-50: DC to 4000 MC.
AT-60: DC to 3000 MC.
VSWR: Better than 1.2 at all frequencies.
ACCURACY: ±½ DB.
RATED POWER:
AT-50: 1W continuous
1KW peak
AT-60: 2W continuous
2KW peak

STEP ATTENUATORS, Models AT-103, AT-104

These units use AT-50 pads in 6 step and 12 step coaxial turret arrangements respectively.

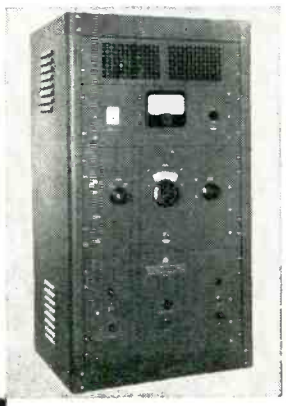
COAXIAL TERMINATION, Model TE-80

1 watt, DC to 4000 MC.



UHF IMPULSE GENERATORS, Models IG-102, IG-115, IG-118

Model	Flat Spectrum (±½ DB)	Peak Output Level	Repetition Rate
IG-102	10 KC to 1000 MC	70,000 μV/MC	2.5 to 2500 cycles
IG-115	10 KC to 1000 MC	100,000 μV/MC	60 cycles
IG-118	100 MC to 10,000 MC	9,000 μV/MC	2.5 to 2500 cycles



VARIABLE FREQUENCY POWER SUPPLY, Model VP-400

POWER OUTPUT: 500 watts
VOLTAGE REGULATION:
2%, no load to full load
HARMONIC DISTORTION:
5% maximum, total, (to 400W).

POWER DIVIDERS, Model PD-90

FREQUENCY RANGE: 800 to 10,000 MC in 5 models,

For complete engineering data, please send for our new Catalog No. 357

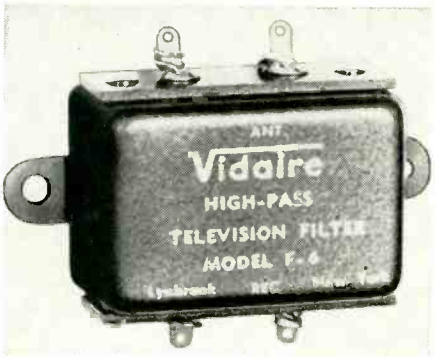
EMPIRE DEVICES PRODUCTS CORPORATION

38-15 BELL BOULEVARD, BAYSIDE 61, NEW YORK

Manufacturers of FIELD INTENSITY METERS • DISTORTION ANALYZERS • IMPULSE GENERATORS COAXIAL ATTENUATORS • CRYSTAL MIXERS

Visit our booths 3818 - 20, Third Floor, at the IRE Show.

for high-speed continuous slicing cycles. **Circle P20 inside back cover.**

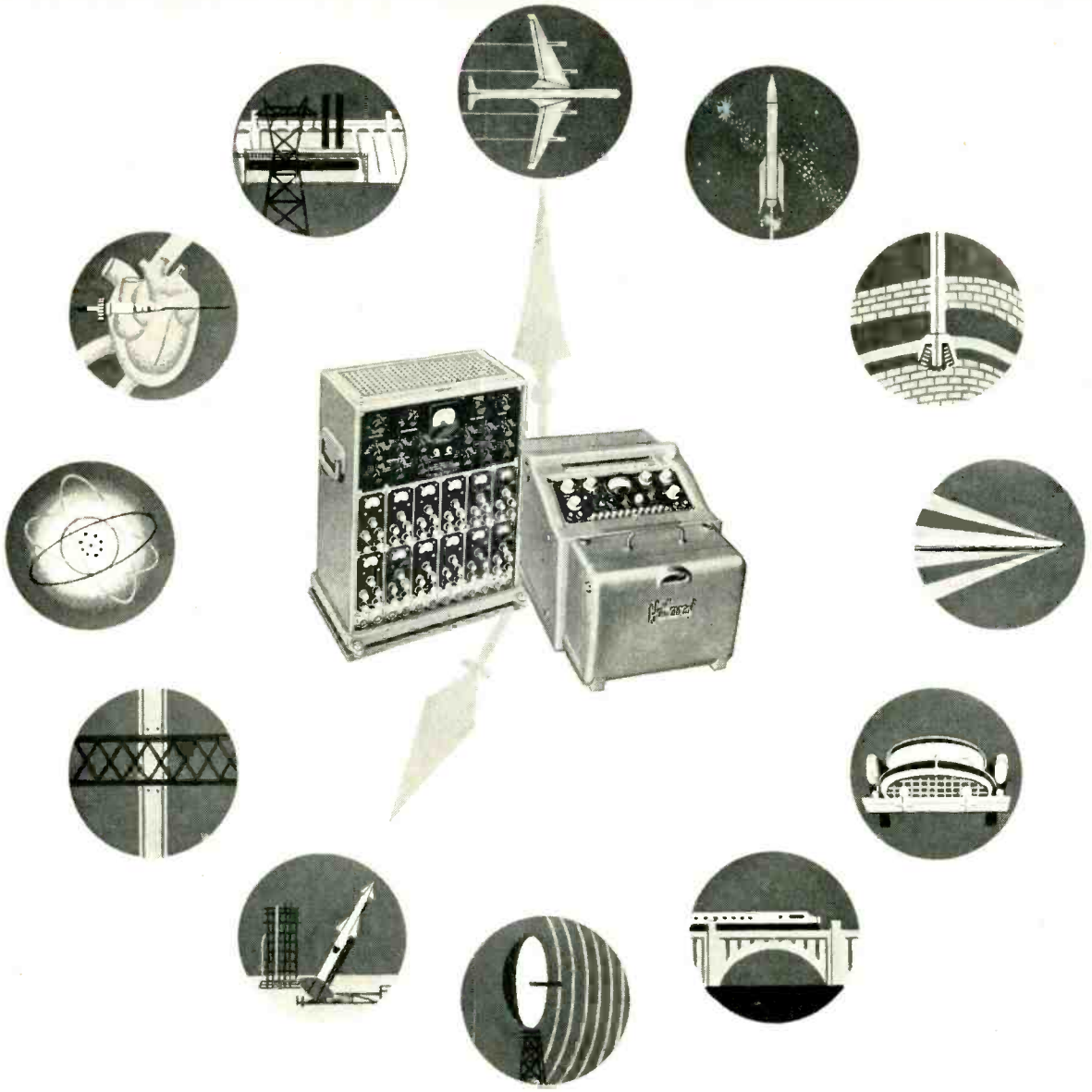


HIGH-PASS TV FILTER
is completely shielded

VIDAIRE ELECTRONICS MFG. CORP., 576 W. Merrick Rd., Lynbrook, N. Y. Model F-6 high-pass tv filter is designed to cut off below 50 mc. It will reduce or eliminate most interference in the 21-mc or 41-mc tv i-f bands. It is completely shielded eliminating the possibility of any stray pickup by the filter itself. Only 1¾ by 1¼ by ⅞ in. in size, the F-6 has mounting tabs for simple mounting right at the tv tuner. High-efficiency coils and ceramic capacitors are used throughout, making the F-6 an effective rejection device for the unwanted frequencies. **Circle P21 inside back cover.**

COMMUTATOR
two-pole telemetering type

INSTRUMENT DEVELOPMENT LABORATORIES, INC., 67 Mechanic St., Attleboro, Mass., announces a new



You can save valuable test and research hours with this system...

The convenient HATHAWAY MRC-21 Strain Gage Control Unit and the S-25 Oscillograph

comprise a measuring and recording system preferred by the military, industrial and research fields. Valuable engineering time is saved by the greater convenience of the system's broader range of channels, exclusive pushbutton selectivity and maximum amplification which results in clearer records.

Only Hathaway can offer you all these advantages for your instrument investment . . .
• up to 36 channels • 1/6 to 160 in/sec chart speeds • pushbutton convenience while operating • up to 30,000 in/sec writing speed • remote operation • carrier or wide band amplification • automatic calibration • 0 to 6000 cps response • 1/10 microinch/in noise level

Write for the facts you want to know—Bulletins 1-2A and 4-2A

Test with convenient, versatile instrumentation by . . .

HATHAWAY INSTRUMENT DIVISION
HAMILTON WATCH COMPANY

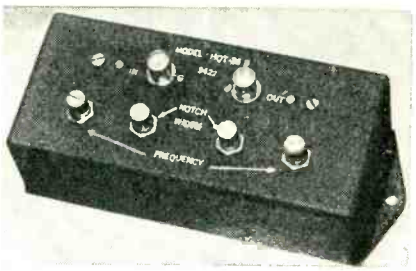
5800 EAST JEWELL AVENUE • DENVER 22, COLORADO

• NEW YORK	• DETROIT	• CHICAGO	• ALBUQUERQUE	• PASADENA
600 Fifth Ave. Plaza 7-7947	1960 E. Lincoln Ave. Birmingham, Mich. Midwest 4-9004	35 E. Wacker Dr. State 2-8411	3221 Silver Ave., S.E. 5-9637	380 E. Green St. Ryan 1-7829

telemetering commutator with a life expectancy exceeding 500 hr without servicing. It is contained in a hermetically sealed case to overcome most of the usual military environmental conditions. Powered by a 400-cps, 115-v, two-phase motor, this unit requires only seven w to provide 10 rps pole speeds and only 15 w for 30 rps pole speeds.

Contact resistances of less than 0.25 ohm are practically invariant during the entire use of the commutator. Intercontact impedances exceed 100 megohms for the life of the instrument.

Measuring only $2\frac{1}{2}$ in. in diameter by $5\frac{3}{4}$ in. long, this two-pole unit has exceeded 1,000 hr life at 10 rps and has withstood 2,000-cps vibration frequencies at 16-g. amplitude. **Circle P22 inside back cover.**



REJECTION FILTERS
feature narrow bandwidth

ENTRON INC., 4902 Lawrence St., Bladensburg, Md. The HQ series are extremely stable, sharp-cutoff, high-attenuation, vhf band-reject filters. They have a wide tuning range and constant bandwidth. The units afford an easy means of improving band edge response of broad-band filters or amplifiers. Their narrow bandwidth allows them to be used to eliminate narrow-band cochannel interference. These traps are particularly well suited for removing adjacent channel interference to color tv signals.

▶ **Bandwidth Ranges**—The HQT has a peak attenuation greater than 70 db and a 30-db bandwidth of 200kc. The HQF has a peak attenuation greater than 90 db and a 30-db bandwidth of 400 kc. They are available with various connector types, matched to main-

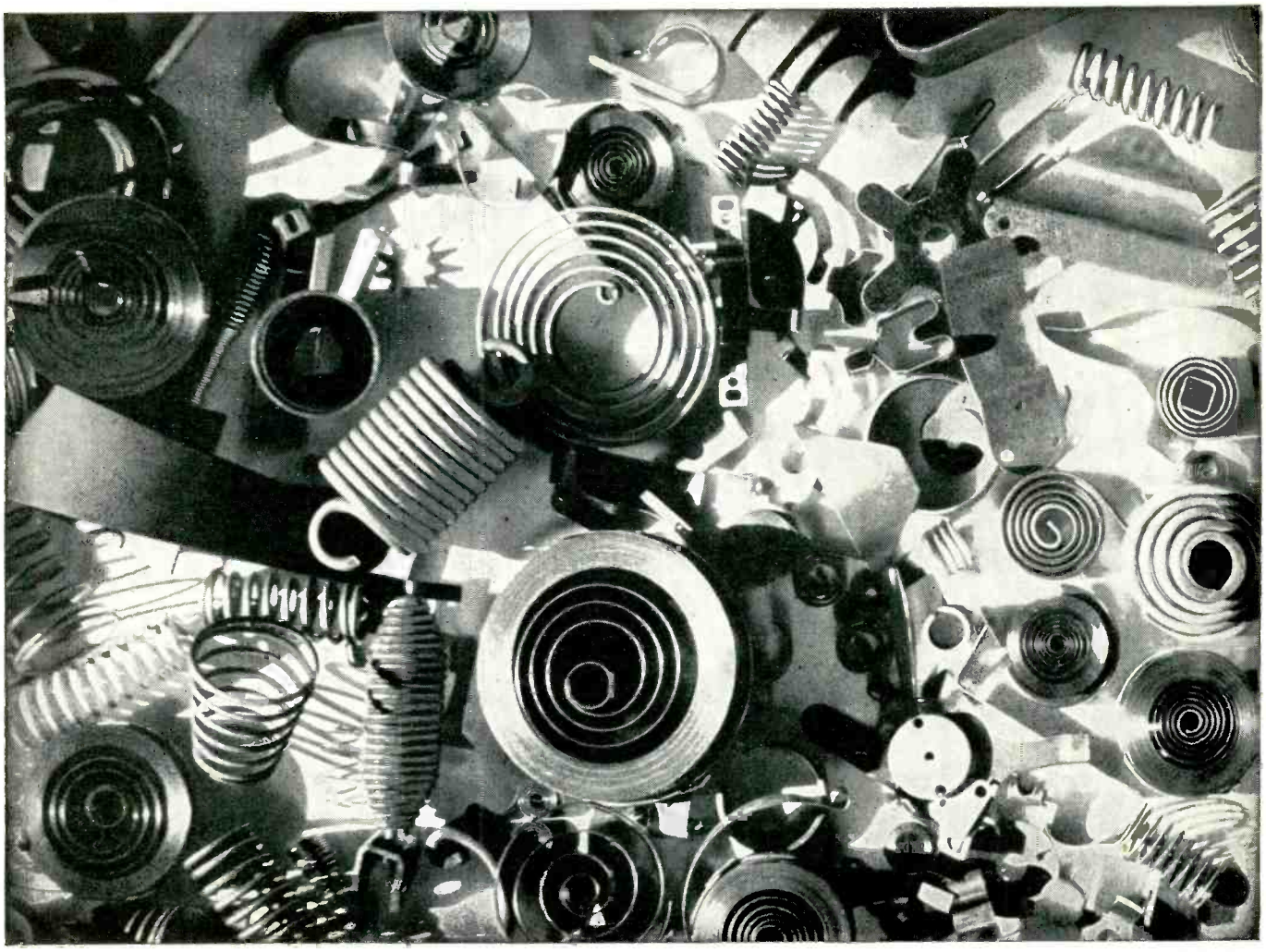


Photo courtesy of Associated Spring Corp.

Need a spring for service above 500° F.?

When it is a question of strength and resistance to fatigue and relaxation under corrosive conditions —

Particularly when temperatures range over 500°F. and other materials do not perform satisfactorily—

That is the time to see how INCO Nickel Alloys may solve the problem for you.

The alloys, Inconel and Duranickel, for example, are widely used for springs that must resist relaxation at stresses up to 70,000 psi and temperatures up to 650°F.

Inconel "X" alloy goes even further. It maintains 90 per cent of its room-temperature mechanical properties up to 900°F., 80 per cent up to 1100°F. Combines excellent resistance to heat, corrosion, and *relaxation* at stresses up to 100,000 psi. (Maximum recommended design stress, corrected, decreases as heat exceeds 700°F.)

Other Inco Nickel Alloys—Monel, "K" Monel, Permanickel—help solve special spring problems. Permanickel alloy, for example, combines good electrical conductivity with excellent heat and fatigue resistance.

Why don't you let Inco engineers help you find the right spring for severe service.

INCO Nickel Alloys

MONEL® • "R"® MONEL • "K"® MONEL • "KR"® MONEL
"S"® MONEL • INCONEL® • INCONEL "X"® • INCONEL "W"®
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Electrical and Electronic Section E-3-57
67 Wall Street, New York 5, N. Y.

Please send me information on:
1. ☐ Springs for use at _____°F.
2. ☐ Names of manufacturers of Inco Nickel Alloy springs.

Name_____ Title_____

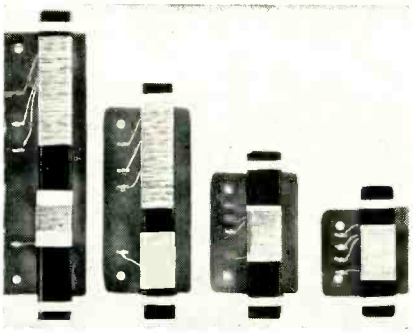
Company_____

Company Address_____

Product_____

tain minimum vswr.

Current models HQT-26 and HQF-26 are tunable in the range of 50 mc to 100 mc and model HQT-73 is tunable in the range of 174 to 220 mc. **Circle P23 inside back cover.**

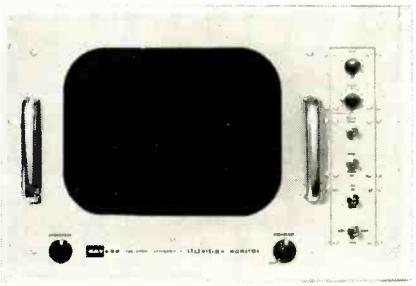


ANTENNA STICKS

for transistor receivers

SUPEREX ELECTRONICS CORP., 4 Radford Place, Yonkers, N. Y. Eleven different transistor-matched Loopsticks are now available. Features include complete electrical adjustability, compactness, maximum signal transfer and increased selectivity.

Each Loopstick is packed with full installation instructions including nine suggested circuits and a summary of transistor receiver design. A descriptive catalog is available. **Circle P24 inside back cover.**

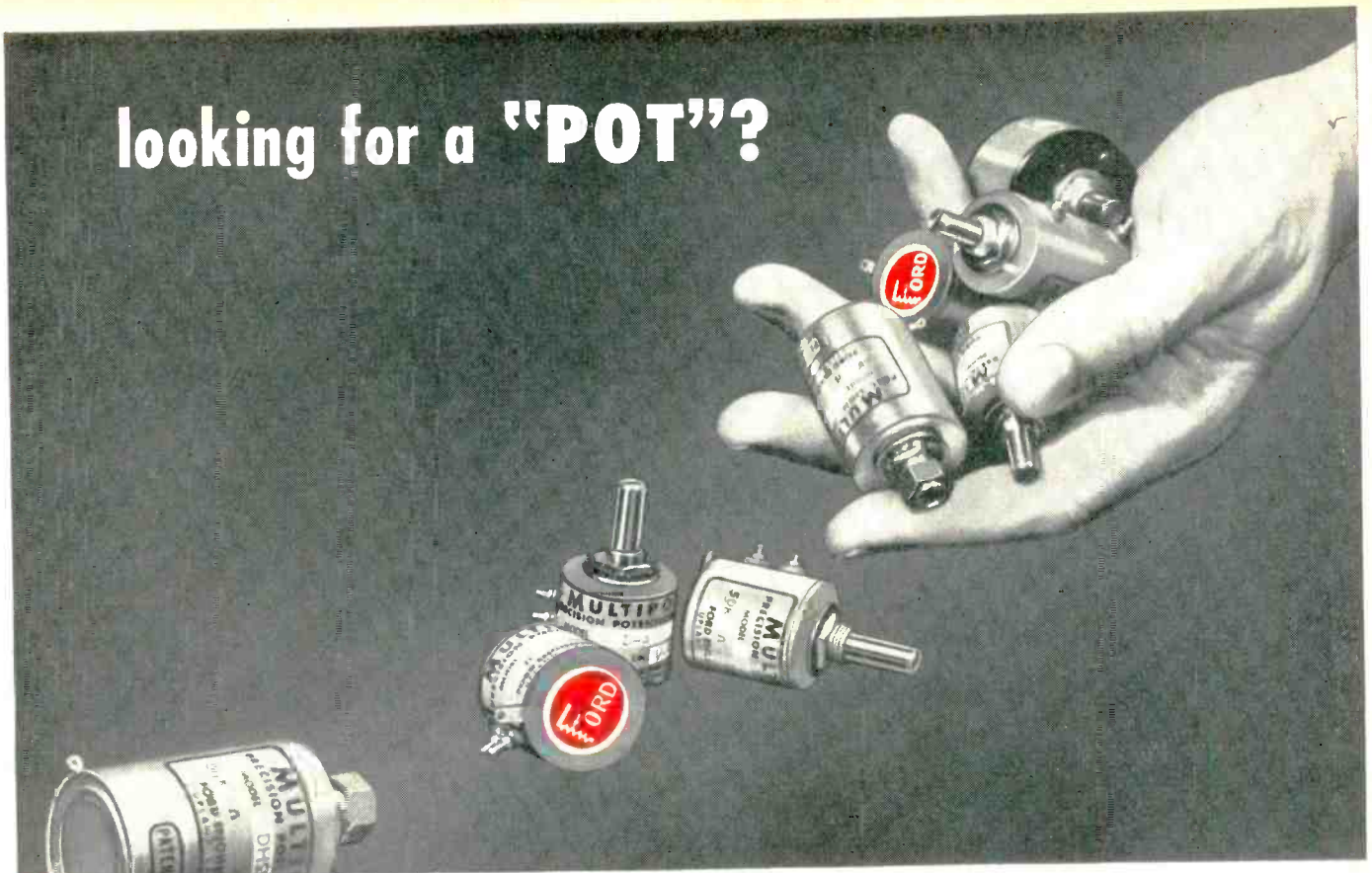


VIDEO MONITOR

for closed circuit use

KAY LAB, 5725 Kearny Villa Road, San Diego 11, Calif. Model ARM-14 is a new 14-in. video monitor designed to provide remote viewing of video information from the company's industrial or broadcast tv camera chains. It contains a precision deflection system and a broadband video amplifier that

looking for a "POT"?



THREE OF THE MANY "MULTIPOTS" IMMEDIATELY AVAILABLE. (All models available in 1, 3, 5 and 10 turn, and wide range of resistance values.)

MODEL "RU" Standard 1 1/16" diameter with 4 watt power, maximum resistance and resolution.

MODEL "D" 1" diameter and minimum length.

MODEL "DH" Sealed and metal clad for operation under adverse humidity and vibration.

FORD "MULTIPOTS" by DAYSTROM PACIFIC CORPORATION

Wire-wound, Precision-built, Multi-turn Potentiometers

WITH:

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- CLOSE LINEARITY
- EXCELLENT PERFORMANCE UNDER EXTREME VIBRATION

The Ford Engineering Company, Inc. "Multipots" compliment the many precision-built, wire-wound, sub-miniature potentiometers already procuced by Daystrom Pacific Corporation, so that Daystrom now can fill all of your potentiometer needs with top-quality production model potentiometers.

ALL FORD "MULTIPOTS" IMMEDIATELY AVAILABLE

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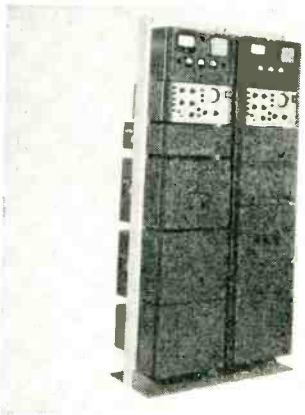
provide exceptional overall picture quality. Horizontal resolution is better than 600 lines. Only one coax cable is necessary between the camera control unit and the monitor. Sync is provided by blanking pulses on the video waveform. The monitor may be positioned up to 1,000 ft from the camera control unit without line amplifiers. The unit is available in a cabinet or a 19-in. rack mountable chassis. The rack-mount model will accept any three remote control panels for remotely controlled pan-tilt, iris-focus, three-lens turret and camera control accessories. **Circle P25 inside back cover.**



MULTIPLEX TERMINAL

sixteen-channel system

RIXON ELECTRONICS, INC., Silver Spring, Md., has developed a 16-channel time-division-multiplex terminal system for use primarily with vhf communications equipment.

To increase reliability and operating efficiency, transistors, germanium diodes and magnetic storage units are utilized in many of the circuits. Plug-in module packages and printed circuits are also used extensively throughout the equipment.

The MUX-16 equipment is designed for 115-v 60-cycle operation and has a total power consumption of under 500 w. A complete system can be mounted in a dual relay rack cabinet 84 in. high. The equipment is capable of two, four, eight and 16-channel operation at teletypewriter speeds of 60, 75 and 100 wpm.

By employing oscillators with a

COMPONENTS TO SYSTEMS FROM

Mack

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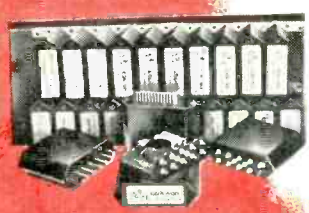
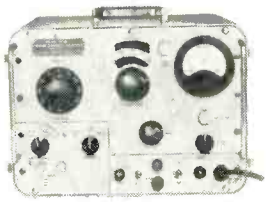
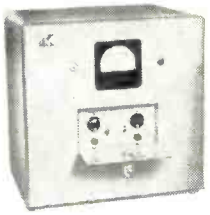
• CONTROLS • ULTRASONICS
• PRECISION TEST EQUIPMENT • INSTRUMENTATION
• RADIATION DETECTION EQUIPMENT • AUTOMATION



COMPUTER COMPONENTS

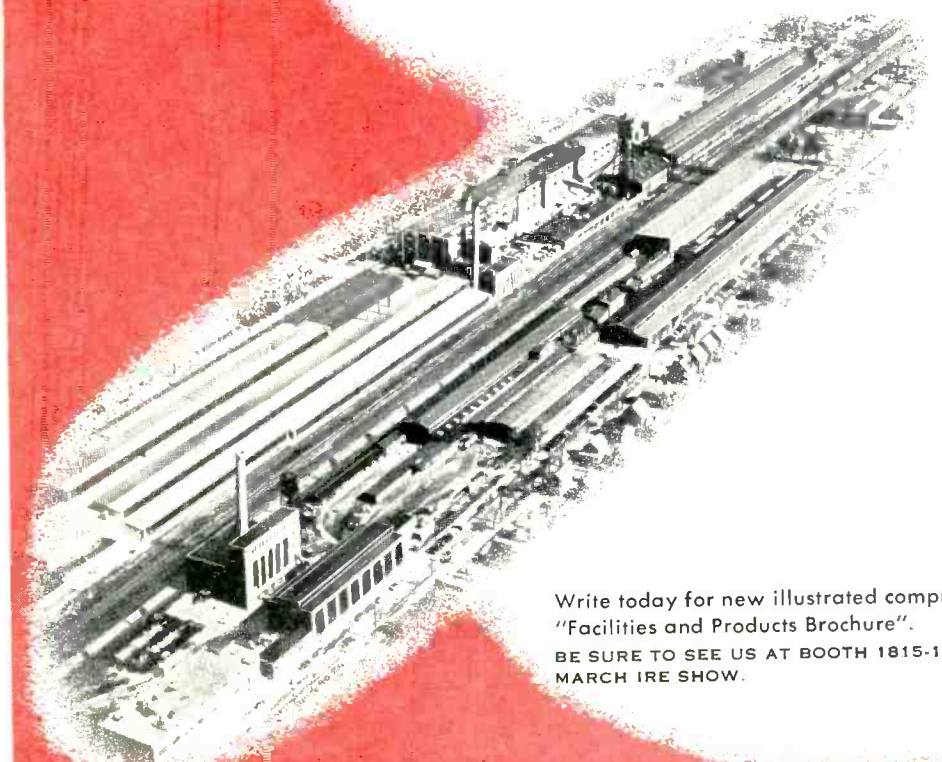


CARRIER FREQUENCY VOLTMETER (WAVE ANALYZER)



ULTRASONIC GENERATOR

AIRPORT TRAFFIC CONTROL MONITOR



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stability better than one part in 10^8 per day, synchronization between transmitting and receiving sections can be maintained over long periods of time. Automatic phasing, simplified channel switching and interchangeability of subassemblies are among the other design features. **Circle P26 inside back cover.**

LOAD ISOLATOR
Ku-band Ferrite type

LITTON INDUSTRIES, 5873 Rodeo Road, Los Angeles 16, Calif. Model U90 Ferrite load isolator is especially designed for new military radar operating in the Ku-band frequencies. It provides a minimum of 10-db isolation over the bandwidth of 16,300 to 16,700 mc at 90 w average power and 90 kw peak. Insertion loss is 0.7 db maximum and the input vswr is 1.05 maximum.

Designed for use under rugged environmental conditions, operating characteristics are guaranteed over a temperature range of — 55 C to + 100 C and under vibration per MIL-E-5272A. A cover totally enclosing the magnet prevents disturbance of the magnetic field and change of electrical characteristics during the operating life of the system. **Circle P27 inside back cover.**

SINGLE-TURN POT
linear in function

BORG EQUIPMENT DIVISION, The George W. Borg Corp., Janesville, Wisc., has announced production of its new 910 series single-turn Micropot potentiometer. It is a high precision instrument, linear in function, and offers such ad-

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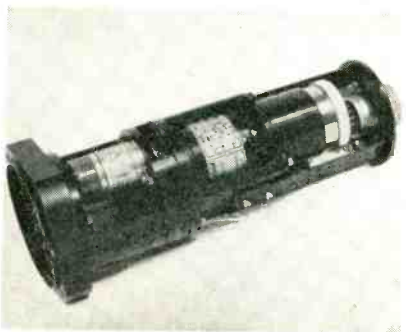
vantages as extreme accuracy, fine resolution, low torque, long life and consistent, reliable performance under adverse environmental conditions.

The resistance element and terminal leads are molded into a single unit for better operation under severe vibration and high temperature conditions. Units may be ganged, and each cup may be individually phased in the field. All models have ball-bearing mounted shafts.

The 910 series Micropot has a power rating of 5 w at 40 C, and a resistance range of 50 to 10,000 ohms. Standard tolerance is ± five percent. Standard linearity accuracy is ± 0.5 percent independent. Starting torque is 0.5 in. -oz. per section. It features continuous mechanical rotation, 340 deg or less electrical rotation. Net weight is four oz per single unit, with 1 oz added for each additional unit. Length of a single unit is 1 3/64 in.; width, 1⅞ in. Shaft is ⅝ in. long, with special lengths available. **Circle P 28 inside back cover.**



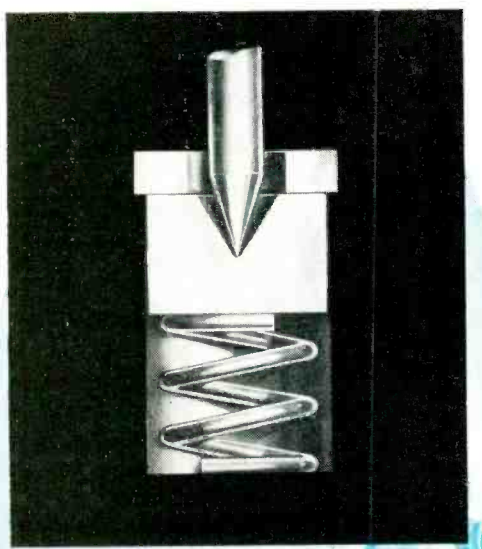
DATA REPEATERS
of the servo type

FEEDBACK CONTROLS, INC., 903 Main St., Waltham 54, Mass., offers a line of servo-type data repeaters with high accuracy and fast response. Designed for use as flight-test instrumentation, the repeaters provide remote indication of angular position and of a-c and d-c voltages. The data repeaters mount in standard aircraft panels with output dials arranged for visual observation or photographic recording.

The first of the two basic types is the synchro-data repeater, a two-speed follow-up servo employ-

SHOCK ABSORBER WEIGHING ONLY

0.0000028 lb!



Tiny shock-absorbing springs, shown greatly enlarged at the left, provide a *second line of defense* against shock damage in Weston ruggedized panel meters. While the entire instrument movement is cradled on an effective overall shock mount of specially formulated rubber, these tiny shock absorbers, mounted in back of each jewel bearing, provide double protection at the critical points. The spring-backed jewel in ruggedized instruments is another Weston FIRST . . . one which assures continuous, dependable service wherever panel meters are subject to severe impact, vibration or shock.

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Weston ruggedized instruments are *approved* in all sizes—1 ½", 2 ½", 3 ½", 4 ½".

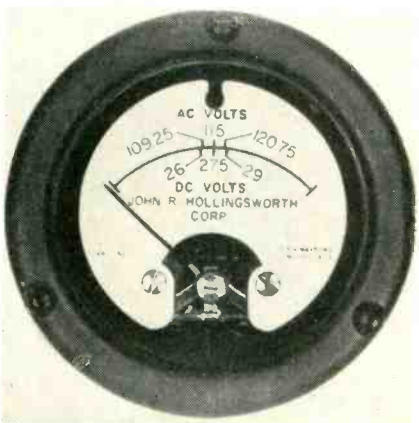
WESTON *Ruggedized* PANEL INSTRUMENTS

A DAYSTROM UNIT

ing standard Bu Ord Mark 54, Mod 2 synchro transmitters. They are available with four different speed ratios between synchros.

The second type is the potentiometer-data repeater, a position servo which utilizes a precision 10-turn Helipot as the follow-up transducer.

Thermostatically controlled viscous-coupled inertia damping is used to achieve high-velocity constants. The units employ v-t preamplifiers and magnetic output stage in the servo amplifiers. **Circle P29 inside back cover.**



BASIC METER
ruggedized and sealed

WACLINE, INC., 35 So. St. Clair St., Dayton 2, Ohio. Illustrated is a 2½-in. round basic meter made to meet the requirements of military specifications MIL-M-6A and MIL-M-10304A. It features extra high sensitivity, high torque to weight ratio, a minimum number of parts and a new simplified pressure-method of sealing and ruggedizing. The meters are available in all standard ranges of microammeters, milliammeters, ammeters and voltmeters. **Circle P30 inside back cover.**

D-C POWER SUPPLY
for computer applications

PERKIN ENGINEERING CORP., 345 Kansas St., El Segundo, Calif., announces a d-c power supply with steady state regulation accuracy of ±0.01 percent for computer applications. This unit has a ripple of less than 50 mv peak-to-peak

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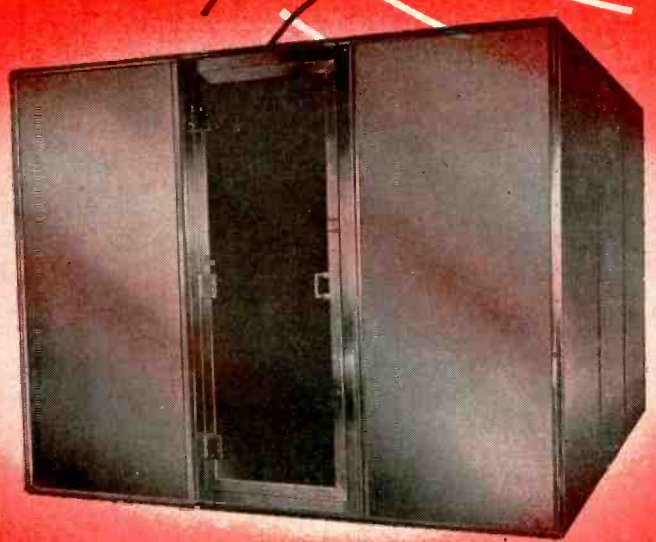

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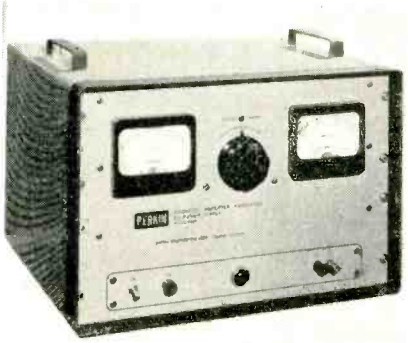
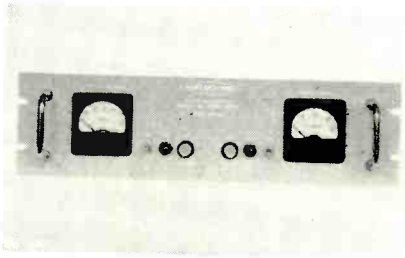


and a d-c output of 200 v ±10 percent at three amperes. The dynamic regulation is: ± one percent for a ±15-percent step change in a-c input; ± one percent for a 50-percent load change. The unit is designed for a three-phase, 60 cps a-c input of 208/230 v, ±15 percent.

The power supply also has an extremely low dynamic impedance and incorporates an ultrafast magnetic amplifier with instantaneous electronic control. No saturating type a-c regulators (with their consequent noise) or large energy-storage capacitor banks are employed. Overall dimensions of the unit are 19½ in. wide by 15 in. deep by 12¾ in. high. **Circle P31 inside back cover.**

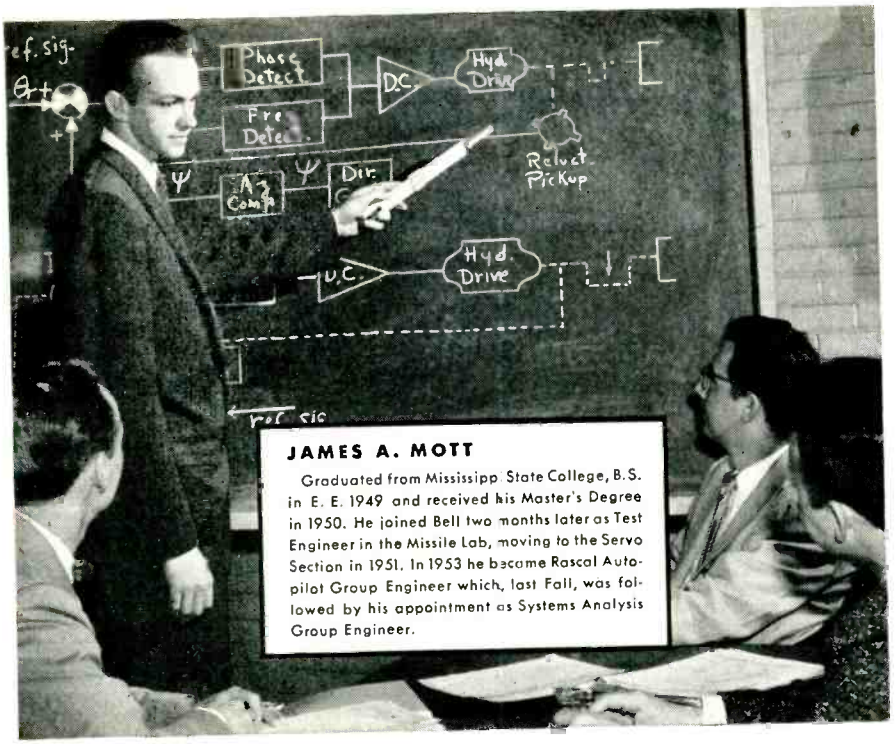


LAB POWER SUPPLIES
mount in standard relay rack

REFLECTONE CORP., Stamford, Conn., has developed two new laboratory power supplies giving different output ranges: model PS-L225 for 125 to 325 v 0 to 200 ma d-c, 6.3 v 10 amperes a-c; and model PS-L425 for the 325 to 525 v d-c range.

The units are designed for continuous heavy-duty operation. They incorporate protection against external overloads or internal failure. Units are electronically controlled and substantially free from noise and hum.

Input of each is 105 to 125 v,



There are NEW Opportunities at BELL

James Mott is typical of the successful engineers who are now teamed together in Bell Aircraft's, newly-created Avionics Division with greatly expanded facilities and a building of its own. This recent divisional reorganization has created many top-flight openings for engineers and technicians and vastly broadened their opportunities for professional accomplishment. That fact, together with the number and wide diversity of Bell's projects, are insurance that your future at Bell will be limited only by your own capabilities.

You'll work in a fast moving, successful organization—in ideal surroundings with associates who have fine professional records. You'll have every opportunity to grow, learn and progress. Pay is high, benefits exceptional, and living conditions the best. If you're not moving fast enough or going far enough in your present position, contact Bell.

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- Field Test Engineers
- Flight Test Engineers
- Flight Test Programmers
- Fuel Injection Specialists
- Gear Designers
- Guidance Engineers
- Gyro Specialists
- Heat Transfer Engineers
- Hydraulic Engineers
- IBM Programmers
- Instrumentation Specialists
- Laboratory Test Engineers
- Magnetic Amplifier Specialists
- Mathematical Analysts
- Mechanical Engineers
- Microwave Engineers
- Miniturization Engineers
- Operations Analysts
- Physicists
- Power Plant Designers
- Pressure Vessel Designers
- Project Engineers
- Publication Engineers
- Radar Systems Engineers
- Rocket Test Engineers
- Servo Systems Engineers
- Servo Valve Engineers
- Statisticians
- Stress Engineers
- Structures Engineers
- Specification Writers
- Technical Writers
- Test Equipment Engineers
- Transformer Design Specialists
- Transistor Application Engineers
- Thermodynamic Engineers
- Telemetering Engineers
- Turbine Pump Designers
- Vibration & Flutter Analysts
- Weapons Systems Engineers
- Wave Guide Development Engineers
- Weights Engineers

50 to 400 cps. The d-c regulation is 0.15 percent or 0.3 v (whichever is greater) against line; 0.25 percent or 0.5 v (whichever is greater) against load. Internal impedance is less than six ohms; ripple is less than three mv rms. **Circle P32 inside back cover.**

PIRANI VACUUM GAGE

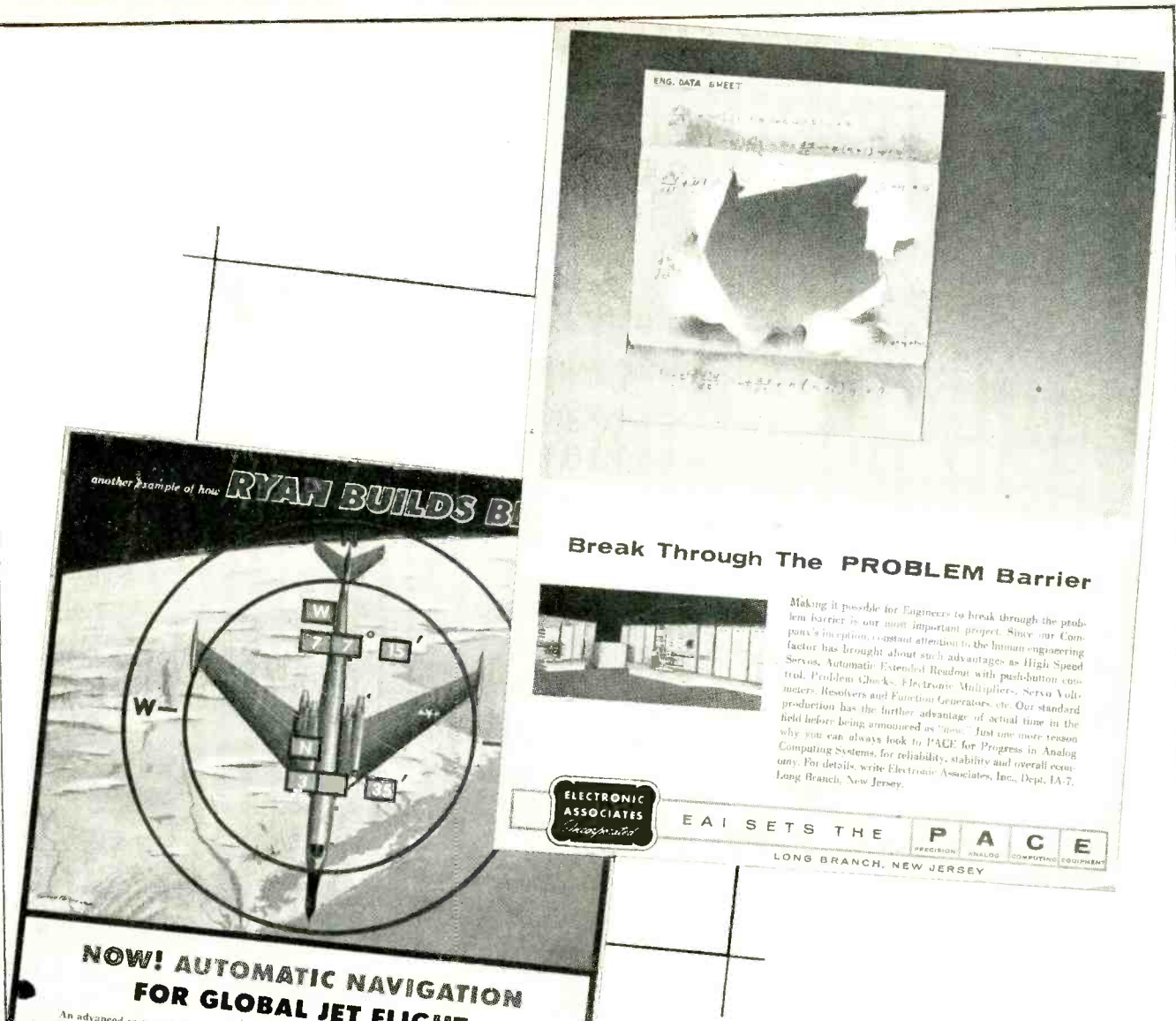
a one-to-four station unit

CONSOLIDATED ELECTRODYNAMICS CORP., Rochester Division, 1775 Mt. Read Blvd., Rochester, N. Y. A new one-to-four station Pirani vacuum gage with a range from one to 2,000 microns of Hg is now available. Type 2203-03 gives direct, continuous readings of the total pressure of condensable vapors and permanent gases on two scales—one to 50 microns Hg and 50 to 2,000 microns Hg.

The instrument features a new sensing tube which greatly reduces zero drift. The tube operates at a low maximum temperature of 250 C. Deposits of carbon on the filament do not change its emissivity. Both the sensing and the compensating tubes are enclosed in a single metal envelope, thus minimizing the effect of changes in ambient temperature. The combined tube is also smaller, more rugged and easier to install.

Automatic voltage regulation provides for easier operation and permits use of a 0 to 10-mv recorder without constant operator attention.

The 2203-03 incorporates a printed circuit for greater compactness, increased operational uniformity and lower cost. It is 6½ in. high, 11 in. wide, 6 in. deep and weighs 10 lb. It is operable from a 115-v power source but is readily adaptable to 230-v opera-



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ELECTRONIC ASSOCIATES Incorporated

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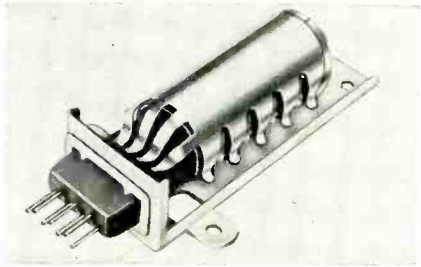
NEW PRODUCTS (continued)

tion. Data sheet No. 9-31 gives further information. **Circle P33 inside back cover.**

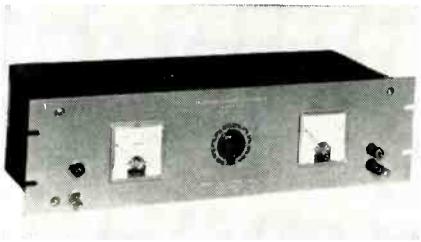


TUBE SHIELD

for flat press subminiatures

INTERNATIONAL ELECTRIC RESEARCH CORP., 145 W. Magnolia Blvd., Burbank, Calif. This new subminiature tube shield mount is of a right-angle design having an integral socket for three, four, five, six and seven-pin flat-press tubes. The design gives engineers a compact, easy-to-install heat-dissipating clamping mount that is ideal for use in confined spaces while permitting ready access for service or tube replacement.

Shields are silver plated overall with inner wrap of pure silver for maximum heat conductivity. The spring clip and right-angle base are of beryllium copper. **Circle P34 inside back cover.**



H-C POWER SUPPLIES

utilize transistors

ELECTRONIC RESEARCH ASSOCIATES, INC., 67 East Centre St., Nutley 10, N. J., announces a series of new designs intended to eliminate the drawbacks inherent in vacuum tube, thyratron or magnetic amplifier equivalents.

Features include fast transient response, small size and weight, close regulation, low ripple content and independence from line response changes.

Electrical design includes line isolation and full-wave rectifica-

...the authors

Most of the books written by Laboratories authors are published by D. Van Nostrand Company. Other publishers include John Wiley & Sons and McGraw-Hill. Subjects include speech and hearing, mathematics, transmission and switching circuits, networks and wave filters, quality control, transducers, servomechanisms, quartz crystals, capacitors, visible speech, earth conduction, radar, electron beams, microwaves, waveguides, antennas, traveling-wave tubes, semiconductors, ferromagnetism.

Harold S. Black, B.S. in E.E., Worcester Polytechnic Inst., author of "Modulation Theory."

John R. Pierce, Ph.D., California Inst. of Tech., author of "Traveling-Wave Tubes."

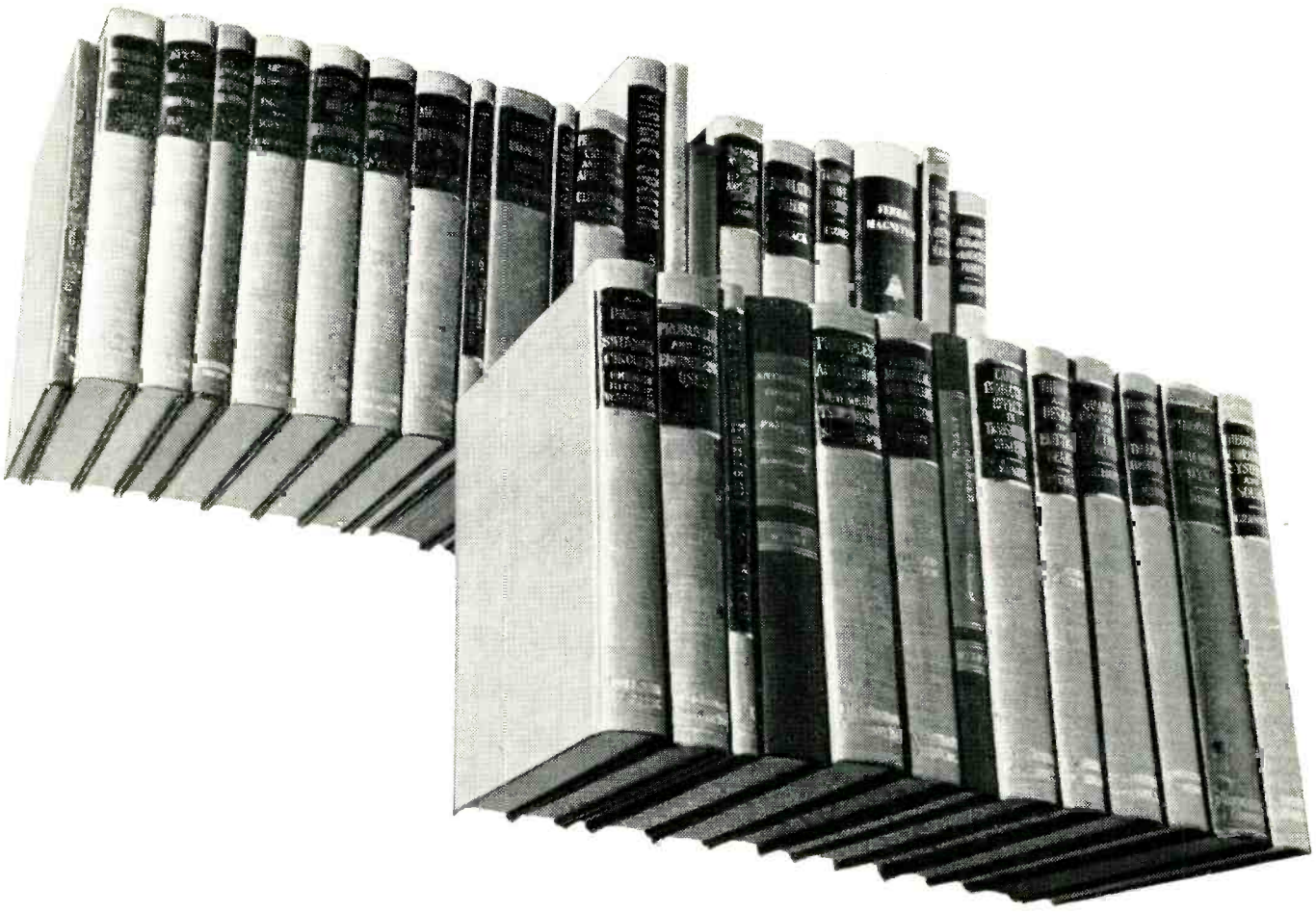
Richard M. Bozorth, Ph.D., California Inst. of Tech., author of "Ferromagnetism."

W. Thornton Read, M.S., Brown University, author of "Dislocations in Crystals."

Hendrik W. Bode, Ph.D., Columbia University, author of "Network Analysis and Feedback Amplifier Design."

Walter A. Shewhart, Ph.D., University of California, author of "Economic Control of Quality of Manufactured Product."

The books...



How the scientific world shares in fruits of the telephone art

In their work to improve telephony the scientists and engineers of Bell Telephone Laboratories make important findings in many sciences. They thoroughly report these findings in professional journals and magazines. But sometimes, as knowledge accumulates in a vital field, a "treatment in depth" is prepared in book form.

Bell Laboratories authors have written 36 books to date and others are in preparation. Many have become classics in the Laboratories' primary field of communications. Many have become standard works of wide application because they provide a fundamental guide for technologies in other fields. For example, the design of automatic switching systems is of primary importance in computers; statistical quality control provides the indispensable basis for economical manufacture. Through their books these scientists and engineers and the Laboratories attempt to repay benefits they receive from the published works of others.

The pictures on the opposite page show some Bell Laboratories authors of technical books. A complete listing of titles may be obtained by sending in this coupon.

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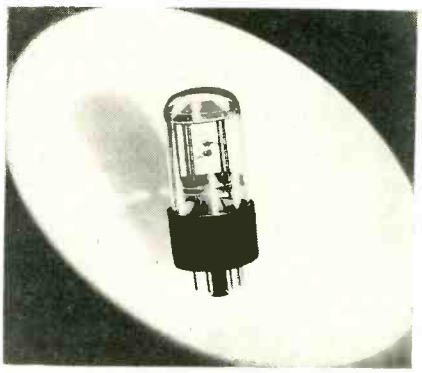
tion utilizing silicon rectifiers. Regulation is accomplished at d-c with germanium junction transistors in special circuitry. References used are silicon zener diodes.

Several stock models are available with adjustable output voltage ranges of 6 to 32 v d-c and current ranges of four, eight, and 12 amperes. All models are designed for 105 to 125 v a-c input, 60 to 400 cps. Line regulation is within 0.5 percent; load regulation, within 0.5 percent (for 20-100 percent load change). Ripple is less than one mv. Prices start at $395. **Circle P35 inside back cover.**



QUARTZ CRYSTAL
sealed-in-glass unit

BLILEY ELECTRIC CO., Union Station Bldg., Erie, Pa. The BG9D-S is a 100-kc sealed-in-glass quartz crystal unit for use in secondary frequency standards. The DT-cut element is designed especially for use in temperature-controlled ovens. Tolerance is ±5 ppm at 70 C. Temperature coefficient is less than 0.7 ppm per deg C between +65 C and +75 C. The BG9D-S is 3 1/8 in. overall in a T-9 bulb with standard octal base. Design specifications, including reference to specific crystal ovens, are found in bulletin No. 492. **Circle P36 inside back cover.**

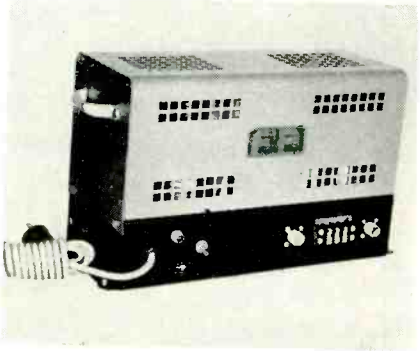
SUBMINIATURE POT
features minimum torque

ACE ELECTRONICS ASSOCIATES, INC., 103 Dover St., Somerville 44, Mass., announces a new jewel bearing, subminiature precision wirewound potentiometer for applications requiring minimum

starting and running torque. This Acepot has precision jewel bearings that provide extremely low torque and also seal against abrasive dust or other foreign matter. These units are ideal for sensitive instrument application and for servo, computer or selsyn use.

Because of the low torque required to rotate the shaft, no appreciable error is introduced and highest accuracy is maintained.

▶ **Specifications**—Torque is 0.01 oz in.; size, ½ in. by ½ in.; resistance range, 10 to 250,000 ohms standard (higher or lower on special order); linearity, ±0.3 percent; power rating, two w for 60 C rise; weight, ¼ oz including lock washer and nut; temperature, −55 C to +150 C. It meets applicable portions of JAN specifications and MIL-E-5272A standards. **Circle P37 inside back cover.**



TRANSIENT CONVERTER
for turbine type flowmeters

FISCHER & PORTER CO., 950 Jacksonville Road, Hatboro, Pa., has developed a transient converter for use with turbine type flowmeters. The converter accepts a sinusoidal input signal of varying frequency and provides either an analog output for recorders and oscillographs or a digital output to counters and computers.

Input frequency range for the new unit is from 0 to 600 cps, operating from a 500-ohm source impedance. The output is a 0 to 100-mv analog signal or a 10-v positive pulse (at eight times the input frequency) to digital devices.

The unit has a short-term analog accuracy and linearity of ±0.5

AER -O- COM

DEFINITELY DEPENDABLE!

Aerocom's Dual Automatic Radio Beacon

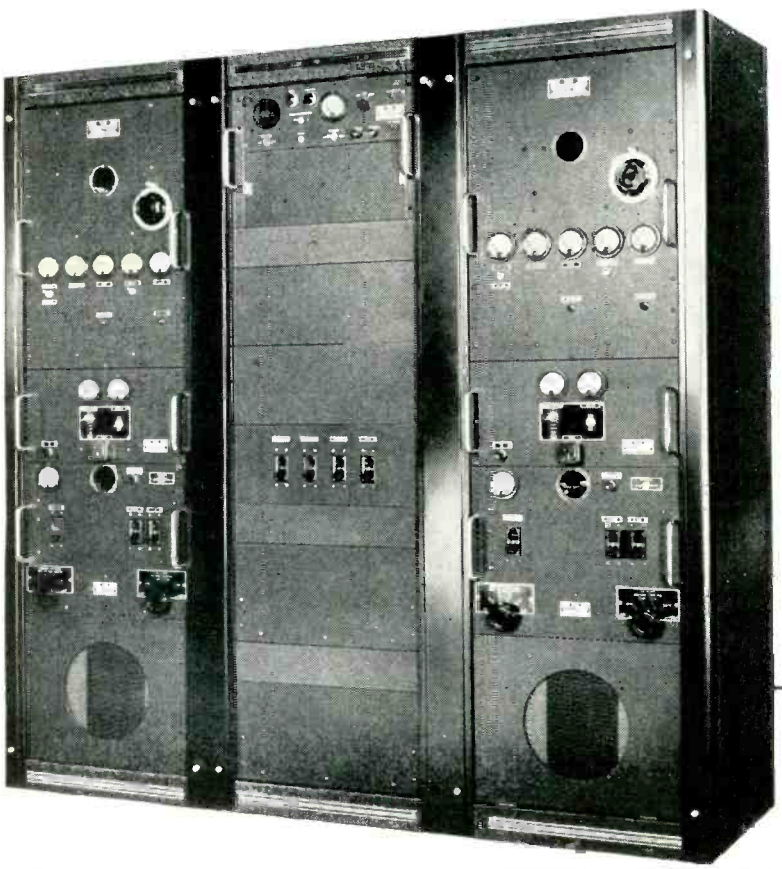
Reliability is built into every part of this dual 1000-watt aerophare unit. Ruggedly constructed and conservatively rated, it provides trouble-free unattended service, and at truly low operating and maintenance cost. It operates in the frequency range 200-415 kcs, using plug-in crystal for desired frequency.

Uses single phase power supply, nominal 220 volts, 50 or 60 cycles. Consists of two 1 kw transmitters with keyer (2 keyers if desired), automatic transfer unit and weatherproof antenna tuner. Each transmitter housed in separate standard rack cabinet, with controls in rack cabinet between the transmitters.

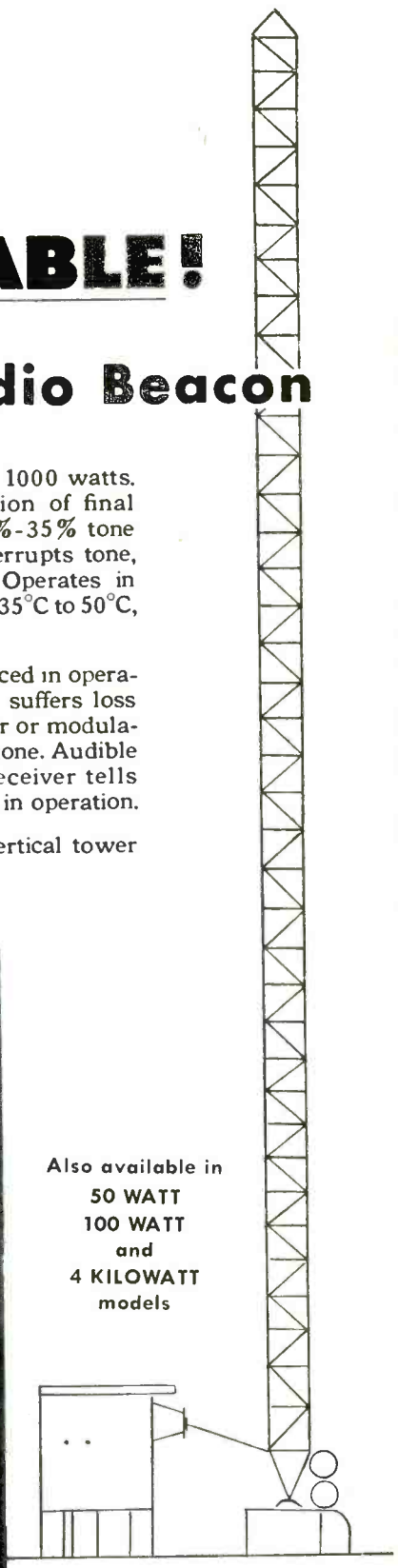
Nominal carrier power is 1000 watts. High level plate modulation of final amplifier is used, giving 30%-35% tone modulation. P-T switch interrupts tone, permitting voice operation. Operates in ambient temperatures from -35°C to 50°C, humidity up to 95%.

Standby transmitter is placed in operation when main transmitter suffers loss (or low level) of carrier power or modulation, or continuous (30 sec.) tone. Audible indication in monitoring receiver tells when standby transmitter is in operation.

Antenna may be either vertical tower or symmetrical T type.



Also available in
50 WATT
100 WATT
and
4 KILOWATT
models

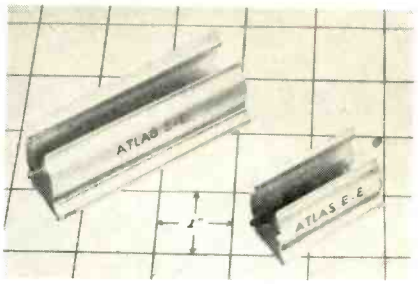


A-101

AER -O- COM

3090 S. W. 37th AVENUE · MIAMI, FLORIDA

percent and a long-term accuracy of ±3 percent. Rise time is 10 milliseconds for a 40 to 600-cps step. Accuracy of the digital output is absolute. The converter features plug-in subassemblies for easy maintenance. **Circle P38 inside back cover.**



COMPONENT HOLDERS

many new variations

ATLAS E-E CORP., 47 Prospect St., Woburn, Mass., has available over 300 new variations in its line of component holders. The clip-type holders have a built-in feature in their design which automatically provides greater holding power as the metal of the holder flexes under heavy vibration and extreme temperature changes. They have been tested to 90 g at 2,000 cycles without resonant frequencies.

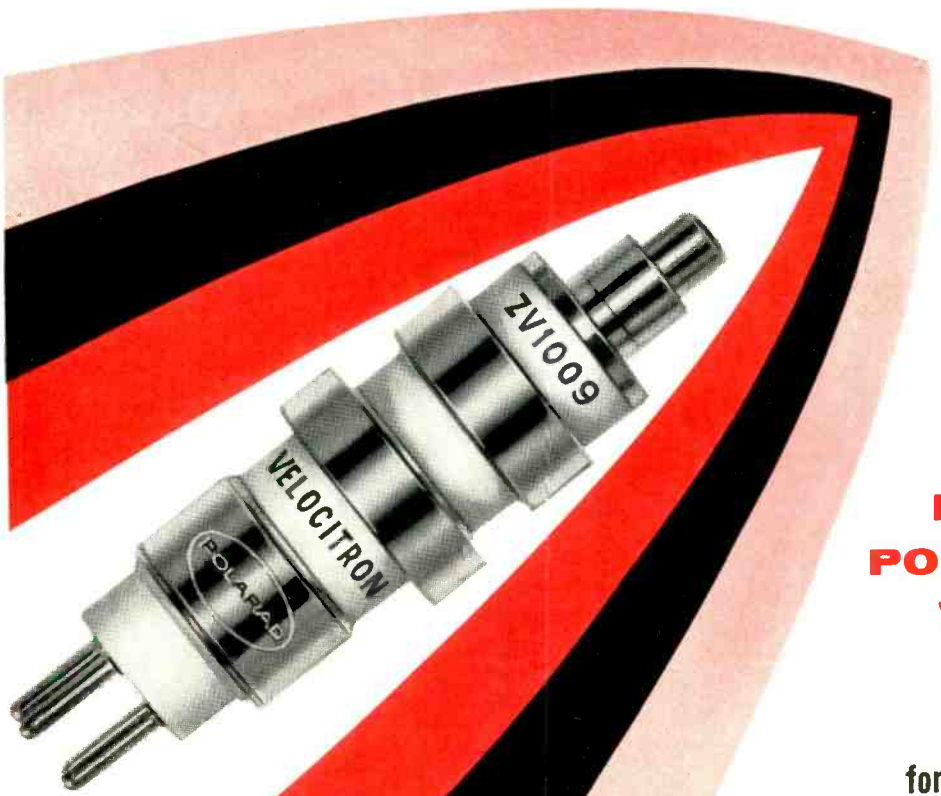
The new variations include light-weight slotted holders for glass, paper and plastic envelopes and cases such as subminiature tubes and capacitors; silver-plated beryllium copper holders for applications requiring non-magnetic material and heat-treatable silver alloy holders for applications requiring maximum heat dissipation. Tests show their function as heat dissipators permits uprating of 2 w to 10 w wirewound resistors by as much as 50 percent. Holders are available in diameters from $\frac{1}{8}$ in. to $1\frac{1}{2}$ in. with lengths from $\frac{3}{16}$ in. to 4 in. **Circle P39 inside back cover.**

POTENTIOMETERS

for high-temperature use

G. M. GIANNINI & CO., INC., 918 E. Green St., Pasadena 1, Calif., announces development of a high-temperature, infinite-resolution po-

NOW! the first all ceramic klystron tube for 1600 to 6500 mc



RUGGEDIZED POLARAD ZV1009 VELOCITRON*†

a physical and electrical replacement for klystron tubes 6BL6, 5836

The new Polarad ZV1009 all ceramic Velocitron is a **premium**, rugged tube designed for high temperatures, vibration and mechanical shock.

As a replacement for glass klystrons: the ZV1009 is less microphonic and less fragile. It is equipped with standard 4-pin connection.

As a basic design element: The all ceramic ZV1009 allows for higher ambient temperatures than any glass tube currents available. It is completely hard soldered.

SPECIFICATIONS: ZV1009 VELOCITRON

Reflector Mode	1¾	2¾	3¾
Cavity Mode	¾	¾	⅝
Frequency	2800	3200	5000 mc
Power Output Cutoff Voltage (approx.)	+3	+3	+3 volts
Reflector Voltage (approx.)	−220	−120	−220 volts
Resonator Voltage	325	325	325 volts
Control Electrode Voltage (Full Power Output)	+10	+10	+10 volts
Cathode Current (average)	28	28	28 ma
Electronic Tuning Range (between Half Power Points—minimum)	6	6	6 mc

Write directly to Polarad for complete data and design information.

*Registered U.S. Trademark

†Manufactured under Western Electric Patents

POLARAD ELECTRONICS CORPORATION

PROVEN RELIABILITY

43-20 34th Street · Long Island City 1, N. Y.

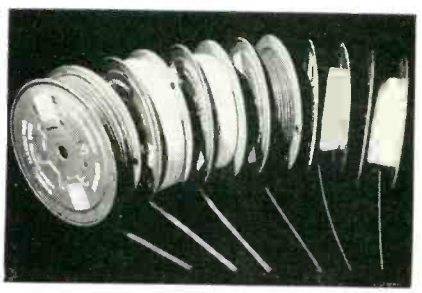
REPRESENTATIVES: Albany, Albuquerque, Atlanta, Baltimore, Boston, Chicago, Cleveland, Dayton, Denver, Englewood, Fort Worth, Kansas City, Los Angeles, New York, Philadelphia, Portland, Rochester, St. Louis, San Francisco, Schenectady, Stamford, Syracuse, Washington, D. C., Winston-Salem, Canada: Arnprior, Ontario.

Resident Representatives in Principal Foreign Cities

tentiometer that has been added to its Spiralpot line of slide-wire type precision pots. Use of special materials and alloys in the winding drum and vital elements allows a power rating of 1.5 w at 150 C.

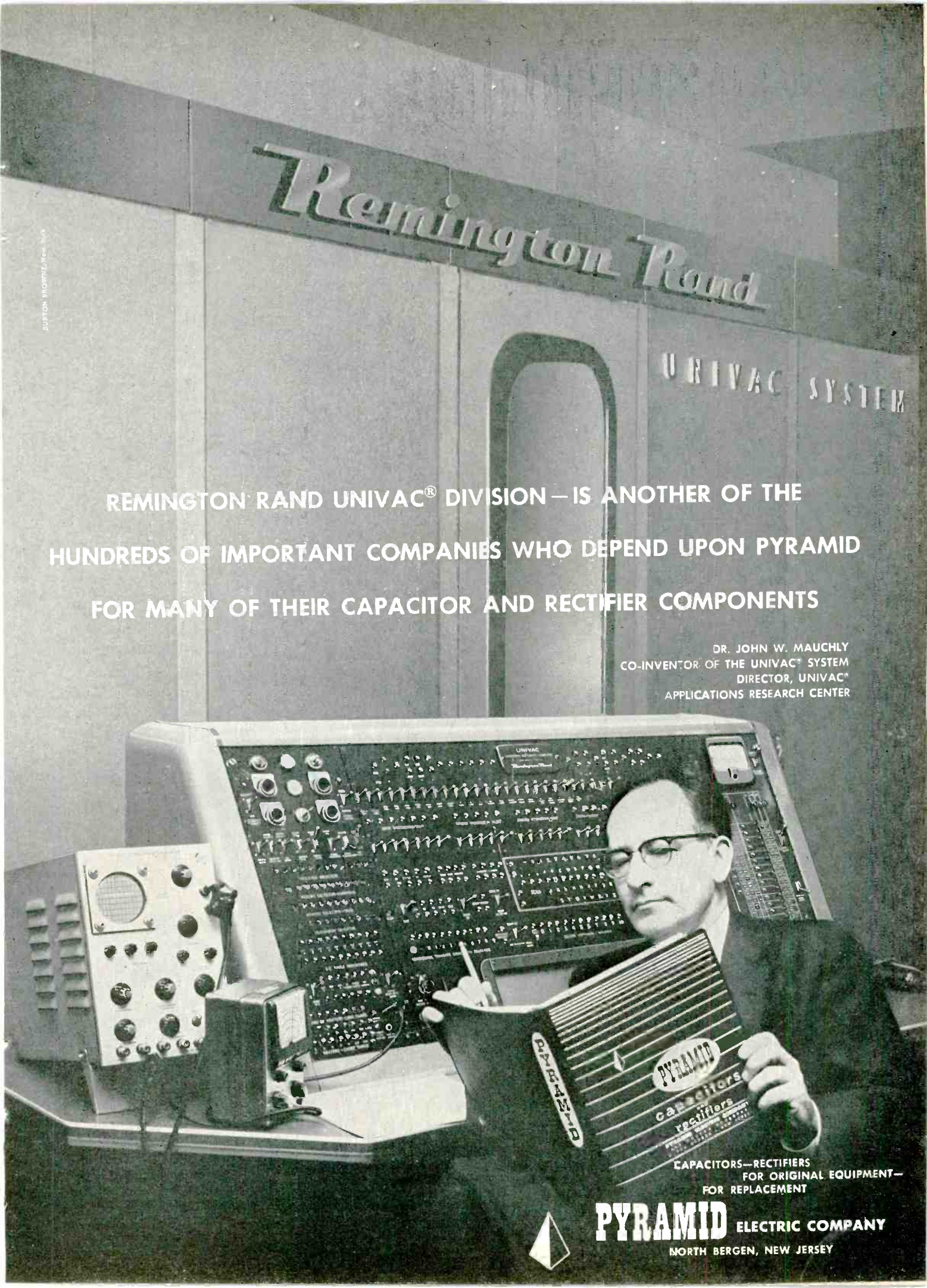
Model 85177A is available with linearities of 0.1 and 0.05 percent in standard resistance values of 50, 100, 150, 200 and 250 ohms per turn in ten-turn units. Other shaft rotations from 1 to 10 turns and other resistance values as low as two ohms per turn are also available.

These pots excel in many applications such as found in high-resolution servo systems, computers or indicating systems, where the presence of elevated temperature does not allow the use of other standard Spiralpots. **Circle P40 inside back cover.**



TEFLON TUBING
available in new sizes

THE POLYMER CORP. OF PENNSYLVANIA, 2140 Fairmount Ave., Reading, Pa. Polypenco Teflon spaghetti tubing is now available in Awg wire sizes of zero, one, two, three, four, five, six, seven, 28 and 30. The high-temperature tubing is used as a low and high-frequency insulation sleeving for electronic component development. The thin wall tubing has a minimum dielec-


Remington Rand
UNIVAC SYSTEM
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REMINGTON RAND UNIVAC® DIVISION—IS ANOTHER OF THE
HUNDREDS OF IMPORTANT COMPANIES WHO DEPEND UPON PYRAMID
FOR MANY OF THEIR CAPACITOR AND RECTIFIER COMPONENTS
DR. JOHN W. MAUCHLY
CO-INVENTOR OF THE UNIVAC® SYSTEM
DIRECTOR, UNIVAC®
APPLICATIONS RESEARCH CENTER
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CAPACITORS—RECTIFIERS
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PYRAMID ELECTRIC COMPANY
NORTH BERGEN, NEW JERSEY

tric strength of 750 v per mil, a low dielectric constant of 2 and a high surface resistivity above 10^{12} ohms per cm^2.

The material permits assembly miniaturization because it combines outstanding electrical properties with a wide temperature service range of −320 F to +555 F, zero water absorption and resistance to flex and vibration. It completely resists soldering heats and is unaffected by bending and flexing during assembly. **Circle P41 inside back cover.**

RELAY ELIMINATOR
has no moving parts

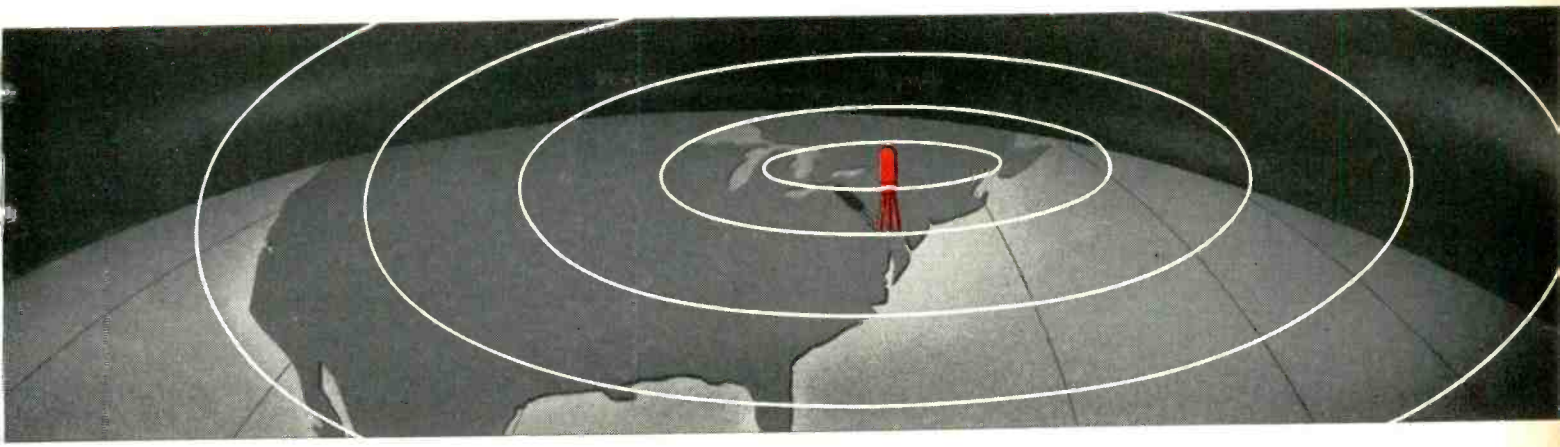
ALCOR ELECTRONICS CORP., 180 Lafayette St., New York 13, N. Y. Model 530 TREPAC (Teleprinter Relay Eliminator Package) consists of a transistorized switching circuit with silicon diodes and a built-in rectifier powered directly from 115 v a-c, 50/60 cps line. As a static unit with no moving parts, it is practically maintenance free. Useful life will exceed the life of relays currently on the market.

Physically, the TREPAC is a small plug-in can equipped with a standard octal plug and designed to be normally installed in the printer housing. It eliminates line relay, rectifier, current limiting resistors, spark suppressing filter and printer table wiring. **Circle P42 inside back cover.**

POWER SUPPLY
priced at $100

TEKTRONIX, INC., P. O. Box 831, Portland, Oregon. Type 126 power supply furnishes the required volt-

F-l-a-s-h!...from Transistor Center, U.S.A.

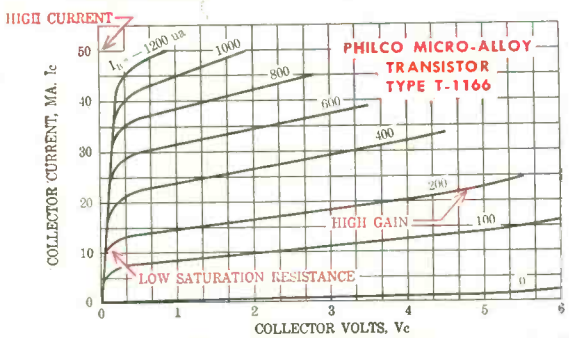


Announcing a new transistor class . . .

The PHILCO Micro-Alloy Transistor (MAT)*

CHECK THESE UNEQUALLED FEATURES

- **Excellent High Speed Switching characteristics.**
- **Low Saturation Voltage (low impedance)**
- **Excellent high frequency amplification.**
- **Excellent low-level amplifier over entire frequency range from D.C. to Megacycles.**
- **Exceptionally Long Life (hermetically sealed)**
- **Permits high speed computer design with Fewer Stages.**



...world's first production transistor with exceptionally high frequency and high gain . . . plus low saturation resistance!

This newest development from Philco Transistor Center features the characteristic high frequency response obtainable with extremely precise base width control. Designed for low voltage operation, the new MAT transistor is especially well suited for high speed applications where low saturation resistance (reduced power consumption) is necessary.

To combine high gain at high currents with high frequency response, the new MAT transistor employs a gallium doped alloy junction for the emitter electrode.

A special short-alloying cycle, combined with precise electro-chemical production techniques (pioneered and developed at Philco Transistor Center for production of SBT), results in the micro-alloy contact for exceptionally high injection efficiency. This new process assures higher gain, and permits operation at higher current. Beta linearity is excellent over the entire range of operating currents . . . up to 50 milliamperes.

● ***Write for complete information** and specifications. Make Philco your prime source of information for high frequency transistor applications.*

**Patent Applied For*

Visit The Unique Philco Transistor Display at IRE Show, New York Coliseum, March 18-21, Booth #1410, 1412, 1414.

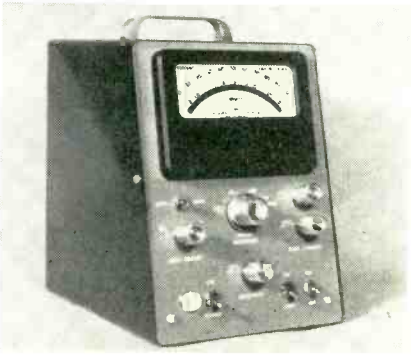
PHILCO CORPORATION

LANSDALE TUBE COMPANY DIVISION

LANSDALE, PENNSYLVANIA

ages and currents necessary to power one type 360 indicator or any one of the type 160-series waveform generators. It mounts beneath the unit to be powered and includes a cabinet to house both the type 126 and the powered unit. Combined with a type 360 indicator it makes a practical, compact slave unit for any Tektronix oscilloscope.

Output voltages are +300 v d-c, unregulated; +225 v d-c, regulated, 45 ma; +150 v d-c regulated, 5 ma; −170 v d-c, regulated, 30 ma; 6.3 v a-c, unregulated, 4 amperes. Weight is 10½ lb. **Circle P43 inside back cover.**



PHOTOMETER
features flexible operation

EL DORADO ELECTRONICS CO., 1401 Middle Harbor Rd., Oakland 20, Calif. High sensitivity and accuracy, low drift, flexibility of operation and modest cost are salient features of the PH-200 universal photomultiplier photometer. Model PH-200 incorporates a highly regulated electronic power supply. It uses no batteries and is com-

The Equation that Shook the World!

A hasty scrawl on a scrap of paper ushered in the Atomic Age. Through this equation, Dr. Albert Einstein revealed to mankind the awesome secret of atomic fission, with all of its tremendous power for good or evil.

This is the kind of a world we live in . . . a world where knowledge is power in a truer sense than ever before. It is an exciting world.

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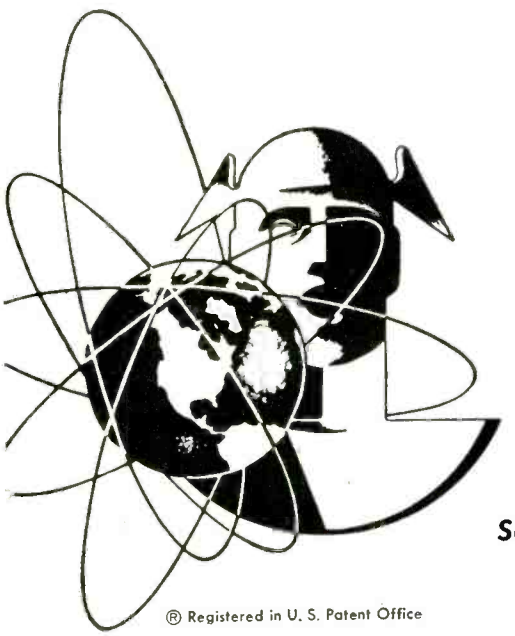
Squarely in the midst of this exciting world are the engineers and scientists of Remington Rand Univac. Their potential for growth and achievement (and the rewards that go with them) is unlimited. *You can be one of them.*



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ELECTRO-MECHANICAL ENGINEERS — Should have bachelor's degree in Engineering. However, extensive mechanical design background may substitute for some college. Men selected will do basic preliminary design and layout of small mechanisms. Requires original ideas and application of logical analysis to design problems.

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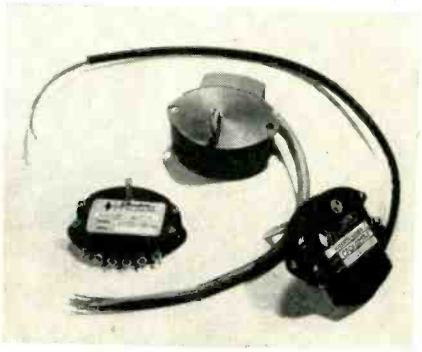
pletely self-contained and portable.

Flexibility of use is further enhanced by the provision of separate zero and dark-current adjustments as well as both decade and continuously variable sensitivity controls. These features, together with provision for oscilloscope and graphic recorder readout permit the PH-200 to be applied to a wide range of light measurement problems.

The instrument is 10 in. high, 7½ in. wide, 9 in. deep and weighs but 12 lb. **Circle P44 inside back cover.**



SECTOR POTS
accurate to 0.5 percent

HUMPHREY, INC., 2805 Canon St., San Diego 6, Calif., has introduced a new line of sector potentiometers engineered for control systems and instrumentation in aircraft and missile systems. They are models CPO1-0103-1; CPO1-0207-1, and CPO1-0204-1. They are designed to measure angles from 0 to a maximum of 90 deg of shaft rotation. Accuracy is achieved to 0.5 percent and resolution to 0.10 deg.

The instruments are of rugged, all-metal construction with high temperature insulation, capable of withstanding up to 300 F. All three models are available with shaft extension from either or both sides; also with terminals or with integral cable; singly or in dual gang units. **Circle P45 inside back cover.**

COLOR TV MONITOR
an improved design

CONRAC, INC., Glendora, Calif. The model CH21B, a new 21-in. color

New Grant 3400 *thinslide*

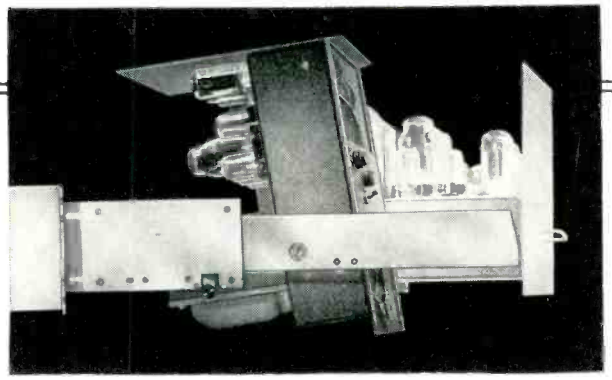
mounts standard 17" chassis in standard 18" rack or cabinets

REQUIRES ONLY 19/64" SPACE PER SIDE—

YET HAS

FULL ROLLER ACTION

(fits RETMA *rack hole spacing)*



The Grant 3400 Thinslide requires only 19/64" space per side—installs readily in standard racks and cabinets. Allows instant access to chassis measuring from 10" to 16" deep. Tilts through 100° for under-chassis servicing. Positive lock in "out" position. Lock has finger-tip release for instant return or removal of chassis. Eight hardened steel rollers carry the rated load of 100 lbs. smoothly and easily—durability insures frictionless rolling for thousands of cycles of use.

Slide mounting not only provides for quick access—it usually eliminates need for rear access doors and rear aisles—a very important saving of space.

The Grant 3400 is a versatile slide, suited for use in your *product*, in *plant equipment, prototype* and *breadboard* work, and in *production line or field test equipment.* Very moderate cost allows a wide range of applications in original equipment.

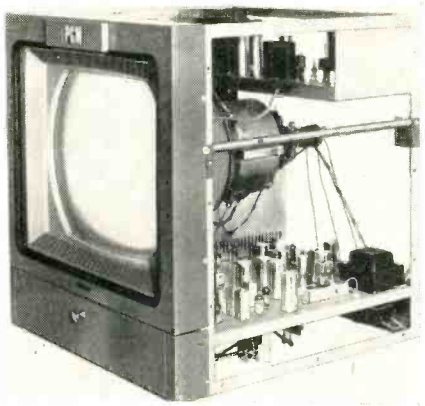
Write today for Grant 3400 Thinslide Technical Bulletin—contains full data and specifications.

Grant INDUSTRIAL SLIDES

Grant Pulley and Hardware Corporation

factories: **31-73 Whitestone Parkway, Flushing 54, N. Y.**
944 Long Beach Avenue, Los Angeles 21, Calif.

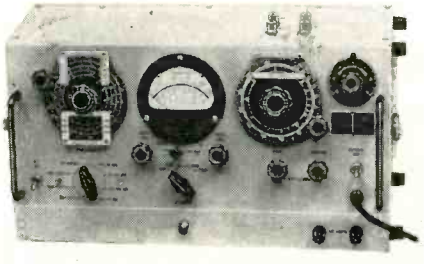
See the Grant Industrial Slide Exhibit at the I.R.E. Show, Booth 1118.



tv monitor, is a self contained unit that operates from either NTSC encoded color video signals or from simultaneous red, blue and green signals. It employs a three-gun, tricolor picture tube of the 21AXP22A type.

All operating and set-up controls, as well as a test point for Y, I, Q, R, G or B signals are accessible from the front. A switch connects the I channel to the red gun and the Q channel to the green gun so that hue and quadrature may be set without the use of an external oscilloscope. Front panel adjustment of field purity is obtained through the use of electromagnetic rim-purity coils fed from a regulated supply.

Overall size is 29 in. high, 27¾ in. wide and 26½ in. deep. Schematics, engineering data and specifications may be had from the manufacturer. **Circle P46 inside back cover.**



Q METER
has varied applications

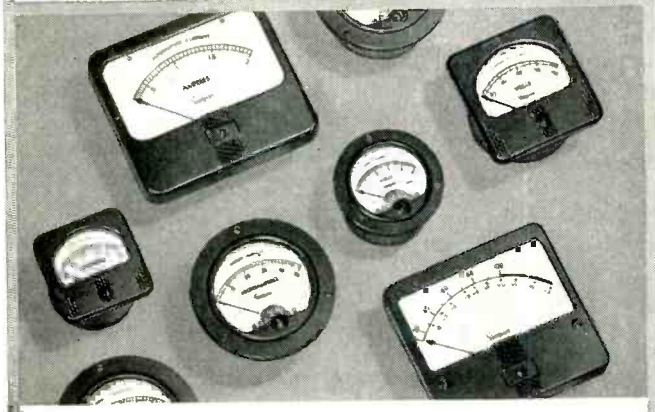
ALPHA INSTRUMENT CO., 43 Hempstead St., New London, Conn. Model 162 Q measuring instrument uses no special tubes, has no thermocouple to burn out, and it is almost impossible to damage the indicating meter with over-

why companies find it

GOOD BUSINESS

to specify panel instruments

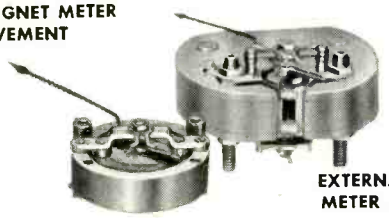
by **Simpson...**



...QUICK SERVICE from HUGE STOCKS!

Over 50,000 stock units, in 800 sizes and types, are available through 1,500 electronic distributors. Wherever you are located, Simpson instruments are obtainable promptly.

CORE MAGNET METER MOVEMENT



EXTERNAL MAGNET METER MOVEMENT

...EXACT NEEDS CUSTOM BUILT!

Many meters quickly built from *standing tools*, or designed to your exact specifications. *Firm* delivery schedules. Movements include the superb, *self shielded* Core Magnet Meter Movement.

• Simpson instruments have established a reputation for laboratory accuracy . . . yet they have the ruggedness to stand up under years of service and severe shocks. Write for new catalog.

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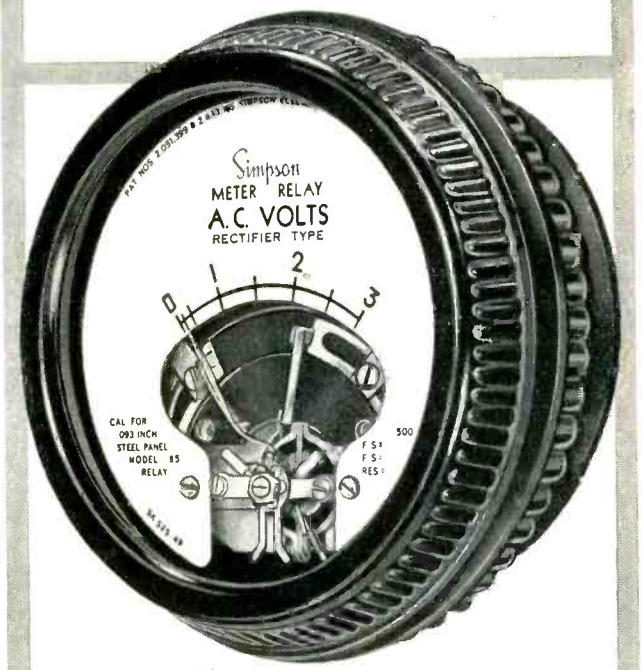
In Canada: Bach-Simpson Ltd., London, Ont.

Instruments that stay accurate

Now...a low cost, reliable

SUPERSENSITIVE RELAY



NEW! Simpson METER RELAYS

of improved design and reliability

Less than 50 Millimicrowatts Control Up to One Watt!

Here is a line of improved Meter Relays that offers lower costs, plus circuit simplification for many alarm, control, and limit setting applications. The new design features platinum alloy contacts and increased contact force which minimizes sticking and provides extreme reliability. Simpson Meter Relays are a nonlocking type, currently available in 2″ DC and 3″ AC and DC models. Write for new Technical Bulletin No. 17, today.

SIMPSON ELECTRIC CO.
5200 W. Kinzie St.
Chicago 44, Illinois
Phone: EStebrook 9-1121
In Canada:
Bach-Simpson Ltd., London, Ont.

INSTRUMENTS THAT STAY ACCURATE

Want more information? Use post card on last page.

loads, thus allowing the instrument to be used by inexperienced personnel without fear of damage. Other features are its wide frequency range of 50 kc to 75 mc, internal regulation on both 110 and 220-v operation, an injection voltage of 20 mv that is readily monitored and the use of a single indicating meter that is easily read.

Among the applications of this Q-meter are the measurement of Q of r-f coils and the determination of their effective inductance, measurement of Q of capacitors, insulating materials, coil forms and for incoming inspection and production line testing. **Circle P47 inside back cover.**

CARRIER AMPLIFIER
with 0 to 1,000 cps response

DAYTRONIC CORP., 216 S. Main St., Dayton 2, Ohio. Model 400A differential transformer amplifier is a highly stable carrier amplifier for use with all differential transformer transducers in dynamic and static measurement of motion, force, weight, pressure, acceleration and similar quantities. The demodulated output signal is suitable for cro's, null-balance recorders, galvanometer oscillograph amplifiers, vtvm's and similar devices.

An internal eight-kc oscillator provides transducer excitation. Frequency response is from 0 to 1,000 cps. Maximum sensitivity is 500 mv/0.001 in. using a typical transducer. Combined noise level and uncorrected zero drift are equivalent to 10 μ in. per hour at maximum gain. Zero set and gain controls are provided on the front panel. It is available in portable or rack mounted styles. Weight

NEW! ultra-stable FM Telemetering Discriminator*

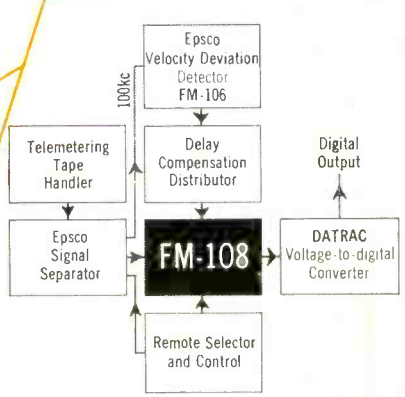
*Epsco Model FM-108 FM-to-Voltage Converter.

EPSCO'S MODEL FM-108 crystal-controlled ultra-stable, all-channel discriminator presents a new *standard of accuracy* . . . better than an order of magnitude more accurate and stable than any other commercially available equipment . . . and with absolutely *no* adjustments! This new standard of FM data processing features:

- **HIGH DYNAMIC ACCURACY:** Absolute accuracy is better than 0.05%, and the dynamic accuracy of the equipment from input to associated band-pass filter through the low-pass output filter is better than 0.2%.
- **LONG-TERM STABILITY:** 0.2% for life of equipment with no adjustments for zero drift, gain and line voltage variations, etc.
- **VERSATILITY:** Converter operates on any of 23 standard IRTWG telemetering sub-carrier frequencies from 400 cps to 70kc. Band switching may be accomplished remotely or by selector switch on front panel.
- **AUTOMATIC WOW and FLUTTER COMPENSATION:** With Epsco FM-106 Velocity Deviation Detector and Epsco CD-601 Velocity Deviation Compensation Distributor, errors from tape speed variations are reduced by a minimum of 35 db.
- **ZERO and 100% DATA CORRECTION:** Produces automatic compensation for variation of transmitting sub-carrier oscillator frequency and gain by a transistorized electro-mechanical servo feature.
- **DYNAMICALLY ACCURATE SELECTABLE LOW-PASS FILTERS:** A 5-pole filter utilizing precision wire-wound resistors and ultra-stable polystyrene capacitors in combination with chopper-stabilized d-c amplifiers provides:
  - Phase linearity deviation not exceeding 0.25 degrees over 90% of bandwidth.
  - Pass band flat within ±0.1% (0.01db) to F_c.
  - Minimum attenuation of 54 db of nearest beat frequency between sub-carrier channels.
  - A total of 62 different low-pass filter bandwidths selectable from 11 cps to 3490 cps.
- **PHYSICAL CHARACTERISTICS**

  SIZE: 10½" of space of standard 19" cabinet.
  WEIGHT: 29½ pounds.
  CONSTRUCTION: Constructed of 8 separate plug-in chassis assemblies containing electronic and magnetic components. All components are accessible on the standard layout forms.

Engineering data sheet available on request.



Epsco Model BF-601 Signal Separatnr units, each of which contains 23 band-pass filters, are available for separating the composite sub-carrier signal prior to input to FM Converter.

Complete FM telemetering receiving stations are available with or without wow and flutter compensation and zero and 100 percent correction features. Also available is the Epsco Model VCO-718 All-Channel Voltage-Controlled Oscillator for FM Discriminator calibration . . . which occupies only 3½ inches of panel space including power supply.

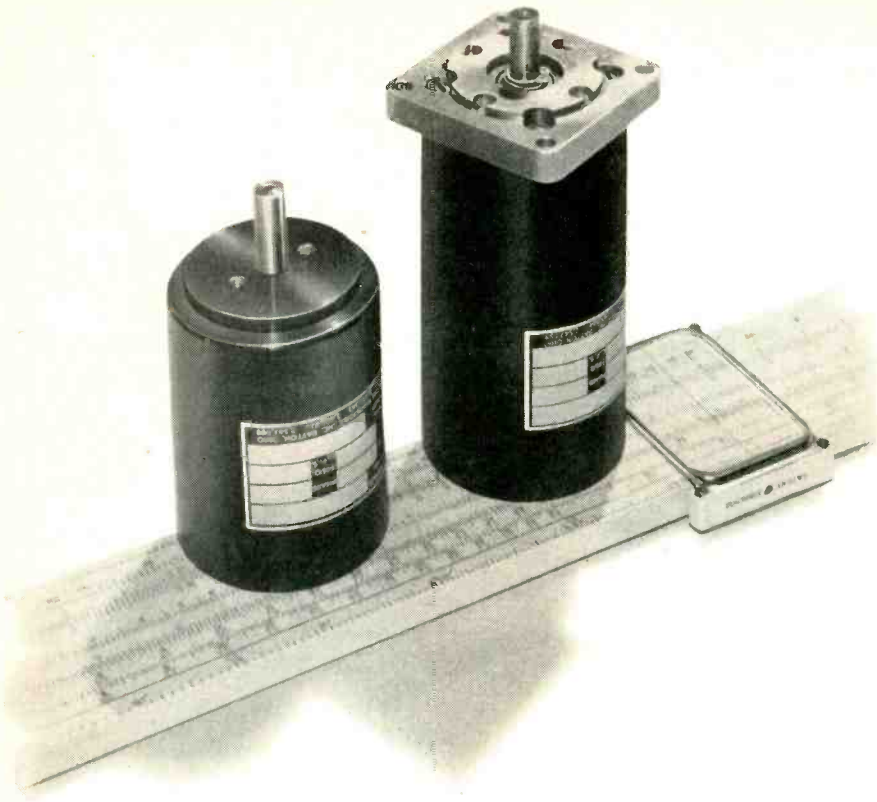
In the West, contact:
Epsco Service Corporation of California
1722 Westwood Boulevard
Los Angeles 24, California

Epsco incorporated

588 COMMONWEALTH AVE., BOSTON 15, MASSACHUSETTS

Want more information? Use post card on last page.

is 13 lb. **Circle P48 inside back cover.**



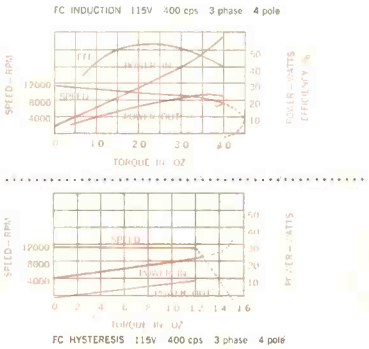
NEW A. C. MOTOR LINE GIVES YOU 10^5 STANDARD VARIATIONS

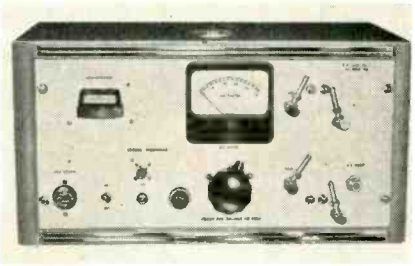
From Globe you can get fast delivery of complete miniature power systems designed around new FC motors—115 or 200 V.A.C., 60 or 400 cycles—induction, hysteresis, or dual speed rotors, wound 3 phase, 2 pole or 4 pole; 2 phase, 2 pole or 6 pole; single phase with a matched capacitor. Units are designed to meet MIL specs; operating characteristics and configuration can be modified.

Package can include integral gearing, either planetary or spur. Choose from 102 standard ratios from 4:1 to 3,000,000:1. Choose from 408 standard speeds. Gear units range in length from 1.043" to 1.953". WRITE FOR FC BULLETINS.

Globe's small AC motor packages are built around units 1.07" dia., 1.25" dia., and the newest 1.675" dia. x 2.250" long. Standard modifications in type, winding, gearing, and performance offer you millions of combinations at reasonable cost. Globe also makes D.C. governed and gear reduced motors, servo motors, actuators, timers, generators, gyros, blowers, fans, and control systems.

GLOBE INDUSTRIES, INC.
Dayton 4, Ohio

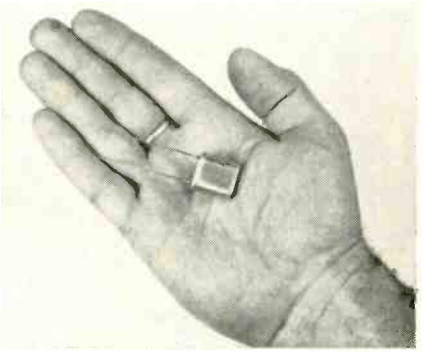




CALORIMETER BRIDGE
continuously self-calibrated

ELECTRO - IMPULSE LABORATORY, INC., 208 River St., Red Bank, N. J., announces a new direct reading calorimeter bridge with frequency range of d-c to 4,000 mc (coaxial) and 1,000 to 12,000 mc (waveguide). It is continuously self-calibrated by an auxiliary a-c standard load and an a-c wattmeter. The vswr of the r-f load resistor is less than 1.25, up to 4,000 mc. Total error in power measurement is less than five percent. Accuracy can be increased by calibrating the instrument against an accurate laboratory type a-c wattmeter.

Power range is 10 to 150 w, 10 to 500 w, and 100 to 5,000 w. Power supply is 115 v, 60 cps, single phase, 250 w. Descriptive literature is available. **Circle P49 inside back cover.**



SNAP-ACTING THERMOSTAT
highly shock resistant

METALS & CONTROLS CORP., Attleboro, Mass., presents a new Klixon snap-acting, disk-type thermostat for applications where maximum shock and vibration resistance are required. These controls feature the Spencer disk thermal element,

TREPAC® MODEL 530

TELEPRINTER RELAY ELIMINATOR PACKAGE

ATTENTION: TELEPRINTER USERS

NOW FOR AS LITTLE AS $39.85 YOU CAN ELIMINATE YOUR

- LINE RELAY • RECTIFIER
- CURRENT LIMITING RESISTORS
- SPARK SUPRESSING FILTER
- PRINTER TABLE WIRING

The Model 530 Trepac is a fairly simple plug-in electronic device composed basically of a silicon-diode power-transistor switch and full wave rectifier circuit. It is powered directly from the 115 Volt AC, 50/60 cycle line.
Normally it is installed within the housing of the teletypewriter machine where its use obviates the need for a line relay and power supply and simplifies the wiring of the printer table and base.
As a static unit having no moving parts, the Trepac requires no adjustment and is, for all practical purposes, maintenance-free. The useful life of this unit will greatly exceed the life of any relay currently on the market.

SUPERIOR PERFORMANCE — REDUCED MAINTENANCE

THE OLD WAY

Teleprinter users have for some years inserted the selector magnet of their printers directly in the incoming signal loop. This has proved troublesome, since the inductive kick of the printer magnet is induced back into the receiving line disturbing other equipment on the loop.
This inductance causes wear on the transmitting contacts, and will in many cases intolerably restrict the range limits of the monitor printer equipment. The inductive overshoot makes it difficult to obtain true distortion test readings and confuses oscilloscope observations.

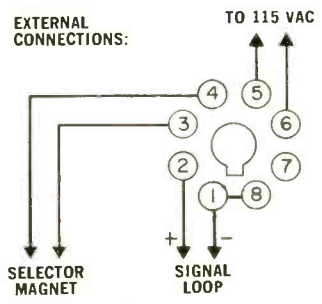
AN IMPROVED WAY

Some improvements in teleprinter performance have been obtained by substituting holding type selector magnets for the older pulling type magnets. Improvement can also be obtained by connecting the holding type magnets in parallel to reduce the overall inductance. Even with these improvements, teletypewriter users generally have found it necessary to interpose a relay to repeat the signal and block the inductive feedback.
The use of relays, however, produces many other difficulties. The relay coil is itself inductive and the large inductive kick of the selector magnet is present on the relay contacts producing arcing, sparking and wear. The use of a relay, with its many troubles, has resulted in a maintenance problem which has plagued the industry. Distortion introduced by a relay is rarely less than 2% even with new, properly adjusted relays, and the bias current requires adjustment whenever the loop current changes.

THE NEW WAY

By using the Model 530 Trepac, the advantages of a relay are gained without accruing any of its numerous disadvantages. The Trepac has an almost pure resistive input, and accordingly gives ideal isolation between the printer loop and the printer selector magnet. It maintains true and accurate repeating of the telegraph signal.
A Trepac will operate with either 20 or 60 ma. signal loop input (polar or neutral keying of either polarity). The output current to the selector magnet is nominally 60 ma. and is insignificantly changed for large variations in the input signal loop current. The distortion is always negligible.
The resistive input and the isolated output characteristics make it possible to insert as many as 15 Trepac equipped monitor printers in one signal loop without any one printer affecting the range limits of any other printer. The life of the transmitting device (contacts or vacuum tubes) is greatly lengthened as a result of the removal of inductance from the signal loop. This reduction of L:R ratio also makes feasible the operation of Trepac-equipped printers from a low voltage battery applied to the signal loop.

SPECIFICATIONS



(See Bulletin 530B for bracket and cable assemblies available for installation of Model 530 Trepacs)

INPUT: Pins 1 & 8 connected: 45 to 100 ma, 195 ohms (resistive). 1 & 8 not connected: 15 to 40 ma, 560 ohms (resistive). Polar or neutral keying (either polarity). 9 VDC min. loop supply.

OUTPUT: 55-70 ma into 210/177/44 ohms inductive. Drives pulling or holding magnets (series or parallel connected). Neutral on-off output current constant over above range of input currents.

POWER: 105-125 VAC, 50/60 cps, instant warm-up. May be connected to printer motor switch to stop relay action when motor is off.

PHYSICAL: Steel can with side ventilators. $3\frac{1}{16}$"W x $2\frac{1}{16}$"D x $4\frac{1}{4}$"H seated. Weight: 19 ounces. Mounting: 4 studs $\frac{8}{32}$ by $\frac{1}{2}$" on $2\frac{3}{8}$" x 2" centers. Finish: Baked Hammertone Gray.

TEMPERATURE: 20 to 130°F. Tests reveal that temperature within a printer near the line relay is generally 101 to 107°F. This area is specified for mounting of the Trepac.

KEYING SPEED: Capable of operating well into kilocycle range. Limited only by speed of selector magnet (125 wpm).

DISTORTION: Negligible (under 1%). No distortion introduced by varying loop current.

SPECIAL FEATURES: Units will deliver STEADY MARK current (nominally 60 ma) regardless of input keying state when pin 7 is tied to pin 3 on mating socket. This is extremely useful for: (1) use of the Trepac as a rectifier to provide 60 ma loop current, and (2) testing and maintenance of the teleprinter (without printer running open) when it is not desirable to interrupt the signal loop. All connections are isolated from the chassis. Trepacs are designed to withstand the shock and vibration normally present in teleprinters. Protection against dust, grease, moisture and fungus is provided by a fungicide chemical coating on all components in the Trepac.

ONE YEAR WARRANTY: Defective units will be replaced, provided they have not been tampered with and have been used for their specified purpose within the above ratings. Trepacs returned to Alcor should be accompanied with a report of their trouble.

QUANTITY—UNIT PRICE—DELIVERY

2-24	$39.85	stock
25-99	38.50	1 week
100-249	37.25	1-2 weeks
250-999	36.00	2-6 weeks
1000-2499	34.85	6-10 weeks

FOB: New York, N.Y.
Terms: ½%-10, net-30

alcor

ALCOR ELECTRONICS CORPORATION
180 LAFAYETTE STREET • NEW YORK 13, N.Y.

fine silver electrical contacts, and a complete hermetically sealed assembly. A copper-nickel plated steel casing protects all parts from contamination and moisture to assure precise circuit operation. Application is especially recommended in aircraft controls and guided missiles. A wide range of possibilities also exists in electronic circuits and components and servomechanisms.

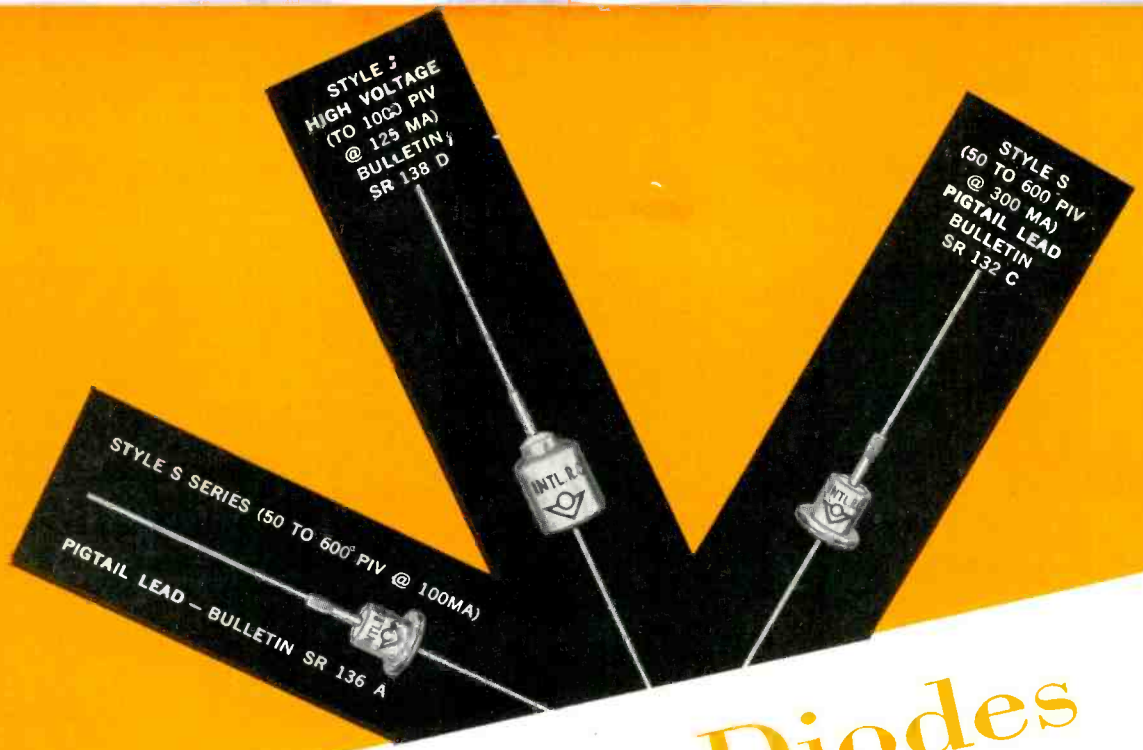
The C7216 thermostat is specially plated for corrosion resistance. Its miniature size suggests its suitability where space and weight accommodations are limited. Standard temperature settings which are fixed, range from −20 F to 400 F. It is available with No. 20 copper wire leads. **Circle P50 inside back cover.**

SERVO ACTUATOR
for airborne applications

WHITE-RODGERS ELECTRIC CO., 4407 Cook St., St. Louis 13, Mo., has developed a D-9 p-m type rotary servo actuator for airborne applications. It is designed for continuous operation at an output rating of 70 in.-lb at 8.5 rpm. Theoretical acceleration at stall is 40,000 radian/sec² and dynamic motor braking is incorporated. The unit has a weight of 1.9 lb, diameter of 3 5/16 in. and an overall length of 4⅞ in., including the AN connector.

The unit features limit and centering switches and a potentiometer for feedback of position information. The servo meets applicable military specifications including MIL-E-5272A and MIL-

See "CAVALCADE OF ELECTRONICS" I.R.E. Show, Booths 3806-3808



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for high reliability over a wide temperature range

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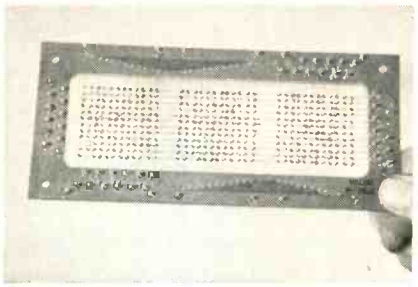
THE WORLD'S LARGEST SUPPLIER OF INDUSTRIAL METALLIC RECTIFIERS

I-6181B. **Circle P51 inside back cover.**



MAGNETIC STORAGE
multiple matrix type

VALOR ELECTRONIC COMPONENTS Co., 5808 Marilyn Ave., Culver City, Calif. Illustrated is a multiple magnetic storage matrix built so all respective X and Y lines are connected in series through each of the separate matrices, but makes available separate sense and inhibit lines for each of the three. This construction offers economy in installation of a matrix store as well as in space required.

Ordinarily a 144-word, 15 digit-per-word storage system would require fifteen 12 by 12 conventional matrices having 28 sets of interconnecting lines. Using the 12 by 12 by 3 matrix shown, only five planes would be required, and it would be necessary to interconnect only eight sets of lines.

The multiple matrix construction is readily adapted to matrices of up to 16 by 16, and as such will find wide use in small computers, as well as buffer storage systems. **Circle P52 inside back cover.**

SYNCHROS
to military standards

NORDEN-KETAY CORP., Commerce Road, Stamford, Conn. The new 3-minute size 23 synchros meet all performance requirements and provide at least twice the accuracy specified in FXS 1066, Rev. 4, MIL-S-16892 (Bu Ord) and MIL-S-12472 (Ord.). They are especially valuable in airborne applications requiring accuracy with minimum bulk and weight.

The units are engineered to en-

DU PONT
Better Things for Better Living
. . . through Chemistry

ELECTRONIC DESIGN NEWS
LATEST PROPERTY AND APPLICATION DATA ON
TEFLON® tetrafluoroethylene resin

Du Pont TEFLON® resists temperature extremes in electronic aircraft equipment

Lead-through bushings of TEFLON® feature hermetic sealing

LEAD - THROUGH BUSHINGS made with Du Pont TEFLON have excellent corona, arc and ohmic resistance . . . are hermetically sealed against gases, vapors, liquids. (Manufactured by the Joclin Manufacturing Company, North Haven, Connecticut.)

Sensitive tests with the mass spectrometer have proven that gases, conventional insulating oils, silicone oils and their vapors cannot penetrate through connectors using TEFLON tetrafluoroethylene resin as their dielectric. The bushings maintain their seal when cycled repeatedly over a temperature range from −85° F. to +302° F.

In addition, the connectors are resistant to shock. The specially prepared insulators of TEFLON provide mechanical resilience not possible with the usual rigid construction. The moisture-repellent qualities of TEFLON make it possible to use the bushings under the most adverse conditions of humidity. They conform to the applicable sections of Specification MIL-E-5272A.

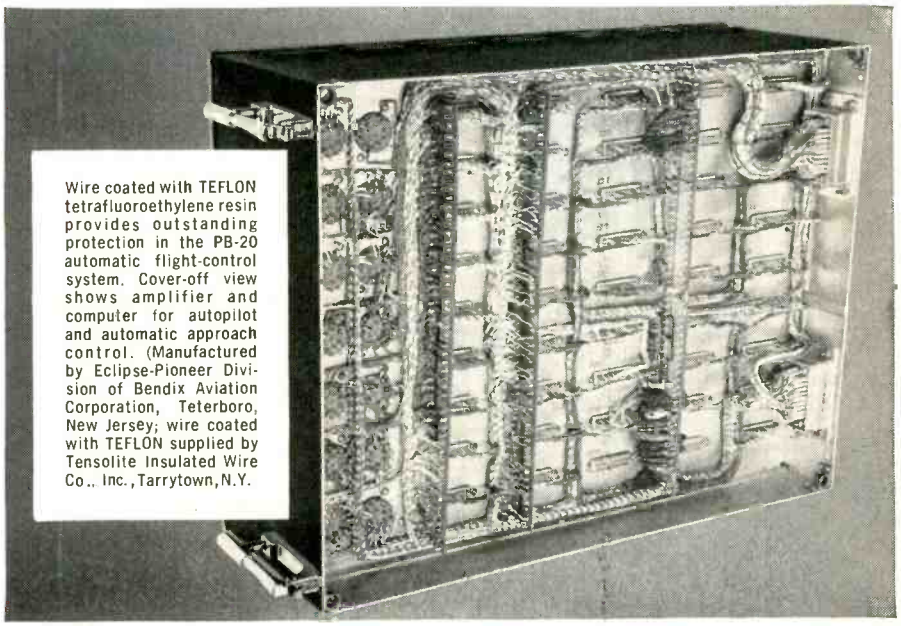
Where components are subjected to a wide range of temperature, pressure, humidity and mechanical shock and vibration, Du Pont TEFLON provides outstanding performance. In your designs, too, components of TEFLON may well be the decisive factor in meeting acceptance standards.

Wire insulated with TEFLON is used in new transistorized flight-control system

The transistorized PB-20 is the latest development in the field of automatic flight-control equipment. It has been specified for use in many advanced aircraft, such as the Boeing 707 jet transport. The PB-20 depends extensively on wire coated with TEFLON for reliable operation.

Tough and durable TEFLON can be used up to 500° F. and displays excellent properties at sub-zero temperatures. Thin-walled coatings on wire will not burn, melt or decompose when connections next to it are soldered. The dielectric strength and arc resistance of TEFLON are excellent. Its dissipation factor of less than 0.0003 from 60 cycles to 3,000 megacycles assures low losses in high-frequency communications equipment. Very few chemicals exist which can injure TEFLON . . . it is not affected by aircraft fuels, lubricants or solvents. It is inert to fungus, rot and mildew and will not absorb moisture. Articles of Du Pont TEFLON will meet the requirements of many military specifications relative to jet-aircraft applications.

You can meet the increasing demands for extreme temperature range, higher frequencies, higher voltages and greater resistance to corrosive environments by specifying TEFLON. Find out now how TEFLON can improve your products.



Wire coated with TEFLON tetrafluoroethylene resin provides outstanding protection in the PB-20 automatic flight-control system. Cover-off view shows amplifier and computer for autopilot and automatic approach control. (Manufactured by Eclipse-Pioneer Division of Bendix Aviation Corporation, Teterboro, New Jersey; wire coated with TEFLON supplied by Tensolite Insulated Wire Co., Inc., Tarrytown, N.Y.

TEFLON®
is a registered trademark...

TEFLON is the registered trademark for Du Pont tetrafluoroethylene resin, and should not be used as an adjective to describe any other product or any component part; nor may this registered trademark be used in whole, or in part, as a trade name for any product.

SEND FOR INFORMATION

For additional property and application data on Du Pont TEFLON tetrafluoroethylene resin, mail this coupon.

E. I. du Pont de Nemours & Co. (Inc.), Polychemicals Dept.
Room 173, Du Pont Building, Wilmington 98, Delaware

Please send me more information on Du Pont TEFLON tetrafluoroethylene resin. I am interested in evaluating these materials for_____

Name_____

Company_____ Position_____

Street_____

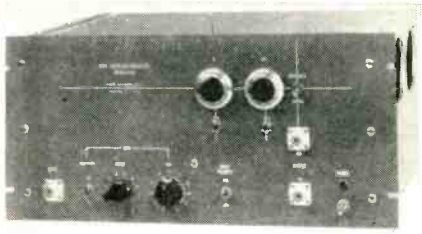
City_____ State_____

Type of Business_____

In Canada: Du Pont Company of Canada (1956) Limited, P. O. Box 660, Montreal, Quebec

able design engineers to increase the accuracy in their control and data transmission systems and servomechanisms. In many instances, three-minute synchros eliminate the need for two-speed synchro systems, thereby reducing cost and effecting economies in weight, size, complexity and gearing problems. Matched pairs of synchros are available to provide even greater system accuracy.

Bulletin No. 409 gives specifications, outline drawings and ordering information. **Circle P53 inside back cover.**



NONOVERLOAD AMPLIFIER
and single channel analyzer

HAMNER ELECTRONICS CO., INC., P. O. Box 531, Princeton, N. J., has developed the model N-302, a stable, nonoverload pulse amplifier together with a precision single channel analyzer—all on one standard sized chassis. The amplifier, which employs delay-line clipping and long-tailed pairs with feedback, has good stability, short risetime and excellent overload characteristics. Overloads as large as a factor of 100 are handled easily. The pulse height selector is of advanced design and provides short time resolution, high base

FROM ALL DIRECTIONS . . .

from Virginia *from New Jersey* *from Oklahoma* *from Pennsylvania* *from Indiana* *from Washington, D. C.*

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Supervisory Engineer
Virginia Polytechnic Institute

Frank H. Tyaack
Supervisory Engineer
Massachusetts Institute of Technology

James L. Van Meter
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Washington State College

John Michael Bentley
Senior Engineer
William & Mary College
Virginia Polytechnic Institute
Syracuse University

Robert C. Jones
Design Engineer
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Leo E. Wilson
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Carnegie Institute of Technology

CAREER ENGINEERS ARE COMING TO BALTIMORE TO JOIN THE LEADERS AT WESTINGHOUSE-BALTIMORE

Today's electronic pioneers are reversing the maxim of Horace Greeley to "go West young man." They're coming East, but, they're going Westinghouse . . . and building their careers at Westinghouse-Baltimore. Here, the frontiers of tomorrow's electronic developments are being charted—and here, the young engineer can assure himself rapid professional growth with a company that respects and rewards its engineers. Wherever you are located—whatever school you attended—whatever your engineering experience and ability—you owe it to yourself to investigate the opportunities open to you at Westinghouse-Baltimore. Find out why so many of your fellow engineers have come to Baltimore to join the leaders in the electronics field. Write that letter today—and get the facts. You have nothing to lose—and a great future to gain.

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ELECTRONIC TRANSFORMER ENGINEERS—Design and development of audio, i-f and r-f coils, flea-power to 600 x 10^6 v-a, frequencies up to 1000 MC, both linear and saturable, involving problems of balance, shielding, bandwidth, insulation, heat transfer, wave shape, efficiency and regulation.

SALARY—TO $9,100.00

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"An Engineer's Company"

Since 1886

line and window stability and low rate dependence. Information on price and specifications is available. **Circle P54 inside back cover.**

TIME DELAY RELAY
for industry and military

G. C. WILSON & Co., 1915 Eighth Ave., Huntington, W. Va., has available an electronic time delay relay requiring no warm-up and consuming as little as one watt. The hermetically sealed unit was developed for military equipment and is used in guided missile, aircraft and other applications having rigid specifications.

Cold cathode tubes unaffected by vibration are employed in a patented circuit to provide accurate delays down to 3 milliseconds and up to 30 seconds. Designated type EHS, the timer is 2 by 2¼ by 3⅛ in. and weighs nine oz. **Circle P55 inside back cover.**

SWEEP OSCILLATOR
covers 5 to 5,000 cps

DYNAC, INC., 395 Page Mill Road, Palo Alto, Calif. The DY-2200 sweep oscillator covers the 5 to

Direct line solution to your closure problems!

COPPER

BRASS

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MU METAL

STEEL

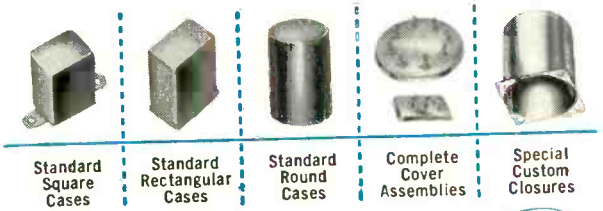
STAINLESS STEEL

MArket 3-7584

A complete solution to your closure problem is as near as your telephone! Chances are, Hudson can supply an economical standard stock item, from factory stocks, that will meet your requirements exactly. Where specifications call for unusual designs, Hudson can produce precision-drawn custom closures to meet your assembly line schedules.

Hudson standard and special closures are available with complete cover assemblies if desired. Quotations on sub-assemblies, including certified spot welding and silver soldering will be supplied promptly on receipt of your drawings and data.

Write or phone for a copy of the Hudson catalog on standard precision-drawn cases and covers



Standard Square Cases | Standard Rectangular Cases | Standard Round Cases | Complete Cover Assemblies | Special Custom Closures

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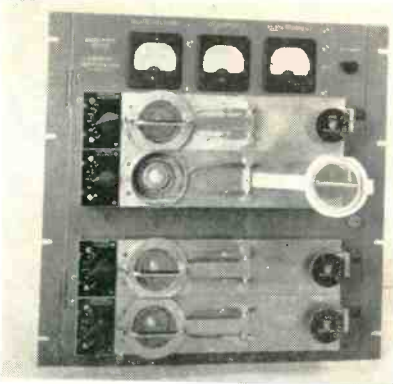
See us at the I.R.E. Show! Booths 4106-4108

5,000 cps frequency range in one continuous band. This single band eliminates range changing, switching transients and dial discontinuities. It requires no zero setting. The large, easily-read dial is calibrated to a true log scale from 50 to 5,000 cps.

To provide for attachment of mechanical sweeping components and other auxiliary equipment, the DY-2200 tuning shaft extends beyond the rear of the cabinet. The instrument is available in standard rack-panel mounting or in a compact, portable cabinet. **Circle P56 inside back cover.**



CAVITY AMPLIFIER
using 4X150A tetrode

AMTRON CORP., 17 Felton St., Waltham 54, Mass., has announced a new uhf coaxial cavity amplifier using the 4X150A tetrode. This is a unique electrical design which permits the use of standard tuning capacitors. Access for tube replacement is provided by an interlocked door in the front panel.

The illustration shows a four-stage linear amplifier tuning from 300 to 400 mc, with overall gain of 50 db. Other models are suitable for lower frequencies. **Circle P57 inside back cover.**

SEALED THERMOSTAT
miniature, snap action type

VALVERDE LABORATORIES 252 Lafayette St., New York 12, N. Y. Reliability has been built into the design and assembly of the VAL 90 miniature snap action, precision set, sealed thermostat. The setting tolerance is ± 3 F or better and the differential is only

new Formica

See it at the IRE Show

Formica booths 4040-1

CIRPRINT©

TV - Radio - Phonograph and other electrical/electronic product manufacturers can benefit from Cirprint, the first copper clad laminated plastics ever to offer exactly the right combination of properties for this application. If you're a large volume consumer of circuitry, it will pay you to check Cirprint today.

Exceeds NEMA standards for XXP . . . meets MIL-P-3115B spec for type PBE-P

New Formica Cirprint is far superior to any XXP ever made. The latest product of Formica-4 research, it is the first and only copper clad especially designed to meet the requirements of large volume manufacturers:

High IR: 250,000 megohms after 96 hours at 35°C and 90% relative humidity.

Cold punching: up to and including 1/16".

Low moisture absorption: 0.80% in 1"x3"x1/16" sample after 24 hours immersion.

You can *see* the quality because Cirprint is translucent. Its smooth structure is free of all impurities. Cirprint is also watermarked for your protection.

Evaluate the contribution Cirprint can make to your products. Check it "in person" at Formica's IRE booths 4040-1 – or mail coupon below for free bulletin 755. Formica Corporation, subsidiary of American Cyanamid, 4530-7 Spring Grove Ave., Cincinnati 32, Ohio.

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FORMICA 4

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- Research
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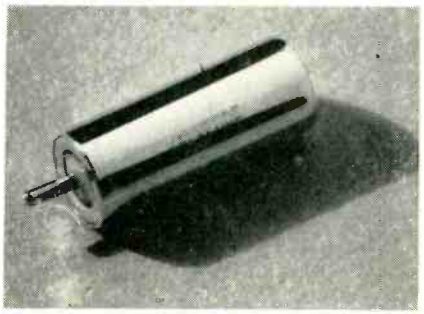

3 F or better. This positive differential, instead of the chatter of the creep type, has several advantages. Commutation is of the best. High g does not cause chatter; contacts are either ON or OFF.

The differential cycle takes a minute or more, totalling about a half million cycles a year compared to over three million cycles for the creep type thermostat if it lasts that long. New degassing techniques before sealing have proven out in practice where reliability is a must. **Circle P58 inside back cover.**

STEPPING SYNCHRO
fits many applications

G. M. GIANNINI & CO., INC., 918 East Green St., Pasadena 1, Calif., has developed a 1-deg stepping synchro. Utilizing an electromechanical positioner to drive the rotor of a differential synchro in fixed increments of 1 deg, these instruments produce an a-c output that is synchronous with rotor position. Rotation of the mechanism is unlimited in both directions, and is operated by an electrical input pulse at any speed up to 60 deg per sec.

Model 89161A-1 stepping synchros have integrated into their design the versatile Rotostepper. Shaft output of the Rotostepper

A Touch here does so much

LIGHT UP... SPUTTER OUT...

A touch of 'Aquadag'® between the electrodes of fluorescent tubes makes sputter a thing of the past, greatly increases lamp life and boosts luminosity.

'Aquadag' acts as a "printed" resistor lowering screen-grid potentials so that electrons are repelled and their narrowed beam focussed on the electrode shell. The electric arc occurs behind the shell, dispersing its heat throughout the length of the shell. Lamps last three times as long and give 100% luminosity throughout their life. 'Aquadag', a colloidal dispersion of graphite in water, replaces silver and platinum which not only are more expensive but so conductive that they soon burn out. 'Aquadag' can be painted on, a faster and more economical method than the soldering of wire.

'dag'® dispersions of colloidal graphite also have good electrical conductivity, are low in photo-electric sensitivity and resistant to electron bombardment.

An Acheson Service Engineer will gladly discuss the many uses for 'dag' colloidal dispersions in electrical and electronic applications. Write for Bulletin No. 433 "Electronic and Electrical Applications." Address Dept. E-3.

dag®

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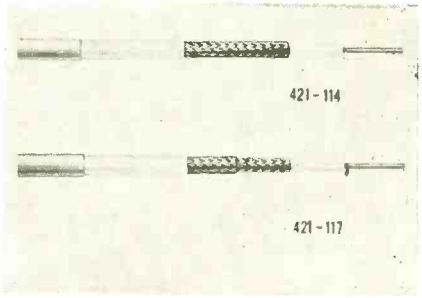
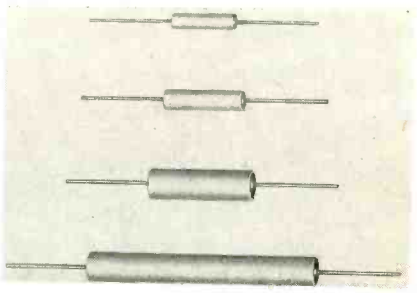
is adapted to accurately position the rotor of the precision differential synchro. The unit will fit a multitude of applications such as often found in complex directional or guidance systems where the need exists for servo actuation in precise increments of rotation. **Circle P59 inside back cover.**



TEFLON CABLES
with nonmagnetic conductors

AMPHENOL ELECTRONIC CORP., Chicago 50, Ill. Types 421-114 and 421-117 coaxial cables are the result of a new Teflon extrusion technique in which the Teflon dielectric is extruded over stranded nonmagnetic silver-plated copper wire. Formerly, only copperweld wire could be used in Teflon extrusion. The new cables are being utilized by several manufacturers where both high temperature and nonmagnetic qualities are desirable. **Circle P60 inside back cover.**



PRECISION RESISTOR
carbon film type

CONTINENTAL CARBON, Division of Wirt Co., 13900 Lorain Ave., Cleveland 11, Ohio. A new precision resistor is recommended for use in test equipment, meters and h-f circuits. New type construction features a layer of pure carbon deposited on a ceramic rod. Silver plated end-caps are expansion

Forethought costs less than Afterthought so . . .

Design These in When you Begin!

Series 1370 High Speed Counter (1500 to 2500 rpm) built into a wide variety of equipment.

If you need mechanical or electrical counters in any of your new products, here's a word to the cost-wise designer: *Design them in, when you begin . . . don't tack them on later.*

For if you'll give us a chance to work with you, right from the beginning, chances are we can save you time and money by adapting or modifying a *standard* Veeder-Root Counter to your needs . . where you might get into a costly special job if you went about it alone. What's more, you save time in your engineering, purchasing and assembly departments.

Count on Veeder-Root to help you in every way . . . from design to delivery. Write:

Everyone . . . Can Count on Veeder-Root

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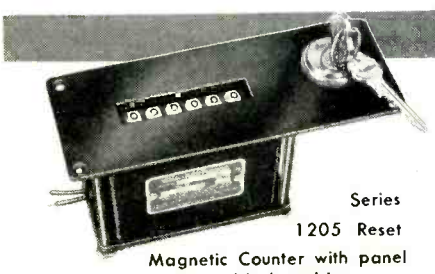
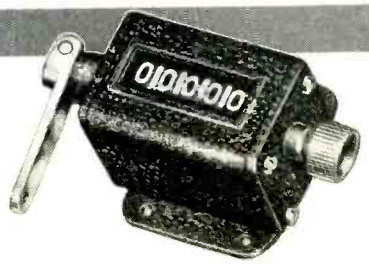
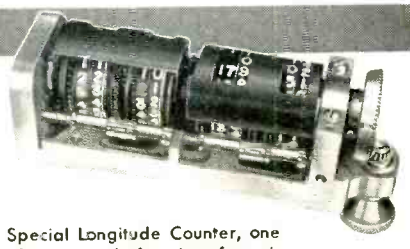


Series 1205 Reset Magnetic Counter with panel mount and lock and key.



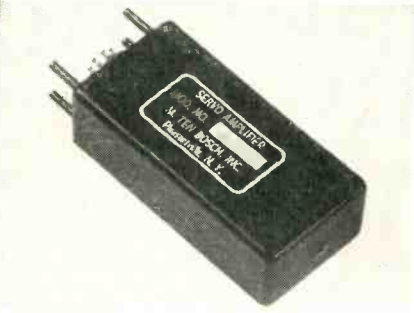
Series 1122 Small Reset Ratchet Counter.



Special Longitude Counter, one of many made for aircraft navigational equipment.

fitted for positive contact and the unit is encased in a nonhydroscopic ceramic tube and hermetically sealed with high temperature solder for improved stability characteristics. They are fully insulated and suited for snap-in component clips.

The resistors conform to MIL-R-10509B specifications and are furnished in standard tolerance of ± 1 percent. Tolerances of ±2 percent and ±5 percent are available on special order. These resistors are furnished in ¼, ½, one and two-w sizes and each unit is marked with resistance, tolerance and manufacturing information. **Circle P61 inside back cover.**



SERVO AMPLIFIER
a transistorized device

M. TEN BOSCH, INC., Pleasantville, N. Y. Model 1800-0700 is a miniaturized, hermetically-sealed, plug-in transistor servo amplifier. It is primarily intended to receive signals from a synchro control transformer and to operate a size 15, 60-cycle, 6.1-w servo motor or equivalent. Input impedance is 10,000 ohms (nominal). Typical voltage gain is 550 at two-watts output. The amplifier is designed to meet the environmental requirements of specification MIL-E-5400. **Circle P62 inside back cover.**

PLASTIC LAMINATES
used in printed circuits

GENERAL ELECTRIC CO., Coschocton, Ohio, has introduced a new, high-insulation resistant plastic laminate designed particularly for printed circuit applications. Textolite cold punch 11572 is a low-cost, paper-base laminate recommended for electronic applications using high voltage at radio fre-

Westinghouse **IGNITRON TUBES** still the industry standard.

Westinghouse invented the Ignitron tube and has maintained a record of improvements that are today the accepted industry standards:

- kovar seals to permit use of steel envelopes • improved ignitors to assure accurate ignition.
- thermostatic control for overload protection and water savings.

For highest quality Industrial and Special Purpose tubes—always specify Westinghouse.

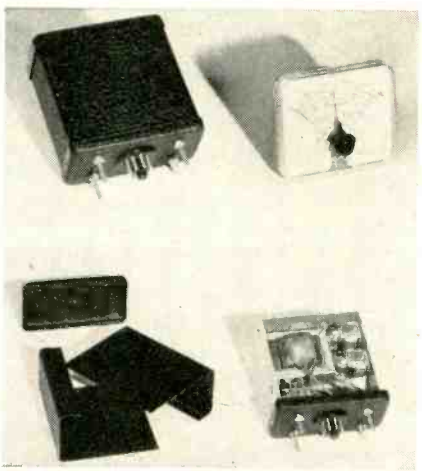
YOU CAN BE SURE...IF IT'S Westinghouse

7ET-4103

quencies. It is available with one or two-oz copper on one or both sides or in the unclad form.

The laminate can withstand exposure to common degreasing solvents used in printed circuit processes. Exposure to trichloroethylene vapors for 15 minutes produces no harmful effects.

The cold fabricating quality of Textolite 11572 elminates dimensional changes resulting from the combination of heat and punching tresses. It punches cleanly at normal room temperatures, in thicknesses up to $\frac{1}{8}$ in. Other significant features include high flexural strength, low power factor, high heat resistance and low moisture absorption. **Circle P63 inside back cover.**



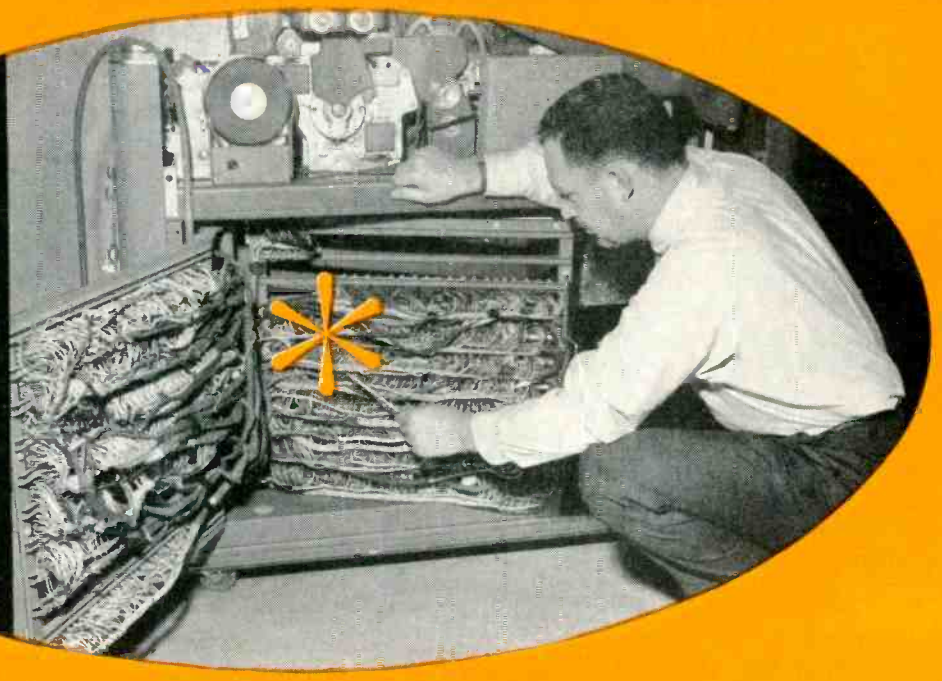
CONTROL PACK
miniaturized, plug-in unit

TIPP-TRONIC, INC., Tipp City, Ohio, has announced a miniaturized plug-in control pack, containing all the basic control circuitry needed for use with contact meter-relays. Because it is unitized, the control pack increases the flexibility with which meter-relays may be designed into original equipment. The pack measures approximately 4 by 2 by 4 in.

Standard minimum parts include an isolation transformer, a d-c power supply (including rectifiers) and slave relays to provide 5-ampere a-c, 115-v contacts. Frequently an interrupter or sampling circuit is also included.

The unit plugs into standard 11-pin octal type sockets. Four mounting studs provide additional

NO CHANCE FOR ERROR



* if conductors are branded with Turbo identification markers!

Positive identification . . . is sure and easy when Turbo identification markers code your circuits, wiring, cable or connections. You're assured of an efficient low-cost operation wherever a multiplicity of electrical operations must be performed with speed and accuracy. They just slip on, yet fit so snugly they will not slide from position.

Permanent identification . . . special inks used in the manufacturing of Turbo Identification Markers provide permanent legibility resisting the effect of high and low temperature, abrasion, chemical action and humidity. Markers are manufactured from Turbo varnished cambric tubing and Turbo extruded plastic tubing and meet all applicable Army, Navy and Air Force specifications.

Merchandise your product . . . with Turbo Markers your trade mark or whatever imprint you want can be applied longitudinally or circumferentially in a variety of colors. Anything that can be drawn, in fact, can be printed. Use them to code component parts or to brand any wire, cable, tube, rod, pipe or hose.

Available . . . in all standard sizes from No. 14 to 1½" I.D. in lengths from ⅜" to 4". Longer lengths or special non-standard sizes or colors furnished upon request. Write for samples.

Permanent identification — available in a wide range of sizes and colors

WILLIAM BRAND
AND COMPANY, INCORPORATED
WILLIMANTIC CONNECTICUT

QUALITY ELECTRICAL AND ELECTRONIC WIRE AND TUBING SINCE 1920

Be sure to visit the William Brand Suite at the Plaza Hotel, New York, during the I.R.E. show March 18-20.

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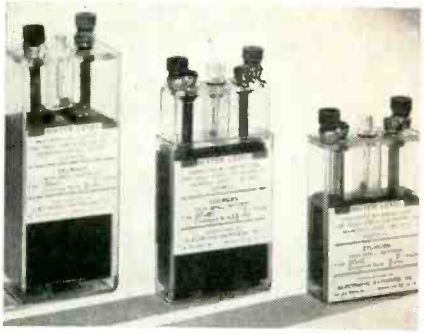
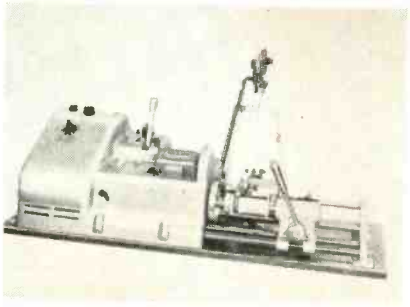
mechanical support. **Circle P64 inside back cover.**



NONSPILL BATTERIES
for portable power

ELECTRONIC BATTERIES, INC., 28-34 35th St., Brooklyn 32, N. Y. Sturges light-weight and ruggedly constructed nonspill storage batteries are assembled from two-volt cells in transparent plastic cases which afford visual inspection of the cells at all times. The bodies of the cases are entirely seamless and the tops or covers are cemented to the bodies forming homogeneous leak-proof nonspill units. The low internal resistance and completely free circulation of the electrolyte in the batteries assures an average output of 13½ watt hours per pound of battery. They have a cycle life of 100 cycles of charge and discharge varying with service conditions.

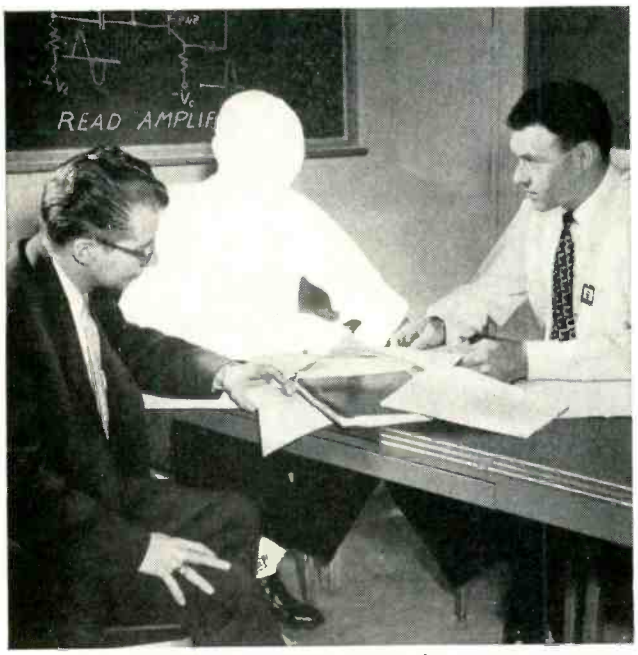
These batteries are now being used in the electronic, aviation, sound recording, television, research laboratory and radio communication fields. Literature is available. **Circle P65 inside back cover.**



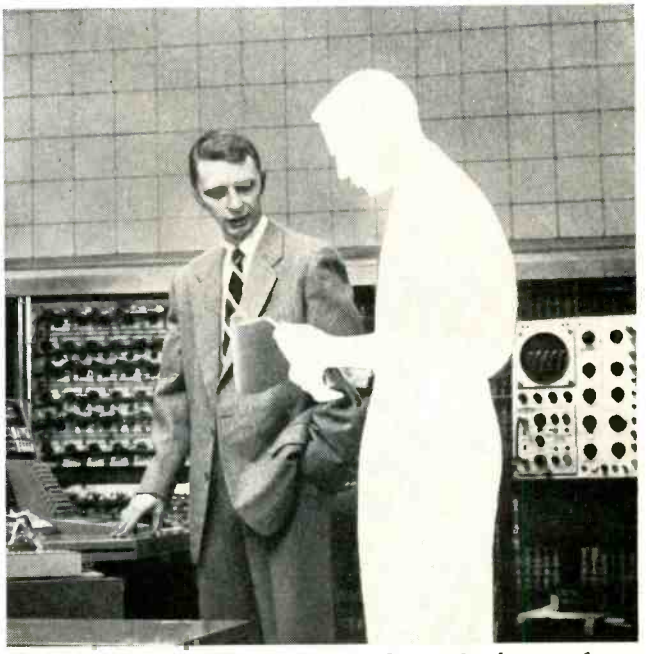
BOBBIN WINDER
gearless, high speed unit

GEO. STEVENS MFG. CO., INC., Pulaski Road at Peterson, Chicago 30,

IBM GROWTH promoted these men



PRODUCT DEVELOPMENT ENGINEER: Before his recent promotion, this man was a member of a small engineering "team" (two M.E.'s, an E.E. and a model maker) in IBM's Poughkeepsie plant. His specific project entailed the creation of the "ultimate package in printed circuitry." His group "brainstormed" the project in continual sessions, putting the results in model form. Then the group would try to "tear the idea to shreds" in order to create something even better.



PRODUCT CONTROL ENGINEER: Promoted recently, this man formerly worked at IBM's Poughkeepsie manufacturing facilities. His job was to design information systems to insure a smooth flow of work through the plant. "It takes *creative* engineering ability to design these systems," he'll tell you, "and *administrative* ability to 'sell' a system to higher management and make it stick. If you possess this rare combination of abilities, this is the job for you!"

Could you handle their responsibilities?

Jobs like these continually open up at IBM—due to rapid expansion. If you are an engineer or scientist—or have equivalent experience—you may be qualified for such a position. Innumerable opportunities exist in:

- Computer systems planning
- Numerical analysis and programming
- Electronic circuit design and packaging
- Electrostatic phenomena
- Real time systems engineering
- Photo and magnetic device memory
- Semi-conductor research, development, and manufacturing
- Manufacturing process control
- Computer systems testing
- Test equipment design

Economic experts rank the electronic computer with automation and nucleonics in growth potential. More than 10,000 electronic computers will be in operation by 1966. IBM sales have doubled, on the average, every five years since 1930. IBM engineering laboratory personnel quintupled in the past five years. IBM spent $19,000,000 on research and new product development in 1956. Salaries are excellent; company-paid benefits set standards for industry today. Personnel turnover at IBM is less than one-sixth the national average.

FOR THE FACTS about an engineering career with IBM, just write, outlining background and interests, to:

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IBM plants and laboratories are located in:

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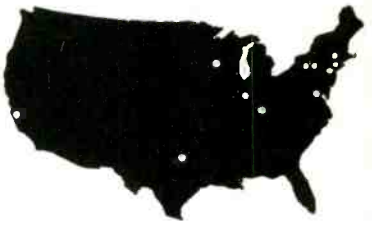


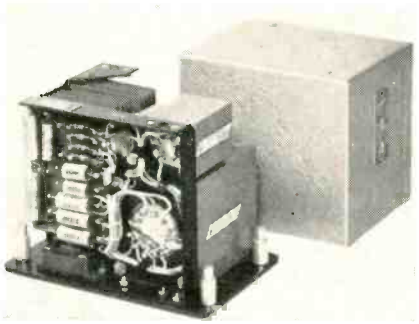
IBM INTERNATIONAL BUSINESS MACHINES CORPORATION

Be sure to visit the IBM booth at the I. R. E. Show, March 18 through 21.

DATA PROCESSING . ELECTRIC TYPEWRITERS . TIME EQUIPMENT . MILITARY PRODUCTS

Ill., has developed a new high-speed direct drive adjustable winding length bobbin winder which eliminates gear changing between jobs. Need for gears is entirely eliminated by a time-saving pitch selector which cuts job changeover time in half. An emergency safety stop button, conveniently located in front, stops the machine instantly.

Model 312-AM winds all types of random wound bobbin, repeater, relay and space wound coils, solenoids, resistors and distributed constant delay lines. Winding speed is up to 8,000 rpm; winding range, 60 to 700 turns per in.; wire sizes wound, 27 to 46; maximum o-d of coil wound, 2 in.; maximum traverse for any single continuous winding, 3½ in.; maximum loading area for multiple winding, 8½ in.; output end of spindle, ½-in. flatted shaft; and winding traverse infinitely adjustable between ⅛-in. and 3½ in. **Circle P66 inside back cover.**



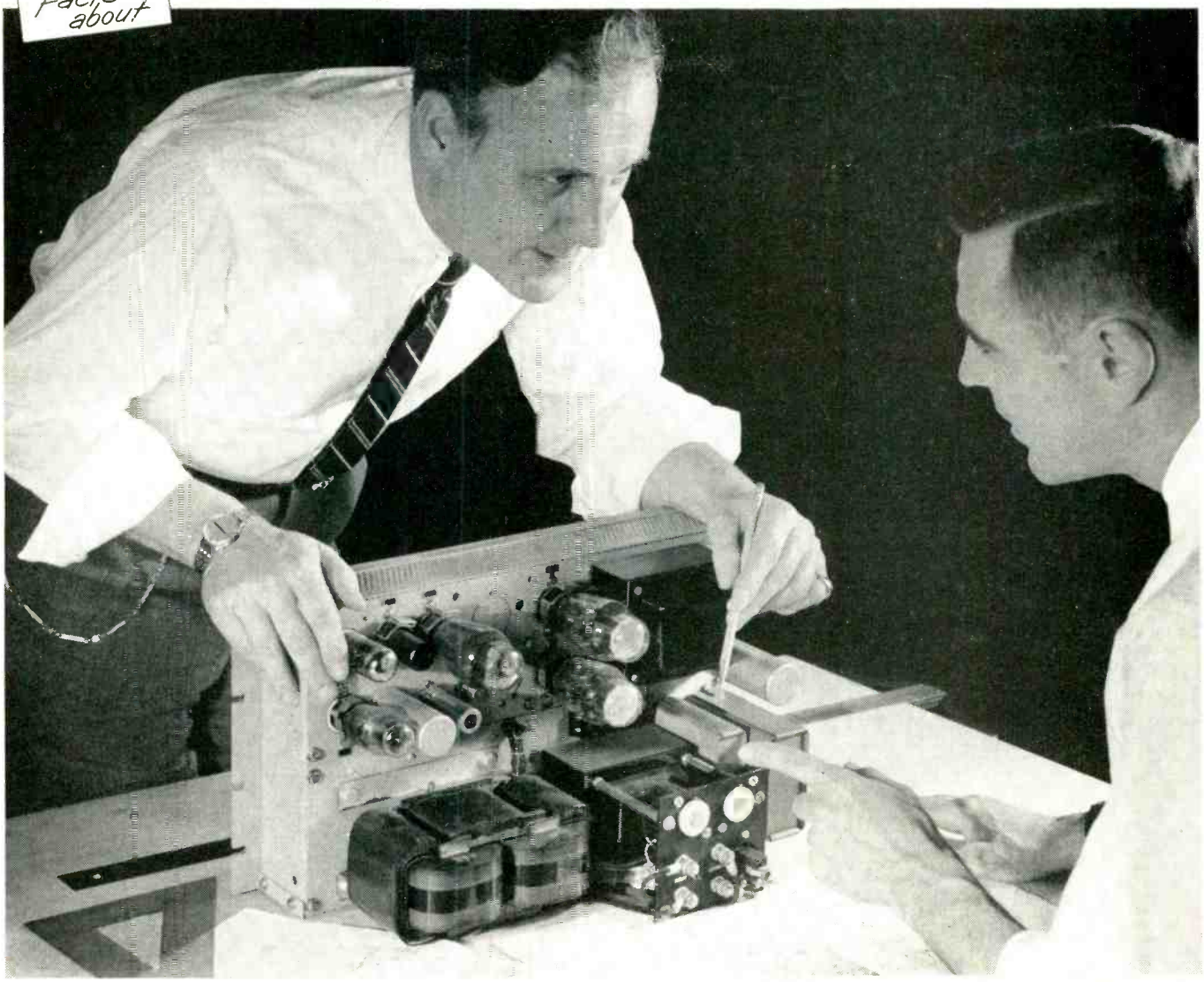
SERVO AMPLIFIERS
for 60 and 400 cps motors

INDUSTRIAL CONTROL CO., Wyandanch, L. I., N. Y., presents a complete line of servo amplifiers for both 60 and 400-cps servo motors, ranging in shaft power from 1 to 50 w. These amplifiers have been designed with universal characteristics and flexible input circuits. Circuit techniques range from vacuum tube to transistor-magnetic and all the most widely used servo motors are covered.

Four packaging styles are offered, including hermetic sealing and plug-in, quick disconnect packages. The input networks are arranged in three groups, for

Facts about

STABILINE® Automatic Voltage Regulators



STABILINE type IE (Instantaneous Electronic) is available in 115 volt units — input range from 95-135v. and 230 volt units — input range from 195-255v. STABILINE type IE5101R shown above.

"Here's how to Build-in Automatic Voltage Regulation"

"No matter how good your control instrumentation is, it is not going to be precisely accurate at all times unless the input voltage is precisely *constant*.

"You just can't get better automatic voltage regulation equipment than with this STABILINE. At no load, full load or any intermediate stage it maintains constant *output* voltage regardless of line fluctuations.

"This sensitive, yet ruggedly constructed, automatic voltage regulator is a must component in today's voltage sensitive apparatus."

Three types of STABILINES are available for individual needs:

Type IE (*Instantaneous Electronic*) is completely electronic, instantaneous in action, with no moving parts. Constant output voltage is maintained regardless of line or load fluctuations.

Type EM (*Electro Mechanical*) has zero waveform distortion. Insensitive to magnitude and power factor of the load. Highly efficient.

Type TM (*Tubeless Magnetic*) has no moving parts . . . no tubes . . . no transistors. Ideal for unattended locations or where failure can never be tolerated.

Be sure to see SUPERIOR ELECTRIC'S Mobile Display when it is in your area

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Please send STABILINE Bulletin S657 ☐
Have your representative call ☐

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Company .....
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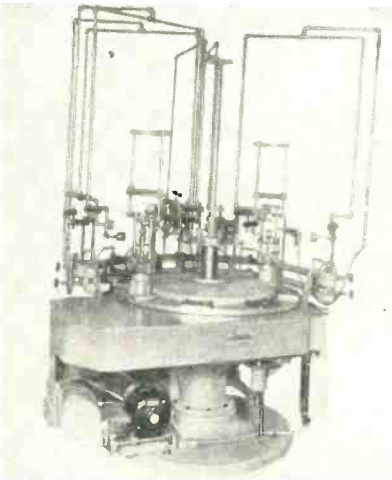
single speed synchro and pot data, two speed synchro data and d-c data. Most amplifiers are completely self-contained operating directly from the power lines. All units are designed to meet applicable military specifications and industrial usage requirements. **Circle P67 inside back cover.**



SEALING MACHINES
for difficult-shape tubes

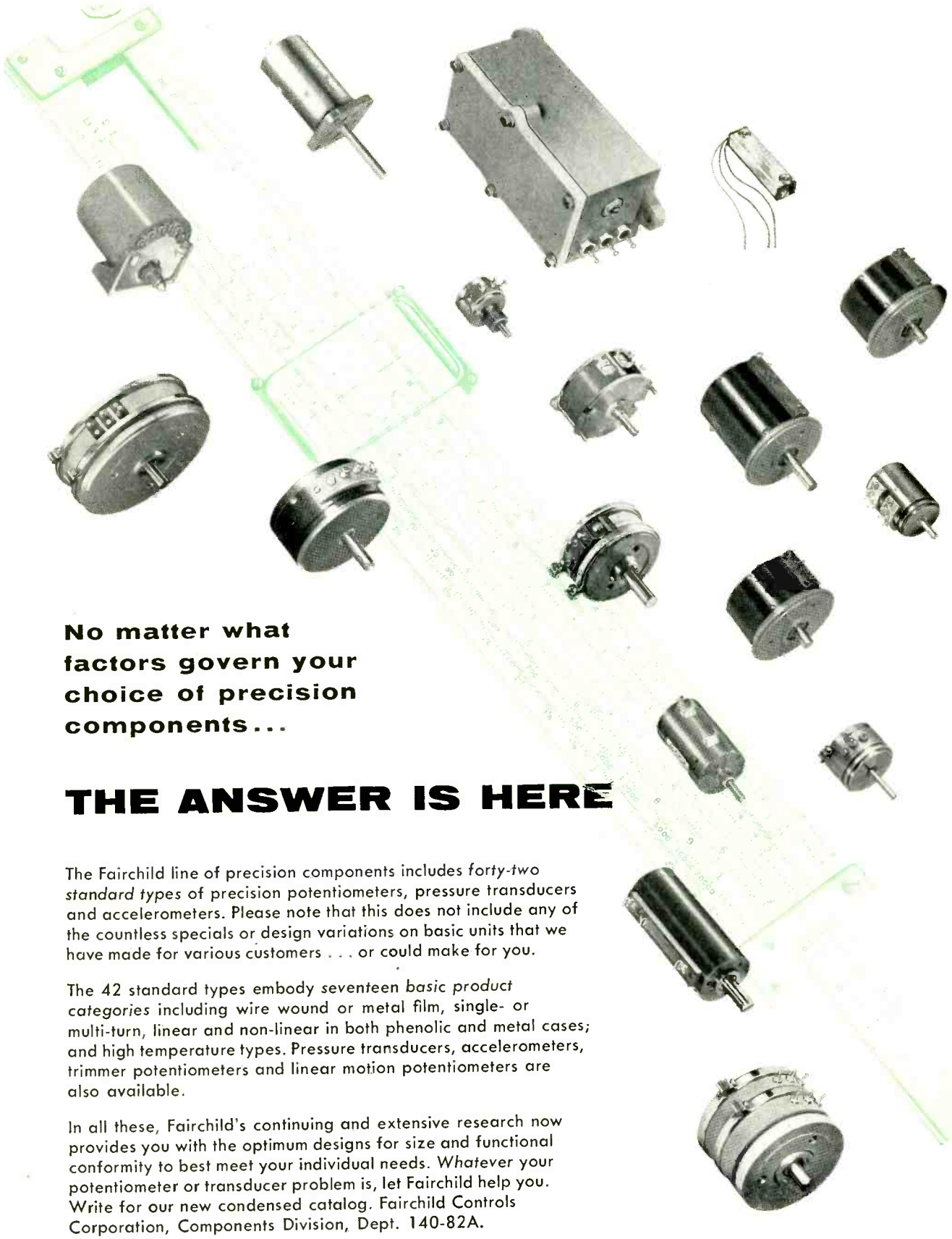
KAHLE ENGINEERING CO., 1400 Seventh St., North Bergen, N. J., has created an improved group of sealing machines to accommodate elongated neck lengths, difficult envelope shapes, increased numbers of components and more exacting precision levels. Machine No. 2815 will accommodate tubes with neck lengths up to 40 in.

Product speeds of up to 140 units per hour are easily maintained. Customized Kahle equipment for any sealing need can be supplied with many optional features which include full automatic programming. **Circle P68 inside back cover.**

SEALED SWITCH
with potted wires

HAYDON SWITCH, INC., Waterbury, Conn., announces a new hermetically sealed potted switch complete with actuator. Primarily for use on aircraft and missile applications, it will operate under the most trying environmental extremes.

Special feature is the threaded actuator plunger guide sleeve



No matter what factors govern your choice of precision components...

THE ANSWER IS HERE

The Fairchild line of precision components includes *forty-two standard types* of precision potentiometers, pressure transducers and accelerometers. Please note that this does not include any of the countless specials or design variations on basic units that we have made for various customers . . . or could make for you.

The 42 standard types embody *seventeen basic product categories* including wire wound or metal film, single- or multi-turn, linear and non-linear in both phenolic and metal cases; and high temperature types. Pressure transducers, accelerometers, trimmer potentiometers and linear motion potentiometers are also available.

In all these, Fairchild's continuing and extensive research now provides you with the optimum designs for size and functional conformity to best meet your individual needs. *Whatever* your potentiometer or transducer problem is, let Fairchild help you. Write for our new condensed catalog. Fairchild Controls Corporation, Components Division, Dept. 140-82A.

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225 Park Avenue
Hicksville, L. I., N. Y.

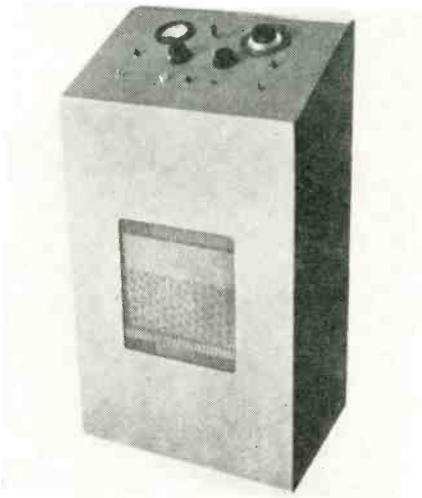
WEST COAST
6111 E. Washington Blvd.
Los Angeles, Calif.

FAIRCHILD
PRECISION POTENTIOMETERS and COMPONENTS

which permits mounting the switch actuator button flush or extended any distance from the mounting board up to $\frac{3}{8}$ in.

Switch No. 9129, mounted on actuator, has $\frac{1}{8}$ in. overtravel with $\frac{1}{8}$ in. pretravel along the plunger. Switches tested have passed the 50-g shock MIL specification.

Information on the 9129 and a copy of the new precision switch catalog are available. **Circle P69 inside back cover.**



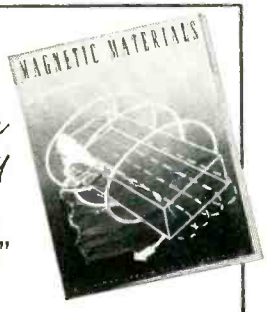
ULTRASONIC GENERATORS
for industrial processing

GULTON INDUSTRIES, INC., 212 Durham Ave., Metuchen, N. J., has announced a new series of ultrasonic generators designed to drive a wide variety of low-impedance ultrasonic transducers. Accenting an untuned output system and featuring 500-w r-f power output plus a varied range of frequency levels, these generators will be found useful for performing numerous electromechanical techniques such as cleaning, chemical

for
HEARING
AIDS

or
RECORDING
HEADS

or *ANY* MAGNETIC MATERIALS JOB . . .



Write for your Copy

"MAGNETIC MATERIALS"

This 32-page book contains valuable data on all Allegheny Ludlum magnetic materials, silicon steels and special electrical alloys. Illustrated in full color, includes essential information on properties, characteristics, applications, etc. Your copy gladly sent free.

ADDRESS DEPT. E-87

You can *rely* on core materials like the Allegheny 4750 components illustrated above, in your receivers, recording heads or microphone assemblies.

In fact, whether your equipment is small or large, the extra-broad line of A-L magnetic materials will solve your magnetic core problems. It includes all grades of silicon steel sheets or coil strip, as well as Allegheny Silectron (grain-oriented silicon steel), and a wide selection of high-permeability alloys such as 4750, Mumetal, Permendur, etc.

Our service on these materials also includes complete facilities for the fabrication and heat treatment of laminations. (For users of electrical sheets and strip, our lamination know-how is a real bonus value!) Either way, we'll welcome the chance to serve you. *Allegheny Ludlum Steel Corporation, Oliver Building, Pittsburgh 22, Pa.*

STEELMAKERS to the Electrical Industry

Allegheny Ludlum

WAD 5335

AL® STEELS FOR THE ELECTRONIC AGE

processing, soldering and drilling.

The series of generators, designated Glennite U-405, are blower cooled and operate at a nominal fixed frequency of 40 kc or at any frequency between 20 kc and 2 mc, depending on model. **Circle P70 inside back cover.**

PREAMPLIFIER
for impedance matching

MADISON FIELDING CORP., 863 Madison St., Brooklyn, N. Y., announces the Micamp, an all-transistorized, impedance-matching preamplifier which permits the direct use of low-impedance, low-gain cartridges and microphones with high-impedance tape recorders, amplifiers, p-a systems and the like. Providing more than 30 db gain, with no hum pickup and no distortion at normal levels, it insures a frequency response of within 1.5 db from 20 to 20,000 cps.

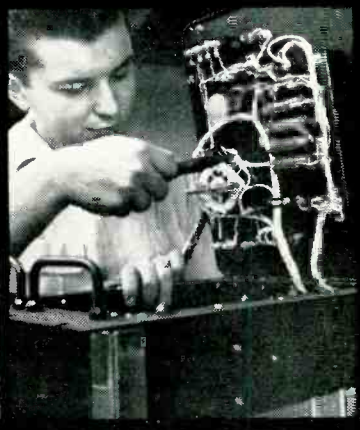
Input impedance is from 50 to 250 ohms; output impedance, 18,000 ohms. Signal-to-noise ratio is better than 50 db. **Circle P71 inside back cover.**

MULTICHANNEL SYSTEM
for temperature measurement

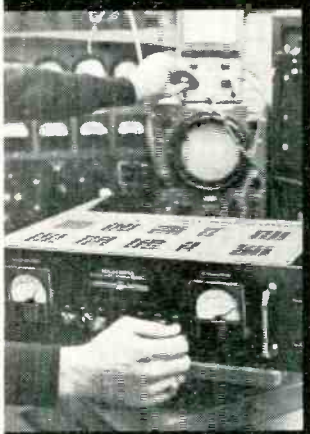
ARNOUX CORP., 11924 W. Washington Blvd., Los Angeles 66, Calif. A miniature multichannel airborne temperature measurement system gives full scale output of five v. Models are offered in seven, 14 and 20-channel capacity. Power requirements are 115 v, 400 cps. Total power consumption of the 20-channel model is less than 20 w. The TME contains two precision mag-amp type regulated d-c power supplies, series connected with common neutral, for excitation of

QUALITY CONTROL assures you of long, dependable service from these assembly-line-produced power supplies.

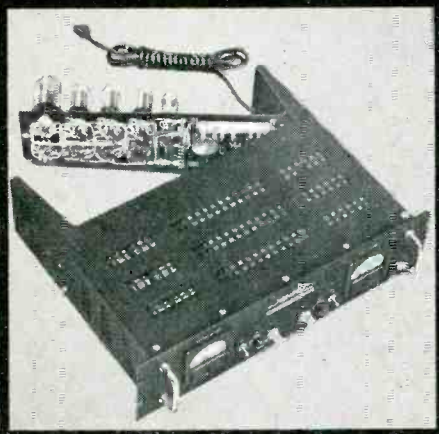
HERMETIC SEALING PROCESS provides for complete quality control. Lambda makes all its own transformers.



MECHANICAL INSPECTION at every relevant point means trouble-free operation for you.



ELECTRONIC INSPECTION is designed to provide consistent quality and eliminate in-service down-time.



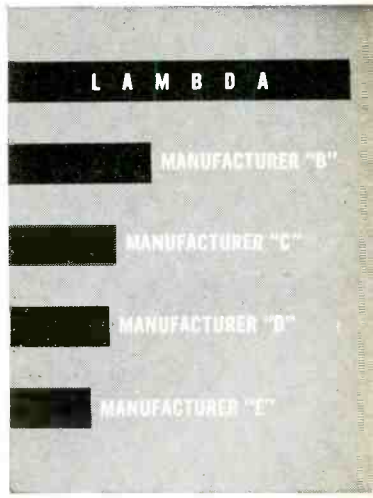
TYPICAL NEW LAMBDA "COM-PAK" MODEL (200-400-800 MA units) occupies a minimum amount of space, delivers maximum performance, is easy to service and maintain.

FOR THE THIRD CONSECUTIVE YEAR

ENGINEERS RATE LAMBDA FIRST

in all Power Supply Surveys

Every independent study of power supply preferences has shown an overwhelming vote for Lambda. In the most recent survey, made by a leading electronics publication, engineers who specify power supplies choose Lambda by more than 2½ times over the next identified manufacturer. This is the greatest margin of preference yet. Here is additional proof that the more opportunities users of power supplies have to try Lambda equipment for themselves, the more they recognize the superiority of these outstanding units.



We suggest that you inspect Lambda power supplies in use in your own area. We will be happy to provide names of nearby users. Ask the candid opinion of the men who work with this precision-engineered equipment daily.

"See the new Lambda Com-Pak series at the IRE Show. New, space saving, 200 MA, 400 MA, 800 MA and 1.45 amp models. Be sure to stop by Booths 2436-2438."

LAMBDA ELECTRONICS CORP.

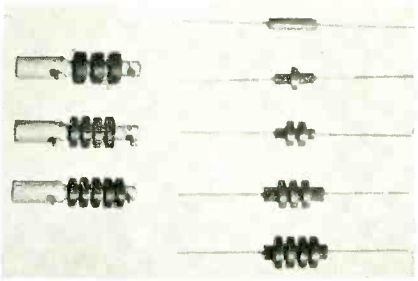
The first name in power supplies

11-11 131 STREET • COLLEGE POINT 56, NEW YORK

SEND FOR NEW CATALOG 57

Just off the presses. Illustrations and specifications for the complete line of Lambda Regulated D.C. Power Supplies.

the temperature transducers in half bridge circuitry. Balance and attenuation controls are provided for each channel. Output voltage and impedance characteristics are directly compatible with f-m subcarrier and pwm coder input requirements. System stability is within one percent throughout MIL-E5272A environments. Dimensions of 20-channel model are 7 by 4¼ by 3 in. Total weight is 5½ lb. **Circle P72 inside back cover.**

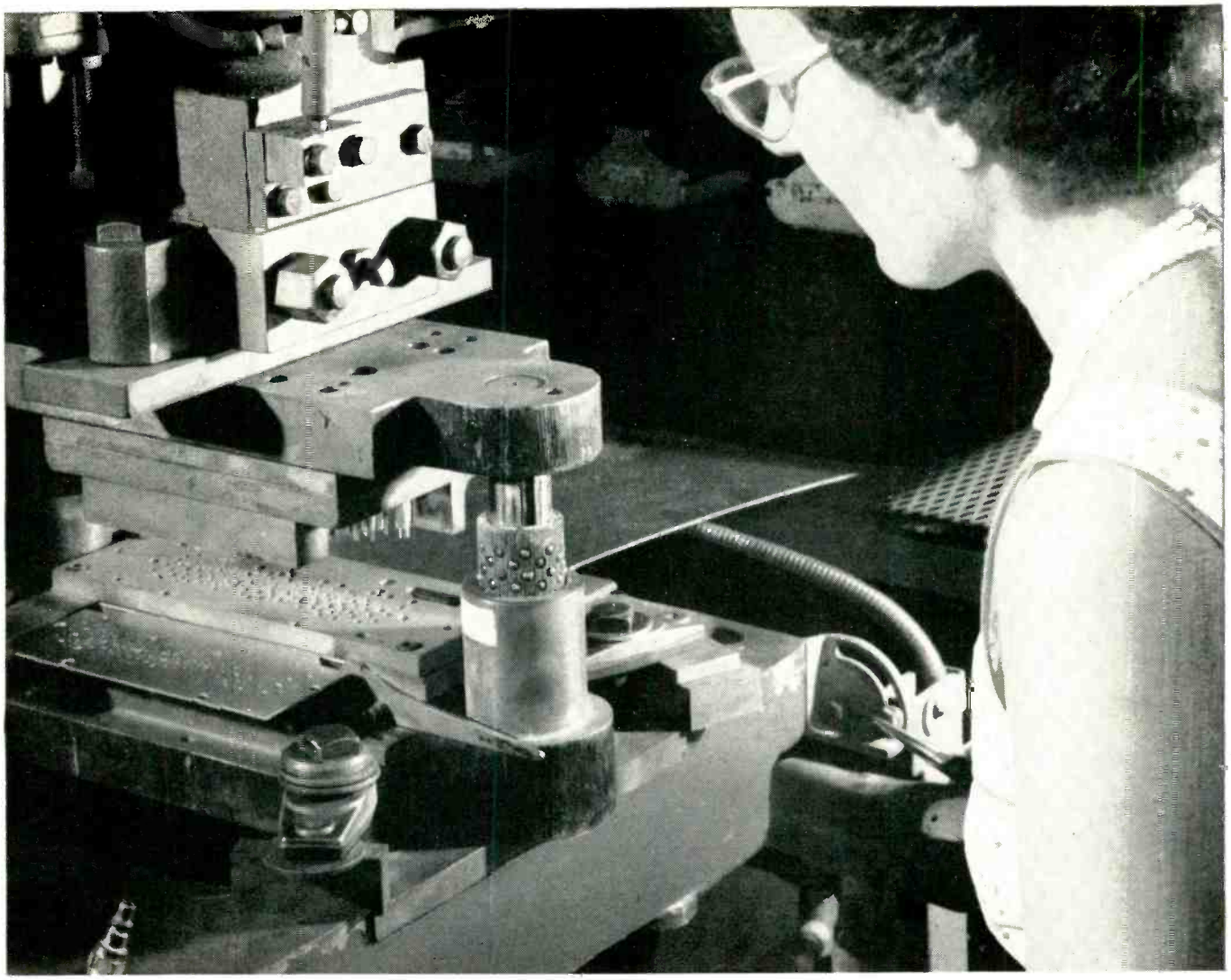


R-F CHOKES
have high Q in small size

WATERS MFG., INC., P. O. Box 368, South Sudbury, Mass. Individually checked, and providing high Q in small size, a new line of r-f chokes has been developed. Five series are available to provide wide choice of characteristics. These series include solenoids on phenolic and powdered-iron forms and pie-wound coils on Ferrite cores, phenolic forms and powdered-iron forms, all with pigtail leads.

Pie-wound coils on ceramic forms have soldering terminals secured to the form. All units have finish conforming to MIL-V-173A; special finishes can be supplied. Inductance ratings are from 1.1 μh and up. Current ratings are from 50 ma to 2,800 ma.

A data sheet giving details of



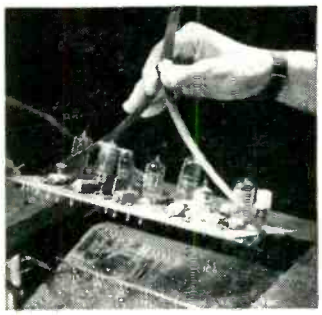
New copper-clad **MICARTA**®
is easy to cold punch—no cracking, no chipping!

All holes in new H-3032 copper-clad MICARTA can be cold punched right on the assembly line in one operation, and there's no cracking, breaking or chipping. That is one of the reasons why this new laminate cuts costs and production time of printed circuits.

In addition, copper-clad MICARTA speeds up soldering, without the normal accompaniment of an increase in rejects and missed connections.

High bond strength — from 10 to 13 pounds versus an industry standard of six pounds — is retained even after heating and cooling are repeated many times, due to a new adhesive process.

If you have a circuit assembly problem, copper-clad MICARTA may be the answer. For further information and for technical data, write to Westinghouse Electric Corporation, MICARTA Division, Hampton, South Carolina. J-06626



CAN BE DIP SOLDERED!
MICARTA will not blister — even when dip soldered for 10 seconds at 500° F. A special adhesive actually increases adhesive strength during soldering.

YOU CAN BE SURE...IF IT'S Westinghouse

NEW PRODUCTS (continued)

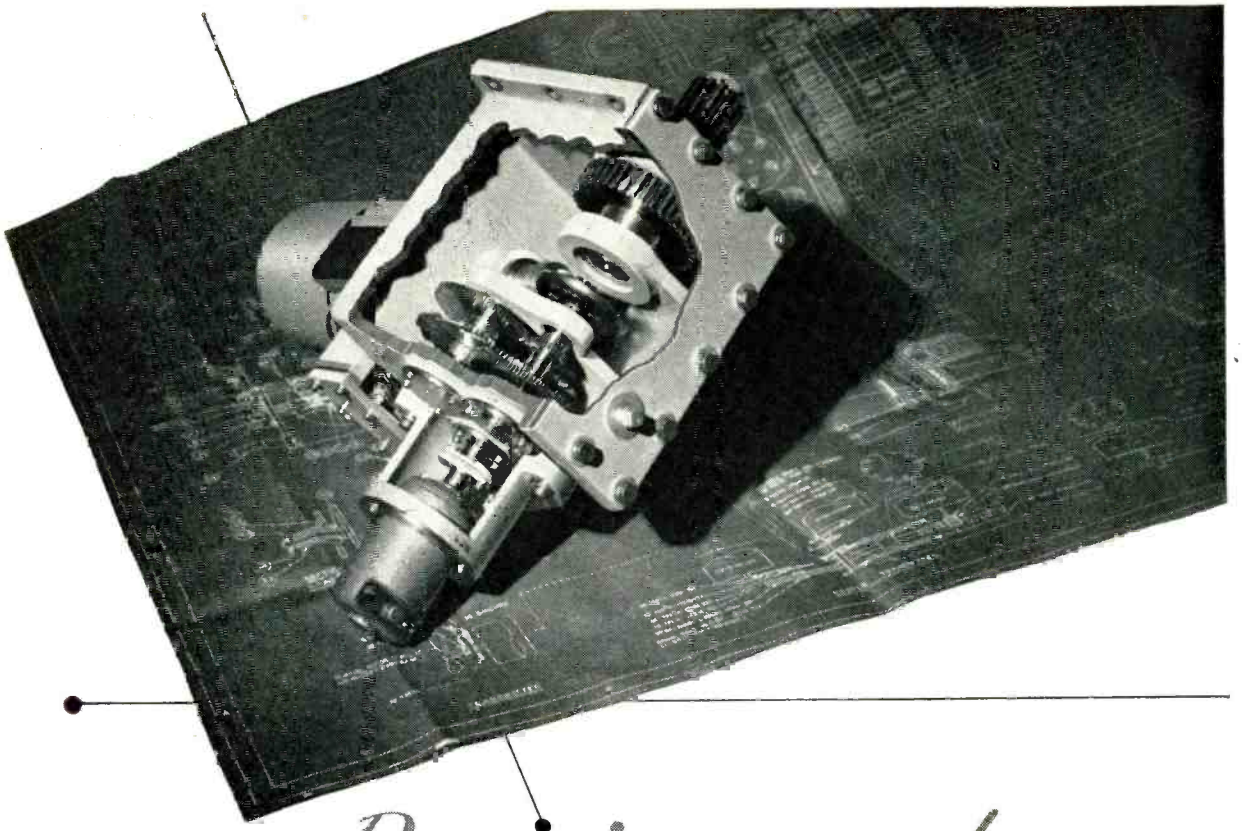
inductance, resistance, Q-vs-frequency, current rating, self-resonant frequency, distributed capacitance and core sizes for all units is available. **Circle P73 inside back cover.**

MAGNETIC SHIELD
for color tv tubes

MAGNETIC SHIELD DIVISION, Perfection Mica Co., Chicago, Ill. A new Fernetic Co-Netic leakproof magnetic shield for color tv tubes that weighs six lb, is produced by rotary extrusion methods and will reduce manufacturers' cost of the color sets, is now available. The Fernetic steel, $\frac{1}{8}$ in. thick, and the Co-Netic steel, 0.020 in. thick, have a coating which prevents the metal from setting up a north-south pole which automatically affects the color purity of one or three-gun tubes. Miniaturization of the chassis is possible because of the shield. Transformers can be put immediately adjacent to each other, with only a shield separating them, disregarding the point of how they are oriented. Components can be mounted on the shield because the shield does not become retentive and will support circulating currents. **Circle P74 inside back cover.**

STACKED SWITCHES
a space-saving system

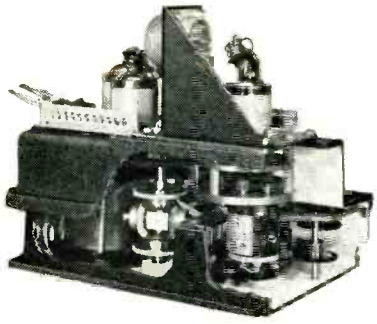
DETROIT CONTROLS CORP., 800 Union Ave., Bridgeport, Conn. A new system of precision stacking of Class 1 TyniSwitches makes it possible to obtain a single actuator switch capable of switching two or more completely independent circuits. Each individual

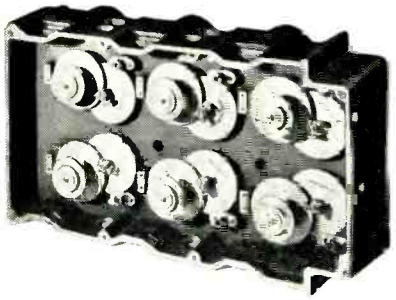


Precision-eered

ELECTRO-MECHANICAL ASSEMBLIES

FROM PILOT STAGE TO PRODUCTION EFFICIENCY

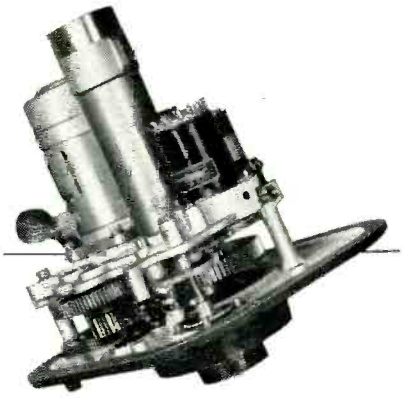




HAVE you a new product on the design boards? Do you have a new contract for radar, missiles, computers or other electro-mechanical devices? Then let Atlas help you from pilot stage to production efficiency.

Atlas experienced production and methods engineers layout the job using new cost-cutting methods, and improved processing techniques. Atlas toolmakers build dies and fixtures to implement these plans. Atlas skilled mechanics and assemblers produce prototypes to your exact specifications *on a job basis*, and can follow thru with production. As many men, machines and hours of work as your electro-mechanical unit requires and no more.

Atlas furnishes the practical engineering step between idea and production line. We've been "precision-eering" on a contract basis for more than a quarter of a century. May we work with you? Write for booklet "Precision-eering Electro Mechanical Equipment." ATLAS Precision Products Co., Philadelphia 24, Pa. (Division of Prudential Industries).



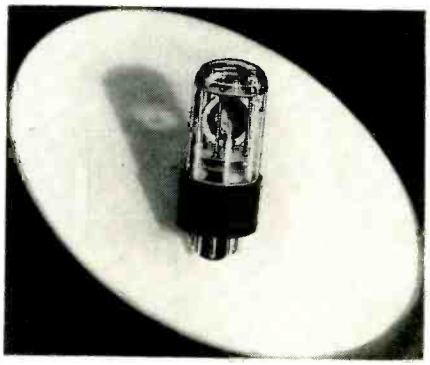
"From Drawing Board . . . to Production Line"

ATLAS
Precision Products

SERVICE ATLAS DEPENDABILITY QUALITY

switch action can be double throw, single throw normally open or single throw normally closed.

In multipole stacked Tyni-Switches maximum pin movement from the first contact actuation of all contacts is 0.015 in. Double-pole switches are considered as standard and are available with any standard Class I actuator. Switches with three or more poles will be built to customer specifications. Detailed information and descriptive literature are available. **Circle P75 inside back cover.**



QUARTZ CRYSTAL UNIT
sealed-in-glass

BLILEY ELECTRIC CO., Union Station Building, Erie, Pa. The BG9A-S, a 1,000 kc sealed-in-glass quartz crystal unit, is designed to provide exceptional stability with minimum ageing in secondary frequency standards.

Tolerance is ±5 ppm at 70 C. Temperature coefficient is less than 0.4 ppm per deg C between +65 C and +75 C. The unit is 3⅛ in. overall, T-9 bulb and standard octal base.

For complete design specifications request bulletin No. 491. **Circle P76 inside back cover.**

LIGHT COMPENSATOR
for tv cameras

BLONDER - TONGUE LABORATORIES, INC., 526 North Ave., Westfield, N. J., has announced an automatic light compensator that electronically compensates for variations in video signal level caused by variations in illumination, thereby eliminating the need for manual or remote resetting of the tv camera lens iris or control gen-

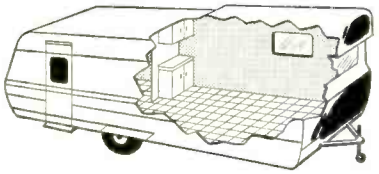
TAYLOR
Laminated Plastics
Vulcanized Fibre

Shop Talk

TAYLOR FIBRE CO.
Plants in Norristown, Pa. and La Verne, Calif.

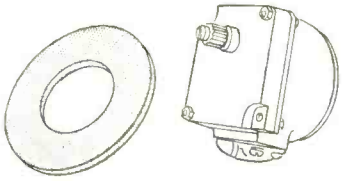
PHENOLIC—MELAMINE—SILICONE—EPOXY LAMINATES • COMBINATION LAMINATES • COPPER-CLAD LAMINATES • VULCANIZED FIBRE

Tips for designers

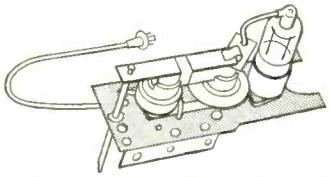


House trailer interior walls are made of plywood faced with Taylor vulcanized fibre, chosen for its combination of light weight and high strength.

Highway signs use Taylor Grade XX phenolic tubing and washers that are long-wearing and do not rust.



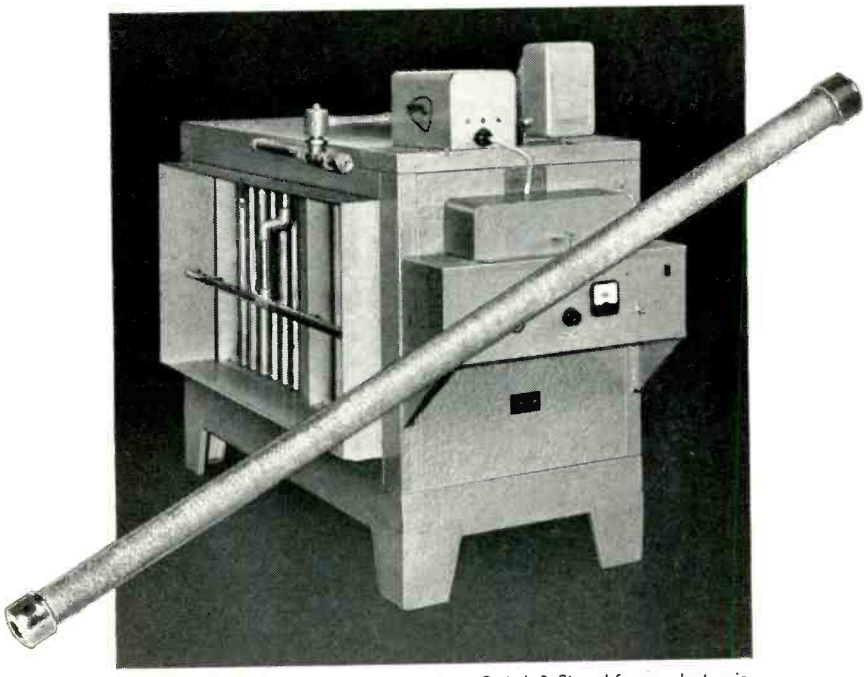
Self-balancing servo motor has stator case insulator which is cold-punched from 1/64" thick Taylor Paper Base Phenolic Laminate sheet.



Base plate for high-voltage TV component, punched from Taylor canvas melamine laminate, has high dielectric strength and arc resistance.

NEW TAYLOR COPPER-CLAD LAMINATES

Taylor GEC (glass epoxy) Copper-Clad and Taylor XXXP-242 cold punching (paper-phenolic) Copper-Clad. Taylor uses high purity rolled copper on base materials with outstanding electrical properties.



A selenium "pencil" rectifier made by Union Switch & Signal for an electronic air cleaner, by Electro-Air Cleaner Co., uses an outer tube of Taylor Grade G-5 laminated plastic. The material has excellent arc-resistance, mechanical properties and low moisture absorption.

Taylor Melamine Laminate solves material selection problems

The pencil-thin outer case of this selenium rectifier presented several unique problems. It required a new concept of high arc-resistance, plus mechanical strength and low water absorption. Taylor Grade G-5 (glass-melamine) laminate solved these problems . . . embodied both the electrical and mechanical properties required for the outer tube. The broad selection of Taylor laminates includes a wide variety of different bases and different grades, each with certain combinations of electrical and physical properties to answer your materials selection problems.

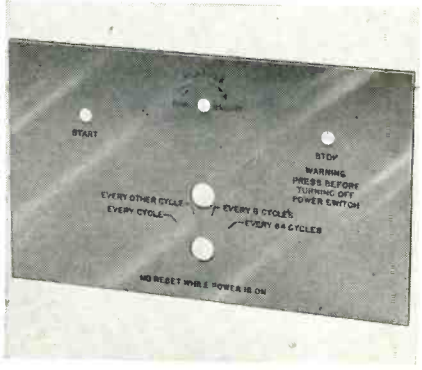
In any application, Taylor laminates bring you important savings in fabrication. Whether you need tubes, rods, sheets or fabricated parts, Taylor laminates come in sheets 49" by 49" . . . tubes with inside diameters as small as 3/32" up to 36", lengths to 49" and a variety of wall thicknesses . . . rods in a wide range of sizes. Or, Taylor can fabricate your part to your specifications . . . on time and at a saving.

To help you choose and use the right laminate, Taylor's engineering staff and fabricating facilities are at your service. Contact your nearest Taylor sales engineer.

Want more information? Use post card on last page.

erator. The ALC can automatically compensate for light variations as great as 150 to one. It is connected between the camera and its control generator. The cable from the camera plugs into the ALC input. A second short cable connects the ALC output to the control generator.

It has four controls: output level, video/target ratio, video agc, and power-off. Complete specifications and further information are available from the company. **Circle P77 inside back cover.**



ENGRAVING STOCK
for instrument panels

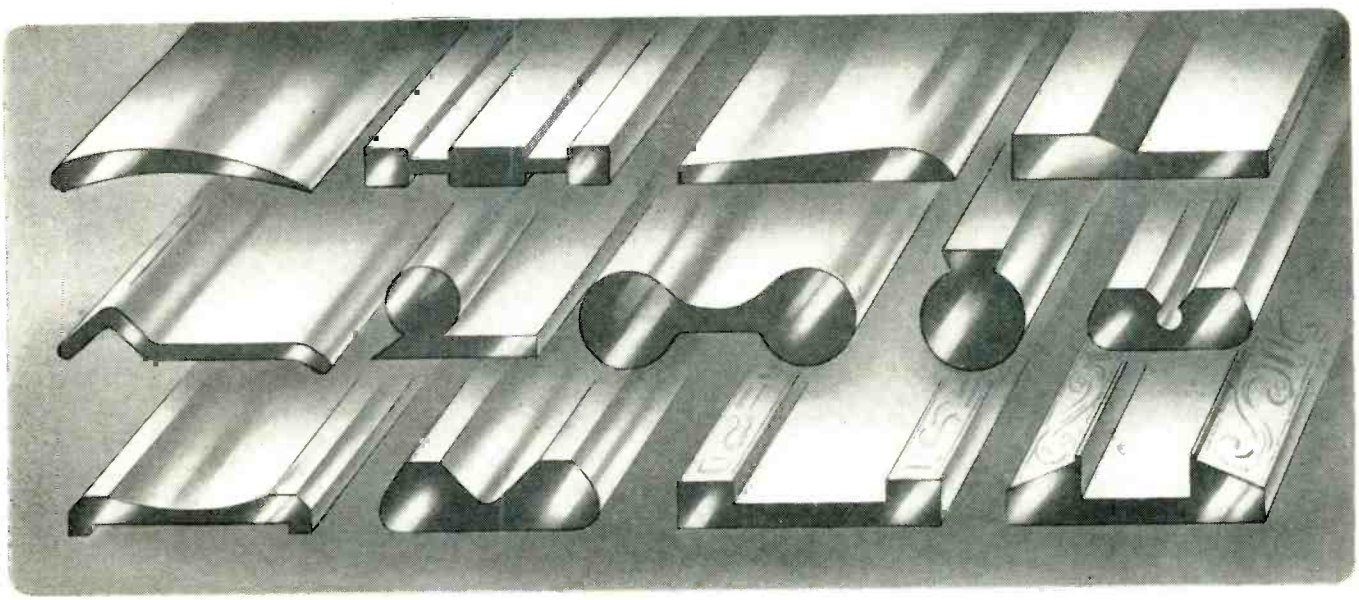
HERMES PLASTICS, INC., 13-19 University Pl., New York 3, N. Y., has announced Gravalum, a metallic engraving stock ideally suited for panels on instrument housings where shielding or grounding effect is required. It is a laminated material with an ebony black phenolic center core bonded between two exterior layers of satin finish aluminum. Engraving through the top layer exposes contrasting black lettering. This eliminates the need of filling in the engraving with paint.

Gravalum is available in sheets, strips or cut nameplates in thicknesses of $\frac{1}{16}$ and $\frac{1}{8}$ in. Samples

General Plate

ROLLED FORM STOCK

- **Cuts Production Costs**
- **Reduces Scrap Losses**
- **Minimizes Stock Inventories**



General Plate craftsmanship can mean substantial production and assembly savings to you, and at the same time minimize your rolled stock inventory problems. Here are some of the advantages available to you in General Plate rolled form stock:

1. Close tolerances in dimensions, contour, and composition.
2. Wide diversification of available metals and shapes.
3. Excellent surface finishes.
4. Heat treating facilities available.
5. Size range from .025″ to 3½″ wide.

These advantages, plus expert toolmaking — skilled production people — efficient delivery service — all resulting from years of experience in producing rolled form material — make General Plate a dependable source of supply for your formed stock needs.

We'd like to figure on your rolled form stock requirements — if you'll send information to help us quote, we'll be glad to estimate tool and material costs without obligation. The information we need is: (1) cross-sectional sketch or drawing and dimensional tolerances, (2) length of strip and tolerances, (3) material specifications, (4) permissible edge curvature and flatness, (5) surface finish required, (6) hardness, and (7) quantities involved.

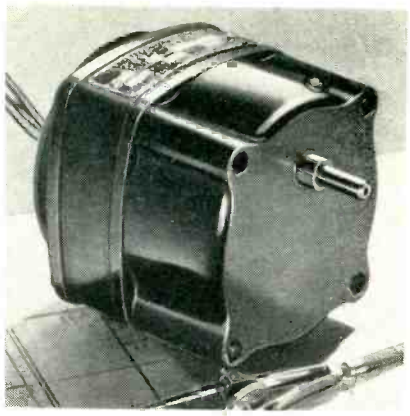
You can profit by using General Plate Rolled Form Stock.

Metals & Controls Corporation

GENERAL PLATE DIVISION

1303 FOREST STREET, ATTLEBORO, MASS.

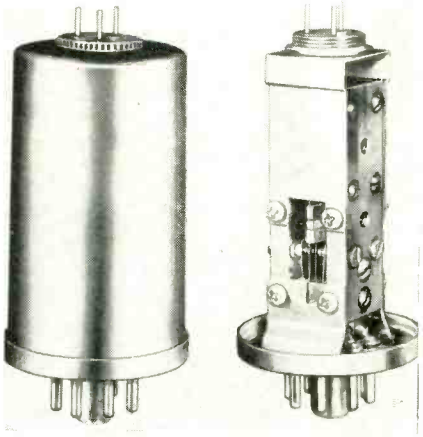
and information are available. **Circle P78 inside back cover.**



SYNC GEAR MOTOR
for strip chart recorders

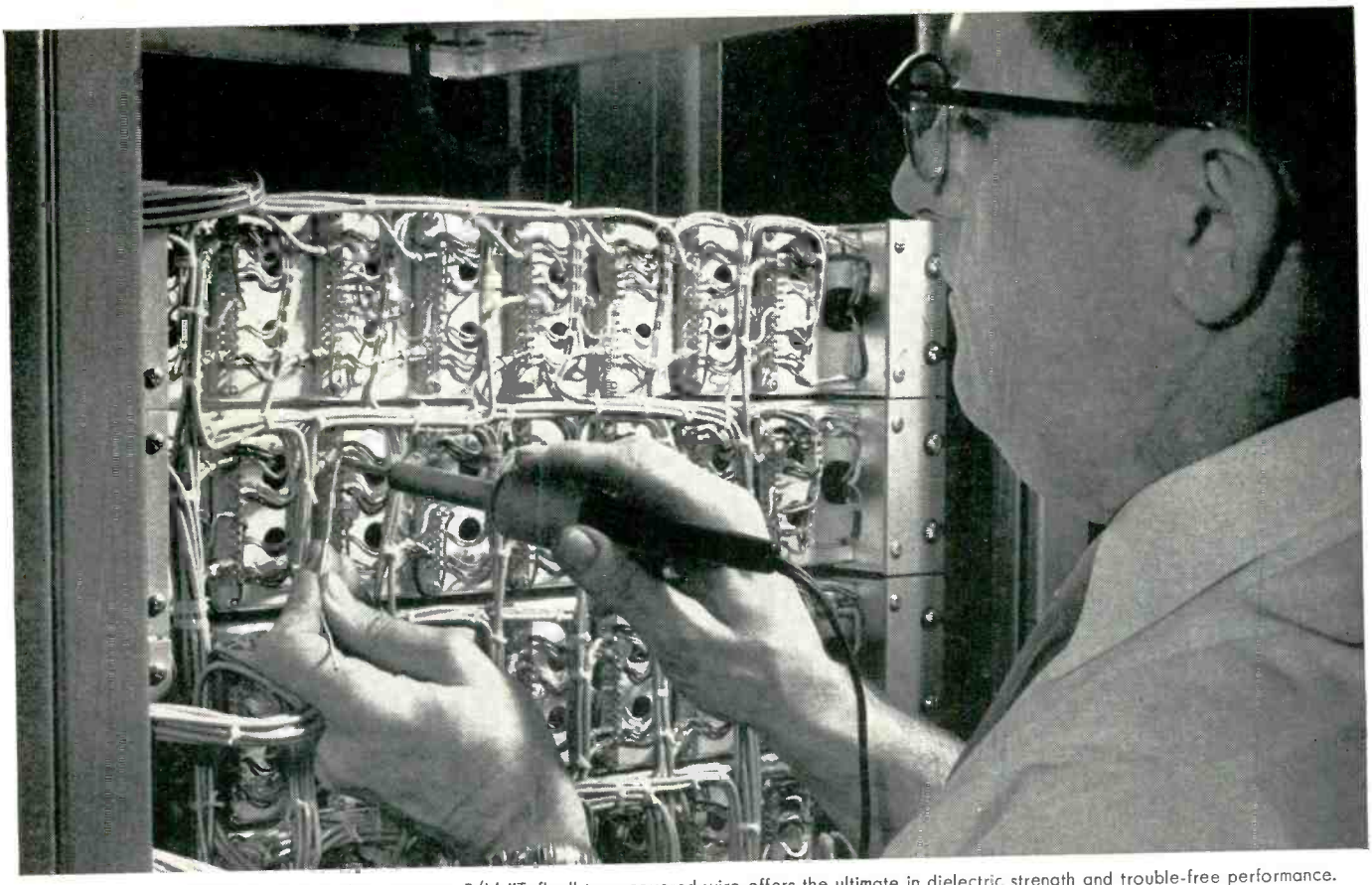
HOLTZER-CABOT MOTOR DIV. of National Pneumatic Co., Inc., 125 Amory St., Boston 19, Mass., has developed a new 400-cycle motor designed for airborne strip chart recorders and other applications.

The new motor, which is physically interchangeable with type RBC-2505 60-cycle motors, is designed for 115 v, 400 cycle, 100 rpm, 7.5 oz in., continuous duty rating. It will also be available with other speeds, both synchronous and induction, with ratings adjusted to corresponding gear reductions. **Circle P79 inside back cover.**



CHOPPER PACKAGE
features reduced size

JAMES VIBRAPOWR CO., 4050 N. Rockwell St., Chicago 18, Ill. The new 1200 series chopper package features reduced size, improved shielding and better dust seal. The chopper is 2⅝ in. high overall,



In hundreds of applications, such as this computer, R/M "Teflon" tape-covered wire offers the ultimate in dielectric strength and trouble-free performance.

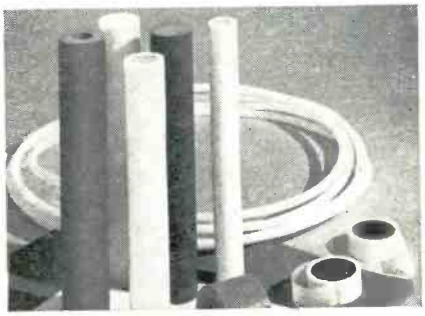
For better design and performance specify R/M Teflon* products

A unique combination of properties—electrical, thermal and mechanical—makes R/M "Teflon" ideal for use as insulation, particularly at high temperatures and high frequencies. R/M "Teflon" Tape, for example, has been extensively used to insulate hookup wire for complex circuits. This tape has great toughness and resiliency, is easy to handle, conforms well to odd shapes, and can be readily adapted to automatic wrapping operations. With the trend toward miniaturization resulting in higher operating temperatures, the excellent heat resistance of R/M "Teflon" permits much greater freedom in design than ordinary dielectric materials.

Here are some of the electrical properties of R/M "Teflon":

1. **Power factor** — less than 0.0003 over entire spectrum from 60 cycles to 30,000 megacycles
2. **Volume resistivity** — greater than 10^{15} ohm-cm, even after prolonged soaking in water
3. **Surface resistivity**— 3.6 x 10^{12} ohms even at 100% humidity
4. **Good arc resistance** — on exposure to an arc, the material vaporizes, leaving no carbonized path
5. **High short-time dielectric strength**— from 1000 to 2000 volts per mil, depending on thickness
6. **Good temperature resistance**— electrical properties are essentially unchanged up to at least 400°F.

R/M pioneered in developing the potentials of "Teflon" for the electrical and electronics industries. So R/M engineers are in a specially good position to help solve your problems—call on them. And remember, we fabricate "Teflon" to specifications or supply it in rods, sheets, tubes, and tape in all standard color codings. Send for our bulletin "R/M Teflon Products."



*A Du Pont trademark

RAYBESTOS-MANHATTAN, INC.

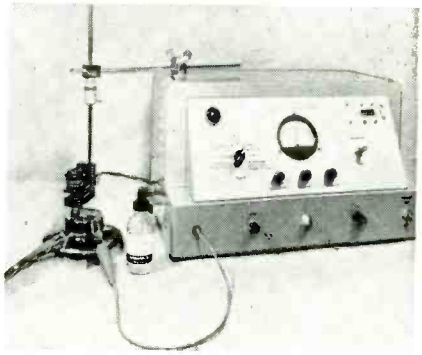
PLASTIC PRODUCTS DIVISION, MANHEIM, PA.

FACTORIES: Manheim, Pa.; Bridgeport, Conn.; No. Charleston, S.C.; Passaic, N.J.; Neenah, Wis.; Crawfordsville, Ind.; Peterborough, Ontario, Canada

RAYBESTOS-MANHATTAN, INC., Engineered Plastics • Asbestos Textiles • Mechanical Packings • Industrial Rubber • Sintered Metal Products • Rubber Covered Equipment • Abrasive and Diamond Wheels • Brake Linings • Brake Blocks • Clutch Facings • Laundry Pads and Covers • Industrial Adhesives • Bowling Balls

1½ in. in diameter and painted to military specifications.

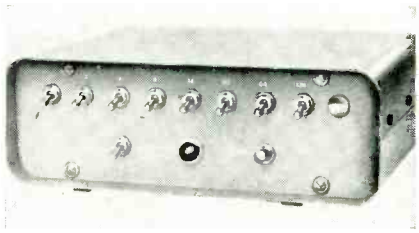
This improved chopper is now in volume production in all models and operating frequencies. Complete specifications and operating characteristics are available on request. **Circle P80 inside back cover.**



THICKNESS TESTER
insures long term accuracy

KOCOUR CO., 4800 S. St. Louis Ave., Chicago 32, Ill. Model 955 electronic thickness tester determines the thickness of plating and other metallic coatings deposited over various metals and non-metallic base materials with an accuracy of 90 to 95 percent. Operation is virtually automatic. Readings are direct. A multiple position switch indicates the plating to be tested.

Accuracy of the instrument can be checked at any time, and a calibration adjustment will automatically correct high or low readings, insuring long term accuracy. A constant pressure device which automatically maintains a uniform pressure between test cell and specimen eliminates reliance on operator's judgment. **Circle P81 inside back cover.**



DIGITAL COUNTER
a transistorized unit

NADER MFG. CO., 2661 Myrtle Ave., Monrovia, Calif., announces a new

Potter & Brumfield *engineering is in this picture*

Which P&B relay would you specify to keep conversation going over a MOBILE 2-WAY RADIO?


MB Series


TS Series


MC Series

When one of America's leading manufacturers of electrical and electronic equipment began the design of a lightweight 2-way car radio, they were faced with several specific requirements in selection of relays. They had to be compact, light in weight and engineered to withstand the shock and vibration of off-the-road service. P&B engineering solved the problem with a modification of the TS series multiple switching relay.

In this application the TS relay has a dual personality. It connects the power supply unit to *both* the transmitter and the receiver. Power supply is controlled through the relay to either unit by the operator.

This is just another example of how P&B engineering is daily adapting standard types of relays or designing completely new types to meet specific requirements of new products. P&B's unique 25 years of engineering experience in relay applications is a source of quick, correct answers to your relay problems. Write today for new compact catalog.

ENGINEERING DATA

SERIES: TS. Miniature off-set springs telephone type.

CONTACTS: 5/64" dia. palladium (rated 3 amps.) ⅛" dia. pure silver (rated 5 amps.).

CONTACT ARRANGEMENTS: Up to 20 springs, maximum 10 in each stack, using any form combinations within max. limits.

VOLTAGE RANGE: DC: up to 220 V. AC: up to 230 V. (4 poles)

COIL RESISTANCE: 30,000 ohms. Shaded coil available for 60 cycle operation up to 230 V. using 4.7 VA nominal.

POWER REQUIRED: 100 mw. per movable arm.

TEMPERATURE RANGE: Stack insulation of XXX phenolic spacers: —55° C. to +85° C. Glass malamine spacers: —55° C. to +125° C.

TERMINALS: Pierced solder lug holes for 2 No. 16 hook-up wires. Also available: Push-on taper tab connectors.

ENCLOSURES: Dust cover or hermetically sealed enclosures: Round: With octal plug (Max. of 8 springs) Rectangular: With octal plug; 4 to 14 pierced solder lugs; header to fit 14-pin miniature relay socket; Multiple solder header 18 springs Max.

DIMENSIONS: (4 Form C) 1-19/32" L. x 1-1/16" W. x 1¼" H. (open) (4 Form C) 1⅜" L. x 1-13/32" W. x 2-3/16" H. (Hermetically sealed) (6 Form C) 1-29/32" L. x 1-5/16" W. x 2-9/16" H. (Hermetically sealed).

The standard TS structure with a life of 100 million operations will soon be available.

P&B STANDARD RELAYS ARE AVAILABLE AT YOUR LOCAL ELECTRONIC, ELECTRICAL AND REFRIGERATION DISTRIBUTORS

Potter & Brumfield, inc. PRINCETON, INDIANA

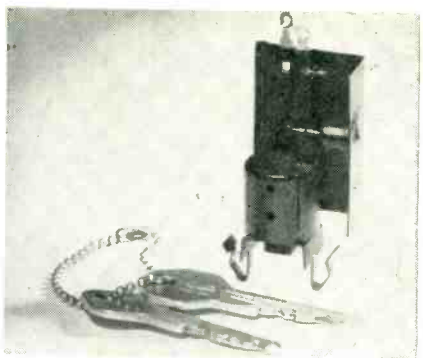
See our catalog in Sweet's Product Design File.

Subsidiary of AMERICAN MACHINE & FOUNDRY COMPANY Manufacturing Divisions also in Franklin, Ky. and Laconia, N. H.

transistorized digital counter. Teamed with appropriate conversion equipment, the unit counts articles, distance, degrees of rotation or angular measurements, at high speeds. Small size and moderate cost are obtained by employing printed circuit boards and modular construction. Total power consumption of the counter (two w) is no more than the filament power required by a typical tube.

▶**Specifications** — Counting frequency is 15,000 cps, with higher speed provided as a special; input power, 60-cycle, 85 to 140 v; and resolution, 10 μsec. Size is four in. high by 11⅝ in. wide by 9⅛ in. deep. The counter can be preset anywhere from one to 500 for batch counting.

In operation, the output of a suitable transducer is sent to transistorized flip-flops within the counter. These in turn, when the desired number is reached, cause an output relay to function. Selling price is below $400 and includes counsel on how to use the unit and help in engineering it into a system. Literature is available on request. **Circle P82 inside back cover.**



GERMANIUM RECTIFIERS
for mass-produced tv sets

GENERAL ELECTRIC CO., Syracuse, N. Y. A new line of germanium rectifiers are the first ones electrically and mechanically designed by the company for tv set power supplies. The complete absence of aging effects in products made from germanium allows full rated performance over the entire life of the new rectifiers.

The new tv rectifiers also feature an extremely low forward

LARGE WAVEGUIDE

Slotted line for waveguide size WR 2100. Covers range of 350-530 mc. Probes tunable over entire band. Inherent VSWR less than 1.02—slope less than 1.01. Features bolted and doweled aluminum construction.

LARGE
WAVEGUIDE & COMPONENTS
WR 770 to WR 2300 (1450 down to 320 mc)

To complement the waveguide presently being supplied for major military and commercial applications in radar and scatter communications systems, we now offer a complete line of components and test equipment.

Terminations. Aluminum construction. Engineered to absorb virtually all incident power. Load is adjustable with locking device to secure it in any position.

Attenuators. Vane type designed to provide 20 db of attenuation with a minimum of mismatch. Calibration curves available.

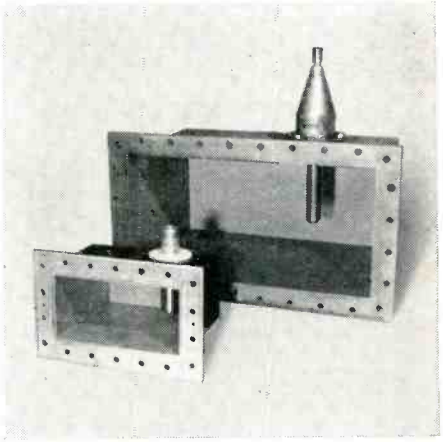
Directional couplers. Bolted and doweled aluminum construction. Power split to customer requirements.

Special components. Including waveguide switches, duplexers, diplexers, series and shunt tees, rotary joints, and special shapes.

All items are in production now and are available on short term delivery. For more information, write I-T-E Circuit Breaker Company, Dept. 55, Special Products Division, 601 East Erie Ave., Philadelphia 34, Pa.

VISIT THE I.R.E. SHOW, March 18-21
See this equipment displayed at Booth 1313-1315

I-T-E CIRCUIT BREAKER COMPANY
Special Products Division

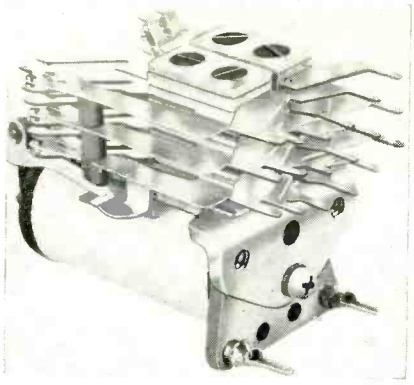


Waveguide to coaxial transitions. High-strength, lightweight aluminum construction. Supplied as standard with 3⅛ in. coaxial connector (for WR 770 size, 1⅝ in.). Adapters to other sizes available. All transitions designed for high power handling capacity.

voltage drop and thus can provide a higher d-c output than any other type of rectifier. They are designed with a mechanical snap-in type structure to help tv manufacturers minimize chassis assembly costs.

The three rectifiers are RETMA type designated 1N573, 1N575 and 1N581. The 1N573 is a half-wave rectifier capable of 250 mw d-c output. The 1N575 is designed for 350-ma d-c output. The 1N581 consists of two germanium rectifiers connected in a voltage doubler configuration and has a d-c output rating of 250 ma.

The full-cycle, average full-load voltage drop for the 1N573 is rated at a maximum of 0.15 v; for the 1N575, 0.30 v, and 0.15 v for each section of the 1N581. The rectifiers are hermetically sealed in metal cases. **Circle P83 inside back cover.**

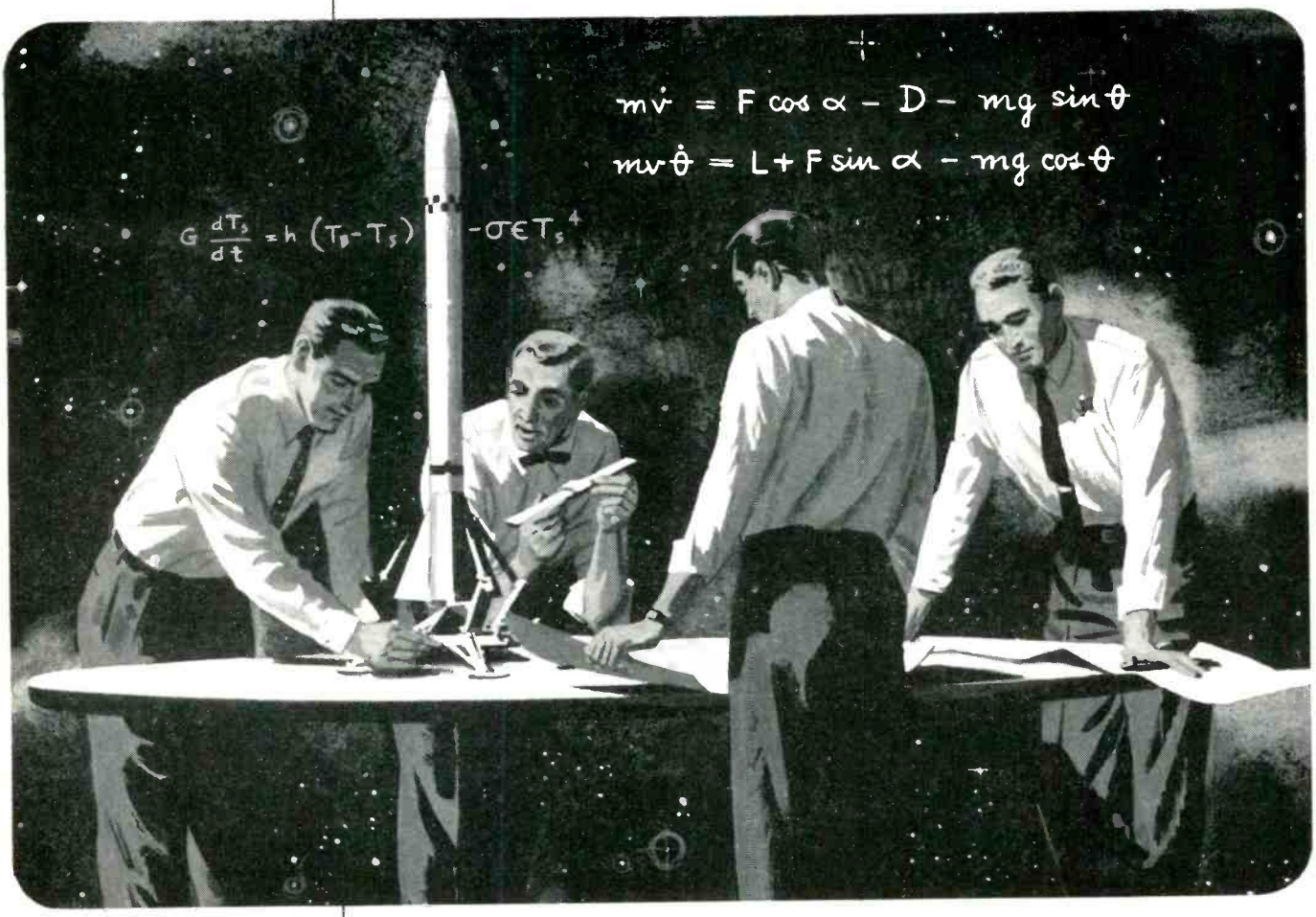


RELAY
printed circuit terminals

PHILLIPS CONTROL CORP., Joliet, Ill. The type 8 relay may now be had with printed circuit terminals. These terminals are available with standard twin contact springs which have been widely used for maximum reliability in switching circuits or with single contact springs or power-type contacts for switching large current loads. For very low-level loads, gold alloy or other special contact materials are available.

Terminals are tinned for ease of soldering and for ready insertion into the circuit board. They are ribbed for added strength, fully supporting the relay and eliminating mounting screws. Terminals for the contact springs are spaced

IMPORTANT ACHIEVEMENTS AT JPL



Engineering Teamwork in Missile Development

The Jet Propulsion Laboratory is a stable reseach and development center located north of Pasadena in the foothills of the San Gabriel mountains. Covering an 80 acre area and employing 1700 people. it is close to attractive residential areas.

The Laboratory is staffed by the California Institute of Technology and develops its many projects in basic research under contract with the U.S. Government.

Opportunities open to qualified engineers of U.S. citizenship. Inquiries now invited.

Engineers and scientists interested in a wide range of activities will appreciate the fluid character of the research and development projects in progress at the Jet Propulsion Laboratory. These projects include research in the fields of Electronics, Physics, Applied Mathematics as well as the design, development and analysis of guided missile systems.

These men, though individually responsible, work together as a thoroughly integrated team on all of the aspects of the entire missile system instead of concentrating on certain highly specialized missile components.

Since this work includes projects involving guidance, electronics, systems analysis, structures, propulsion etc., which are constantly influenced by continuing Laboratory research, the comprehensive program contains problems which are challenging to individuals with interests in virtually every phase of engineering and science.

The great diversity of activity and constant progress being made in the various fields of endeavor by the staff of the Jet Propulsion Laboratory has proved to be a stimulating attraction to qualified people interested in pioneering in basic research, applied research and development engineering in the guided missile field. The result of this has been to bring together a congenial group of forward-looking engineers and scientists who are intensely interested in the pioneering projects now in progress at the Laboratory.

Additional men of this type are needed and if you are interested and feel you are qualified, send your resume today for immediate consideration.

JOB OPPORTUNITIES ARE NOW AVAILABLE

jpl

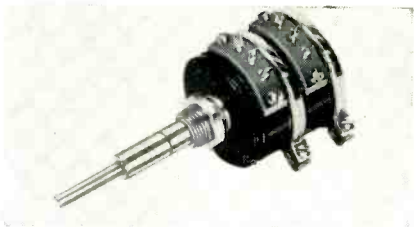
ELECTRONICS • PHYSICS • SYSTEMS ANALYSIS
COMPUTER DEVELOPMENT • INSTRUMENTATION
TELEMETERING AND MECHANICAL ENGINEERING

JET PROPULSION LABORATORY

A DIVISION OF CALIFORNIA INSTITUTE OF TECHNOLOGY

PASADENA • CALIFORNIA

for maximum clearance but do not exceed standard dimensions of the type 8 relay. Coil terminals are located on the same centers as on the standard relay and dual coils employing four coil terminals are available. **Circle P84 inside back cover.**



PRECISION POTS
concentric-shaft design

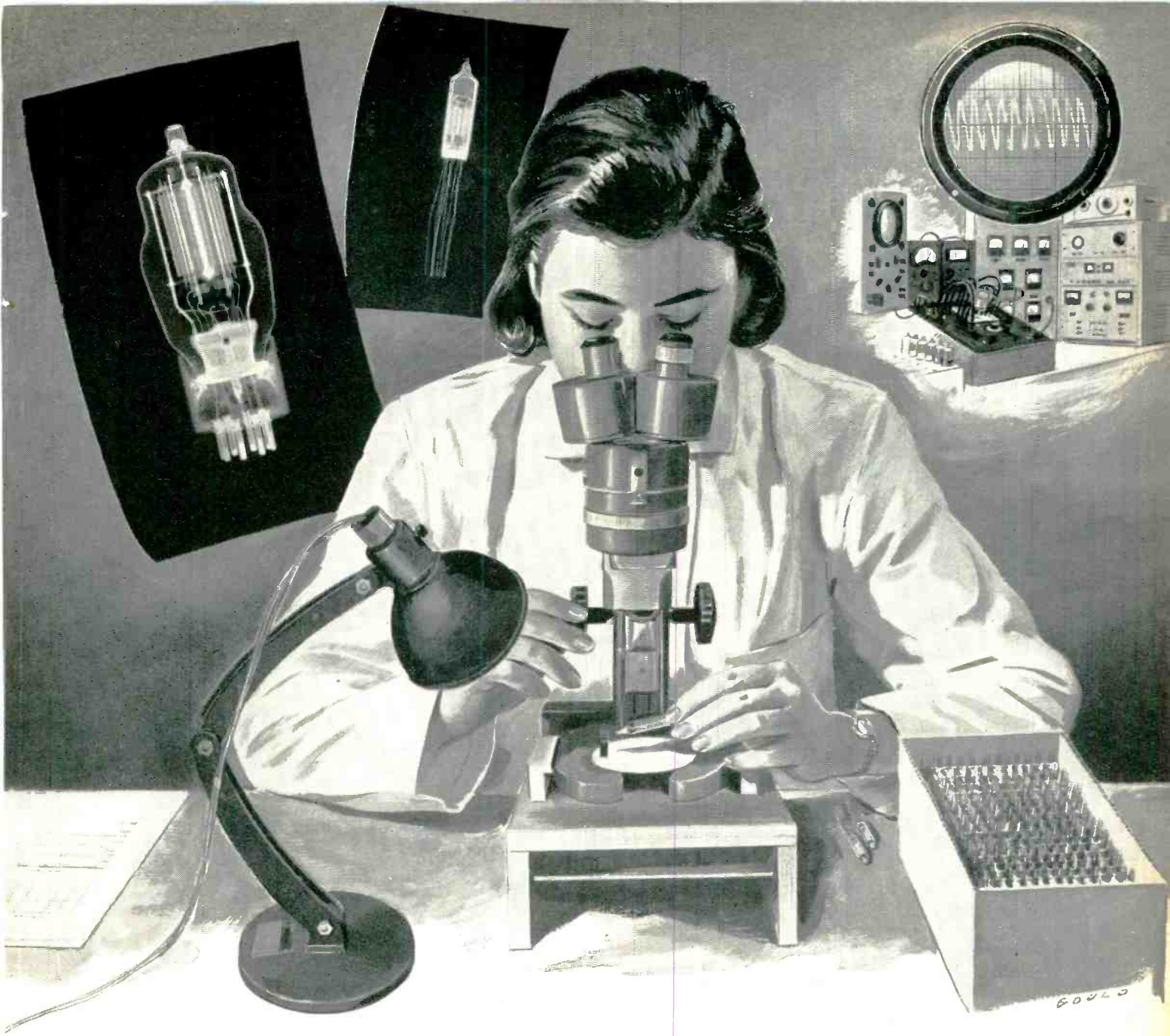
WATERS MFG., INC., P. O. Box 368, South Sudbury, Mass. The new concentric-shaft design, available in the company's precision pots, permits two potentiometers to be single-hole mounted for control by a dual knob. The tandem-mounted pots have standard $\frac{1}{8}$ and $\frac{1}{4}$-in. shafts. The assembly is mounted by the usual $\frac{3}{8}$-in. threaded bushing or can be supplied with servo-style mounting.

The concentric-shaft potentiometer assembly, type APC-1-$\frac{1}{4}$, can be furnished with any combination of the resistance ranges available in Waters AP-1-$\frac{1}{4}$ or RTS-$\frac{3}{8}$ pots, with stops, or for continuous rotation of either or both elements. **Circle P85 inside back cover.**

CAPACITORS
with ceramic dielectric

CAMBRIDGE THERMIONIC CORP., Cambridge, Mass., announces a rugged new series of stand-off capacitors with ceramic dielectric, series X2122. Available in a group of values, they are general r-f bypass capacitors for use in high quality electronic equipment.

The encapsulating resin provides exceptional rigidity and durability under extreme condi-



"An infinite capacity for taking pains"

The above familiar phrase is usually given as a definition of genius. We borrow it as a job description.

The lengths to which our Quality Control people go, to insure the reliability of our complex products, are truly painstaking, and are applied equally to components we make ourselves and those we purchase from outside suppliers.

For example, consider vacuum tubes, the heart of hundreds of projects in our Electronics Division. No spot check satisfies here (even if that's all our customer specifies)—but a whole series of critical tests, including such precise evaluations as these:

Inspection of tube characteristics to rigid Stromberg-Carlson specifications—performed on special equipment which can do in a half-hour what would take days on conventional testing devices.

Inspection by X-ray, looking for deeply hidden potential faults which could cause malfunction at any time after first use.

Inspection by microscope, seeking welding faults, minute cracks in glass, and even infinitesimal loose particles inside the tube.

And tubes are only one concern. *All* components must pass similarly rigid tests, to assure operating performance, ruggedness and reliability in the completed equipment.

You can't put a price on "taking infinite pains." You *can* place your confidence in a company where this is everyday procedure.

S-C STROMBERG-CARLSON

STROMBERG-CARLSON COMPANY

A DIVISION OF GENERAL DYNAMICS CORPORATION

General Offices and Factories at Rochester, N. Y.—West Coast plants at San Diego and Los Angeles, Calif.

GD GENERAL DYNAMICS

tions of shock, vibration and humidity. A unique design feature minimizes breakage of the dielectric ceramic due to flexing of the chassis and mounting surfaces.

The X2122 capacitors mount by a single 6-32 threaded stud, ¼ in. long. Overall height when mounted is less than ⅜ in. The mounting stud is 7/16 in. hexagonal brass that has been gold flashed. The solder terminal is also gold-flashed brass. **Circle P86 inside back cover.**

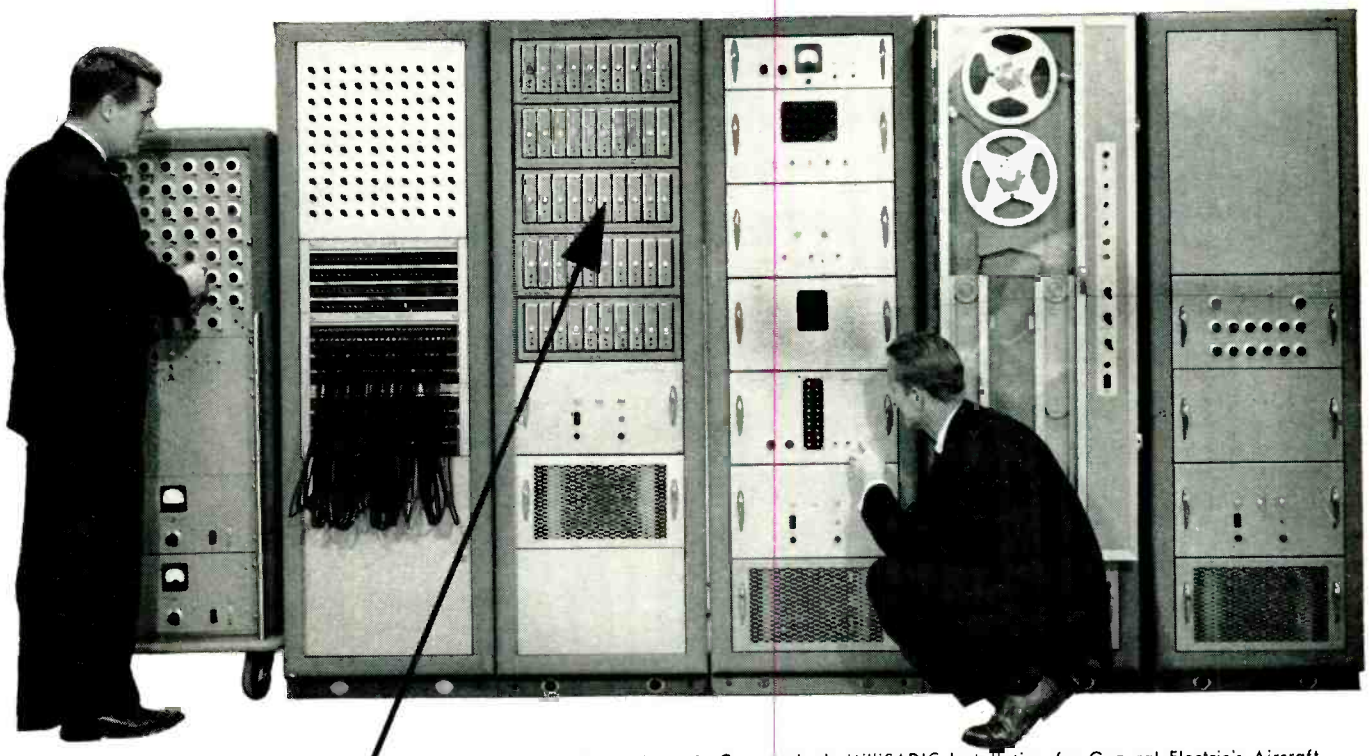
ARMORED RELAYS
in 1, 2 and 3-pole models

EBERT ELECTRONICS CORP., 212-26 Jamaica Ave., Queens Village 28, N. Y., has available a full line of accident-proof armored mercury plunger relays. Ilustrated is one of the many models, the spst HDC-1 for all loads up to 60 amperes at 115 v, a-c.

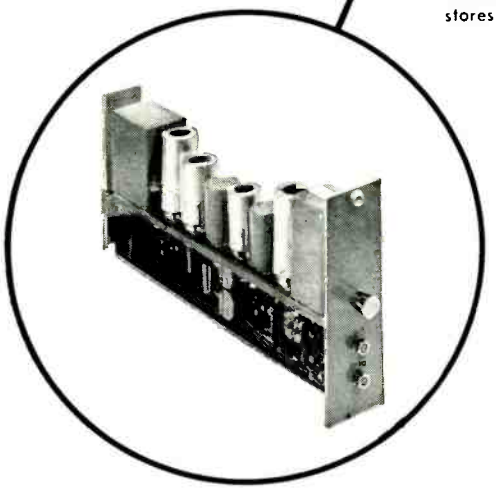
These rugged encapsulated-tube relays were specifically designed to withstand shocks, blows and physical impact. The standard 35-ampere or heavy duty 60-ampere hermetically sealed, mercury-to-mercury action contactor tubes are potted in special high-temperature material and plasticoated, rigid aluminum shells.

For corrosive atmospheres, the company's relay coils are also available in all standard operating voltages, fully encapsulated in approved polyester resin compound. By carrying their own armor and

Honeywell Preamplifiers combine isolated input with accuracy of 1 part in 2,000 in the CEC MilliSADIC



Consol dated Electrodynamic Corpo atian's MilliSADIC Installation far General Electric's Aircraft Nuclear Propulsion Dept., Cincinnati samples 400 jet engine temperatures per second and stores this information in digital form.



Honeywell Data Handling D-C Amplifier, Model 2HDH-2. This type is used as preamplifiers in the CEC MilliSADIC shown above.

The *isolated input* of the Honeywell Data Handling D-C Amplifiers, Model 2HDH-2 makes them ideally suited as preamplifiers to raise the input signals from thermocouples and strain gauges to the level required by the analog-to-digital conversion system of CEC's MilliSADIC installation at General Electric's Aircraft Nuclear Propulsion Dept., Cincinnati. The low noise level, high degree of linearity and zero and gain stability of these amplifiers provide the accuracy of 1 part in 2,000 required for this application. The exclusive Honeywell Second Harmonic Converter as the input element of these amplifiers provides the bonus features of ultra high common mode rejection and resistance to pick-up.

Honeywell Data Handling D-C Amplifiers, 2HDH Series, are compact plug-in, rack-mounted units specifically designed for use as preamplifiers in data processing systems. These amplifiers are available in the input range, rise time, frequency response or gain specifications required by many data processing systems. Other amplifiers in this series can accept as many as 150 separate D-C signals per second. *Write for Bulletin 2HDH* . . . Minneapolis-Honeywell, Boston Division, Dept. 7, 1400 Soldiers Field Road, Boston 35, Mass.

MINNEAPOLIS **Honeywell** H HONEYWELL

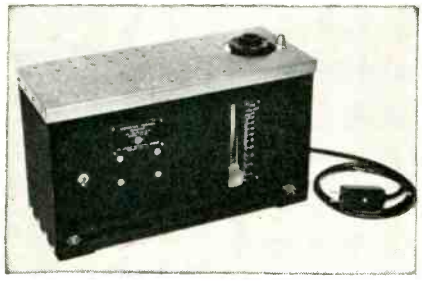
BOSTON DIVISION

having hermetically sealed non-wearing contacts, these mercury plunger relays require no more than ordinary general-purpose enclosures in most applications. Detailed information and prices are available. **Circle P87 inside back cover.**

DETECTOR UNIT
checks missing pulses

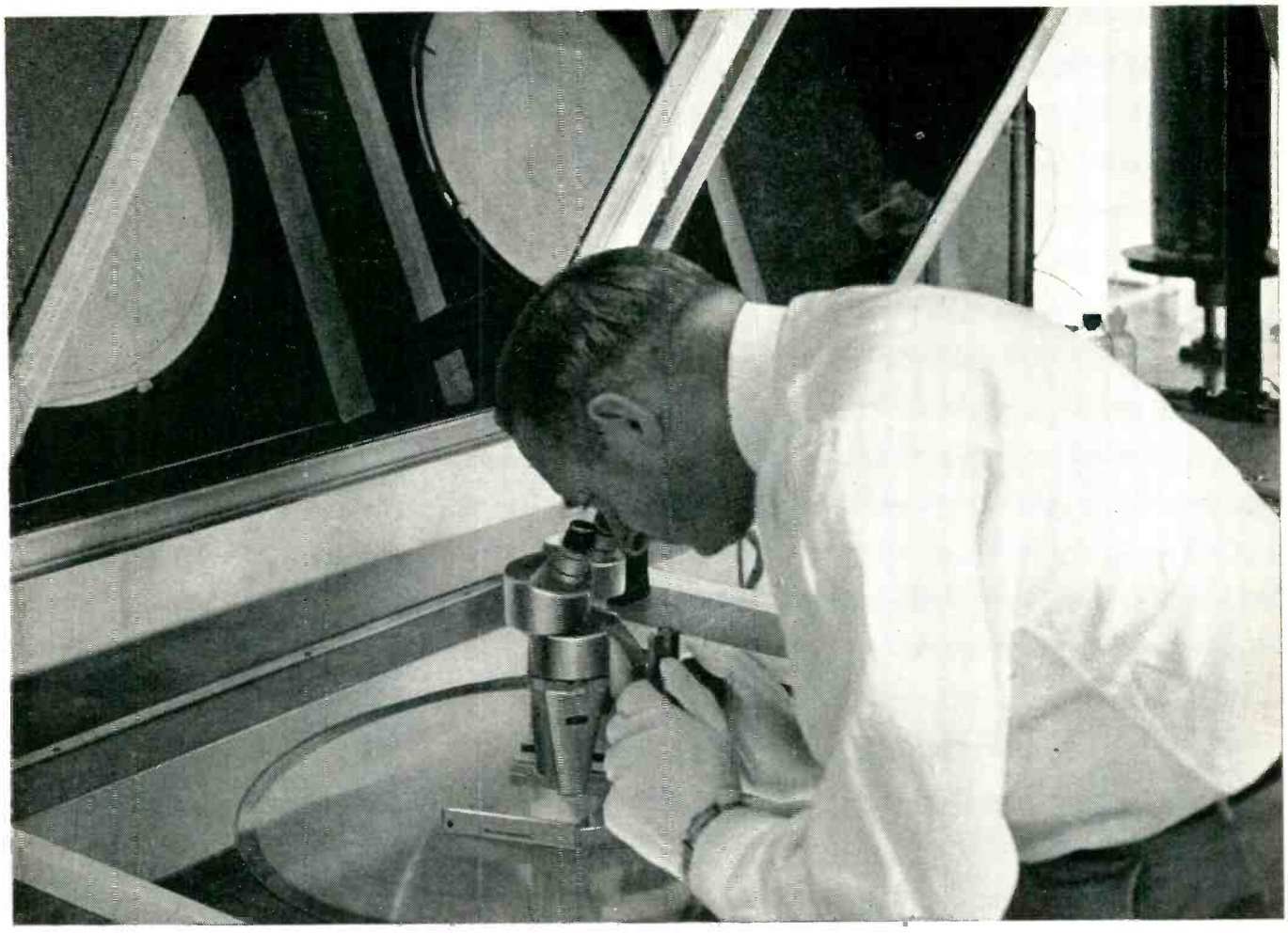
MANSON LABORATORIES, 207 Greenwich Ave., Stamford, Conn. Model PD11A is a precision instrument for checking the performance of pulse-modulated magnetrons, klystrons and similar types. The set incorporates two input connectors, one for the negative detected r-f pulse, the other for a negative reference trigger. The r-f pulse is integrated and used to fashion a negative gate for squelching the reference trigger. In the case of a missing pulse, the output is a positive 15-v pulse registered on a counter.

Complete technical specifications are available in a descriptive bulletin. **Circle P88 inside back cover.**



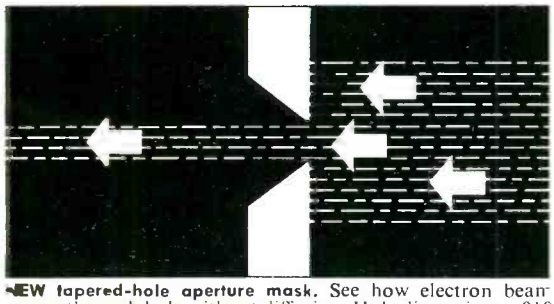
VIBRATION TESTER
meets MIL-Std-202 specs

THE AHRENDT INSTRUMENT CO., 4910 Calvert Road, College Park, Md. Model 14-28 vibration test-

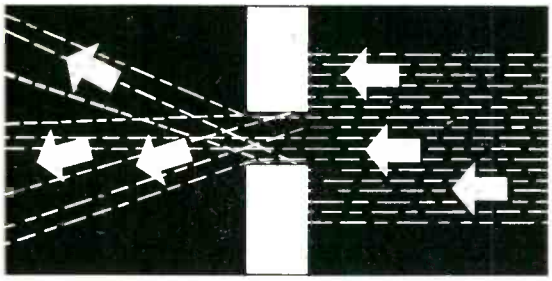


Get Sharper, Truer Color TV Pictures

New tapered-hole aperture mask reduces beam diffusion . . . minimizes false color . . . can be used in present design picture tubes



NEW tapered-hole aperture mask. See how electron beam passes through hole without diffusion. Hole dimensions: .010 in. small diameter; .015 in. large diameter. There are nearly 500,000 of these holes in each mask—all controlled to close tolerance.



OLD cylindrical hole aperture mask. Electrons striking aperture walls are scattered over several dots.

Here's another long step forward toward better color television—one that doesn't require radical changes in circuitry or picture tube construction. It's an improved aperture mask made by Superior Tube* that can be used in the picture tubes you are now using.

Ideally, an aperture mask should have zero thickness. Because electrons impinging on the walls of cylindrical holes are deflected out of the narrow beam and sometimes strike adjacent color dots instead of the single dot they are directed at. The result is a hazy picture or false color. But with these new Superior Tube tapered-hole aperture masks, beam diffusion is practically eliminated. The walls of the tapered holes lie outside the path of beam electrons—even at the extreme edges of the picture. The electrons see only the holes.

These new aperture masks demonstrate how accurate and to what close tolerances Superior Tube can fabricate metal components. For complete information, write for Data Memo No. 5. Superior Tube Company, 2500 Germantown Ave., Norristown, Pa.

**Manufactured by Superior Tube Co. under license from Buckbee Mears, Co., St. Paul, Minn.*

Other parts Superior Tube makes for use in color TV receivers include three different types of disc cathodes (miniature, narrow neck and standard), seamless anodes, and a complete line of sleeve-type cathodes. Superior Tube is the world's largest independent supplier of cathodes for use in electron tubes.

Superior Tube

The big name in small tubing

NORRISTOWN, PA.

Johnson & Hoffman Mfg. Corp., Mineola, N.Y.—an affiliated company making precision metal stampings and deep-drawn parts such as those used in the electron guns that go with this new cathode.

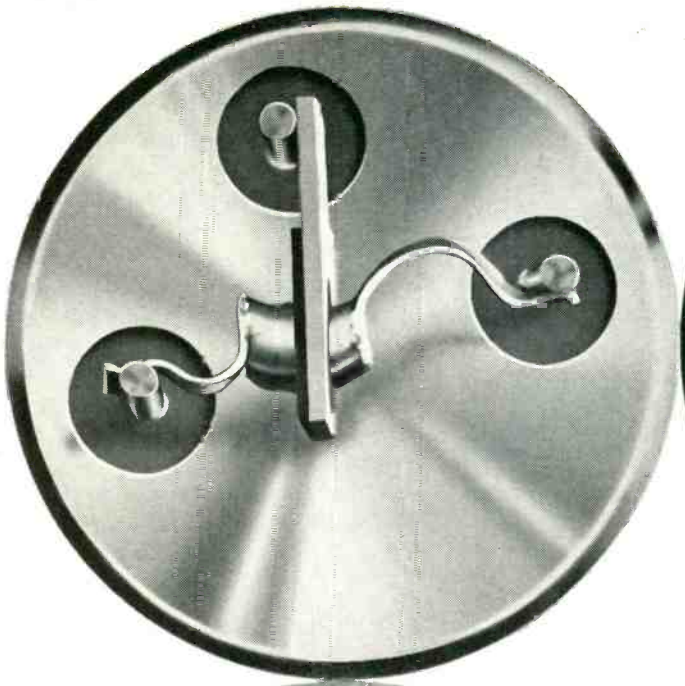
ing machine is constructed on a rugged cast aluminum base which houses the drive motor and variable speed drive mechanism. Linear sinusoidal motion is imparted to the spring flexure mounted table by a connecting rod driven by a ball bearing mounted eccentric cam. The eccentric cam is driven by a cone-type variable speed drive powered by a 1/15-hp split-phase induction motor. Frequency adjustment is provided on the front of the machine. Amplitude setting is provided at the top right side of the table by means of the eccentric adjustment. Unidirectional table vibration is assured by table rigidity and unique flexure suspension system.

Specifications and an outline drawing are available on request. Price of the machine is $295. **Circle P89 inside back cover.**

PULSE GENERATOR
completely transistorized

CUBIC CORP., 5575 Kearny Villa Road, San Diego 11, Calif. Model 502 pulse generator is a completely transistorized test equipment using printed circuitry. It provides a pulse length from 0.5 to 3 μsec in three steps with a 20-v peak into an 800-ohm load. The positive or negative pulses are continuously variable from zero to full amplitude and the instrument may be easily modified to accomplish external modulation.

With negligible jitter, the pulse shape shows a rise and decay time of 0.1 μsec or less; tilt and overshoot is less than ±2 percent over average amplitude at maximum pulse output. Repetition rate on internal sync is from 50 to 5,000 pps, and on external sync



WHEN CAN ONE TRANSISTOR REPLACE 2?

In computer or in other applications where current must be amplified in either direction, you can now specify General Transistor's new GT-34S bi-directional transistor.

As developed by GT, this symmetrical transistor can also be used as a bi-directional switch when placed in series with the load. For greater reliability, to save production time, and for compactness you should examine GT's-34S . . . another reason for General's leadership in the manufacture and development of transistors for computers.

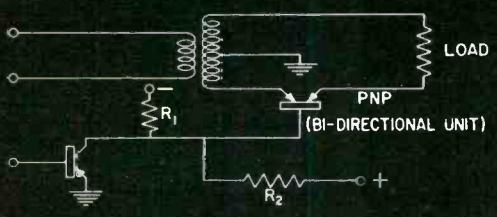
Write for Bulletin GT-34S for complete specifications.

I.R.E. Booth 3828

GT's-34S magnified 10½ times.

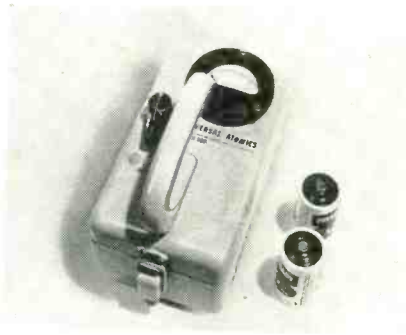
Maximum collector to base voltage	40 volts
Maximum emitter to base voltage	40 volts
Peak current	½ amp.

DC current gain is > 10 when I_b = 20 ma, Vce ≦ .3 V.



GENERAL TRANSISTOR CORP. 91-27 138th Place, Jamaica 35, N. Y. OLympia 7-9700

from 0 to 5,000 pps. Internal impedance is 100 ohms or less on either pulse polarity. Sync may be positive or negative at 1 v minimum to 20 v peak-to-peak maximum. Sync output provides positive or negative 10 v peak into a 2,000-ohm load with a duration of approximately 1.5 μsec at the half voltage point and a rise time of 0.5 μsec. Pulse position is available in two ranges: 0 to 20 and 0 to 200 μsec after sync output. Price is $325 including battery and instruction manual. **Circle P90 inside back cover.**



SURVEY METER
with transistorized circuit

UNIVERSAL ATOMICS CORP., 143 E. 49th St., New York 17, N. Y., has developed a highly efficient radiological survey meter model No. 407 for civilian defense units and laboratories with limited budgets. The 3½-lb unit was designed for surveying radiation dosage, leakage and contamination. It operates on two standard flashlight cells for long life; has three methods of indication (a meter, flashing light and earphone) and, due to a high gain transistorized circuit, features high efficiency. Complete cost is only $79.50. **Circle P91 inside back cover.**

FILTERS, CAPACITORS
smaller, more efficient

AIRBORNE ACCESSORIES CORP., Hillside, N. J., has added to its line of aircraft equipment smaller, more efficient custom-designed filters and capacitors which meet specifications JAN-C-25, MIL-I-61-81-B and MIL-M-8609. As an example of the advantages offered by the new line, the company cites

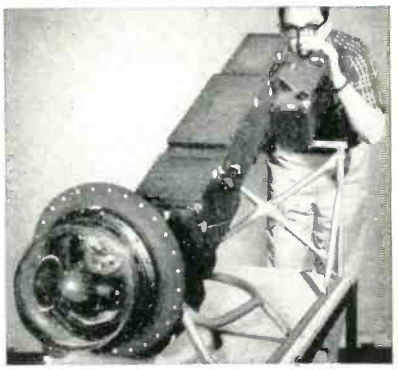
PIONEERING SCIENTIFIC FRONTIERS AT GENERAL MILLS

He's getting new basic knowledge on properties of semi-conductors

Here Dr. Rolf K. Mueller determines electrical properties of a semi-conductor specimen having a low angle grain boundary. He and his colleagues in the Electron Physics Laboratory of the Mechanical Division of General Mills grow their own pure specimens with carefully oriented crystal structures (germanium in this case). They then mount specimens very precisely for basic research involving the effect on physical properties of varying angles of junction. Variation of the angle of crystal orientation at the junction (the "grain boundary") has a predictable effect on the electrical reactions of the semi-conductor.

Semi-conductor work is but one facet of an integrated program in solid state physics. Studies of chemical, mechanical and surface properties of solid crystals and "sputtering" of metals under ion bombardment are among several other areas presently being researched in the Electron Physics Laboratory.

Some of this research is still basic, but it typifies the advanced and creative work we do. In many fields, this "research for tomorrow" is translated regularly into practical applications for industrial and military use today. If you have product or production problems, possibly you can profit from these applications and from our precision production facilities.



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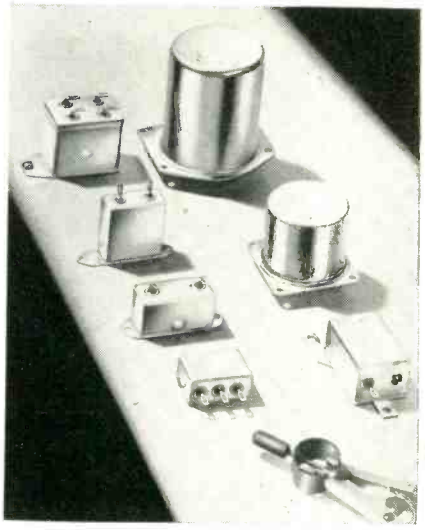
MECHANICAL DIVISION

CREATIVE RESEARCH AND DEVELOPMENT + PRECISION ENGINEERING AND PRODUCTION

General Mills



a 2½-oz capacitor which, at triple the voltage, has twice the capacitance of a conventional 10-oz capacitor. Use of Mylar dielectric and a special conductor permits these reductions in filter and capacitor size and weight while maintaining or increasing capacitance and dielectric strength. Vacuum impregnated with polyamide resin and hermetically sealed in drawn steel cans, these r-f filters and starting capacitors have excellent resistance to vibration, fungus, salt spray and humidity. They retain their properties throughout the temperature range — 65 to + 300 F. **Circle P92 inside back cover.**

ALIGNMENT INSTRUMENT
for the 10 to 145 mc range

KAY ELECTRIC CO., 14 Maple Ave., Pine Brook, N. J. The Radaligner model V is a complete alignment instrument designed for the 10 to 145 mc range. It includes a sweeping oscillator, calibrated variable-frequency marker and fixed crystal-controlled markers.

The new fundamental-frequency sweeping oscillator is continuously variable in six overlapping bands ac-

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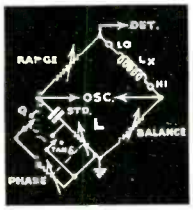
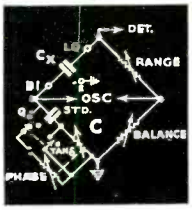
Inductance from 1 μH to 100 H, Capacitance from 1 $\mu\mu$F to 100 μF, and Resistance from 0.1 Ω to 10 MΩ Single direct-reading LCR dial — no multiplying factors involved. Continuously variable a.c. bridge voltage and automatic detector sensitivity control.

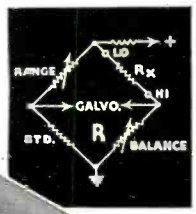
L at 1 or 10 kc



C at 1 or 10 kc



R at d.c.



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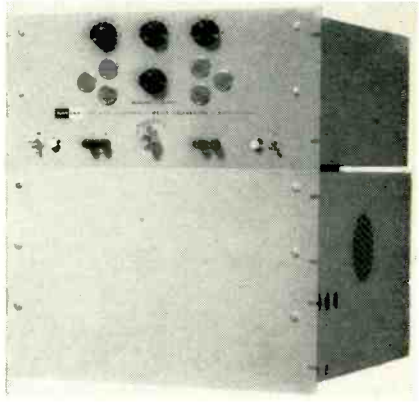
curately calibrated on a direct-reading dial. Sweep widths are provided variable to 60 percent of center frequency below 50 mc, 30 mc above 50 mc. The r-f output voltage is 1.0 v rms into 70 ohms, agc'd for ±0.5 db flatness over widest sweep and tuning range.

The variable marker is a birdie pip marker generated by a separate c-w oscillator continuously variable from 5 to 170 mc in six overlapping bands and calibrated to ±1 percent on a separate direct-reading dial.

Eleven individually-switched, crystal-controlled pulse-type markers at customer-specified frequencies are provided for both separate and simultaneous operation. **Circle P93 inside back cover.**

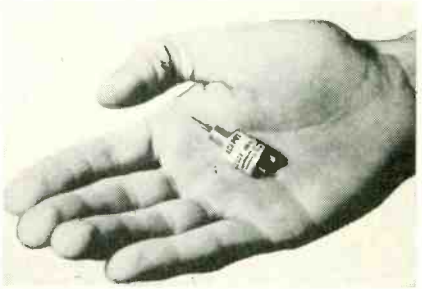


METER CALIBRATOR
has many applications

KAY LAB, 5725 Kearny Villa Road, San Diego 11, Calif., announces a new improved model M100A-20 meter calibrator which provides d-c from 0 to 1,000 v at 0 to 200 ma with 0.01-percent long-time stability, 0.01-percent line and load regulation, 0.2-millisecond response time, 0.05-percent calibration tolerance, less than 2-mv hum and noise and less than 0.01-ohm output impedance.

The instrument employs high gain chopper amplifiers to constantly compare the output voltage with an internal standard cell, providing high accuracy and stability regardless of line or load variations. Direct-reading calibrated dials permit instant selection of the desired output voltage. Outputs are provided for both regulated voltage and current. The

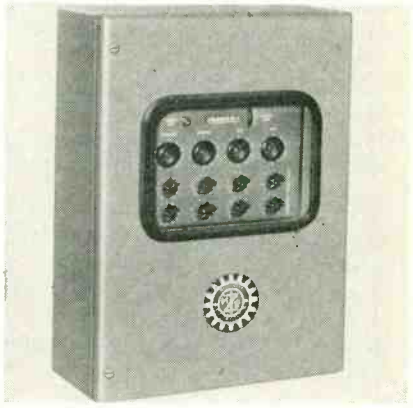
M100A-20 is ideal for laboratory and production meter calibration, standards laboratories computer facilities, nuclear research and many other applications. **Circle P94 inside back cover.**



SUBMINIATURE POTS
rated to 250,000 ohms

ACE ELECTRONICS ASSOCIATES, INC., 103 Dover St., Somerville 44, Mass., announces new Acepots with resistance range from 10 ohms to 250 K and the extremely fine linearity of ±0.3 percent. They measure only ½ in. by ½ in.

▶ **Other Specifications**—Weight is ¼ oz; power, two w for 60 C rise; ambient temperature, −55 C to 150 C. The potentiometers are available in standard threaded bushing, servo or flush mountings, and ganged units. All units are fully sealed, moisture-proofed, and antifungus treated. They meet applicable portions of JAN specifications and MIL-E-5272A standards. **Circle P95 inside back cover.**



PRESET COUNTER
for industrial applications

MACHINERY ELECTRIFICATION, INC., Northboro, Mass. The MEK-2094-AG electronic counter was de-

signed for all industrial counting applications and will count from 0 to 5,000 counts per sec without special adjustment or circuit changes. The counter will operate with photoelectric, semiconductor, magnetic or contact making pick-ups. At the end of the warning and final count, plug-in relays are energized for control purposes. After reaching the end of count the counter can be reset to zero.

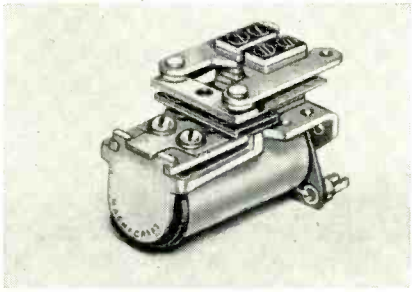
Operating personnel will be interested in the enclosure design which provides visible observation without opening the dust-tight, oil-tight (NEMA 12) enclosure. When a change in setting is required, the enclosure can be opened by nonelectrical personnel as the unit is dead front (NEMA 1) with the door open.

Features, specifications and general information are presented in a looseleaf catalog section and price list. Application data and diagrams are shown with photographs of the various forms available. **Circle P96 inside back cover.**

STORAGE SCOPE
available in two models

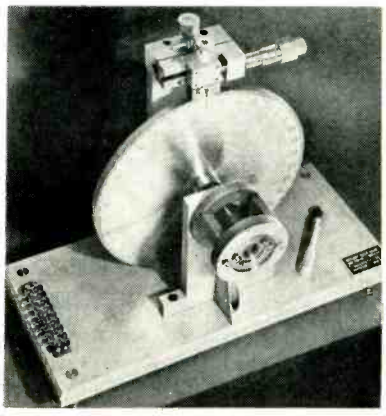
HUGHES PRODUCTS, International Airport Station, Los Angeles 45, Calif. Model 103 Memo-Scope incorporates the Memotron Ray storage tube. The instrument combines the unique quality of information persistence with all the features of a superior quality laboratory oscilloscope. It captures and retains any number of traces indefinitely at a constant intensity until intentionally erased. Traces are readily visible in a brightly lighted laboratory and may be easily photographed. The scope is available in two

models: portable (13 in. wide, 14 in. high, 20 in. deep) and rack mounted (14 in. by 19 in.). **Circle P97 inside back cover.**



SMALL RELAY
switches heavy current

MAGNECRAFT ELECTRIC CO., 3350 W. Grande Ave., Chicago 51, Ill. Reliable switching of heavy current in limited space through long service life is achieved by a new class 22D telephone type relay. A unique feature is specially designed double break contacts that switch up to 20 amperes, noninductive load. Contacts are spst, normally open. Overall dimensions are 2 1/16 in. long, 1 3/16 in. high, 1 1/16 in. wide. It is available for operating voltages to 230 d-c and 440 v, 60 cycle, a-c. **Circle P98 inside back cover.**



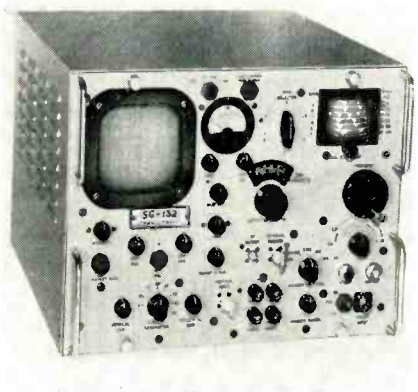
ROTARY TEST HEAD
for shaft position indexing

MILLITEST CO., 88 Madison Ave., Hempstead, L. I., N. Y., has added to its line of component test instruments, the rotary test head, designed to permit rapid and accurate indexing of shaft position on rotary components such as potentiometers, resolvers, synchros and the like.

This fixture consists of a pre-

cision gear fixed to a shaft and chuck. The wheel can be positioned in half-degree steps through a rack engagement. A micrometer advance on the rack mechanism permits fine phasing to within one-half minute. The repeatability of settings is to within one part in 200,000.

The test fixture is supplied with a case-holding nest carrying pilot diameters for standard potentiometers. Adapters of various types to accommodate special components are available. **Circle P99 inside back cover.**



SWEEP GENERATOR
for vhf-uhf operation

TRANSITRON, INC., 186 Granite St., Manchester, N. H. Model SG-132 combines all the essential features of a standard c-w and a-m signal generator and a wide-band sweep generator. Among its many applications are testing and aligning vhf-uhf communication receivers, measuring sensitivity, selectivity, image rejection and gain of receivers, i-f amplifiers, broadband amplifiers, tv and other equipment. It offers a wide sweep width—40 percent of the center frequency, from 15 to 400 mc, with a dial accuracy of 0.1 percent, crystal corrected.

The output, which is entirely fundamental (not beat-frequencies), is calibrated from 0.1 to 150,000 μv throughout the frequency range. An unusual feature is the constancy of this output which varies less than $\pm$0.2 db over the entire range. The equipment also has an integral d-c coupled oscilloscope. **Circle P100 inside back cover.**

New Literature

Digital Computer. Bendix Computer Div., Bendix Aviation Corp., 5630 Arbor Vitae St., Los Angeles 45, Calif. A six-page illustrated bulletin describing the G-15D general-purpose digital computer and its digital differential analyzer accessory, is now available. With the two units discussed, linear and nonlinear differential equations are solved accurately and rapidly. New programming techniques and a complete new line of input and output equipment are also described. **Circle L1 inside back cover.**

Facilities Brochure. Neutronics Research Co., 165 Lake St., Waltham, Mass., has published a prospectus showing the company background and indicating its availability for R & D contracts and subcontracts in the fields of countermeasures, communications, medical electronics, educational devices, instrumentation and control circuits. **Circle L2 inside back cover.**

Instrumentation Tape Recorder. Ampex Corp., 934 Charter St., Redwood City, Calif. Capabilities and characteristics of the FR100 instrumentation tape recorder are described in an attractive 20-page booklet. Detailed specifications are also provided in the four-color booklet.

Numerous illustrations show transports, heads and modular electronic assemblies used with the FR100. Where necessary, graphs are provided to clarify specifications and recorder operation.

The recorders discussed are used in data acquisition, storage, analysis and reduction, in machine and process programming and in dynamic simulation. Data may be recorded and reproduced in the d-c to 100-kc frequency range on one to 14 tracks at any of six standard tape speeds, 1⅞ to 60 ips. **Circle L3 inside back cover.**

H-F Resistors. International Resistance Co., 401 North Broad St., Philadelphia 8, Pa. Catalog data bulletin F-1a covers types MP and HFR high-frequency and miniature high-frequency resistors. Comprehensive data on construction, characteristics, applications, types, resistance values, tolerances, terminals and installation are detailed in charts and graphs. The eight-page bulletin is available on request. **Circle L4 inside back cover.**

Dynograph Recorders. Offner Electronics Inc., 5320 North Kedzie Ave., Chicago 25, Ill., has issued a 12-page, two-color catalog describing the new Dynograph recorder models. The Dynograph, a high-speed direct-writing oscillograph for the recording of a variety of dynamic and static variables, combines in one unit, three media of recording: ink, heat sensitive, or electric sensitive with either curvilinear or rectilinear coordinates.

Described in detail are the principles of operation, specifications, assemblies and construction of the four models—console, computer console, rack mounted and portable.

A special selection chart shows the many features available in the various types of assemblies and the alternate mountings. For low-gain applications such as telemetering and computer write-out, specially designed simplified assemblies are supplied. **Circle L5 inside back cover.**

Test Equipment and Components. Northeastern Engineering, Inc., Manchester, N. H., has available a 24-page catalog of electronic test equipment and components. It contains illustrated descriptions and technical specifications for decade counters, a frequency meter, spectrum analyzer, electronic multimeter, f-m radio receiving set, electronic counter and a signal generator. **Circle L6 inside back cover.**

Precision Switch. Micro Switch, a Division of Minneapolis-Honeywell Regulator Co., Freeport, Ill. Preliminary data sheet 115 covers the 1RA1 subminiature screw-

driver-actuated switch. The switch described gives designers of computers, electrical devices and electronic equipment a switch that is handy where limited access is desired or when the switch is used only occasionally. Price, quantity discounts and electrical ratings are shown. **Circle L7 inside back cover.**

Micromicroammeters. Leeds & Northrup Co., 4907 Stenton Ave., Philadelphia 44, Pa. Two types of micromicroammeters for nuclear-reactor control systems are described in data sheet E-03(1).

One of the nuclear control system components discussed, with integral range switch and meter, is designed for control-panel mounting. The other utilizes a bidirectional Ledex mechanism and can be installed remotely from the panel.

Complete engineering features and ordering information for each model are listed. **Circle L8 inside back cover.**

Alloy Guide. Techalloy Co., Inc., Rahns, Pa. A new selector guide for high-temperature, heat-resisting alloys is now available. The chart gives vital data on comparative strengths at high temperatures, scaling resistance, individual characteristics and comparative prices. Alloys covered are Inconel, Inconel X, Incoloy, Techalloy 80 Ni 20 Cr, stainless and heat-resisting steels—types 330, 310, 314, A-286 and N-155. **Circle L9 inside back cover.**

Microphone Calibration Apparatus. Brush Electronics Co., 3405 Perkins Ave., Cleveland 14, Ohio. The new microphone calibration apparatus, model BL-4119, is illustrated and described in a new catalog sheet. The apparatus discussed enables both a calibration procedure which is a simplified form of the standardized reciprocity calibration technique in accordance with the ASA standard Z24.4, and the determination of the complete frequency-response curve of the microphone with the aid of an electrostatic actuator.

The free literature contains de-

tailed design, operating and installation information which suggests various application opportunities. One side of the sheet covers detailed specifications of the instrument. **Circle L10 inside back cover.**

Autopilot Control. Minneapolis-Honeywell Aeronautical Div., 2600 Ridgeway Road, Minneapolis 13, Minn., has published a six-page pamphlet that describes in detail its MB-3 automatic flight control system for supersonic aircraft. More than two dozen of the principal components of the system are described and pictured in a cutaway of the plane that will use the system. The MB-3 discussed weighs just 98 lb, yet has more than 5,000 different individual parts. **Circle L11 inside back cover.**

Digital and Analog Systems. Mack Electronics, a division of Mack Trucks, Inc., 40 Leon St., Boston 15, Mass., has available data sheets covering a complete line of digital building blocks featuring magnetics and semiconductors. They deal with design and construction of digital and analog systems featuring latest technological developments, stringent environmental capabilities, reliability, compactness and low power. Electrical characteristics and mechanical data are included. **Circle L12 inside back cover.**

New Alnico. Thomas & Skinner, Inc., 1120 E. 23rd St., Indianapolis, Ind. Bulletin DMF-3 gives a description of Alnico 5Cb, including its physical properties, dimensional limitations and a typical demagnetization and energy product curve. It also contains a description of the comparative properties of all of the company's standard permanent magnet materials. **Circle L13 inside back cover.**

TV Transmitter Specifications. Standard Electronics Corp., 285 Emmet St., Newark 5, N. J. Two new tv transmitter specifications bulletins describe the S-E 500 watt and 10-kw vhf tv transmitters (high and low band). The

bulletins contain photographs of the transmitters, complete explanations of how the equipments operate, descriptions and illustrations of major design features, electrical and mechanical specifications, tube lists and block diagrams of both aural and visual transmitters. **Circle L14 inside back cover.**

Silicon Junction Diodes. Hughes Products, A Division of the Hughes Aircraft Co., International Airport Station, Los Angeles 45, Calif., has published new data sheets covering eight types of its standard silicon-junction diodes. They contain the latest information concerning the design, characteristics and specifications of these diodes, which have sharp back-voltage breakdown and evidence extremely low saturation current throughout wide temperature ranges. **Circle L15 inside back cover.**

Enamel and Magnet Wires. General Cable Corp., 420 Lexington Ave., New York 17, N. Y., has published a small reference handbook and guide to the currently available coatings and magnet wires which helps to eliminate the confusion resulting from the great increase in the types of wires available and also in the number of trade names used by the different manufacturers.

The guide lists the basic types with their main advantages and disadvantages and, in addition, gives the trade names and manufacturers under each type. Wires are classified in 10 groups: oleoresinous enamel, Formvar, self-bonding Formvar, nylon, Formvar nylon combinations, polyurethane, class B film insulated, class H film insulated, special types and magnet wires. **Circle L16 inside back cover.**

Glass Products. Croname Inc., 3701 Ravenswood Ave., Chicago 13, Ill., has issued a new bulletin on glass entitled "New Dimensions In Product Design With Decorative Glass." The brochure discusses the properties of glass and the characteristics of glass which make it a versatile material

for producing glass products for radios, television, electronic cabinets, control panels and the like. **Circle L17 inside back cover.**

Epoxy Glass Cloth. Standard Insulation Co., East Rutherford, N. J. Technical data, suggested curing cycles and samples of Stanpreg flame-resistant epoxy resin preimpregnated glass cloth are available. The material described is being used in laminates exhibiting such electrical characteristics as 83,000,000 megohm-centimeters volume resistivity, 25,000,000-megohms surface resistance, and 18,000,000-megohms insulation resistance. It has been engineered primarily for critical electrical and electronic laminates as in printed circuits. **Circle L18 inside back cover.**

Data Recording Cameras. Flight Research, Inc., P. O. Box 1-F, Richmond 1, Va. Multidata cameras, the multiple-purpose precision data recording cameras, are the subject of an eight-page illustrated brochure. Small and lightweight, the Multidata cameras permit automatic synchronized motion picture or single-frame operation. The brochure shows how the cameras have eliminated hundreds of hours in such diversified applications as airborne systems analysis, missile tracking, radar evaluation, stereoscopic recording and automatic systems evaluation. **Circle L19 inside back cover.**

Galvanometers. Consolidated Electrodynamics Corp., 300 North Sierra Madre Villa, Pasadena, Calif. Bulletin 1528 covers the series 7-300 galvanometers. It outlines uses, principle of operation, construction features, galvanometer characteristics and application circuitry. Information on accessories is also given. **Circle L20 inside back cover.**

Magnetic Shift Registers. Magnetics Research Co., 255 Grove St., White Plains, N. Y., has issued technical bulletin No. 128 concerning the production of miniature magnetic shift registers of eight bits each—models MSR-1 and MSR-0—which can be used together to form a small 16-bit

shift register for serial read-in and read-out. The units discussed can be used in many military applications as well as in radar, computer and business-machine systems. **Circle L21 inside back cover.**

Insulating Materials. Insulation Manufacturers Corp., 565 W. Washington Blvd., Chicago 6, Ill. Catalog 20 is an illustrated, completely indexed 32-page booklet on electrical insulations for repair and maintenance of motors, generators and electrical or electronic equipment. The catalog contains descriptions, photos, prices and ordering data. **Circle L22 inside back cover.**

Long-Life Soldering Tips. Hexacon Electric Co., 130 W. Clay Ave., Roselle Park, N. J., announces a new catalog (No. 144), showing a greatly expanded line of Hexclad long-life soldering tips. There are 40 stock sizes and shapes and many special styles to choose from.

The various shapes of plug and screw tips are illustrated and in the catalog data the tip diameter and length, style of tip point and size of tip point are given. Also indicated are the various soldering iron models each tip fits. Instructions on use and care of the tips are included. **Circle L23 inside back cover.**

Silicon Rectifiers. Sarkes Tarzian, Inc., 415 N. College Ave., Bloomington, Ind., has published a series of design notes on a wide variety of silicon rectifiers. Each of the catalog sheets shows features, electrical ratings, characteristics and output voltages. **Circle L24 inside back cover.**

Automatic Exposure Control. Flight Research, Inc., P. O. Box 1-F, Richmond 1, Va. AUTEX, a versatile electronic device for the automatic control of exposure in motion pictures, is described in an illustrated brochure. Designed to adapt to any motion picture camera and to be used with many lenses, AUTEX is a new tool for the professional, industrial and scientific photographer contend-

ing with uncontrollable light conditions. The brochure describes the Accent Control feature of AUTEX, that permits the photographer to deliberately change the aperture setting from the correct value for the average lighting of the scene, to produce the best exposure for the object of chief interest. An advanced transistorized circuit permits response speeds that provide full travel from f/2 to f/22 in as little as one second. The brochure includes specifications. **Circle L25 inside back cover.**

Universal Potentiometer. Leeds & Northrup Co., 4934 Stenton Ave., Philadelphia 44, Pa. A new six-page data sheet E-51(6) describes the type K-3 universal (guarded) potentiometer. It lists complete specifications of the instrument and gives typical applications in laboratories. A full-page illustration of the type K-3 is shown as well as components such as slidewires, switches and binding posts. A complete description of the circuit operation including schematic diagrams is included. The uses of the auxiliary potentiometer are discussed and recommended accessories and ordering instructions are given. **Circle L26 inside back cover.**

Radio and TV Components. N. V. Philips Gloeilampenfabrieken, Eindhoven, Holland, has published a radio and tv components handbook. This is a loose-leaf publication containing characteristics of variable, electrolytic and trimming capacitors, several kinds of loudspeakers, output-transformers, h-f coils, a-m and f-m permeability tuners and tv components.

The handbook can be kept up-to-date by the issue of supplementary sheets, published four or five times a year. Price of the handbook is $3. Subscription to the supplementary sheets is $1 per year. **Circle L27 inside back cover.**

Silicone-Resin Spray. Ed-Berl Products, Inc., 87 Merrick Rd., Baldwin, L. I., N. Y., has available descriptive literature on three of

its latest products—Silikone, Sil-Lube and stainless steel pin straightener sockets. Silikone, used as a moisture repellent on electronic components, eliminates h-v corona discharge. Sil-Lube cleans, lubricates and restores volume controls and gang switches. The seven and nine-prong miniature tube pin straightener socket is designed for panel and chassis mountings. **Circle L28 inside back cover.**

Molded Tubulars. General Electric Co., Schenectady 5, N. Y. An eight-page publication on molded PVZ tubular capacitors is now available. Designated GET-2671, the bulletin contains descriptional information and lists ratings and dimensions.

The capacitors discussed are for application in computers, missiles, telephone equipment and other high grade military and commercial electronic equipment and were introduced to meet the need of the electronic industry for a moderately priced, high quality, 125-C paper tubular capacitor. **Circle L29 inside back cover.**

Time Delay Relays. The A. W. Haydon Co., Waterbury, Conn., has announced the release of two new bulletins to supersede page 13 of their current catalog. These bulletins contain details on the function of the three dial adjustable time delay relays, along with catalog part numbers for the standard ranges and voltages in a-c, d-c and 400 cycles. Bulletin AWH TD404 describes the surface mounting type and bulletin AWH TD405 describes the flush mounting type for panel installation. The timers discussed are especially useful where frequent change in time setting is necessary. Catalog is free on written request on firm's letterhead.

Silicone Rubber. Union Carbide and Carbon Corp., 30 E. 42nd St., New York 17, N. Y. A new 28-page data sheet and compounding study on W-96 Silicone rubber gum stock provides detailed information and instructions for manufacturers, fabricators and product designers. It includes numerous tables and

charts not previously available. **Circle L30 inside back cover.**

EPUT Meters and Controllers. Berkeley Division, Beckman Instruments, Inc., 2200 Wright Ave., Richmond 3, Calif. Magnetic events-per-unit-time meters and magnetic dual preset controllers are described in two new technical bulletins. Both bulletins illustrate the use of Ferristors, small magnetic amplifiers, as vacuum tube replacements. The only tubes used in either instrument are in the r-f power supply.

Series 7600 magnetic EPUT'S discussed consist of input amplifiers, a gate opened and closed by a tuning-fork controlled time base and a series of magnetic decade counting units. The series 5800 preset controllers described combine an input circuit, cascaded preset decimal counting units and two identical output channels.

Design details and application data are contained in both bulletins. **Circle L31 inside back cover.**

Magnetically Controlled Counter. Magnetics Research Co., 255 Grove St., White Plains, N. Y. Technical bulletin No. 145 illustrates and describes the Magnivider, a magnetically controlled counter featuring magnetic core reliability, long life, low power drain, small size, rugged construction and low cost. **Circle L32 inside back cover.**

Laboratory Standards. Measurements Corp., Boonton, N. J., has published two new technical bulletins describing its latest instruments—model 275 i-f converter and model 95 standard f-m signal generator.

Also available is a revised bulletin describing the model 505 standard test set for transistors. **Circle L33 inside back cover.**

Hermetic Seal Terminals. International Resistance Co., 401 North Broad St., Philadelphia 8, Pa. Catalog data bulletin LT-1 contains comprehensive data on construction, applications, specifications, properties, designations, dimensions and installation sug-

gestions on type LT hermetic seal terminals. Detailed charts and diagrams are shown in the four pages. **Circle L34 inside back cover.**

Electronic Wire. General Electric Co., Bridgeport, Conn., has issued a four-page folder on high-temperature electronic wire that meets all the requirements of specifications MIL-W-16878B. The wires described, designed for the internal wiring of electrical and electronic equipment, meters and panels, are available with three types of insulation—thermoplastic, Nylon and silicone for various voltages.

Publication No. 19-586 gives complete specifications and application data. **Circle L35 inside back cover.**

Switches. Donald P. Mossman, Inc., Brewster, N. Y. Four-page catalog No. 200 covers a complete line of push button, lever and turn switches.

Included are illustrations, ratings, dimensions and all other specifications necessary for ordering these switches. A section is also devoted to the company's Electronics Division which specializes in assembling and wiring of control panels, cableforms and the like, to individual customer requirements. **Circle L36 inside back cover.**

Custom Design and Development. Nelson Instrument Co., 607 Howard St., Evanston, Ill. A six-page brochure describes the company's electronic research, development and production facilities. The brochure illustrates a wide range of custom-built controls, research apparatus, industrial automation, medical instrumentation and other electronic equipment.

The publication also shows how the company takes an idea, develops it into a working prototype and then, if desired, manufactures the product with standard production procedures. **Circle L37 inside back cover.**

Cooling Fans. McLean Engineering Laboratories, P. O. Box 228, Princeton, N. J. A full line of fans for standard 19-in. racks is illustrated and described with detailed

 For additional information on all items on this page, use post card on last page.

specifications in a four-page two-color catalog. Standard RETMA notching allows mounting on rack—no cutting or fitting is necessary. Filters are replaceable. Grills are stainless steel. Copies of the catalog are available free. **Circle L38 inside back cover.**

Boron Carbon Resistors. International Resistance Co., 401 N. Broad St., Philadelphia 8, Pa. Catalog data bulletin B-6b covers a line of boron-carbon Precistors. The four pages contain comprehensive data on construction, characteristics, applications, types, identification, resistance element, terminals and insulation. Detailed charts and graphs are included. **Circle L39 inside back cover.**

Passive Cathode Material. Superior Tube Co., 1523 Germantown Ave., Norristown, Pa. Catalog section No. 51 presents complete information on Cathaloy P-51, a new passive cathode material featuring a hot yield strength of approximately 5,000 lb per sq in. at 800 C. The material is designed for electronic tubes which require the low rate of barium evolution, minimum sublimation and freedom from interface impedance characteristic of passive cathodes, but at the same time must operate under conditions of shock and vibration. **Circle L40 inside back cover.**

Variable Capacitors. Hammarlund Mfg. Co., Inc., 460 W. 34th St., New York 1, N. Y., has available a new catalog on variable capacitors. The publication lists all standard Hammarlund variable capacitors, providing complete electrical and mechanical information on each. **Circle L41 inside back cover.**

Component Sales Catalog. Atlas E-E Corp., 47 Prospect St., Woburn, Mass. A loose-leaf perforated sales catalog contains descriptions and price information on a wide variety of components. Among those included are a variety of clips and clamps, subminiature-tube holders and shields, shield inserts, Lucite cap nuts, Nylon screws and rivets, adhesive preforms, printed circuits, name-

plates and micropin sockets. **Circle L42 inside back cover.**

Data Handling System. Berkeley Division, Beckman Instruments, Inc., 2200 Wright Ave., Richmond 3, Calif., has issued a technical bulletin containing design features of the 5780 data handling system which offers high-speed storage on magnetic tape. The system discussed converts four items of encoded data and encoded time into a form for operation into an electric typewriter or summary punch. Basic units listed consist of high-speed gated counters, tape converters and magnetic shift registers. Operation of the system is described. **Circle L43 inside back cover.**

Products Catalog. American Rectifier Corp., 95 Lafayette St., New York 13, N. Y. Now available is the latest catalog of equipment manufactured and designed by the company. It illustrates everything from components to complete power supplies and explains the company's method of custom engineering. **Circle L44 inside back cover.**

Aircraft Switches. Micro Switch, a Division of Minneapolis-Honeywell Regulator Co., Freeport, Ill. Catalog 78 is a 32-page booklet covering the complete line of phenolic encased aircraft switches as well as small, metal-covered hermetically sealed switches and high-temperature switches.

Complete with photographs, dimensional drawings, electrical data and operating characteristics, it describes over 140 different switches, auxiliary switch actuators and terminal enclosures. Switches are shown in a variety of actuator designs, terminal structures and contact arrangements, including spdt, dpdt, double-break, two-circuit, four-circuit and split. Many of the switches are AN, JAN and/or MS approved. **Circle L45 inside back cover.**

Tubular Capacitors. Good-All Electric Mfg. Co., 120 First St., Ogallala, Nebraska, has released a brochure containing detailed information on six new upright

mounting tubular capacitor types. The information is of particular interest in connection with printed circuit applications. **Circle L46 inside back cover.**

L-F Transformers and Reactors. Southwestern Industrial Electronics Co., P. O. Box 13058, Houston, Texas, has published an eight-page catalog describing a full line of miniaturized l-f transformers and reactors. Catalog 105 describes the complete line of input, output, interstage and avc output transformers, and includes a listing of reactors. Complete design and application information is given, including mounting information and space requirements. **Circle L47 inside back cover.**

Transformer Laminations. Tempel Mfg. Co., Bryn Mawr at Damen, Chicago 26, Ill., has available a new catalog page on ⅛ in. E & I transformer laminations. Complete technical specifications are given including dimensional drawings, data applying to core stacks with square cross sections, three basic formulas for core stacks with square cross section at 60 cycles and weight and count in sets. **Circle L48 inside back cover.**

Nickel Cadmium Storage Batteries. Nickel Cadmium Battery Corp., 66 Pleasant St., Easthampton, Mass. To help engineers evaluate the practicability of miniature nickel-cadmium batteries for electronic, aircraft and communications equipment — NICAD's high output sintered plate nickel-cadmium storage batteries are described in an eight-page technical report. Details of development, construction and operation are shown along with curves of discharge and charge characteristics. **Circle L49 inside back cover.**

Tapping Linear Pots. Helipot Corp., Newport Beach, Calif. Technical paper 804 graphically describes a method of tapping linear pots to reproduce a particular function. The procedure discussed limits loading errors to the best resolution of a single-turn pot while using a minimum number of taps and resistors. Two, four and five-tap pots are dis-

cussed. **Circle L50 inside back cover.**

Data Handling System. Berkeley Div., Beckman Instruments, Inc., 2200 Wright Ave., Richmond 3, Calif. Design features of a data-handling system offering high-speed storage on magnetic tape are contained in a new technical bulletin.

The 5780 system described converts four items of encoded data and encoded time into a form for operation into an electric typewriter or summary punch. Basic units discussed consist of high-speed gated counters, tape converters and magnetic shift registers.

Operation of the system is described. **Circle L51 inside back cover.**

Balancing Machines. Stewart-Warner Corp., 1826 Diversey Parkway, Chicago 14, Ill. Form 24-1 is a 16-page folder illustrating and describing a line of versatile, wide range electronic balancing machines for industry. Chief features and specifications are included. **Circle L52 inside back cover.**

Autotransformers. General Radio Co., 275 Massachusetts Ave., Cambridge 39, Mass. The new 24-page bulletin 0 describes a complete line of Variac adjustable autotransformers. Dimension drawings, in addition to photographs, are included for all models, and complete specifications and prices are tabulated. **Circle L53 inside back cover.**

Gages, Instruments and Accessories. Baldwin-Lima-Hamilton Corp., Waltham, Mass. A new line of flat-grid, fine-pitch Bakelite gages, superior replacements for small sizes of wrap-around gages, is among the new products listed in the new price list on SR-4 strain gages, instruments and accessories.

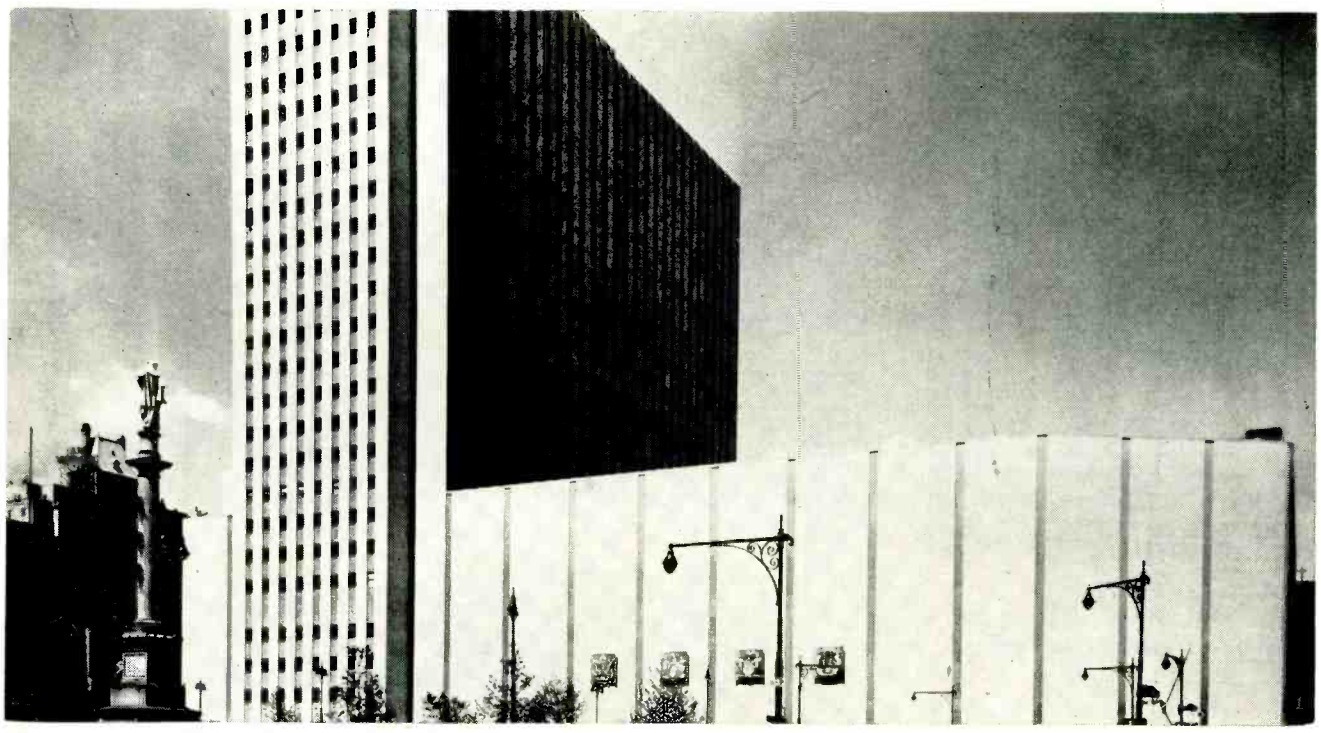
In addition to offering the new flat-grid gages and other new products, the price list contains a thorough discussion of gages and methods of using them and constitutes a complete guide to the proper selection of gages. **Circle L54 inside back cover.**

Plants and People

Edited by WILLIAM G. ARNOLD

Industry gets ready for 1957 IRE Show and Convention to be held March 18-21 in New York City. Electronics manufacturers continue plant and facility build-up. Engineers and executives in the industry move to new positions of responsibility

IRE National Convention For 1957 Set For New York Coliseum



New York's $35 million Coliseum will be the home of this year's IRE Convention in Manhattan

THE 1957 IRE national convention program will feature 840 exhibits of new apparatus, 275 papers reporting new developments and a new exhibit location for the 50,000 people expected to attend. The Radio Engineering Show has been expanded and moved to the New York Coliseum in midtown Manhattan. The four-day program of technical papers is highlighted by two special symposia on Tuesday evening, March 19. One deals with the topic of a national system of air traffic control, and the other with microminiaturization—the ultimate technique.

► **Show**—Hours for the Radio Engineering Show are 10 a.m. to 9 p.m., Monday through Thursday, March 18-21. The show's 840 exhibits will cover all four floors of the Coliseum. For the convenience of visitors, the exhibits will be grouped, with computers and communications on the first floor, component parts on the second, instruments and microwaves on the third and production tools, materials and services on the fourth.

The annual meeting will be at 10:30 a.m., Monday, March 18, in the grand ballroom of the Waldorf-Astoria Hotel. Principal speaker at the meeting will be Donald G. Fink, director of research of Philco Corp.

The IRE annual cocktail party will be held at 5:30-7:30 p.m., Monday, March 18 in the grand ballroom of the Waldorf-Astoria Hotel.

► **Sessions** — The technical program will start at 2.30 p.m. Monday, March 18, and continue through 5:00 p.m., Thursday, March 21. A program of 55 sessions has been organized. Thirty-three sessions will be held at the Waldorf and 22 at the Coliseum. The program of papers and authors begins on page 461 of this issue of ELECTRONICS.

The annual IRE banquet will be held at 6:45 p.m., Wednesday, March 20, in the grand ballroom of the Waldorf-Astoria Hotel. Presentation of IRE Awards by John T. Henderson, IRE president, will be made.

The spokesman for the IRE fellows will be Major General James D. O'Connell, U.S. Army Signal Corps. Toastmaster will be Rear Admiral C. F. Horne of Convair.

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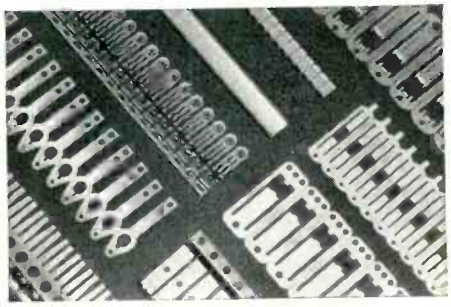

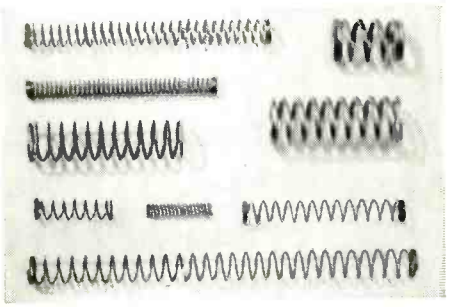

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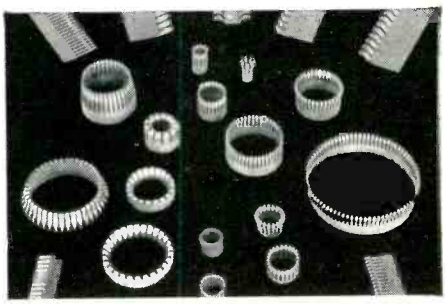

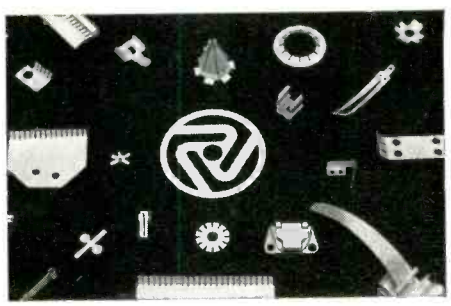

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West Coast Manufacturers Elect Officers For 1957

CALVIN K. TOWNSEND was elected president of the West Coast Electronic Mfrs. Association.

He is executive vice-president of Jennings Radio Mfg. Corp. in San Jose, manufacturers of vacuum capacitors and high voltage vacuum switch equipment.

The West Coast Electronic Manufacturers Association is composed of 225 member companies in the West. The organization consists of three councils located in San Diego, San Francisco and Los Angeles.

The WCEMA board named Hugh P. Moore, board chairman of Lerco Electronics, Inc., vice-president and member of the board; S. H. Bellue, material manager, Hughes Aircraft Company, secretary and George Koth, vice-president of Lenkurt Electric Company, treasurer. Moore replaces Gramer Yarbrough who resigned from Elgin Electronics to form Yarbrough Sales Co.

Front row—Left to right, George Koth, Thomas P. Walker, Calvin K. Townsend, Hugh P. Moore, S. H. Bellue, F. E. Gilbert, Jr. Back row—Left to right, Richard B. Leng, J. M. Loge, John A. Chartz, D. C. Duncan, Cortlandt Van Rensselaer, Gerald L. Osborne, Winfield G. Wagener

Navy Honors Godschall Of Philco For Underwater Missile Work

THE Distinguished Service Award was presented to Charles H. Godschall, manager of tooling and tool engineering for the government and industrial division of Philco Corp., for outstanding work in the development of a new underwater weapon.

The citation, the second to be received by Godschall, reads, "For outstanding service to the U. S. Navy in which he served as a specific consultant to the Chief of the Bureau of Ordnance from 1 April 1954 to 31 May 1956. As a direct result of Mr. Godschall's recommendation concerning major improvements in research and development procedures and underwater ordnance, the Navy has now thoroughly documented the design disclosure of a new and advanced anti-submarine weapon. The producibility of this weapon is assured, the functional performance has been demonstrated by in-service testing, and production costs have been reduced by about 40% from the estimated figure. Godschall also worked on Navy's missile Sidewinder currently being produced by Philco.

Charles H. Godschall and Sidewinder

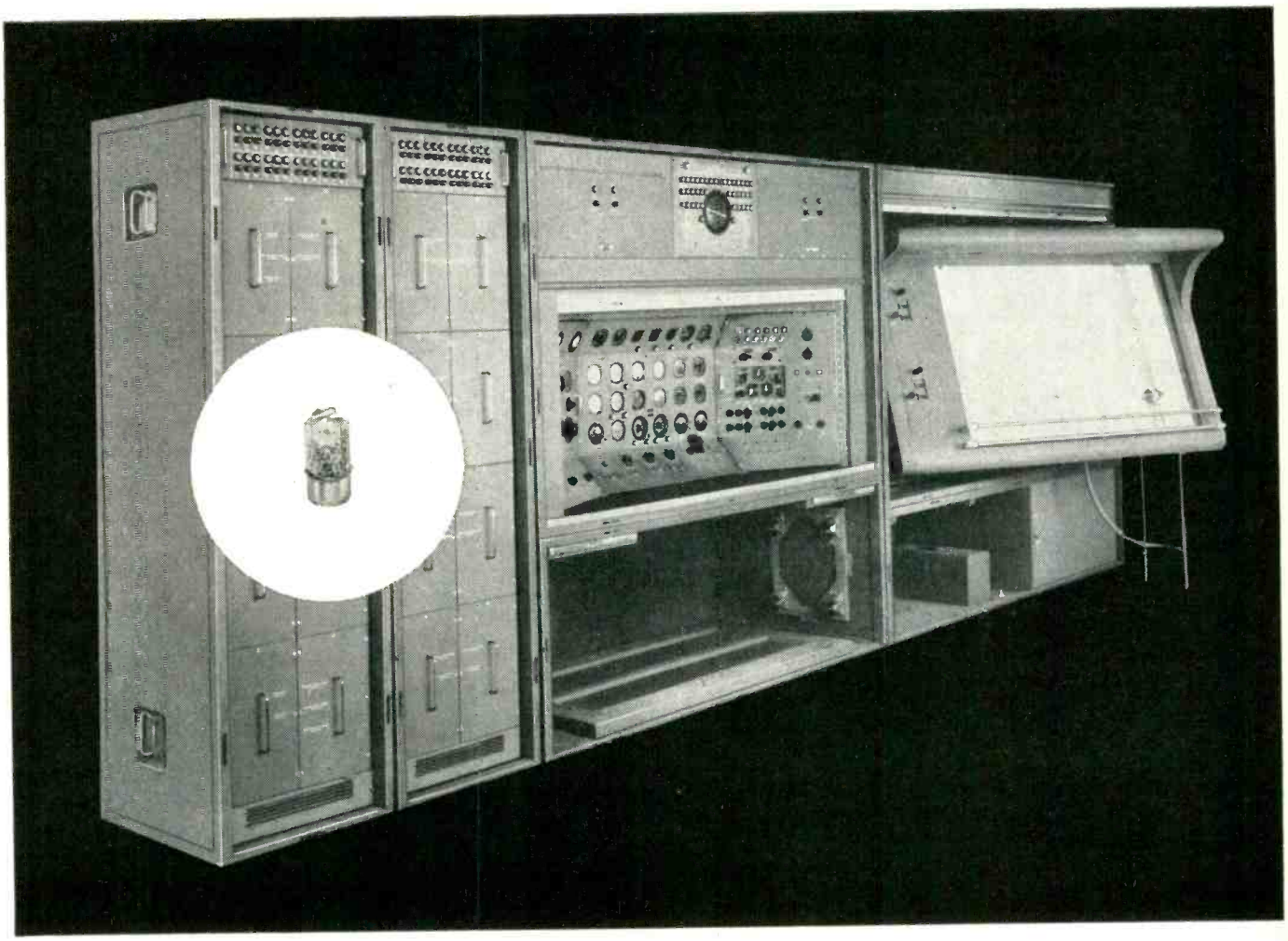
Fischer & Porter Plans Expansion Of Research And Production

Left to right: Kermit Fischer, president; C. B. Foster of Bucks County and Nathaniel Brewer

FISCHER & PORTER CO. purchased two tracts in central Bucks county, Pa. for expansion plans.

The larger of the two areas will accommodate buildings for offices, research laboratories and additional production facilities. The proposed buildings will occupy but a third of the 120 acre tract.

A nearby 65 acre tract will be developed as a recreational facility for Fischer & Porter personnel. A company country club is planned. There is to be an eighteen hole golf course as well as several tennis courts. A proposed club house will include a restaurant, a day nursery



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- *Auxiliary Power Supplies*
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and a number of meeting rooms to be available to both company and community groups.

Chapman Named CBS-Hytron President

ARTHUR L. CHAPMAN has been appointed president of CBS-Hytron. Formerly vice-president-manufacturing of Sylvania Electric, he succeeds Charles F. Stromeyer, who resigned as president of CBS-Hytron.

During his 24-year association with Sylvania, Chapman served in virtually all phases of tube, parts and set production. In 1933, he joined the firm as supervisor of the radio tube material inspection department. After working for several years on special divisional programs, including production of the lock-in radio tube, he was named general foreman of the radio tube plant in Emporium, Pa. in 1942. A year later he became superintendent of the wire and weld plant in Warren, Pa., and in 1944 manager of the plant. In 1950 he was appointed general manager of both the parts and radio and television divisions. He was made a vice-president in 1951.

Arthur L. Chapman

In 1953, he was appointed vice-president in charge of electronic operations. In this capacity he was responsible for the operations of Sylvania's radio and television, parts, electronics, radio tube, and television picture tube divisions.

In 1956, Chapman was appointed vice-president-manufacturing of

Sylvania. In this assignment, he provided on a company-wide basis planning and coordination in the areas of automation and equipment development, purchasing, traffic and industrial engineering. He also had the responsibility for evaluating the manufacturing facilities of new acquisitions or ventures which Sylvania wished to investigate.

Motorola Selects TV Engineers

GAIRTH J. HEISIG has been named director of television engineering for Motorola. William Hinton was named assistant to the director of television engineering.

Heisig has been with Motorola since 1945, starting in the communications and electronics division. He was transferred to television engineering in 1950 and was named staff consultant. Heisig succeeds Edward Passow, who has resigned.

Before his association with Motorola, Heisig was associated with the M.I.T. Radiation Laboratory for two years

Karl H. Horn was appointed chief television engineer for the firm. Lawrence Mattingly was named assistant chief television engineer.

In his new appointment Horn succeeds George Fyler, who has resigned.

Horn has been with the firm since 1953 starting as engineer. In 1954 he was named chief engineer of the Canadian operation. Before his association with Motorola, Horn was located for two years with the Menzel Radio Manufacturing Co. and two years with Canadian Comstock.

Electronics Conference Elects Officers

CHRISTOPHER E. BARTHEL JR., assistant director of Armour Research Foundation of Illinois Insitute of Technology, has been elected president of the National Electronics Conference for 1957.

Other officers named for the 1957 conference, to be held Oct. 7-9 at the Hotel Sherman in Chicago, are:

Chairman of the board, Howard

H. Brauer, Bell and Howell Co.; executive vice-president, Joseph H. Enenbach, Illinois Bell Telephone Co.; secretary, John S. Powers, Bell and Howell Co.; treasurer, Charles W. McMullen, Northwestern University; executive secretary, Gordon J. Argall, De Vry Technical Institute; legal advisor, Alois W. Graf, Graf, Nierman and Burmeister, and assistant treasurer, James H. Kogen, Askania Regulator Co.

The conference is sponsored by the Illinois Institute of Technology, AIEE, IRE and Northwestern and Illinois universities, in cooperation with Notre Dame, Purdue, Michigan State, Michigan, and Wisconsin universities, RETMA and SMPTE.

Officers For 1957 Appointed By IRE

THE IRE board of directors appointed six members to the board for 1957.

Reappointed as treasurer of the IRE was W. R. G. Baker, vice-president of General Electric. Haraden Pratt was appointed to his fifteenth term as IRE secretary. Donald G. Fink, director of research of Philco Corp., was reappointed as editor of the IRE.

Appointed as director were Alfred N. Goldsmith, consulting engineer and editor emeritus of the IRE; A. W. Graf, partner of the law firm of Graf, Nierman and Burmeister; and William R. Hewlett, vice-president of Hewlett-Packard Co. and past president of IRE.

▶ **Award**—The Institute of Radio Engineers' 1957 Medal of Honor, the highest technical award in the radio and electronics field, will go to J. A. Stratton, Chancellor of MIT. The award is to be given "for his inspiring leadership and outstanding contributions to the development of radio engineering at a teacher, physicist, engineer, author, and administrator."

The formal presentation of the award will be made at the annual IRE banquet, to be held at the

Waldorf-Astoria Hotel, New York City, on March 20, 1957 during the IRE National Convention.

Dr. Stratton joined MIT in 1925 and served on the staff of the electrical engineering and physics departments for twenty years. In 1945 he was appointed head of the Research Laboratory of Electronics. He became vice-president and Provost of MIT in 1949, and this year was appointed to the specially created position of Chancellor.

Westinghouse Tube Names Two

GEORGE C. SZIKLAI has been named technical assistant to R. T. Orth, vice-president and general manager of the Westinghouse electronic tube division.

Sziklai, holder of 110 patents in electronics and other fields, will be a general consultant to the division on electronic systems and the applications of tubes and semi-conductors to these systems.

In addition to electronics, Sziklai has done work in physics, chemistry and mathematics. He has worked for several American concerns, the most recent one being RCA.

G. C. Sziklai

Franklin P. Hinman has been appointed operations manager of the cathode-ray and power tube departments of the tube division.

In his new position he will be responsible for all phases in the design, development, engineering and manufacturing of cathode-ray and power tubes, as well as the industrial relations and administra-

tion of the Elmira plant. The creation of this new post is part of an overall reorganization of the electronic tube division into product groups.

Hinman joined Westinghouse in 1951. Prior to that, he had been associated for nine years with RCA in manufacturing and engineering. In 1953, he was named product manager for the Elmira plant, and in 1954 manager of manufacturing.

Audio Engineers Honor Farmer

THE Audio Engineering Society Award was presented to Herbert E. Farmer, in recognition of his service to the Society. In addition, the Society awarded six fellowship certificates.

Farmer, who has served as secretary and chairman of the Society's Los Angeles section, is director of audio-visual services at the University of Southern California. He joined the University in 1942, as assistant professor in the department of cinema. He is also a private consultant in motion picture production and sound facilities design. In 1947 he worked on Project Sandstone at the University of California.

Honeywell Forms Boston Division

MINNEAPOLIS-HONEYWELL'S Doelcam and Transistor divisions in Boston have been consolidated into a single unit to be known as the Boston division.

The new division is composed of two sections: a semi-conductor product section (power-type transistors), and an instrument section (synchro motors, gyroscopic instruments, electronic control and test equipment).

Over-all direction will be under George J. Schwartz, vice-president and general manager of the new division. John J. Wilson, formerly president of the Doelcam division, will direct policy as senior corporate vice-president in the area.

Production of the various prod-

ucts will be centered in the recently purchased, 250,000-sq-ft plant in Boston. Engineering and administration will be consolidated in the division's existing two-story building there.

NCR Electronics Promotes Edwards

WALTER G. EDWARDS was named engineering department manager of the National Cash Register Company electronics division in Hawthorne, Calif.

Formerly the facility's chief systems engineer, Edwards now assumes responsibility for all engineering activities of the division.

Walter G. Edwards

He has been with the organization since 1952, when it was the Computer Research Corp. During the past four years, he has designed a readout system using ferro-resonant flip-flops, supervised installation of the NCR 105 computer in Washington, D. C., and developed various digital computer systems devices for which patents are now pending.

Presidential Aid To Address IRE Group

EDWARD P. CURTIS, President Eisenhower's special assistant for aviation facilities planning will report the results of his group's year-long study to come up with recommendations for meeting the growing needs of U.S. aviation

during the next 20 years at a luncheon meeting jointly sponsored by the IRE professional groups on Aeronautical & Navigation Electronics (PGANE) and Military Electronics (PGMIL).

The luncheon is scheduled for March 19, 12:30 pm. (during the national IRE convention) at the Belmont-Plaza Hotel in New York City.

Brooklyn Polytech Appoints Weber

ERNST WEBER was appointed to the newly-created position of vice-president for research at the Polytechnic Institute of Brooklyn.

Research projects at Polytechnic now represent annual expenditures of more than $2,250,000.

Prior to assuming this post, Dr. Weber was director of Polytechnic's Microwave Research Institute. Under his direction, MRI annually expended almost $1 million on research projects for the armed forces.

Dr. Weber came to Polytechnic in 1930 as a visiting professor. Since 1945, he has been head of the department of electrical engineering and director of the Microwave Research Institute.

RCA Labs Selects Two Directors

AT RCA Laboratories Rolf W. Peter was appointed director of the physical and chemical research laboratory and Allen A. Barco director of the systems research laboratory.

Dr. Peter, research physicist at RCA Laboratories since 1948, succeeds Humboldt W. Leverenz, who was named assistant director of research, RCA Laboratories. Barco, who has been engineer-in-charge of the industry service laboratory at the David Sarnoff Research Center, succeeds Dr. George H. Brown, who was appointed chief engineer, RCA commercial electronic products.

Since 1953, Dr. Peter has supervised microwave and gaseous electronics research in the Electronic Research Laboratory of RCA

Laboratories. He has been named chairman of the 1957 Electron Tube Research Conference to be sponsored by the IRE and the AIEE.

Barco recently has directed the new devices applications section of the systems research laboratory. He joined the RCA Industry Service Laboratory in New York as a student engineer in 1947, and was section head when he was transferred to Princeton in 1949.

TASO Names Transmitter Head

RALPH N. HARMON, vice-president for engineering of Westinghouse Broadcasting Co. has been appointed vice-chairman on transmitting equipment for the Television Allocations Study Organization (TASO).

His committee will study television transmitting equipment capabilities, costs, etc., as they might affect television allocations, both uhf and vhf.

Harmon's appointment was made by Dr. George R. Town, executive director of TASO.

Research Award Goes To Shannon

CLAUDE E. SHANNON received the 1956 Research Corporation Award for his work in establishing "Information Theory."

It is concerned with the most efficient way to carry out the communicating process between both man and machine and man and man.

The award consists of an honorarium of $2,500, a plaque and a citation. It was presented to Dr. Shannon by Joseph W. Barker, chairman and president of Research Corporation.

Dr. Shannon is a professor at Massachusetts Institute of Technology and a mathematical consultant in Bell Telephone Laboratories research department.

Research Corporation is a nonprofit foundation established in

1912 by the late inventor-scientist Frederick Gardner Cottrell to support scientific research in colleges, universities and scientific institutions.

Other award winners have included: Robert B. Woodward, Vannevar Bush, Percy W. Bridgman, Ernest O. Lawrence, Bruno Rossi, Edwin M. McMillan, Edward C. Kendall, Samuel A. Goudsmit, George E. Uhlenbeck, and H. S. Black.

Dr. Shannon, who has been with Bell Laboratories since 1941 has made outstanding contributions to the communications field, especially in mathematical theory of communications, Boolean algebra, cryptography, and computing circuits.

In January, 1956, he was appointed visiting professor of electrical communications at Massachusetts Institute of Technology.

Curtiss-Wright Appoints Christaldi

P. S. CHRISTALDI has been appointed assistant to the general manager of the electronics division of Curtiss-Wright Corp. in Carlstadt, N.J. In his newly-created position, Dr.

P. S. Christaldi

Christaldi will be responsible for the development, manufacture, and sales of highly-specialized nuclear and electronic equipment for both military and commercial uses.

Previous to his new position with Curtiss-Wright, he had been associated with A. B. DuMont Laboratories where he pioneered in cathode-ray tube and cathode-ray

oscillograph development. During his career with DuMont, beginning in 1938, he served in such capacities as chief engineer, engineering manager of the instrument division, assistant manager of the division and division manager.

Mallory Names Two Vice-Presidents

G. A. GODWIN and Edward L. Nung were elected vice-presidents of P. R. Mallory & Co. in Indianapolis, Indiana.

Godwin is general manager of the Mallory metallurgical divisions; president of P. R. Mallory Plastics Co. in Chicago and chairman of the board, Electronic Timers Company, Warsaw, New York. Mallory Plastics and Electronic Timers, formerly wholly-owned subsidiaries of P. R. Mallory & Co., Inc., have recently been made divisions of the parent company.

Nung is general manager of the Mallory electronic divisions, with plants in Indianapolis, Frankford and Crawfordsville, Indiana and in Huntsville, Alabama. Prior to joining Mallory four years ago, he had been a plant manager with Sylvania Electric and had been associated with RCA.

Systems Labs Selects Two

JAMES A. MARSH has been appointed vice-president of Systems Laboratories Corp. Richard H. De Lano, secretary of the corporation, had been appointed director of the company's systems integration division.

Before joining Systems Laboratories, Dr. Marsh was radar group leader in the autonetics engineering department of North American. He had the direction of all missile and manned aircraft antenna designs accomplished at the N.A.A. Downey plant.

De Lano has had ten years experience in electronics and radar and was instrumental in the development of the Falcon air-to-air guided missile as senior staff physicist at Hughes Aircraft Corp. He

has conducted theoretical and analytical studies in a wide variety of subjects dealing with radar, missile trajectories, navigation and control systems.

Systems Laboratories Corp. was founded last year as a scientific organization specializing in the research and development of interplanetary space travel. The professional staff has more than doubled in the last eight months.

Stromberg Picks Sonar Head

VICTOR SAVCHUK JR. was appointed head of the sonar group in the research and advanced development department of Stromberg-Carlson.

He was head of the acoustic measurements branch of the U. S. Navy Underwater Sound Laboratory in New London, Conn., before joining Stromberg-Carlson in 1956.

From 1947 to 1949 he served as a staff member in the MIT Acoustics Laboratory and in 1949 became a junior research engineer for the Sanborn Company of Cambridge, Mass. In 1950 he joined the Navy's Underwater Sound Laboratory as an electronic scientist, specializing in electroacoustics.

Varian Names Two Engineers

TWO engineers were promoted at Varian Associates.

Forrest Nelson will head up the advanced development group in the instrument division's research department. He joined Varian Associates in 1950, where he has been engaged in product engineering of spectrometers and other instruments.

Robert H. Watson was appointed chief product engineer. He came to Varian in 1955, from Ryan Aeronautical Co., where he was an electronics group engineer.

Technology Instrument Completes Expansion

TECHNOLOGY INSTRUMENT CORP. of Acton, Mass. completed a half-million dollar addition to its modern plant in Acton. This latest plant

expansion is expected to increase production capacity by as much as 100 percent.

The new addition incorporates a filtered air system for control of dust and humidity. It minimizes final-test rejects, speeds production, and provides maximum protection against latent corrosive elements that will affect potentiometer performance in the field, according to the firm.

Delco Appoints Transistor Chief

Frank Jaumot

FRANK JAUMOT was appointed director research and engineering in semiconductors for the Delco Radio division of General Motors.

Dr. Jaumot joins Delco Radio from the Franklin Institute at Philadelphia where he had been chief of physics of metals section.

At the University of Pennsylvania, he taught physics until 1952 when he joined the Franklin Institute. While at the Institute he continued at the U. of P. as an assistant professor of metallurgical engineering.

Filtors Selects Research Director

B. LAZICH has been appointed director of the research and engineering division of Filtors, Inc., manufacturers of sub-minature hermetically sealed relays.

Prior to joining Filtors, Lazich was senior research engineer at

the Robertshaw Research Center in Irwin, Pa., where he specialized in work on electrical and thermostatic control devices.

He has been granted more than 30 United States and foreign patents—with a number still pending—for his developments of relays and other control devices.

University Of Chicago Appoints Biberman

LUCIEN M. BIBERMAN has been appointed by The University of Chicago to the position of director of the electronics division of Chicago Midway Laboratories.

Since 1944 he has been a member of the technical staff of the Naval Ordnance Test Station, China Lake, Calif. He was responsible for the design of the NOTS Aeroballistics Laboratory and for the early Sidewinder seeker design. His most recent work included missile vulnerabilities and countermeasures studies.

At Chicago Midway Laboratories Biberman will be concerned with infrared, optical and electronics projects.

General Telephone Forms Lab Unit

GENERAL TELEPHONE CORP. has formed General Telephone Laboratories in Chicago.

The newly created organization has acquired the research and development personnel and facilities of Automatic Electric Co., principal manufacturing unit of the General Telephone System, and will embark on a greatly expanded program of basic research and product development in the telephone switching and related communication fields. The work of the new laboratories will also extend into all areas of remote control by electronic and electro-mechanical means. The new unit will eventually be housed in new quarters being built in Northlake, Ill.

In addition, the new laboratories will undertake a comprehensive program of quality analysis and

measurement for all units of the General Telephone System.

Robert M. Wopat, Automatic's vice-president in charge of research and engineering, has been elected president of the new organization.

Battelle Names New Director

B. D. THOMAS has been appointed director of Battelle Memorial Institute. He succeeds Dr. Clyde Williams in the management of Battelle's research operations in the United States and Europe.

A member of the Institute's executive and technical staff since 1934, Dr. Thomas was appointed assistant director in 1942. Subsequently, he was named secretary of the Battelle Memorial Institute Corp. and in 1955, he became vice-president.

B. D. Thomas

He established and headed Battelle's first division of chemical research in 1939, and was a key figure in the establishment of Battelle's research laboratories in Frankfurt, Germany, and Geneva, Switzerland, and in the development of the Institute's recently completed Nuclear Research Center.

Daystrom Adds Computer Engineer

ERIC WEISS, formerly senior staff physicist for Hughes Aircraft Co., has joined the engineering staff of Daystrom Systems division of Daystrom. He will concentrate on

the application and usage of computers in automatic systems.

While with Hughes, Weiss was responsible for the design of large scale, special-purpose military data handling systems. His design and general supervision were responsible for the Northrop's Maddida 44A. His design record also includes Computer Research Corporation's special purpose, high-speed computer, decimal differential analyzer and high-speed printer.

Kaiser Electronics Selects Walden

LLOYD H. WALDEN has been appointed chief engineer of the West Coast electronics laboratory of Kaiser Aircraft & Electronics Corp.

He joins the laboratories at Palo Alto after serving for the past two

Lloyd H. Walden

years as chief electronic scientist for the U. S. Army Signal Corps electronics research unit at Mountain View. There, he supervised technical direction of research and development in the field of electronic countermeasures.

In 1946, he joined the U. S. Navy Electronics Laboratory at San Diego as an electronics engineer, engaged in the development of shipboard electronics equipment.

In 1950, Walden was appointed director of radar equipment de-

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velopment at the Navy Laboratory and supervised design of a number of radar equipments for the Navy and Marine Corps.

Convair Adds Two Engineers

Two electronics engineers have been added to the staff of Convair, division of General Dynamics Corp. in San Diego.

They are John P. Day, engineering staff specialist, who will coordinate research activities in the fields of antennas, radomes and microwaves; and Forrest E. Huggin, design specialist, who will coordinate research in advanced electronic systems and servomechanisms.

Day was with the Naval Electronics Laboratory in San Diego for 11 years and was also at National Aircraft Corp., San Diego, and Lockheed Corp., Los Angeles. He has been an engineering instructor at the University of California for the last six years.

At NEL he headed the instrumentation section of the research division.

Huggin held several key electronics positions in a civilian capacity with the Navy and with Lockheed's missile systems division as radar section chief. His Navy work included the development of pulse command guidance systems of Navy missile use and cathode-ray indicators for nuclear weapon tests.

AIEE Nominates New President

WALTER J. BARRETT, New Jersey Bell Telephone Company engineer, has been nominated to be president of the American Institute of Electrical Engineers. Five vice-presidents and three directors were also nominated.

Barrett, who is transmission engineer of New Jersey Bell will serve as 1957-58 president of the Institute which has a world-wide membership of 51,000. He has been president of United Engineering Trustees, Inc., since 1955. He has been with the Bell System since his graduation from the Polytechnic

Institute of Brooklyn in 1920. He has served as the AIEE treasurer since 1953.

Sperry Award Goes To Jude

George F. Jude

THE Institute of Aeronautical Sciences awarded the Lawrence B. Sperry Award to George F. Jude, director of flight control engineering at the Sperry Gyroscope Co.

The citation reads: "for significant contribution to the advancement of precision automatic flight and safe all-weather flying."

Jude's achievements, since joining Sperry in 1942, were climaxed last year when he led a team of engineer-scientists to successful development of the SP-30, an electronic system for controlling jet airliners in flight.

Thiokel Acquires National Electronics

NATIONAL ELECTRONICS LABORATORIES of Washington, D. C., has been acquired by Thiokol Chemical Corp.

National will operate as a wholly-owned subsidiary under its present name.

Thiokol is engaged in the manufacture of special purpose synthetic rubber and special chemicals. It operates plants in Trenton, N. J. and Moss Point, Miss.

It also operates plants for the research, development and manufacture of solid propellant engines for rockets and guided missiles for

the government at Redstone Arsenal, Huntsville, Ala. and Longhorn Ordnance, Marshall, Texas. It has its own operations for similar projects at Tremonton, Utah, and Elkton, Md.

National Electronics Laboratories has been active in the electronic field since 1946, specializing in instrumentation and communications for the U. S. Government and industry.

Ace Appoints New Division Heads

ACE Electronics Associates of Somerville, Mass. appointed William Lyon and Abraham Osborn to head up the newly formed precision nonlinear potentiometer division. Both have had experience in nonlinear potentiometer design and application.

Lyon was formerly a design engineer with Technology Instrument Corp. for four years. He supervised the electrical engineering department and was responsible for the development of the techniques required in the design of nonlinear potentiometers.

Osborn was with Technology Instrument Corp. for three years on design and application engineering of precision potentiometers. His experience also includes engineering with Fenwal Laboratories, Picker X-Ray, General Radio, and the U. S. Signal Corps.

Du Mont Selects Display Manager

ROBERT W. DEICHERT has been named manager of the newly formed data and display department of A. B. Du Mont Labs.

He will be responsible for development work in the application of data and display techniques to electronic equipment.

Immediately prior to his promotion, Deichert served as head of the division's data equipment development section. He joined Du Mont in 1951 and has been active in the

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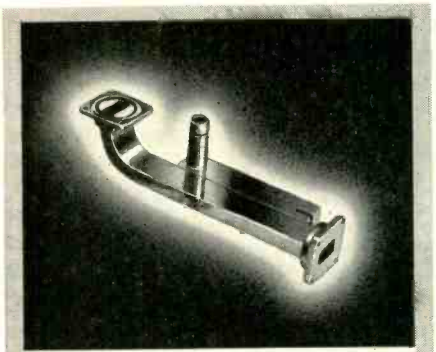

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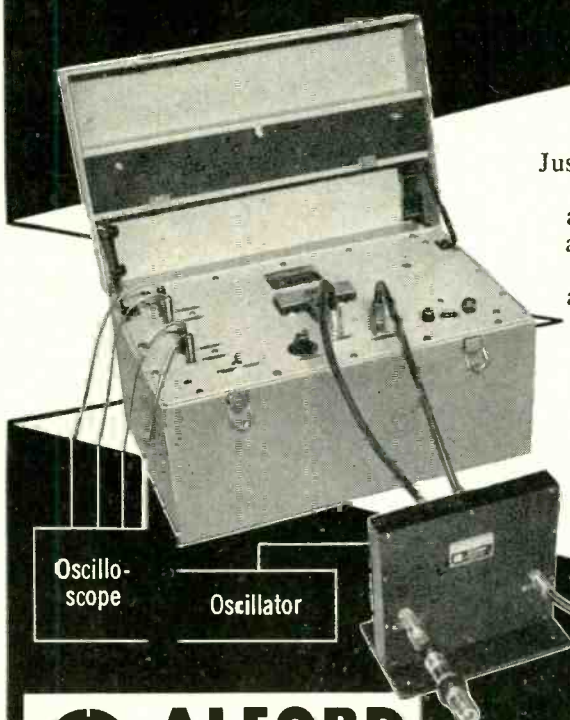

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INSTRUMENTS — ANTENNA SYSTEMS — COMPONENTS — AIR NAVIGATION AIDS

division's work in multipler phototube evaluations, color tv studio equipment and other special projects.

For three and a half years previous to joining the company, Deichert was an instructor of electrical engineering at Pratt Institute's School of Engineering in Brooklyn, New York and at Stevens Institute of Technology in Hoboken, N. J.

Arvin Promotes Three Engineers

JOHN J. CROUCH, former manager of the electric appliances plant of Arvin Industries in Columbus, Ind., has been named director of engineering in the firm's electric appliances department.

John J. Crouch

John P. Sohn, former assistant chief engineer, now is chief engineer for the department, and Eugene E. Ball, who has been factory superintendent, succeeds Crouch as plant manager.

J. Robert Munn, who has been manager of the radio plant in the electronics and appliances division, has been named plants manager of both the radio and electric appliance factories. Francis M. Crockett has been promoted to manager of the radio factory.

Crouch joined Arvin as a radio

engineer in 1933. He became radio and television factory manager in 1950. He was transferred to the electric appliances department in 1952 as plant manager.

IRE Sets Technical Papers For 1957 Convention

Following is the complete list of technical papers and program events to be presented at the 1957 IRE National Convention in New York City on March 18-21:

Monday Afternoon, March 18

NONLINEAR CONTROL SYSTEMS

Nonlinear Compensating Networks for Feedback Systems for E. Mishkin and J. G. Truxal.

Direct Synthesis through Block Diagram Substitutions by O. J. M. Smith.

A Nonlinear Control System for Wide Range Input Signals by J. Tou and Y. H. Ku.

Switching Discontinuities in Phase Space by J. C. Hung and S. S. L. Chang.

Nonlinear Techniques Applied to the Analysis of Pilot Induced Oscillations by I. Van Horn.

VEHICULAR COMMUNICATIONS

How Far Can We Go in Narrowing Channels in the Land Mobile Radio Services– by C. B. Plummer.

Practical Modern Network Theory Design Data for Crystal Filters by M. Dishal.

Recent Developments in Mobile Radio in Britain by J. R. Brinkley.

A Manually Operated Demand Repeater for the 450-470 MC Band by S. F. Meyer.

Sinad Interference Evaluation by Vosim by N. H. Shepherd.

PROPAGATION

The Refractive Index of the Atmosphere as a Factor in Tropospheric Propagation Far Beyond the Horizon by R. E. Gray.

Attenuation and Fluctuation of Millimeter Radio Waves by C. W. Tolbert and A. W. Straiton.

New Evidence of Anomalous Transequatorial Ionospheric Propagation by O. G. Villard, Jr., S. Stein, and K. C. Yeh.

Foreground Terrain Effects on Overland Microwave Transmissions by L. G. Trolese. Mountain Obstacle Measurements by R. E. Lacy.

Passive Repeater Using Double Flat Reflectors by R. F. H. Yang.

ULTRASONICS ENGINEERING

1—AN EDUCATIONAL SESSION

(In Cooperation with the Acoustical Society of America)

The Training of an Ultrasonic Engineer by F. V. Hunt.

Ultrasonic Analysis by T. F. Hueter.

Some Fundamentals of Transducer Design for the Sonic and Ultrasonic Range by F. Massa.

The Ethics, Standards, and Objectives of the Recently Formed Ultrasonics Manufacturers Association by S. R. Rich.

AERONAUTICAL ELECTRONICS

A New Aircraft Static Discharger by R. L. Tanner.

Thermal Design of Commercial Airborne Electronic Equipment by H. M. Passman.

The New Look in Electronic Controls by R. J. Meyer.

Field Test Equipment for Airborne Radar by W. W. Keith and F. E. Sears III.

Hazardous Environmental Factors and Effects Related to the High-Supersonic-Speed Bomber Defense Program by I. Katz.

MULTIPLEX COMMUNICATIONS SYSTEMS

Signal Mutilation and Error Prevention on Short-Wave Radio-Telegraph Serv-

ices by J. B. Moore.

Time Division Multiplex System with Addressed Information Packages by R. Filipowsky and E. Scherer.

A New Time Division Multiplex system by W. J. Bieganski and L. M. Glickman.

48-Channel PCM System by S. M. Schreiner and A. R. Vallarino.

Portable Multichannel 11,000 MC Radio Link by H. Engelmann, H. A. French, M. W. Green, and J. Harvey.

INFORMATION THEORY: CODING AND DETECTION

Optimum Decision Feedback Systems by B. Harris, A. Hauptschein, and L. S. Schwartz.

Sequential Decoding for Reliable Communications by J. M. Wozencraft.

A Non-Mean-Square Error Criterion for the Synthesis of Optimum Sampled-Data Filters by A. R. Bergen.

Message Redundancy vs Feedback for Reducing Message Uncertainty by W. B. Bishop and B. L. Buchanan.

The Analysis of Post Detection Integration Systems by Monte Carlo Methods by R. Dilworth and E. Ackerlind.

SOLID STATE DEVICES

A New High Frequency N-P-N Silicon Transistor by A. B. Phillips and A. M. Intrator. Noise Figures in Semiconductor Dielectric Amplifiers by J. M. Walker, R. E. Smith, and E. M. Williams.

Determination of Thermal Resistance of Silicon Junction Devices by H. C. Lin and R. E. Crosby, Jr.

An Alloy Type Medium Power Silicon Transistor by H. G. Rudenberg and G. Franzen.

A New Semiconductor Device by C. A. Aldridge.

Cadmium Sulfide Photocapacitors by F. Gordon, Jr. P. A. Newman, J. Hamden, H. Jacobs, and A. Ramsa.

Tuesday Morning, March 19

AUTOMATIC CONTROL—GENERAL

Digital Controllers for Feedback Systems by J. R. Ragazzini.

Sampling in Linear and Nonlinear Feedback Control Systems by J. Kukel.

The Role of Automatic Control in the Modification of Aircraft Dynamic Flight Characteristics by W. N. Turner.

Solution of Statistical Problems by Automatic Control Techniques by R. L. Cosgriff. Design of Optimum Filters and Predictors by C. W. Steeg.

NAVIGATION

A Realistic Radar Clutter Simulator by J. Atkins, H. J. Bickel, and M. R. Weiss.

A Precision Multipurpose Radio Navigation System by W. N. Dean, R. L. Frank, and W. P. Frantz.

Some Final Approach System Requirements for High Landing Rates by F. H. Battle, Jr. General Characteristics of a 1000 MC Instrument Landing System by A. Casabona.

NEW BROADCAST DEVELOPMENTS

An Analysis of Packing Density of Information in High-Velocity Transverse Video Magnetic Recording by W. Selsted.

High-Light Aperture Equalizer, by M. V. Sullivan.

Single Sideband Broadcast Developments by L. Kahn.

UHF High-Power Transmitting Developments by J. E. Young, L. L. Koros, and I. Martin.

A Dynamic Standard Signal for Color Television Systems by R. C. Kennedy.

ULTRASONICS ENGINEERING II—TECHNICAL SESSION

Sea Clutter in Radar and Sonar by R. M. Hoover and R. J. Urick.

Transducer Comparison Methods Based on the Electromechanical Coupling Coefficient Concept by R. S. Woollett.

Polarization of Barium Titanate Ceramic by J. G. Froemel.

Ultrasonic Liquid Level Sensor by R. L. Rod.

Precision Calibration of Ultrasonic Fields by Thermoelectric Probes by W. J. Fry and F. Dunn.

New Magnetostriction Filters for the MF Band by R. T. Adams.

ENGINEERING MANAGEMENT VIEWPOINTS

Education: Academic Training for Engineering Management by E. Shapiro.

Finance: Wall Street Looks at Engi-

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neering Management by O. C. Roehl.
Industry: Development of Engineering Managers With Industry by E. I. Greene.

ANTENNAS I—GENERAL

On Ferrite Loop Antenna Measurements by J. L. Stewart.
Ground Antenna Phase Behavior in a Differential Phase Measuring System by I. Carswell and C. Flammer.
Limits on the Information Obtainable from Antenna Systems by W. White.
Antenna Problems in Radio Astronomy by R. N. Bracewell.
High Altitude Breakdown Phenomena by J. Ashwell, E. B. Cole, A. Pratt, and D. Sartorio.

INFORMATION THEORY: REVIEW AND RECENT ADVANCES

Cost of Transmission Reliability by R. M. Fano.
Channel Capacity Without Coding by P. Elias.
Coding a Television Source by J. L. Kelly, Jr.
What Good is Information Theory to Engineers? by J. R. Pierce.

Tuesday Afternoon

MICROWAVE TUBES

The Selection and Applications of Traveling-Wave Tubes by A. H. Nielsen and N.W. Hansen.
X-Band Traveling-Wave Tube Feedback Oscillator by V. G. Price.
A Light-Weight, Low-Level Traveling-Wave Tube Amplifier for S Band by A. G. Peifer.
The Duplexer as a Means of Eliminating Interference from Nearby High-Power Radar Systems by I. Reingold and J. L. Carter.
A New Method of Modulating Electron Beams for Pulse Applications and Linear Amplitude Modulation Systems by G. M. W. Badger.
Behavior of a Backward-Wave Oscillator with External Feedback by F. L. Vernon, Jr.

GENERAL COMMUNCATIONS SYSTEMS

SSB Modulation for Scatter Propagation by F. H. Gerks and R. P. Decker.
FM Scatter System Measurements by R. W. Britton and H. D. Hern.
Theory of Feedback Around the Limiter by E. J. Baghdady.
General Systems Approaches to Telecommunication Optimization Problems by R. E. Kalaba and M. L. Juncosa.
The Future Airforce Communication System by C. K. Chappuis.

MEDICAL ELECTRONICS

A Magnetic Tape Recording System for Teaching Electrocardiography by G. N. Webb and W. R. Milnor.
Ultrasonic Dosimetry for Medical Use by V. T. Tomberg.
An Electrical Circuit Analogy for Isotope Kinetics by R. L. Schoenfeld and M. Berman.
Electronic Control of the Artificial Respiration Cycle by L. H. Montgomery.
The Incorporation of Picture Storage With the Technique of X-ray Fluoroscopy by W. Gombash, Jr.

NEW OPERATIONAL TECHNIQUES CONCERNING VIDEO TEST SIGNALS—A PANEL DISCUSSION

J. R. Popkin-Clurman, F. Davidoff, J. W. Wentworth, R. M. Morris, W. B. Whalley, H. C. Gronberg, V. Hatch, and E. W. Chapin.

HIGH FIDELITY AND HOME MEASUREMENTS

Intermodulation Distortion: Its Measurement and Evaluation by A. Peterson.
Testing High-Fidelity Amplifiers in the Home by W. W. Dean.
Disk and Manetic Tape Phonoraph Systems by W. H. Erickson.
Improved Low-Frequency Loudspeaker Performance by S. Zuerker.
A Low-Pressure Phonograph Cartridge by W. E. Glenn.
A High-Fidelity Phonograph Reproducer by B. B. Bauer, and L. Gunter.

ANTENNAS II—BROADBAND ANTENNAS

High-Frequency Steerable Beam Antenna System by E. Hudock.
Constant Beamwidth Broadband Anten-

nas by C. F. Parker and R. J. Anderson.
Broadband Traveling-Wave Antennas by D. K. Reynolds.
Evaluating the Impedance Broadbanding Potential of Antennas by A. Vassiliadis and R. L. Tanner.
A. Frequency Independent Antennas by V. H. Rumsey.
B. Broadband Logarithmically Periodic Antenna Structures by R. H. DuHamel and D. E. Isbell.

INFORMATION THEORY: APPLICATIONS

An Inductive Inference Machine by R. J. Solomonoff.
Multicase Binary Codes for Nonuniform Character Distributions by F. P. Brooks, Jr.
Binary Transmission Through Noise and Fading by Masonson.
An Estimate of the Degradation in Signal Detection Resulting from the Addition of the Video Voltages from Two Radar Receivers by H. L. McCord.
The X Carrier: A Telephone Carrier System Employing Bandwidth Compression by J. W. Halina.

TELEVISUAL SYSTEMS DEVICES

The Development of 110° Television Picture Tubes Having on Ion Trap Electron Gun by L. E. Swedlund and L. C. Wimpee.
Image Tube Utilizing Bombardment Induced Conductivity by R. W. Decker and R. J. Schneeberger.
New Development in the Panel Light Amplifier by B. Kazan.
An Electrostatic Character-Writing Tube by K. Schlesinger, B. Maggos, and A. F. Hogg. A High Speed, Low Voltage Light Modulator by A. C. Koelsch.

Tuesday Evening

APPLICATION OF THE ELECTRONICS ART TO THE CIVIL-MILITARY NATIONAL COMMON SYSTEM OF AIR TRAFFIC CONTROL

Moderator: J. L. Anast

S. Alexander, C. Wheeler, L. Perper, V. Weihe, and S. Barkowitz.
A discussion of plans, research, and development on national aviation air traffic control facilities and systems and the use of electronics in the program.

MICROMINIATURIZATION—THE ULTIMATE TECHNIQUE

Philosophy of Microminiaturization Technique by C. Brunetti.
The Challenge of the Environment by E. F. Carter.
Material Constituents and Components by H. A. Stone, Jr.
Today's Applications and Equipments
—Military, Brig. Gen. E. R. Petzing (ret.);
—Missiles, J. R. Moore.

Wednesday Morning March 20

ELECTRONIC COMPUTERS I—DIGITAL COMPUTERS

An RCA High-Performance Tape Transport System by S. Baybick and R. E. Montijo. A Magnetic Uulse-Current Regulator by J. D. Lawrence, Jr. and T. H. Bonn.
Diodeless Magnetic Core Logical Circuits by L. A. Russell.
Digital Computer Designs Circiut for Longest Mean Time to Failure by Alman, P. L. Phipps, and D. L. Wilson.
The Design of a Logic for the Recognition of Printed Characters by Simulation on the IBM 650 MIDDPM by E. C. Greanias, C. J. Hoppel. M. Kloomok, and J. S. Osborne.

MAGNETIC RECORDING

An Approach to Quantitative Methods for Evaluation of Magnetic Recording System Performance by C. B. Stanley.
The Application of WOW and Flutter Compensation Techniques to FM Magnetic Recording Systems by R. L. Peshel.
Design of Instrumentation Magnetic Tape Transport Mechanisms, by K. Schoebel.
The Reverbetron by P. C. Goldmark and J. M. Hollywood.
A Multichannel Transducer for Magnetic Recording by H. A. Johnson.

NUCLEAR INSTRUMENTATION

Track Recognition System for Scan-

ning Nuclear Emulsions by S. Becker and J. Franceschini.

Multichannel Analyzer for Time-of-Flight Experiments by H. L. Garner, R. E. Miller, S. H. McMillan, and R. R. Graham.

0.1-Microsecond, 2000-Channel, Electrostatic Storage System for Time-of-Flight Experiments by J. Hahn.

New Double-Line Linear Amplifier by G. G. Kelly.

Radioisotope Thermoelectric Generator by J. L. Briggs.

CIRCUIT THEORY I—SYMPOSIUM ON MODERN METHODS IN NETWORK THEORY

Synthesis Techniques and Active Networks by J. C. Linvill.

The Frequency-Time Representation of Signals Using Natural Components by W. H. Huggins.

Signal Flow Graphs and How to Avoid Them by S. J. Mason.

Panel Discussion on Current Problems in Net work Theory.
Moderator: S. Darlington.
J. G. Linvill, W. H. Huggins, and S. J. Mason.

ENGINEERING MANAGEMENT TECHNIQUES

The Art of Slection of Engineering Management by C. W. Randle.

The Art of Human Relations: Manipulation or Motivation by A. Levenstein.

The Art of Delegation of Authority by W. J. E. Crissie.

TRANSISTOR APPLICATIONS

Circuit Considerations for High-Frequency Amplifiers Using Drift Transistors by J. W. Englund and A. L. Kestenbaum.

Design Considerations in the First Stage of Transistor Receivers by L. A. Freedman.

A Six-Transistor Portable Receiver Employing a Complementary Symmetry Audio Output Stage by D. D. Holmes.

Transistor Receiver Circuits by A. Proudfit, K. M. St. John, C. R. Wihelmsen, and R. J. Farber.

Transistor Circuit Problems in TV Receiver Design by E. M. Creamer, Jr., L. H. DeZube, and J. B. McCallister.

MICROWAVE ANTENNAS

A Versatile Multiport Biconical Antenna by R. C. Honey and E. M. T. Jones.

Recent Annular Slot Array Experiments by K. C. Kelly.

Radiation from Modulated Surface-Wave Structures—I by F. J. Zucker and A. S. Thomas.

Radiation From Modulated Surface-Wave Structures—II by R. L. Pease.

The "Sandwich Wire" Antenna: A New Microwave Line Source Radiator by W. Rotman and N. V. Karas.

Recent Developments in the Study of Printed Antennas by J. A. McDonough and R. G. Malech.

ELECTRON TUBES—GENERAL

Practical Design Theory for Minimization of Vibration Noise in Grid-Controlled Vacuum Tubes by G. Gross.

Electrolytic Tank Measurements of Mesh Grid Characteristics by H. Hsu and and C. E. Horton.

Rare-Earth Oxide Cathodes by L. J. Cronin and J. H. Apelbaum.

Temperature Distribution in Anode Structure for Pulse Input by R. N. Ghose.

A Positive Grid Voltage-Space Current Division Test for Power Vacuum Tubes by J. A. Jolly.

Electron Tubes for Critical Environments by W. H. Kohl.

Wednesday Afternoon

SYMPOSIUM: LONG RANGE TELEMETRY AND REMOTE CONTROL

Electronic Control and Instrumentation of Extra-Atmosphere Space Craft by M. V. Kiebert, Jr.

Progress in Telemetering of Data from High-Velocity Missiles in Upper Atmosphere by R. J. Burke.

Long-Range Telemetering Reception by J. B. Wynn.

Some Dynamic Aspects of Control at

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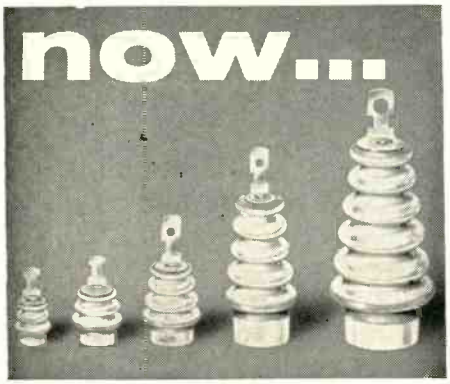

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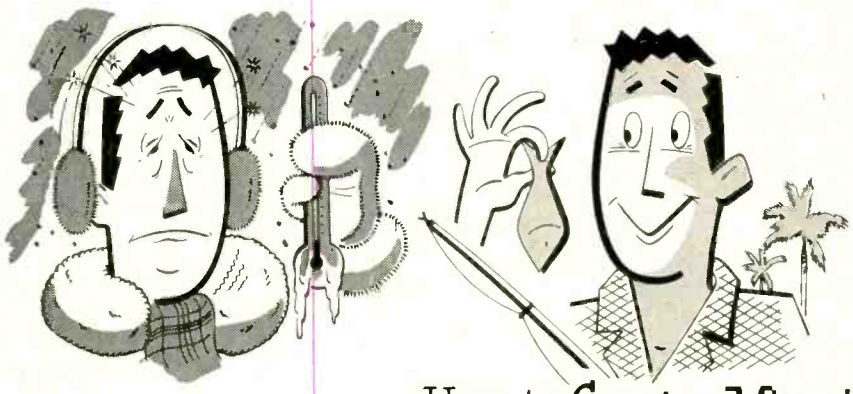

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Circuit Considerations for Audio Output Stages Using Power Transistors by R. E. Minton.

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An Advanced Color Television Receiver Using a Beam Indexing Picture Tube by R. A. Bloomsburgh, A. Hopengarten, R. C. Moore, and H. H. Wilson.

MICROWAVES I—COMPONENTS

A Broadband Fixed Coaxial Power Divider by J. Reed and G. J. Wheeler.
Broadband Waveguide-to-Coax Transitions by G. J. Wheeler.
Transmission Properties of Hybrid Rings and Related Annuli by H. T. Budenbom.
Development of Circulary Polarized Microwave Cavity Filters by C. E. Nelson and W. L. Whirry.
Design of Improved Microwave Low-Pass Filters Using Strip-line Techniques by R. A. Van Patten.
Broadband Frequency Stablization of a Reflex Klystron by Means of an External High "Q" Cavity by M. Magid.

PRODUCTION TECHNIQUES

The Use of Mechanized Wiring for Short Run and Long Run Production of Electronic Assemblies by F. Rosenthal.
An Approach to Airborne Digital Computer Equipment Construction by P. E. Boron and E. N. King.
An Automatic Dip Soldering Machine by V. O'Gorman.
Encapsulation of Electronic Circuits by R. Callcchia.
Development of Interconnecting Wiring by D. J. Keller.

Thursday Morning, March 21

ELECTRONIC COMPUTERS II —SYMPOSIUM ON COMPUTERS IN SIMULATION, DATA REDUCTION, AND CONTROL

E. L. Braun, W. F. Gunning, W. F. Bauer, A. K. Susskind, L. R. Turner, and J. H. Rawlings.

CIRCUIT THEORY II—TRANSISTOR AND AMPLIFER CIRCUIT DESIGN

Some Useful Techniques for Overcoming Frequency Limitations of Distributed Amplifiers by P. H. Rogers, B. F. Barton, and L. A. Beattie.
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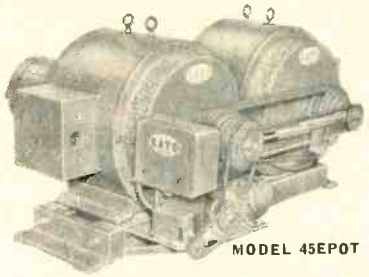

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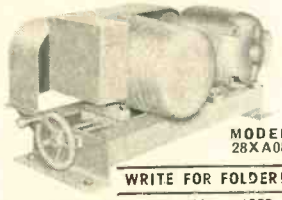

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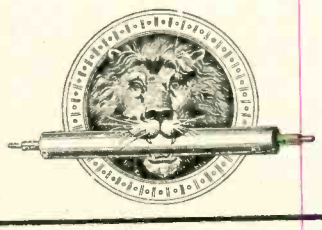

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Circuit Applications of Semiconductor Junction Capacitance by F. H. Dill, Jr., and L. Depian.
Pulse Circuit Applications of a New Semiconductor Device by R. A. Stasior.
Design of Junction Transistor Multivibrators by Driving-Point Impedance Methods by J. J. Suran.

COMPONENTS PART I

Ceramic Filter Capacitors for VHF and UHF by H. M. Schlicke.
Manufacture and Measurement of Close Tolerance Temperance Compensating Ceramic Capacitors by N. Rudnick.
New Subminiture Metallized Paper Capacitors by P. P. Grad.
The Use of Pulse Packages in Line-Type Pulsers by A. Luna.
The Silver Oxide-Cadmium Alkaline Secondary Battery by P. L. Howard.

INDUSTRIAL ELECTRONICS

Coding Problems Related to the Electronic Mail Handling System by M. M. Levy and A. Barszczewski.
Stablized Magnetic Amplifier Circuits by H. W. Patton.
New Techniques for the Control of Resistance Welding Machines by J. L. Solomon.
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Air Force Ground Electronic Equipment Reliability Improvement Program by J. J. Naresky.
A Reliability Program by R. E. Kuehn.
A Reliability Program for R&D Projects by E. F. Dertinger.
The Role of Quality Engineering in Procuring and Producing Reliable Products by R. A. Hulnick.

SYMPOSIUM: DIGITAL TECHNIQUES FOR PROBLEMS IN TELEMETERING AND REMOTE CONTROL

High-Speed Digital Data Handling System by G. F. Anderson.
Magnetic Tape Playback and Digital Conversion of Telemetered Flight Data for Entry into Digital Computers by G. C. Dannals.
Design Considerations for Super Speed Perforated Tape Digital Recording by J. Bellinger, J. MacNeill, and C. F. West.
A High-Speed Binary-to-Binary-Decimal Translator by C. A. Campbell.
Simplicity for Reliable Low-Cost Operation in a Digital Data Processing System by J. W. Prast.

MILLIMICROSECOND INSTRUMENTATION — SPECIAL TOPICS

Millimicrosecond Photography with an Electronic Camera by R. C. Maninger and R. W. Buntenbach.
Electronic Detection and Photography of Incipient Rupture of High Speed Rotors by A. Warnick, R. Condit, J. Patraiko, and H. Peithman.
A Millimicrosecond Pulse Generator Using Secondary Emission Tubes by J. A. Narud.
A Fractional Microsecond Light Source of High Intensity by R. L. Forgacs.
The Electrograph by R. A. Broding, J. C. Westervelt, and J. D. Schroeder.
Low-Level Transistorized DC Amplifier With Improved Stability by A. Warnick and C. N. Savage.

MICROWAVES II—SWITCHES

Precision High-Speed Microwave Switch by W. E. Fromm, S. H. Klug, and K. S. Packard.
Fast Acting Microwave Switch by H. H. Weichardt.
High-Speed Ferrite Microwave Switches by G. S. Uebele.
An L-Band Ferrite Coaxial Line Modulator by B. Vafiades and B. J. Duncan.
Ferrite Microwave Detector by D. Jaffe, J. C. Cacheris, and N. Karayianis.

Thursday Afternoon

ELECTRONIC COMPUTERS III —MAINLY ANALOG

Cimputation with Pulse Analogs by N. Rubenfeld.
A Cyclic Digital-to-Analog Decoder by G. H. Meyers.
An Automatic Analog Computer Method for Solving Polynomials and Finding Root

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Loci by L. Levine and H. F. Messinger.
Magnetically Controlled Counters by E. A. Sands.
Systematic Tracing of Discrepancies in Analog Computers by M. Plotkin and E. Grosswald.

CIRCUIT THEORY III—
NETWORK DESIGN
TECHNIQUES

Pulse-Forming Networks Approximating Equal-Ripple Flat-Top Step Response by A. D. Perry.
Interstage Network Design with Practical Constraints by B. F. Barton.
Synthesis of Lumped Parameter Precision Delay Lines by E. S. Kuh.
On the Approximation Problem in Filter Designs by A. Papoulis.
Recent Advances in the Synthesis of Comb Filters by W. D. White and A. E. Ruvin.
Explicit Formulas for Tschebyscheff and Butterworth Ladder Networks by L. Weinberg.

COMPONENT PARTS II

Thermistors for the Gradual Application of Heater Voltage in Thermionic Tubes by J. J. Gano and G. F. Sandy.
New Levels of Performance for General Purpose Resistors in Army Applications by R. A. Osche.
Measurements and Effects of Error Rate in Precision Potentiometers by S. B. Rasmussen.
Theory, Measurement and Reduction of Precision Potentiometer Linearity Errors by F. Fritchle.
Vibration and Shock Resistant Delay Designs by A. P. Boylan and J. L. Pfeffer.

ANALYSIS AND TECHNIQUES
FOR IMPROVED RELIABILITY

Guided Missle Reliabilty vs Complexity by S. W. Lichtman.
Narrow Limit Gage Sampling Procedure by H. G. Harding and S. Price.
Increased Reliability Through DC Overpotential Testing of Electronic Components by V. Wouk.
Reliability Calculations for Complex Systems by H. E. Blanton.
Analysis and Engineering Study of the Environmental Vibrations and Shock Characteristics of New Military Airborne Gimbaled Equipment by D. Ehrenpreis.

SYMPOSIUM: LOW LEVEL
MULTIPLEXING FOR
TELEMETERING AND
REMOTE CONTROL

A Low-Level Electronics Switch by E. Dorsett.
Low-Level Signal Multiplexing by D. W. Hill and A. S. Westneat, Jr.
Reliable Operation of Commutation Switches of the Stationary Disk and Rotating Brush Assembly Variety at Relatively High Sampling Speeds by W. L. Switzer.
A Unique Wideband Transistorized Pulse Amplifier by W. T. Eddins.
Completely Transistorized Strain Gage Oscillator by W. H. Foster.

INSTRUMENTATION II

A Microwave Spectrometer for Industrial Use by J. F. Marion and G. J. Neumann.
A Unique Standard-Frequency Multiplier by J. K. Clapp and F. D. Lewis.
Measurement of the Complex Permeability of Magnetic Materials Over the Frequency Range of 50 to 500 Megacycles by I. Brady and R. J. Franklin.
An Automatic Impedance Plotter Based On a Hybrid-Like Net Work with a Very Wide Frequency Range by C. B. Watts, Jr. and A. Alford.
Automatic Indication of Receiver Noise Figure by A. J. Hendler and F. G. Haneman.
High Precision Sawtooth Generator by L. J. Torn.

MICROWAVES III—GENERAL

The Optimum Spacing of Bead Supports in Coaxial Line at Microwave Frequencies by D. Dettinger.
Multiple-Line Directional Couplers by J. P. Shelton, Jr.
Effects and Measurement of Harmonics in High-Power Waveguide Systems by M. P. Forrer and K. Tomiyasu.
Microwave Dielectric Properties of Solids for Applications at Temperatures to 3000° F by D. M. Bowie.
Traveling-Wave Cavity for Ferrite Tensor Permeability Measurements by L. A. Ault, E. G. Spencer, and R. C. LeCraw.
The Principle of a Nongyromagnetic Ferrite Phase-Shifter by S. Wenglin.

New Books

Man of High Fidelity: Edwin Howard Armstrong

By Lawrence Lessing
J. B. Lippincott Co., Philadelphia, Pa., 1956, 320 *p*, $5.00.

Biographer Lessing has described Major Armstrong in terms of his environment, a condition necessary if the unacquainted reader is to understand even a fraction of Armstrong's genius and his mission. In thus contrasting his actions with those of the majority, the author may have made him seem less than human. There are few clear allusions to Armstrong's genuine courtesy, his consideration and his warm but unpublicized charity. His humility as a craftsman, doing what he could not quite trust others to do, is not entirely apparent.

The picture Lessing paints of a commercial atmosphere automatically inimical to the individual engineer and inventor may or may not be true for others as it was for Armstrong. It could be chilling and provocative reading for engineers of lesser strength and attainments than those of the Major. And it points up the real problem of financing modern research without destroying individual initiative.

► **History** — The biographer has been something less than tactful in dealing with historical facts. Assuming that today's young engineer is willing to accept Armstrong's contributions without considering their source, he is still baffled by situations in which Armstrong tried unsuccessfully to show the path out of the swamp. Current communications problems based on propagational facts are examples.

► **Prophecy**—Simply summed up, trouble from ionospheric interference is, indeed, now plaguing users of the 50-mc band vacated by the f-m broadcasters under a 1945 FCC order. Armstrong had taught that the superior interference protection of wide-band f-m would obviate such trouble—that trouble could occur for services with lesser protection.

Engineers can, however, be most grateful to Lessing for unraveling and displaying for laymen the incredibly tangled skein of patent legalities that finally impoverished a multimillionaire inventor and cost the world his life.—A. A. McK.

Communication Engineering

By W. L. Everitt and G. E. Anner.
McGraw-Hill Pub. Co., Inc., 1956. 642 *p*, $9.00.

The new edition of "Communication Engineering" treats a limited number of areas basic in the field of communications, chiefly covering networks and transmission lines. These subjects are preceded by an excellent discussion of fundamental communications principles and followed by a useful chapter on electromechanical devices.

Widespread use of the second edition makes it worthwhile to compare the new greatly revised third edition with that earlier one. The present edition has eliminated not only a number of sections covering material topical in 1936, but has also eliminated sections that represented specific design details; circuits of class A audio and radio amplifiers, detectors, modulators, antennas, propagation, etc. The book's orientation has thus been changed from one which somewhat emphasized handbook design to one of emphasis on principles which are likely to be as applicable in the future as they are today.

► **Well Correlated**—In comparison with other recent texts in the field of communication electronics, the limited scope of Everitt and Anner's book is offset by an unusual degree of coherence. For example, illustrations showing various aspects of a subject are well correlated, so that the reader can refer from one illustration to another and see readily the effects of changing some parameters while leaving others constant. Interrelationships between various chapters are also skillfully handled.

Understanding of the book does not require advanced mathematics;

an effort has been made to familiarize the reader with hyperbolic functions and with Fourier transforms.

There are a few subjects whose inclusion (under chapter headings already in the book) might have better fulfilled the author's intent to concentrate on fundamental areas. These include more thorough discussion of multichannel systems and of pulse systems under modulation theory, greater emphasis on circuit duality in the sections on networks, and a fuller coverage of feedback's close relationship to amplifiers. However, these subjects and others deliberately omitted by the authors are treated in a variety of other texts.

Various minor errors, such as the incorrectly-drawn exact and approximate resonance curves in Figure 4-11, should not lead the reader astray; they will undoubtedly be corrected in the next printing.

In conclusion, the clarity and coherence within individual chapters and throughout the book should be of distinct advantage in understanding the background of a rapidly changing subject. This version represents enough of a change to be worthy of purchase even by those owning the second edition. ALFRED J. POTE, *Hycon Eastern, Inc., Cambridge, Mass.*

Electronics

BY A. W. KEEN. *Philosophical Library, New York*, 1956, 256 *p*, $7.50.

THOUGH written for a nontechnical audience, this book covers a remarkable amount of advanced electronics and applications.

Starting with an answer to the question "What is Electronics?", the author Keen leads his readers through a simplified, yet concentrated, introduction to electron physics. The next few chapters introduce the basic components and control devices.

▶ **Circuits** — Before getting into equipment applications, the author gives a lucid explanation of the various basic circuit functions in amplification, rectification, wave shaping, switching, oscillation and

the like. With this foundation, he proceeds to show the varied applications of these fundamental processes.

The applications discussed include, to mention a few, audio; radio communication and broadcasting; radio navigational aids and radar; television; switching, counting and computing; industrial electronics and instrumentation. The profusion of block diagrams and simplified schematic diagrams greatly adds to the readability and understanding of these sections.

The descriptive style of this book recommends it for those interested in electronics who are limited by only a basic knowledge of electricity, but who want to know more about counters, rotary switching tubes, gating circuits and similar building blocks of our present-day electronic devices.—H.A.M.

Pulse and Digital Circuits

By Jacob Millman and Herbert Taub.
McGraw-Hill Book Company, Inc., 1956, 673 *p*, $12.00.

Drs. Millman and Taub have produced a book which should prove extremely valuable to the practicing engineer in the field of nonlinear circuits, possibly more valuable even than to the undergraduate electronics student for which it is intended. The authors have done an admirable job of collecting and lucidly analyzing a large number of the basic circuits which are the tools of the engineer in this field.

The book starts with a review of amplifier circuits with particular emphasis upon the cathode follower and the operational amplifier. This is followed by material on linear wave shaping, linear pulse or video amplifiers and nonlinear waveshaping (a somewhat illogical grouping possibly). The chapter on linear pulse amplifiers is particularly impressive because of the relevance of the material chosen for presentation to practical design problems.

▶ **Waveform Generation** — A following group of chapters deals with waveform generation and describes various multivibrator circuits, time

base generators and blocking oscillators. The operation of numerous specific circuits is explained, analyzed and their application discussed. Blocking oscillator operation is treated in considerable detail.

The characteristics of distributed and lumped parameter delay lines are discussed as are some delay line applications including their use in distributed amplifiers. There is considerable discussion of counting and frequency-division methods in which again the operation of numerous specific circuits is explained including the use of binary counters with feedback, blocking oscillators, multivibrators and phantastrons.

► **Computer Circuits** — A chapter on fundamental digital computer circuits describes various building blocks such as the OR, AND, NOT circuits, shift registers, inhibitor circuits, etc. There is a too short discussion of magnetic binary elements and their application. Various transmission gates, voltage comparators, and time modulation and measurement means are discussed and analyzed.

The chapter on pulse and digital systems is, in our opinion, incomplete since the authors have chosen to discuss only television and radar as examples of pulse and digital systems leaving out any discussion of actual digital computation systems. We realize that a detailed discussion would require at the least another book the size of this, but a discussion of the principles involved and examples of how some of the circuits described in previous chapters are combined to perform the necessary operations would not have been amiss.

► **Transistors** — The book concludes with an excellent chapter on transistors which includes some semiconductor physics, a discussion of the fundamentals of transistor operation and the application of the transistor to linear and nonlinear circuits.

As can be seen from the foregoing the book is primarily a compendium of circuits with explanations and analyses. Because of this we must take issue with the au-

thors' recommendation of the book as the concluding course in a sequence of three undergraduate electronics courses. It is our strong feeling that the student's time would be better spent learning more of the fundamentals of circuit design and analysis than can possibly be taught in two courses. We share the authors' preference for four undergraduate electronics courses in which case "Pulse and Digital Circuits" would serve admirably as a text for the final course.—L. L. POURCIAU, *General Precision Lab. Inc., Pleasantville, N. Y.*

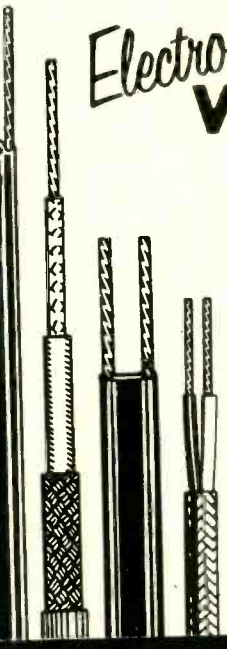
Handbook of Semi-Conductor Electronics

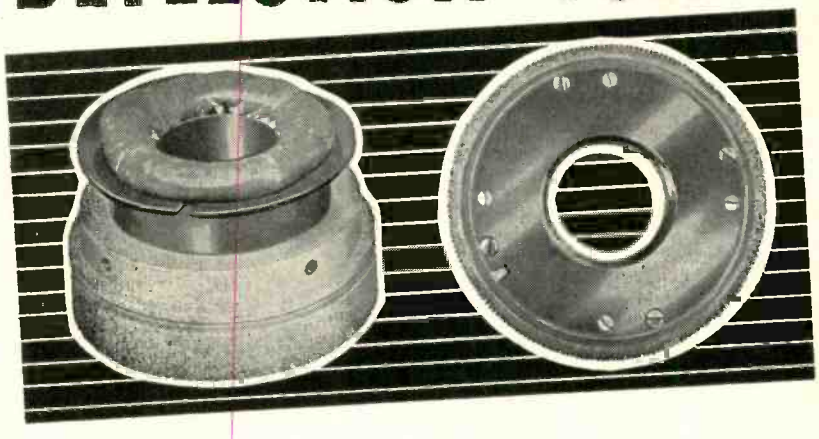
BY L. P. HUNTER.
McGraw Hill Book Co., Inc., New York, 1956, 832 *p*, $12.00.

THIS VOLUME is a book of slightly over 800 pages, which is not large compared to many other handbooks, but does manage to deal with most aspects of this field in varying degrees of completeness and detail. It consists of four Parts and 20 Sections, as well as an excellent bibliography and essentially complete and well organized author and subject indices.

▶ **Parts I and II**—Entitled "Physics of Transistor Diodes and Photocells" and "Technology of Transistor, Diodes and Photocells", the subjects covered in these sections range from electronic conduction in solids through transistor action, and from preparation of semiconductor materials through device design considerations. L. P. Hunter has contributed all of Part I, as well as Section 10 of Part II. Such well known names as H. F. Priest and W. C. Dunlap, Jr. are responsible for other sections.

The intentions of these Parts are for ". . . the one purpose of supplying only those principles needed to understand the mechanisms of transistor and diode action" and ". . . to provide the engineer with a basic understanding of the limitations imposed upon the finished devices by the various methods of fabrication." Within these limitations, as stated in the prefaces, the





results are admirable and the range of subjects is entirely adequate for the purpose.

The emphasis on energy level diagrams and the neglect of the somewhat more familiar symbolic structures, may make Part I somewhat difficult reading for non-physicists. It is also unfortunate that no information on radiation effects is included. However, once it is understood that Parts I and II are not intended to serve as specifically handbook material, it may be stated that the combination of Parts I and II makes an excellent introduction to the general problems and characteristics of device design.

These parts are recommended to the circuit designer as a desirable adjunct to his knowledge of the circuit characteristics of these devices.

▶ **Part III**—Containing the "red meat" of this book, this part approaches closest to meeting the requirements one might wish to put on a handbook. A generally successful attempt is made in most sections to provide design information for the subjects under discussion.

The weakness in Part III lies in the tendency in some sections to depend too much on descriptive material and not enough on tables, monographs, lists of significant equations, graphs, etc. The sections on oscillators and special semiconductor devices are probably least satisfactory from this point of view.

The sections on low-frequency amplifiers, d-c amplifiers, and switching circuits are closest to what may be termed the ideal handbook structure, but also suffer to some extent from an excess of discursive treatment and an insufficiency of the sort of design aids a handbook should provide to justify its title, if not its existence.

A few specific instances of success and partial failure from this point of view may be adduced. H. J. Woll, in Section 11 on low-frequency amplifiers, is to be complimented on the yeoman work he has done in trying to bring some order out of the chaos into which the transistor equivalent circuit situation has begun to deteriorate. How-

ever, both the class B power amplifier and operating point stabilization discussions seem inadequate.

This reviewer can state, unequivocally, that stabilization against both device and temperature variations is of far more significance than the limited treatment in the text might lead one to believe. For example, the equation at the bottom of p 11-53 seems as though it should be $I_c \cong [I_{co} + E_c/(R_b + R_c)]/[1/h_{cb} + R_c/R_b]$, but without more information about the author's assumptions it is impossible to verify this.

The presentation of regulated power supplies in Section 13 on d-c amplifiers by C. Hurtig is also inadequate for design purposes. A much more elaborate exposition is necessary to prepare the circuit designer for dealing with this problem.

► **Oscillators**—Most of Section 14, by E. Eberhard, on oscillators, is devoted to point contact types. The treatment of junction, crystal and nonsinusoidal circuits is little more than a cursory introduction. A more complete description of nonsinusoidal types is included in Section 15 by J. C. Logue on switching circuits, but does make up for part of this lack. This latter section is the longest single section and contains a great deal of useful and well organized information on both switching and logical circuits. However, it is perhaps unfortunate, in view of the trend to junction transistors, that so much space is used for point contact transistor circuits, while no junction transistor regenerative amplifier is included.

Section 12, by J. B. Angell, on high-frequency and video amplifiers is largely unexceptional and is essentially limited by the general lack of knowledge. The same comment might be made about George H. Royer's treatment of circuits using special semiconductor devices.

► **Part IV**—The "Reference Material" consists of two sections by H. Fleisher applying familiar techniques of graphical and matrix analysis to the specific problems of transistor circuits and two sections

by G. Knight, Jr. and J. C. Logue on measurement of semiconductor and semiconductor-device parameters. This is not reference material in the usual handbook sense, but does provide an understanding of the methods whereby the analytical and empirical material of previous sections was obtained.

▶ **Conclusion**—A few editorial or proof reading lapses may be found in this book. These include the absence of numbering for the equations in Section 10 and the repetition in Section 13 of some of the material covered in Section 10, without establishing a proper relationship between the symbols and formulas used in the two sections.

The same stricture might be applied to Sections 17 and 18 on analysis. It was also surprising to find no discussion of the *pnip, npin* transistors and no reference to J. M. Early's article on junction transistor design at the end of Section 10 on device design considerations.

However, considering the gargantuan task involved, one can have nothing but praise for the general coherence and readability of the result of L. P. Hunter's editorial labors. While it is not the ultimate semiconductor electronics handbook, this is not surprising considering the newness of the subject and the rapid advances still being made.

As another entry in the still inadequate group of transistor texts, this volume has a great deal to commend it. Therefore the inadequacies mentioned above do not denigrate it and may be condoned in terms of an ambitious undertaking which succeeds far more frequently than it fails.—SOL SHERR, *General Precision Lab., Inc., Pleasantville, N. Y.*

Thumbnail Reviews

Elements of X-ray Diffraction. By R. D. Cullity, Addison-Wesley Publishing Co., Reading, Mass., 1956, 514 p, $10.00. A student's book of solid-state X-ray diffraction principles and

methods covering X-rays and crystal structure, followed by treatments of the theory of diffraction, experimental methods and applications. Electron and neutron diffraction are discussed in an appendix. Other appendices contain many numerical constants useful in this work.

Elements of Radio, Third Edition. By Charles I. Hellman, D. Van Nostrand Co., Inc., Princeton, N. J. 1956, 354 p, $4.95. Up-to-date introductory text for high school students starts with fundamentals and leads up to such relatively sophisticated topics as transistors and television.

Studien über einkreisige Schwingungssysteme mit zeitlich veränderlichen Elementen. By Bruno Rudolf Gloor, Verlag Leemann, Zurich, Switzerland, 1955, 236 p. Analytical and experimental investigations of the theory and applications of the super-regenerative receiver.

Studien über Traveling-Wave Tubes. By Gerhard E. Weibel, Verlag Leemann, Zurich, Switzerland, 1956, 93 p. Theoretical analysis of traveling-wave tube as an active eight-terminal network and description of demountable experimental tube.

The Art and Science of Protective Relaying. By C. Russell Mason, John Wiley & Sons, Inc., New York, 1956, 410 p, $12.00. Introductory text to basic principles of relay design and application to all elements of a power system against abnormal operating conditions. One of a series by General Electric authors.

Management Control in Aircraft Subcontracting. By Niel E. Harlan, Harvard Business School, Division of Research, Boston, 1956, 256 p, $4.00. Problem of reestablishing the control system that is disrupted when a part of a production job is lifted from the plants of a prime contractor and placed in the hands of an outside company under a subcontract arrangement.

Symposium on the Application of Transistors to Military Electronics Equipment. Committee on Electronics, Office of the Secretary of Defense, Nov. 1953, 508 p, $5 (paper). Thirty-two papers mainly concerned with fabrication of transistors by laboratory or pilot-line techniques or combinations of both. May be ordered from OTS, PB 111680 U. S. Department of Commerce, Washington 25, D. C.

The Oscilloscope at Work. By A. Haas and R. W. Hallows, Philosophical Library, New York, 1954, 171 p, $10.00. Practical guide to application of oscilloscope to investigation of radio and tv circuits. Text is profusely illustrated with waveforms. Book is expanded version of French "L'Oscillographe au Travail".

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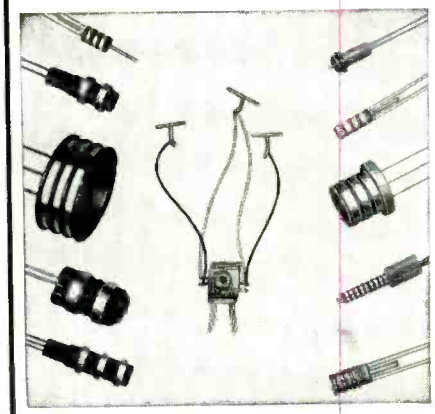

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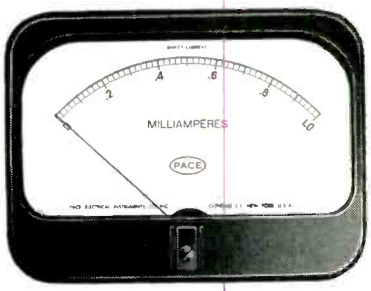

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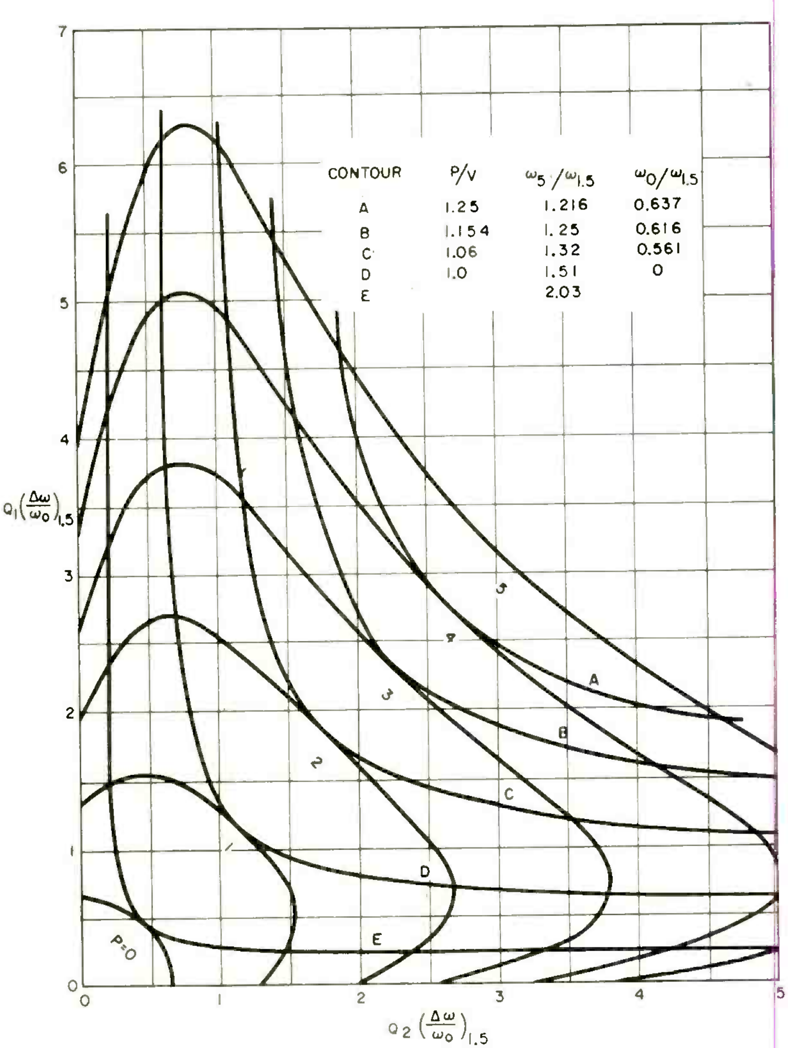


Transformer Curves for Reference Sheet

DEAR SIRS:

WE found the article, "Design Charts for Tuned Transformers," which appeared on p 182 of the November 1956 issue, of great interest. Unfortunately, the curve shown for Fig. 5 is identical to that shown as Fig. 2. Would it be possible to print the correct Fig. 5 in a future issue?

Your publishing work is very much appreciated in Japan, especially in the area of automation and peaceful uses of atomic energy. ELECTRONICS is a great help to us in studying transistor circuits. It gives us practical and useful suggestions in our major fields.

We hope your editing and publishing activities will be greatly expanded in the future.

TOMOHIKO SUZUKI
Research Division
Iwasaki Communications Apparatus Co.
Tokyo, Japan

Editor's note: For Mr. Suzuki and other readers, the correct Fig. 5 is shown above.

Gravity Hypothesis

DEAR SIRS:

THE explanation for gravity proposed by Littell (ELECTRONICS, March, 1956) is not a true explanation in that, when examined carefully, it results in an observable modification of existing law.

The description of the universe

under Littell's hypothesis can be studied mathematically and, if normalized to the observer, its analysis becomes quite simple. Omitting mathematical details, the reasoning follows.

The explanation allows two interpretations, either (1) the acceleration of the expansion is proportional to the gravitational force of a body, $r = kr^{-2}$ for a "point" source like the planets or the sun for $r >$ the radius of the object or (2) The space surrounding a gravitating mass expands as a "rigid" body with acceleration independent of distance and equal in magnitude to that of the surface of the mass.

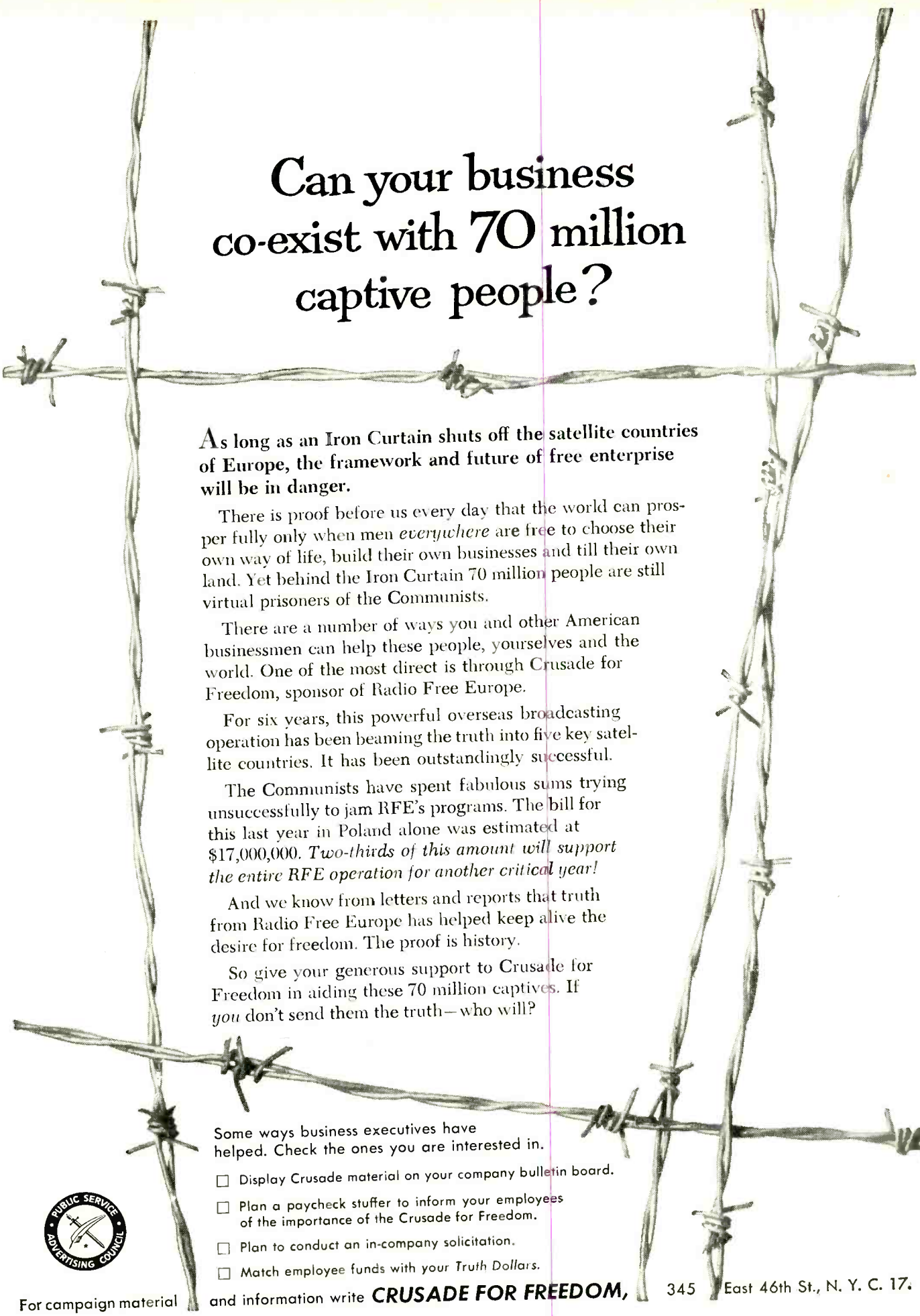
The impossibility of reconciling alternative 2 with the actual universe is so evident that it will not be further considered. The sun's gravity would affect us 20 times as much as the earth's in every respect and we would either be crushed to the earth's surface during the night or else go shooting off toward the sun during the day.

The first possibility, if it did occur, could easily be detected in the laboratory and moreover would violate all astronomical observations. Since its contradiction to these observations would be most spectacular, we will examine this case especially.

The apparent size or diameter of objects depends linearly upon their true relative diameter and is inversely proportional to their distance from the observer. This is a simple fact from geometry and merely requires normalization with respect to the observer to be also true in Littell's universe.

For objects whose distance is great in proportion to their mass (so that the expansion of an orbit is small compared to that of the central body), like the sun, moon, and almost every other celestial object, the apparent size (relative to the earth) would, applying Littell's explanation, be proportional to the gravitational field of the object and would be either expanding (relatively) or contracting depending upon whether its gravity were respectively greater or less than ours.

This relative change could be detected in a matter of minutes and would eventually result in the moon shrinking from view and the sun



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growing until it covered the whole sky!

Littell's hypothesis could only be made consistent with our observations by denying the law of conservation of matter and the fundamental assumption, which underlies all physical science, that the universe is composed of classes of similar nonmultiplying particles which are the electrons, protons and so on.

Deny these fundamental assumptions and the very existence of science would be impossible.

FRANKLYN G. CREESE
California Forest and Range Experiment Station
University of California
Berkeley, California

Dempa Gizitsu

DEAR SIRS:

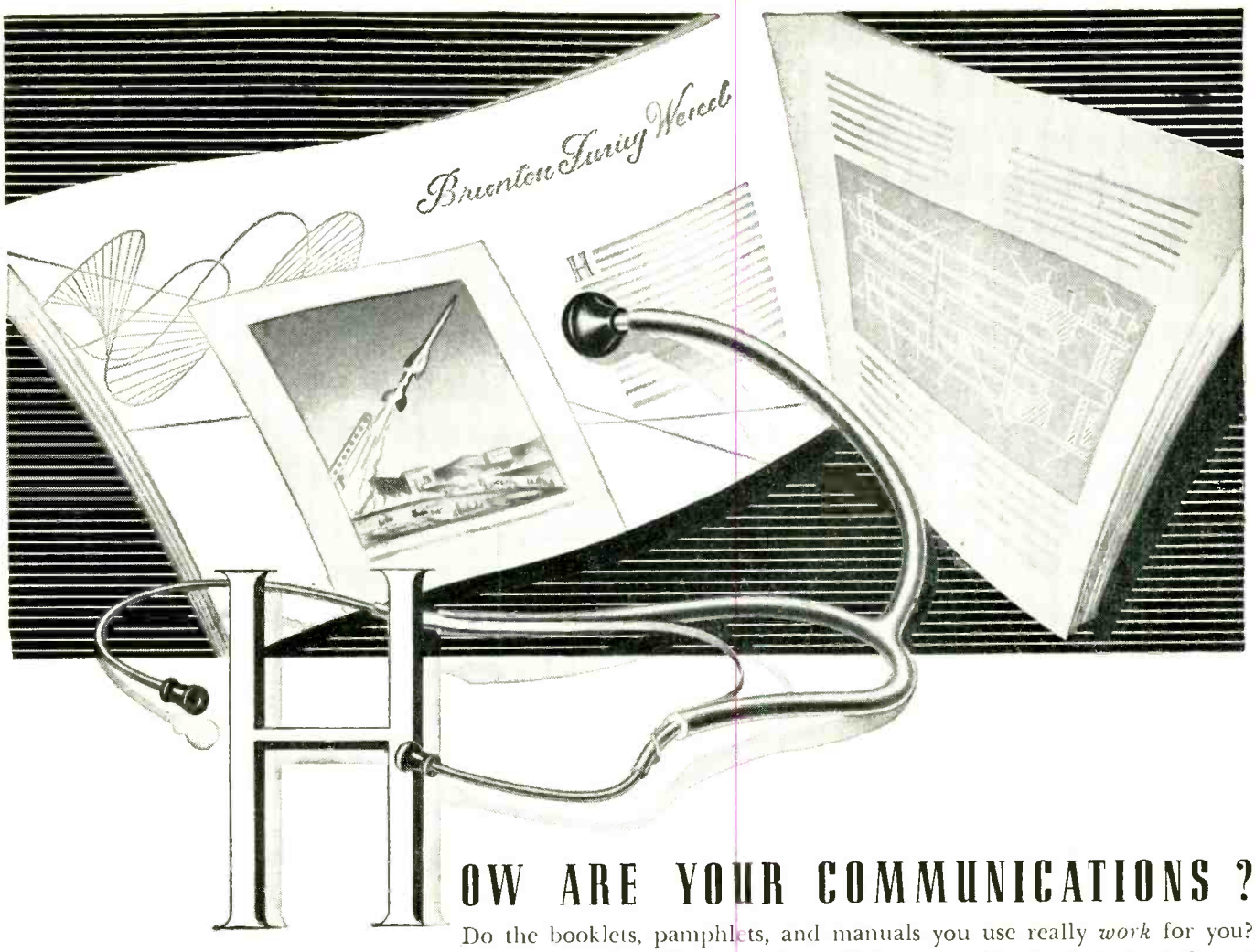
As a reader of ELECTRONICS and a student of the Japanese language here in Japan, I feel inclined to add my two yen worth of comment on the dempa gizitsu subject.

There are two main systems of transliterating the Japanese language into the Roman alphabet. They are the official government system, "Kunrei" (meaning "Orders") and the Hepburn system which is named after its founder, James C. Hepburn.

The two systems have somewhat conflicting aims. In the case of the Kunrei system, the intent is to maintain the regularity in spelling various conjugations of verbs etc. To this end it is necessary for the syllable pronounced SHEE to be spelled SI; TSOO is spelled TU; CHEE is TI; JEE is ZI; FU is HU and so forth, although many syllables are the same in both systems.

To most foreigners accustomed to the Roman letter equivalent in their own language, the Japanese Kunrei system is awkward. For instance the famous mountain of Japan is spelled HUZI although pronounced FOO-JEE. Because of this, the system has not been received with much enthusiasm by anyone, although serious students of the language will point out that it has certain definite advantages over the Hepburn system.

The Hepburn system attempts to



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retain the conventional pronunciation of the Roman letters so that it is much easier for the untrained foreigner to read. Thus the word SHEEM-BAH-SHEE is spelled Shimbashi in Hepburn instead of Simbasi as in Kunrei.

Either denpa or dempa is an acceptable Romanization because it is customary to change an "N" to an "M" if it precedes a "P" or a "B". In either case, the word is pronounced DEM-PAH. The gizitsu, however, is an error in any Romanization. It should be GIJUTSU in the Hepburn system. (Note: "G" is always pronounced as in the English word "GO": never as in "GEM".)

Most foreigners, especially Americans, would tend to pronounce this word gijutsu as gee-JOO-tsoo, putting an incorrect accentuation on the middle syllable. The Japanese pronounce it something like geej'ts' almost failing to voice the u's. For this reason, it would be pronounced almost exactly alike whether it were gijitsu or gijutsu. Thus when writing the word in Roman letters it is easy to confuse the two. This is especially true because of the fact that very little of the language is ever so transliterated. It is generally written in the Kanji (ideograms) and the two syllabaries Hiragana and Katakana. Anyone who wants to learn the written language must learn fifty Hiragana symbols, fifty Katakana symbols and approximately two thousand Kanji ideographs.

Since the war, the close ties between Japan and the United States have caused a considerable number of American words to become accepted into the Japanese language. But due to the limitations of the Japanese syllabary, some ordinary English words take on rather strange sounds and spelling: "miruku" is as close as they can come to the word "milk"; butter is "bata"; a word like television comes out terebijon, although it is usually shortened to terebi. Tape-recorder would have to be written te-pu rikoda, and that would probably be shortened to your word teriko.

As for ordinary words and older words such as your superregeneration, they are arrived at thusly: The

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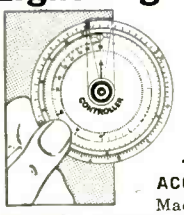

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Kanji symbol for SAI means "twice" or "again"; the symbol for SEI means "to live" or "to be born". Thus the combination of the two symbols, SAISEI, means to regenerate. The symbol for CHO means "to surpass" or "super". All three symbols in combination, CHOSAI-SEI, have the rather obvious meaning of superregenerate.

The Japanese language is quite interesting in itself, but the country of Japan is sheer fascination.

FRANK LESAGE
RCA Field Engineer
APO, San Francisco, Cal.

On Transistor Symbols

DEAR SIRS:

JUST noted Mr. James E. Pugh's letter, page 436, Sept. 1956, in regard to a proposed new symbol for junction transistors. Would like to add my two cents worth to any contemplated change from present usage.

While I, for one, am in favor of progress and agree wholeheartedly that some change in transistor symbology may be needed eventually, I can't help but feel that Mr. Pugh's suggestion is a bit premature.

In the case of vacuum tubes, the symbols are all basically the same, with but minor modification to indicate the type. A triode and tetrode, for example, differ by only the addition of a grid symbol.

However, what Mr. Pugh suggests is a radical change in symbology, change which would, at one stroke, obsolete the great mass of existing literature.

His primary reason for change appears to be to differentiate between point-contact and junction transistors. This would leave the field using an almost obsolete symbol, for the point-contact transistor is, like "old soldiers," fading away. Relatively few transistor manufacturers include point-contact types in their lines.

More important, perhaps, are the many new types of semiconductor devices rapidly coming up . . . the drift or field-effect transistor, GE's Unijunction or double-based diode transistor, Marvelco's

tandem transistor, IBM's thyratron transistor (a combination of a junction and a point-contact unit), various types of surface barrier transistors, including Philco's new sbdt type, and, of course, thyratrons, phototransistors and many special purpose types.

If Mr. Pugh's suggestion were followed to the letter, we would need a different symbol for every type of transistor . . . with the field in such a fluid state we could easily end up with more transistor symbols than all other component symbols combined.

Personally, I would suggest a waiting period, at least until the field is less fluid, in the meantime retaining the present, and widely used, symbol. But we could think about a symbology that would permit adding new types (as easily as we can add a new vacuum tube type, by adding a grid or plate line). Later, when basic transistor types, at least, have crystallized, a general meeting of representatives of all interested groups . . . standards groups, the military, the IRE and AIEE, and other recognized authorities, could consider a more formal standardization of symbology.

LOUIS E. GARNER, JR.
Technical Consultant
Silver Spring, Md.

Self-Sustained Emission

DEAR SIRS:

IN the January 1, 1957 issue, under *Electrons At Work* some results of studies on self-sustained emission from cold cathodes were described (p 190).

While secondary emission formerly was the means of starting the self-sustained emission, it is not a factor in the operation. Field emission and avalanche effects in the coating are believed to be the essential mechanism.

The work was initiated in the Signal Corps Engineering Laboratories and is now being continued under a Signal Corps Contract.

A. M. SKELLETT
Director of Research
Tungsol Electric Inc.
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Advanced degree or equivalent in math, physics or engineering. Minimum 3 to 5 years' experience. Position at Airborne Systems Laboratory, Waltham, Mass.

TRANSDUCER DEVELOPMENT ENGINEER

Salary to $12,500

Interesting position for Acoustical Engineer to work with small group in design and development of devices and systems. Prominent in the microphone and transducer field, RCA has interesting work in the following areas: headsets, and loudspeakers, noise and vibration measurement and analysis, speech compression systems, noise cancellation microphones, psychoacoustics. RCA has facilities ideal for the man who desires advanced work. Position is located in Greater Philadelphia area at Camden, New Jersey.

INFRARED SYSTEMS ENGINEER

Salary to $15,000

Engage in overall coordination and design of infrared systems for Airborne Fire Control Defense and Missile Guidance. You should be experienced in general performance specifications, servo design, displays, infrared heads and optical systems. You also must be capable of giving technical guidance to Junior Engineers. Minimum of 5 years' experience necessary. EE or Physics degree. The location is Camden, New Jersey, in the Greater Philadelphia area.

EQUIPMENT DEVELOPMENT ENGINEER—MECHANICAL

Salary to $11,500

Opportunity for work of advanced development nature in areas of receiving tubes and semiconductors. Conception, design and development of prototype equipments. Education, background and experience in mechanization, and related fields required. Knowledge of electromechanical systems desirable. Air-conditioned area, with complete shop and laboratory facilities. Position at Harrison, N.J. . . . 30 minutes from N.Y.C.

MANAGER MICROWAVE TUBE ENGINEERING

Salary—Open

Supervise fifteen engineers and technicians investigating application problems and development of new applications for Microwave tubes. Work with equipment customers and field personnel on Microwave tube applications. Preparation of new technical data and specifications. Supervision of laboratory test sections in performance of life, design, and environmental tests. Located at Harrison, N.J. . . . 30 minutes from N.Y.C.

COMMUNICATION DEVELOPMENT ENGINEER

Salary to $12,500

An ideal opportunity for a development engineer. Work in Advanced Development Information Handling and Control Group. Develop techniques for application to PCM for voice and data transmission. Work will involve development of both digital and analog transistor circuits for application to pulse cone modulation voice and data transmission systems. One to two years' experience in digital and/or communication techniques is required. EE or Physics degree. Location in Camden, New Jersey, in Greater Philadelphia area.

ELECTRONICS TEST ENGINEER—MICROWAVE

Salary to $11,000

Interesting opening for a top quality, creative man to design and develop electronic test equipment for evaluation of magnetrons and traveling-wave tubes. Microwave and pulse circuit background required. Work will be in development of measurement techniques and adaptation to developmental and production tube testing. The right man will find exceptional opportunities for advancement. Located at Harrison, N.J., just 30 minutes from mid-town Manhattan.

TRANSMITTER DESIGN SUPERVISOR

Salary to $14,000

This position requires a BSEE and eight to ten years' experience in High Power UHF or VHF television transmitter design. You should be capable of supervising a small group of design engineers and providing technical and administrative direction for the group. If you possess this experience and are looking for an opportunity to advance, you are invited to visit RCA, in suburban Moorestown, New Jersey.

Modern benefit program . . . relocation expenses paid . . .

SCIENCE at RCA

STARTING SALARIES: NON-MANAGERIAL TO $15,000 . . . MANAGERIAL OPEN

FIELDS OF ENGINEERING ACTIVITY		MANAGERS	TYPE OF DEGREE AND YEARS OF EXPERIENCE PREFERRED											
			Electrical Engineers			Mechanical Engineers			Physical Science			Ceramics Glass Technology Metallurgy		
			0-2	2-3	4-15	0-2	2-3	4-15	1-2	2-3	4-15	1-2	2-3	4-15
• **SYSTEMS** (Integration of theory, equipments and environment to create and optimize major electronic concepts.)	AVIATION ELECTRONICS • CONTROLS		W	W	W C	W	W	W C	W	W	W C			
	DIGITAL DATA HANDLING DEVICES	M C		M C	M C		C	C		C	C			
	MISSILE WEAPONS SYSTEMS • RADAR	M W	W	M W X C	M W X C	W	M W C	M W C	W	M W X C	M W X C			
	INERTIAL NAVIGATION			W C	W C		W C	W C		W C	W C			
	COMMUNICATIONS		C	C N	C N	C	C				C N			
• **DESIGN • DEVELOPMENT** MISSILE WEAPONS SYSTEMS—Planning and Design—Radar—Fire Control—Servomechanisms—Computers		C M	W C M X	W C M X	W C M X	W C M	W C M	W C M X	W C M	W C M X	W C M X			
AVIATION ELECTRONICS—Radar—Computers—Servomechanisms—Shock and Vibration—Circuitry—Remote Control—Heat Transfer—Sub-Miniaturization—Automatic Flight—Automation—Transistorization—Infrared—Airborne TV		W C	W C X	W C X	W C X	W C	W C X	W C X	W C X	W C X	W C X			
RADAR—Circuitry—Antenna Design—Servo Systems—Gear Trains—Intricate Mechanisms—Fire Control—Information Handling—Displays		M C	W M C X	W M C X	W M C X	W M C X	W M C X	W M C X	W M C X	W M C X	W M C X			
COMPUTERS—Systems—Advanced Development—Circuitry—Assembly Design—Mechanisms—Programming—Digital Data Handling Devices		M	C W	M C X W	M C X W	C W	M C X W	M C X W	C W	M C W	M C W			
KINESCOPES (B & W and Color), OSCILLOSCOPES—Electron Optics—Instrumental Analysis—Solid States (Phosphors, High Temperature Phenomena, Photosensitive Materials and Glass to Metal Sealing)		&	L	L Y	L Y	L	L Y	L Y	L	L Y	L Y	L	L Y	L Y
RECEIVING TUBES—Tube Design—Test and Application Engineering—Chemical and Physical Development—Methods and Process Engineering—Advanced Development			H	H	H		H	H		H	H		H	H
SEMICONDUCTORS—Transistors—Semiconductor Devices—Materials			V	V	V	V	V	V	V	V	V	V	V	V
MICROWAVE TUBES—Tube Development and Manufacture (Traveling Wave—Backward Wave—Magnetron)		H	H	H	H		H	H		H	H		H	H
GAS, POWER AND PHOTO TUBES—Photosensitive Devices—Ceramic to Metal Sealing—UHF and VHF—Super Power			L	L	L	L	L	L	L	L	L	L	L	
COMMUNICATIONS—Specialized Systems—Microwave—Mobile—Aviation—Audio—Propagation Studies—Acoustics—Transducers			C N	C N	C N		C	C	C N	C N	C N			
BROADCAST AND TV—Monochrome and Color Studio Equipment—Cameras—Monitors—High Power Transmitters			C	C	C	C	C	C	C	C	C			
• **SYSTEMS APPLICATION** (Evaluation and Planning—Design and Development—Modification—Specification)														
MISSILE TEST INSTRUMENTATION (Data Acquisition and Processing)—Radar—Telemetry—Timing—Communications—Optics—Computers		F	F S	Z F S	Z F S	F S	F S	Z F S	F S	Z F S	Z F S			
RADAR—Airborne—Surface—Shipboard—Sonar—Fire Control		F	F S	Z F S	Z F S	F S	F S	Z F S	F S	Z F S	Z F S			
COMMUNICATIONS—Radio—HF—VHF—UHF—Microwave—Telephone—Teletype—Telegraph Terminal Equipment—Wave Propagation		F	F S	F S	F S	F S	F S	F S	F S	F S	F S			
• **MACHINE DESIGN** Mechanical and Electrical—Automatic or Semi-Automatic Machines			L H	L H	H	L	L H	H		L	L			

Locations: **C**—Camden, N. J. **F**—Cocoa Beach, Fla. **H**—Harrison, N. J. **L**—Lancaster, Pa. **M**—Moorestown, N. J. **N**—New York, N. Y. **S**—RCA Service Co. (Cherry Hill, N. J.; Alexandria, Va.; Tucson, Ariz.; Dayton, Ohio; San Francisco, Calif.) **V**—Somerville, N. J. **W**—Waltham, Mass. **X**—West Los Angeles, Calif. **Y**—Marion, Ind. **Z**—White Sands, N.M.

Please send resume of education and experience, with location preferred, to:

Mr. John R. Weld, Employment Manager
Dept. A-16C, Radio Corporation of America
30 Rockefeller Plaza, New York 20, N.Y.

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Raytheon Systems Laboratories in New England

Bedford Laboratory, Bedford, Mass.

Raytheon is the only electronic company with prime contracts in both air-to-air and ground-to-air missiles—Sparrow III for the Navy, Hawk I for the Army. Over-all responsibility for the development and production of these systems rests with Raytheon's Missile Systems Division, which besides the engineering Laboratory at Bedford, Massachusetts, has production plants in Lowell and Andover (Shawsheen), Massachusetts and in Bristol, Tennessee, supplemented by flight test facilities at Oxnard, California and White Sands, New Mexico. The success of this Division's work has resulted in developmental contracts for future generations of guided missiles. In a period of ten years it has grown from a small laboratory to an organization of over thirty-four hundred employees, including more than five hundred engineers.

If you are interested in investigating the many opportunities for scientists and engineers at any of these facilities write: G. P. O'Neil, Raytheon Manufacturing Company, Missile Systems Division, Bedford, Massachusetts.

Maynard Laboratory, Maynard, Mass.

The recently formed Maynard Laboratory is engaged in the design and development of unique & advanced coherent Radar Systems used in the fields of navigation, fire control, guidance & countermeasures. Specializing primarily in the navigation and guidance of supersonic aircraft but embracing specific applications of countermeasures equipment and shipborne radar, the laboratory has a nucleus of some of the country's finest engineers & scientists working on the application of Electronics to the needs of our rapidly expanding Aircraft Industry. As is common to all healthy youngsters, this new engineering organization is growing fast and presents unmatched opportunities for engineers who want challenging, interesting work with the prospect of real progress.

Staffing activities are currently under way at all levels. If you are interested in these or similar projects, contact us to discuss details.

Write John J. Oliver, Raytheon Manufacturing Company, Maynard Laboratory, P. O. Box 87, Maynard, Mass.

Representatives of each Laboratory will be in New York during the I.R.E. Show. They'll be glad to talk about Raytheon and YOU.

New England?

devoted exclusively to Electronics and

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Raytheon's new Wayland Lab has over 5 acres of enclosed working area with a "completeness" of facilities that is difficult to match. This Lab has four independent creative departments:

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1. Ground based surface and air search.
2. Airborne navigational, search, tracking, and fire control.
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SONAR—submarine, ship, and airborne sonar equipment.

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If you're interested in learning more about the work being done at Wayland, please write Donald B. Stillman, Staff Assistant to Manager, Wayland Laboratory, Wayland, Mass.

Raytheon is a unique organization. It has found through experience that the greatest progress is made by decentralization. This is the reason it is made up of several "Operations" each with its "Divisions" which have prime responsibility for the success of their specific tasks. This encourages initiative and promotes individual growth. An engineer works with the minimum of supervision but can confer with men of national reputation. Raytheon is a growing company with young ideas and young executives many of whom have engineering background and experience.

Raytheon's Systems Laboratories are located in suburban areas where easy commuting, good living in uncrowded urban or country communities, is the rule. There is easy access to the cultural, medical, educational and research advantages of Boston as well as to the recreational opportunities of New England's mountains, lakes and seashore.

Starting salaries are excellent. Recognition both professionally and financially is dependent on ability and performance. Adequate supporting technical personnel is provided and the fringe benefits are liberal. You can take advanced courses at Harvard, M.I.T., Boston University, Northeastern — and Raytheon pays the major costs! You may attend meetings and seminars at company expense.

Our contract commitments are growing as a result of increased demand for our services — we need additional scientists and engineers interested and experienced in the work we are doing to GROW with us. We welcome the opportunity of arranging an interview to tell you more. Contact us soon!

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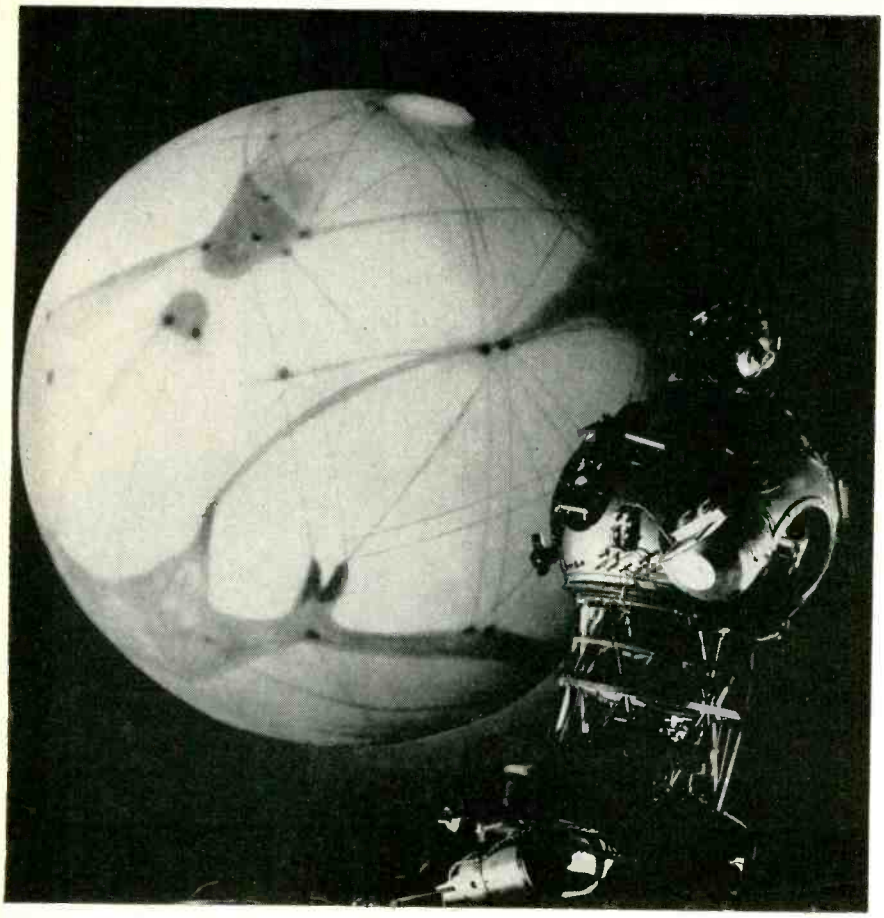

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Right or wrong, *we* can tell you this: Within months, the first man-made earth satellite will be Martin-launched, and we're already "running some numbers" on the first moon vehicle.

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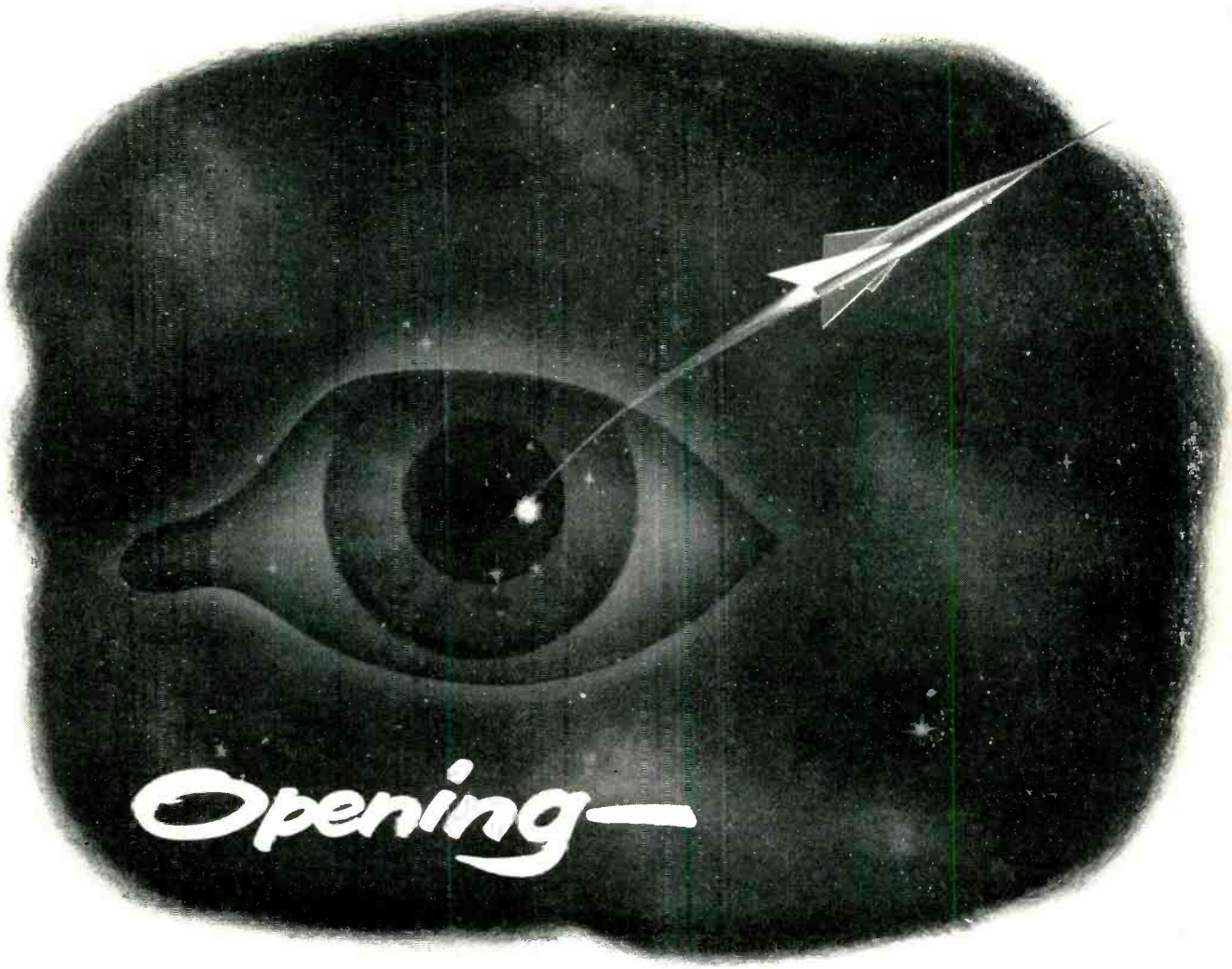

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Our creative engineers are men of talent and training, of course. But beyond that, they are men gifted with an uncanny capacity to look ahead, think ahead and above all, see ahead.

Their materials are the progress of the past. Their genius is the promise of the future.

To fulfill that promise, our engineers have at their disposal the most modern facilities, including one of the largest computer laboratories in the world. They have unlimited opportunities in the field of their choice — whether it be airships, missiles, electronic guidance equipment, structures — or countless other challenging activities.

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If you have faith in your ideas and confidence in your ability to make them work, a rewarding career can be yours at Goodyear Aircraft. Our continued growth and diversification have required expansion of our engineering staffs in all specialties at both Akron, Ohio, and Litchfield Park, Arizona.

You'll find salaries and benefits agreeable. If you wish to continue your academic studies, company-paid tuition courses leading to advanced degrees are available at nearby colleges.

For further information on your career opportunities at Goodyear Aircraft, write: Mr. C. G. Jones, Personnel Dept., Goodyear Aircraft Corporation, Akron 15, Ohio.

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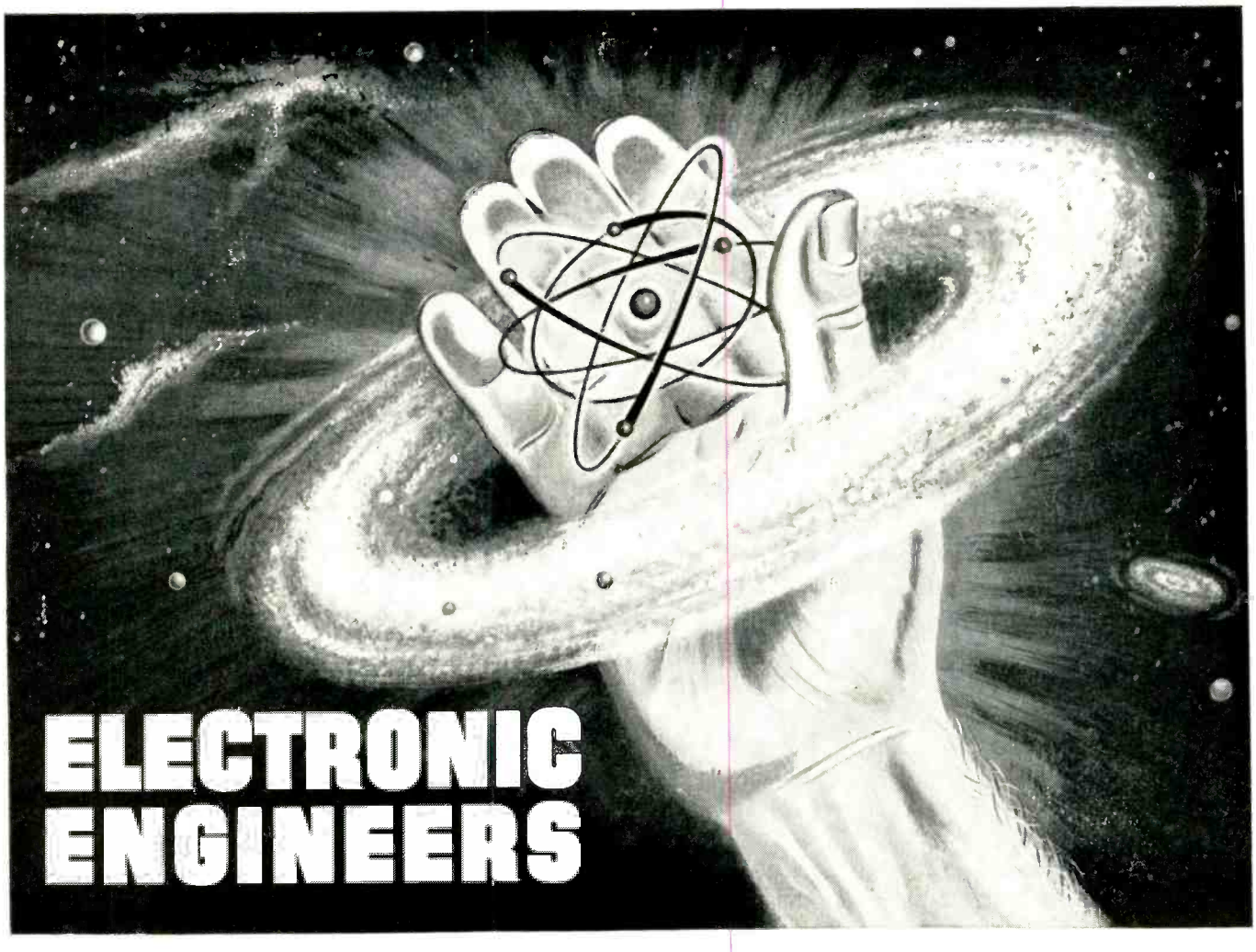

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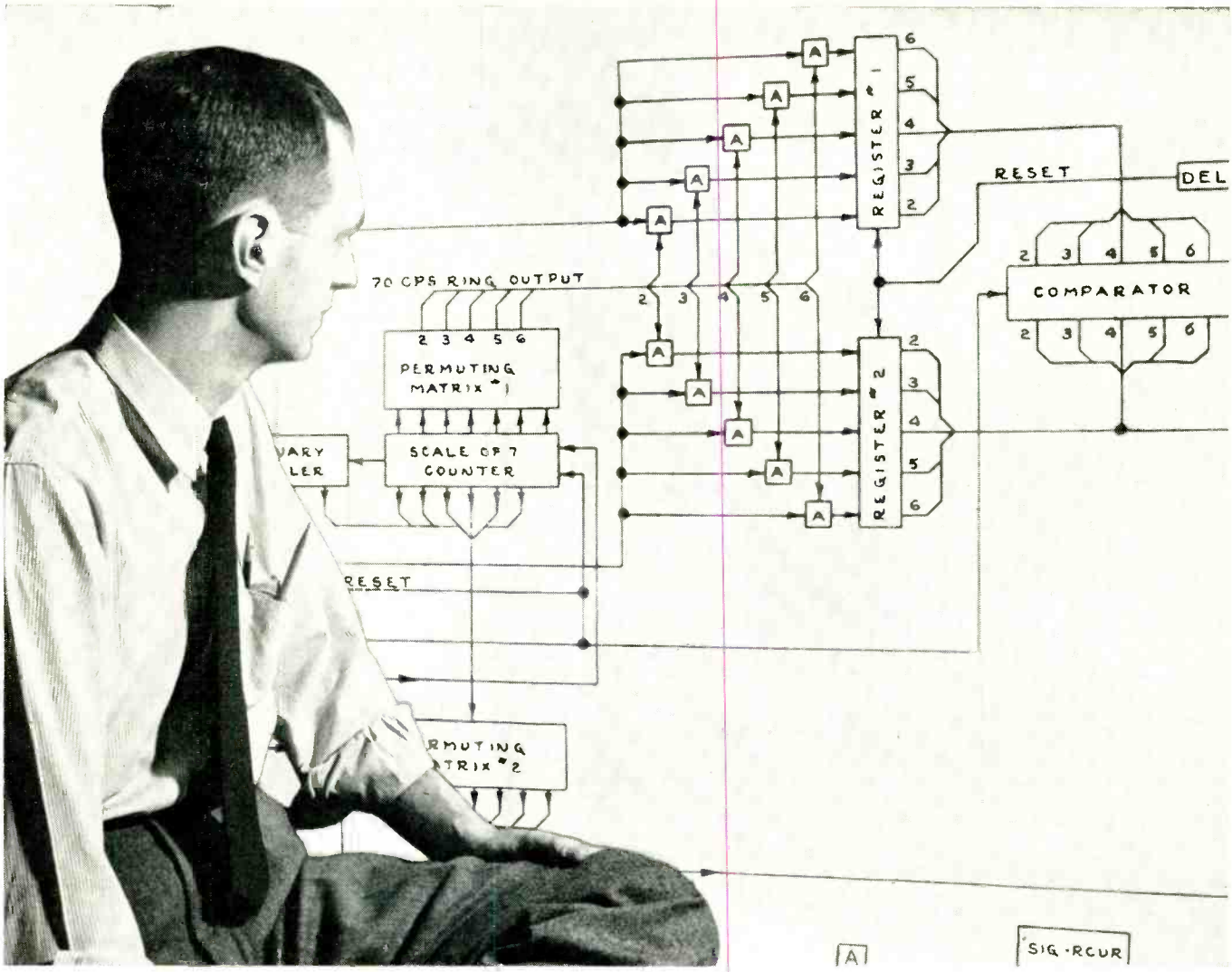

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(Reliability)

ME or EE degree with design experience and/or application experience. Job will be to recommend types of parts to be used and how these parts shall be used.

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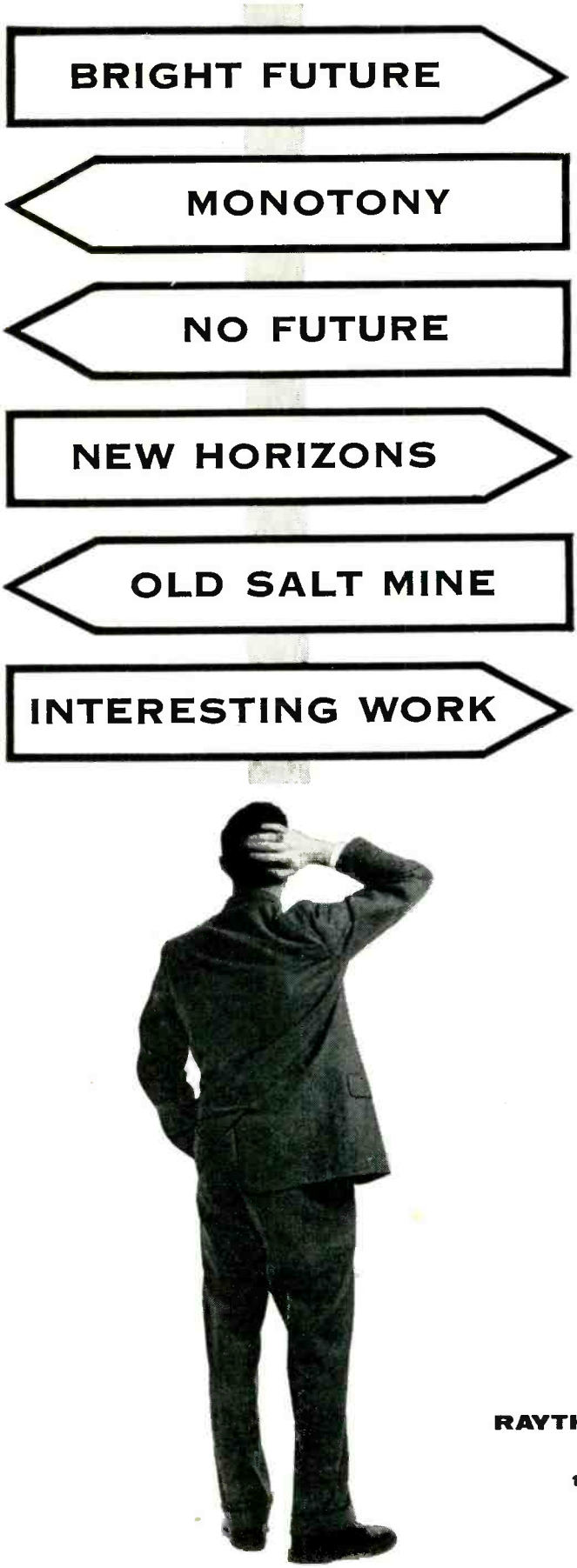

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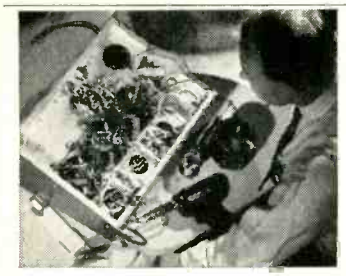
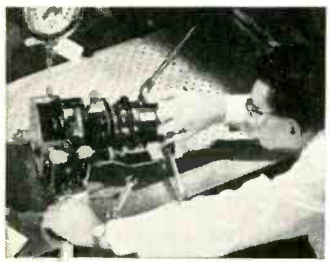
Government Service Department
100 River Street, Waltham 54, Massachusetts



TEST EQUIPMENT

The Test Equipment Engineer is engaged primarily in the design of specialized missile check-out equipment. As missiles push the state of the art, test equipment must exceed the missiles in precision and reliability. Automatic programing, go-no-go evaluation, and automotic data processing add up to automotion in missile testing.

This engineer is evaluating his design of a precision power supply—one of the building blocks that will be system engineered into a family of versatile matched missile and sub-system test equipment. Engineers work as individuals.



HYDRAULIC DESIGN

Excellent opportunities are available for the engineer to observe the performance of his design. Here, under the watchful eyes of its designer, a hydroulic power unit is undergoing adjustment and setting prior to severe testing at simulated high altitude conditions.

Many components, which a few months ago seemed almost impossible to design, are now being tested under the severe conditions required to qualify them for flight operotion—and passing with flying colors.

STEERING INTELLIGENCE

Two Steering Intelligence Engineers discuss space allotment in a new guidance component. This close association of engineers with the "flying" equipment is typical of the Steering Intelligence Section. Engineers in this section are primarily and *directly* concerned with refining the guidance equipment to steer the missile with greater accuracy, at greater ranges and with simpler and more reliable electronic equipment and, consistently, with minimizing the cost. Work is actively in progress in every principal field from microwave equipment to inertial end instruments.

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Offers more interesting and challenging job opportunities!

If you are interested in guided missiles, you will be especially interested in Bendix. As prime contractor for the important and successful Talos Missile, the job opportunities here cover the widest possible scope, and the opportunities for advancement are practically unlimited.

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If you can accept a challenge, want an opportunity to grow with a leader in its field, and can accept the responsibility that goes with opportunity, send for the thirty-six-page book "Your Future in Guided Missiles". It gives the complete, detailed story of the function of the various engineering groups and the many job opportunities available for you.

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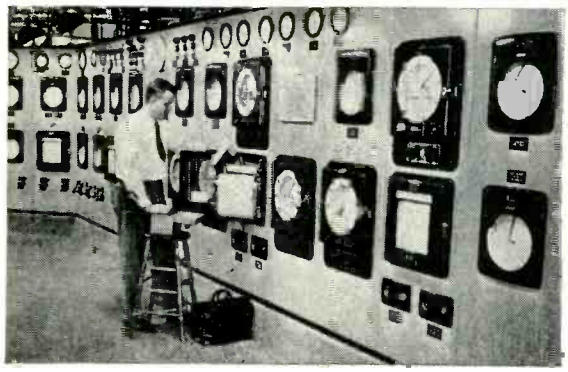

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MICROWAVE PHYSICS LABORATORY

- Magnetic Ferrites
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For positions in either of these two laboratories at Mountain View, Calif. please send resume to J. C. Richards, Box 205 Mountain View, Calif.

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For research, development and production on Traveling Wave Tubes, Backward Wave Oscillators and Klystrons

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Emerson Electric is a medium size company (5000 employees, 850 engineers) and a national leader since 1940 in design, development and manufacture of electronics and avionics products. Our Commercial Division, established 1890, produces a complete line of fans, motors, air conditioners, heaters, welders and power tools. This perfect balance of electronic, aircraft and consumer production assures stability and security in your career at Emerson.

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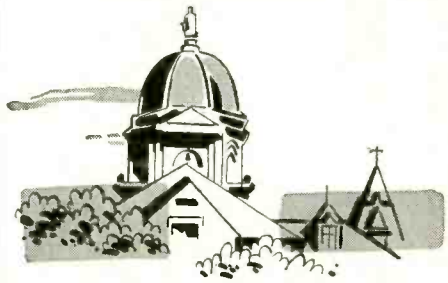

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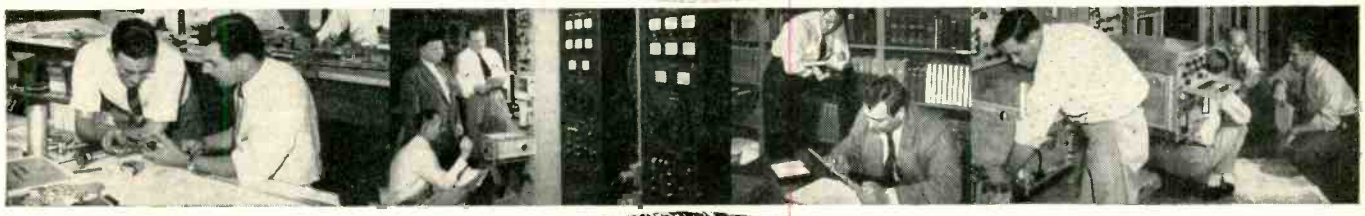
The expanding scope of advanced communications projects has created several unique positions in fields related to VHF, UHF, microwave transmission and reception, forward scatter and single sideband applications at Hoffman. Electronics engineers with appropriate backgrounds will find these new assignments professionally stimulating and financially rewarding. Please write Vice President of Engineering.



I.R.E. CONVENTION

March 18th-21st

Senior Members of the Hoffman Technical Staff will be available for interview at the Convention Hotel – Please telephone EL 5-3456 for appointment.

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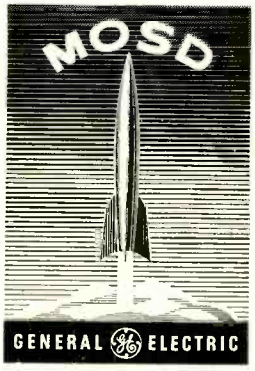

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ELECTRONIC SYSTEMS SPECIALISTS

A message of interest to all electronics men

Why Republic Aviation is forming its own Electronics Research Group

Electronic mechanisms take so vital a role in high performance jetcraft and missiles that it is no longer permissible to limit their performance with "ground engineered" components. Republic has recognized this critical need for electronic units developed and designed by air-minded men. Because of this, electronic *flight* research is being made an integral part of integrated research in aerophysics at Republic—a "first," we believe, for Republic in the aircraft industry.*

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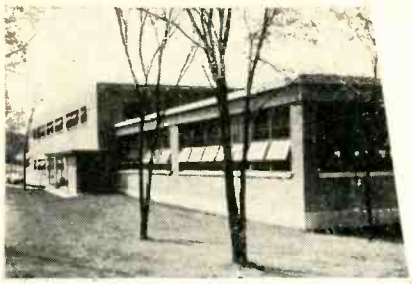
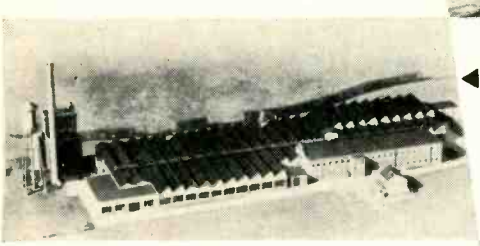
*Other firsts were Republic's Thundercraft, latest, most lethal and versatile of which is the incredible F-105 Thunderchief, supersonic USAF fighter-bomber, capable of delivering nuclear loads.



Plant of Westchester manufacturing subsidiary, Pleasantville Instrument Corporation; additions are under construction.

Electronics Engineers

Latest GPL engineering building, for which ground was broken recently.



Plant of Bloomfield, N. J., manufacturing subsidiary, Simplex Equipment Corporation; added in 1957.

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GPL keeps GROWING

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In connection with
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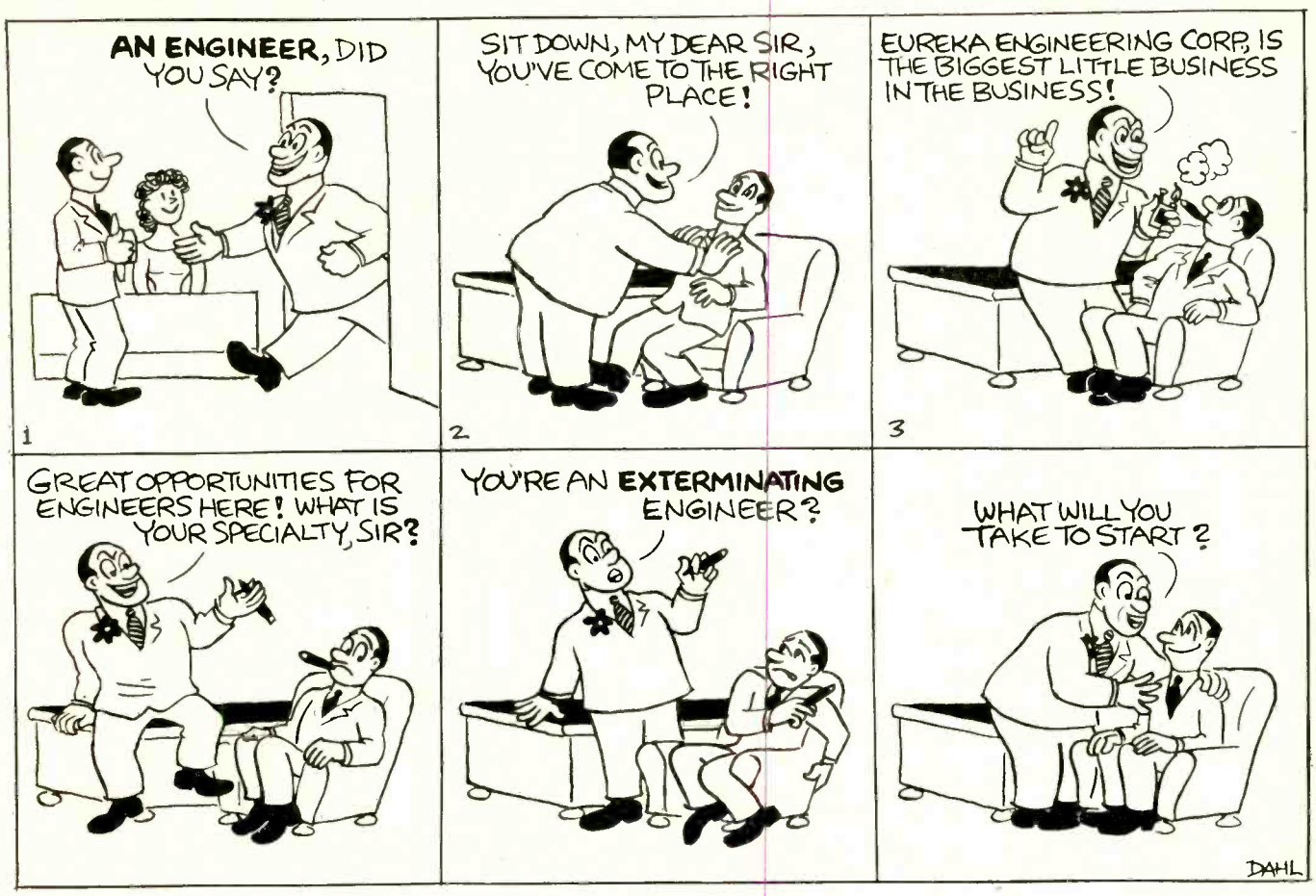

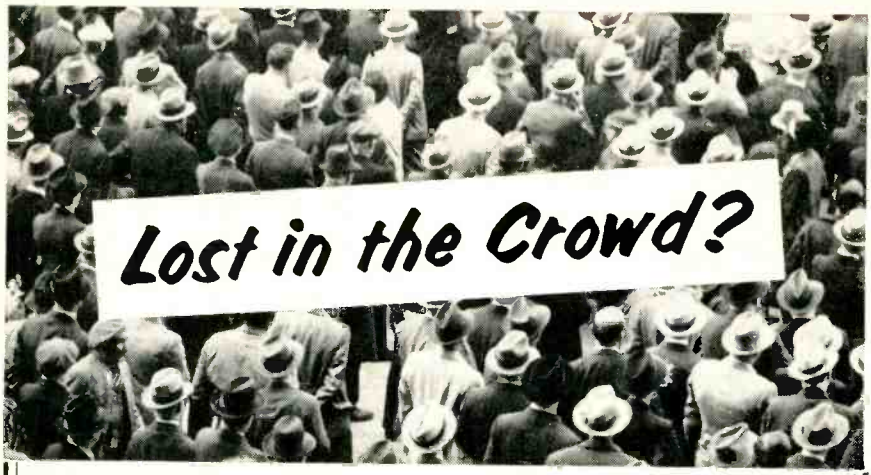

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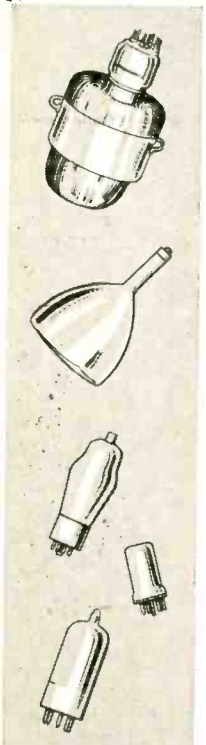

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Should have 10 years experience and ability to supervise the work of a group of advanced research engineers searching for the solutions to problems in multipath transmission as a function of frequency; vector scatter propagation, broad band antenna design, etc., which are necessary in the utilization of new communications systems.

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Opening for an engineer with vision and creative ability to derive and direct applications of new techniques developed in Buffalo Engineering Laboratory to existing and newly developed systems. These techniques now permit solution of many long-standing problems which exist in fields ranging from radio to radar or sonar from radio teletype to DME. Should have at least 10 years experience in communications field and an interest in system synthesis and analysis. Advanced degree in Electrical Engineering, Physics, Mathematics or equivalent in course work on a graduate level is desirable.

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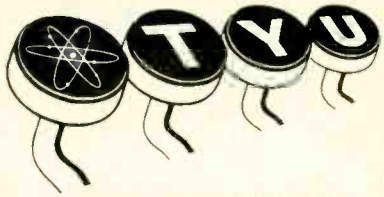

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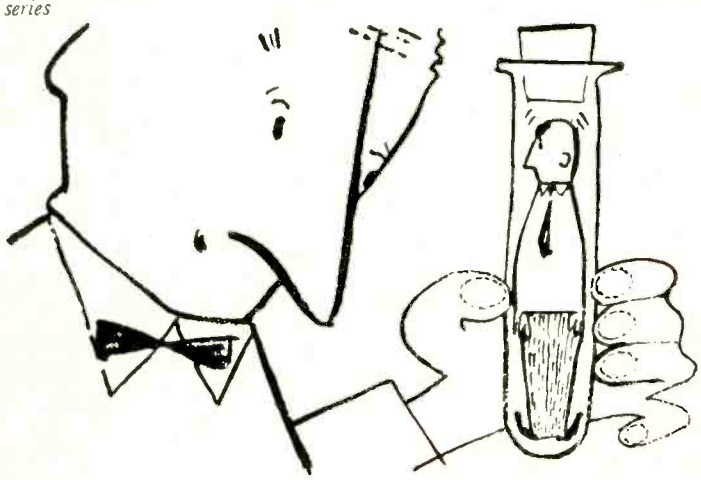

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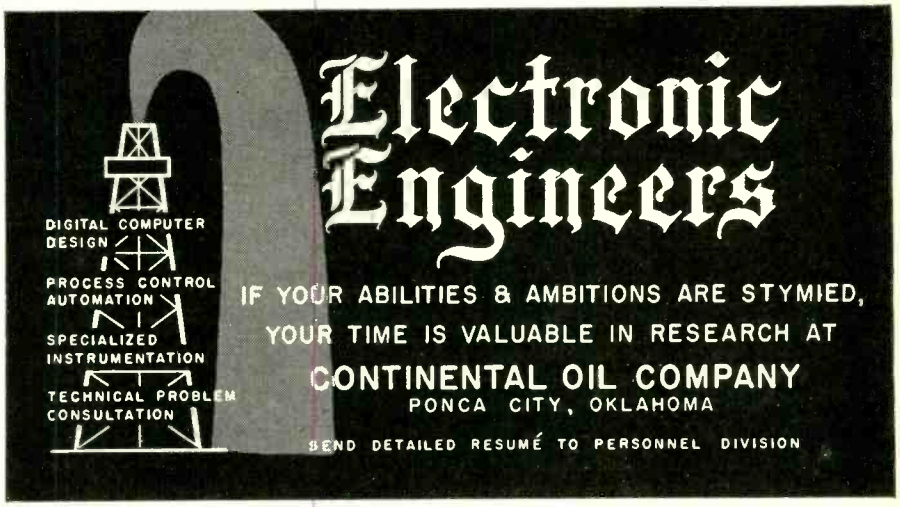

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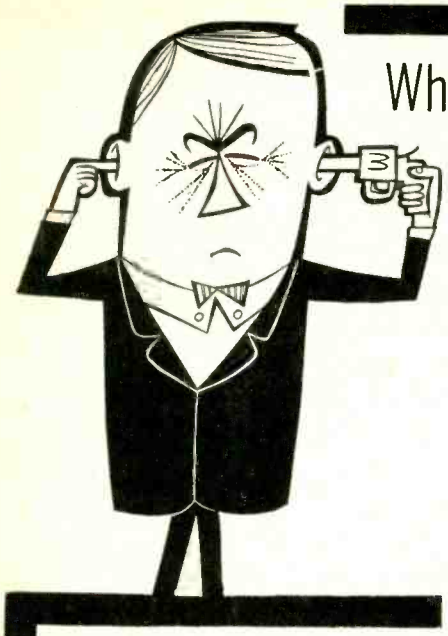

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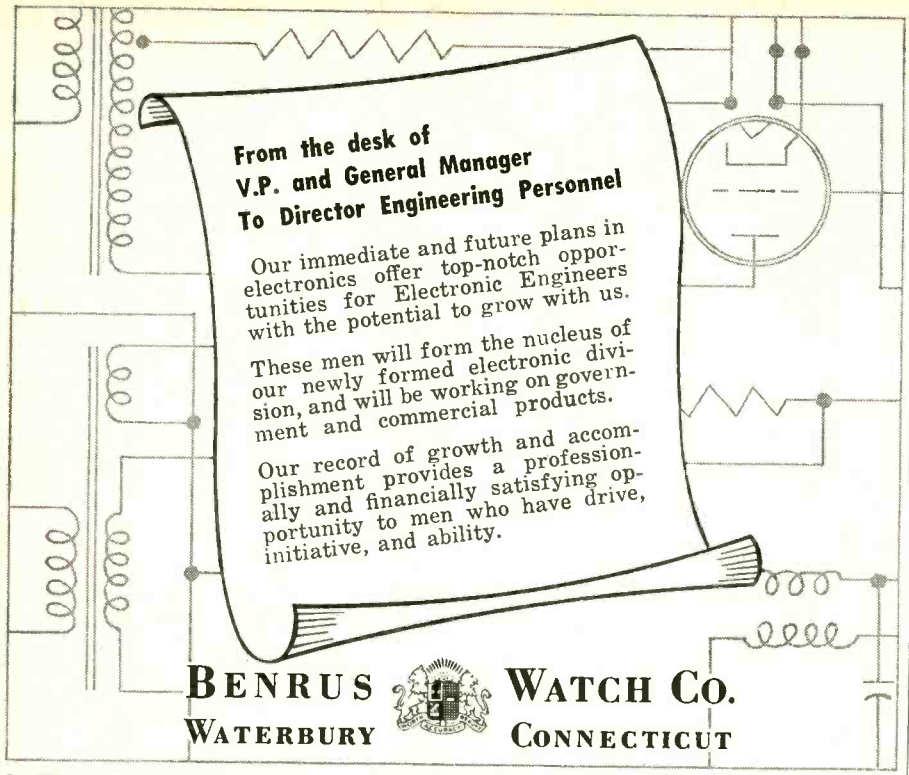

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1C8 .99	3BY6 .89	6AQ5W 1.98	6SH7 .69	12SH7 .89	58 .79	421A 4.85	872A .95	5783 4.25	2511A5 45.00
1C21 1.99	3BZ6 .79	6AQ6 .56	6SJ7 .69	12SJ7 .75	59 1.49	434A 1.98	874 .90	5784 4.75	2500SA5 45.00
1D21/SN4 4.70	3B5 2.39	6AQ7 1.12	6SK7 .72	12SK7 .75	RK59 1.89	446A .69	875A Q	5787 14.75	2501A3 45.00
1E5 .56	3B7/1291 2.06	6AR5 .99	6SL7 .89	12SL7 .79	APR60A Q	446B 1.49	878 .45	5812 .95	2523N1 45.00
1E7 .38	3B23 3.29	6AR6 1.95	6SN7 .72	12SN7 .69	RK60 1.17	450TH 43.50	884 1.15	5814 1.20	1N21 6/$1
1G4 .40	3B24W 4.56	6AS5 .99	6SQ7 .74	12SQ7 .69	RK61 2.50	450TL 43.50	885 1.00	5820 50.00	1N21A .69
1G5 .40	3B25 5.99	6AS6 1.79	6SR7 .69	12SR7 .69	HY65 2.00	CL451 2.00	889A 75.00	5829 1.75	1N21B 1.10
1G6 .38	3B27/836 3.42	6AS7G 3.49	6SS7 .89	12V6 .79	KT66 Q	HK454 Q	891R 170.00	5838 2.50	1N21C 2.45
1H4 .38	3B28 3.84	6AS8 .99	6ST7 .99	12W6 .89	FG67 12.51	460 11.50	892 237.00	5840 4.00	1N23B .69
1H5 .68	3C22 64.99	6AT6 .49	6SU7 2.01	12X3 1.49	HY69 2.20	464A 2.25	923 1.35	5841 4.00	1N23C 2.45
1H6 .38	3C23 3.99	6AT8 .99	6SV7 1.29	12X4 .55	70A7 1.39	471A 3.95	925 1.89	5844 .50	1N25 2.15
1J5 .64	3C24 1.72	6AU4 1.29	6SZ7 1.89	12Z3 .99	70L7 1.39	473 164.95	927 1.00	5842 18.00	1N26 3.45
1L4 .82	3C33 6.42	6AU5 1.19	6T4 1.19	14A4 1.08	71 .70	501AX 1.29	930 1.50	5851 3.80	1N31 1.75
1L6 1.09	3C34 5.96	6AU6 .59	6T7 1.19	14A5 1.49	RK73 .92	502AX 1.50	931A 3.95	5852 2.25	1N33 8.95
1LA4 1.04	3C37 19.52	6AU8 .99	6T8 .98	14A7 .85	75 .81	503AX 1.49	932 Q	5870 1.95	1N34A .45
1LA6 1.19	3C39 79.90	6AV6 .59	6U4 .59	14AF7 1.00	HY75 5.00	503AX 1.00	954 Q	5875 1.65	1N38A .50
1LB4 1.19	3C45 6.99	6AW8 1.12	6U5 .85	14B6 .95	75TL 15.50	505AX 1.49	954 10/$1	5879 1.20	1N39 2.50
1LC5 1.09	3CB6 .79	6AX4 .79	6U7 .89	14B8 1.19	76 .49	506AX .95	955 3/$1	5881 2.85	1N43 .55
1LC6 1.08	3CF6 .79	6AZ8 1.19	6U8 .98	14C5 1.08	77 .39	507AX 1.49	956 3/$1	5899 3.75	1N44 1.00
1LD5 .98	3CS6 .78	6B4G 1.39	6V3 1.39	14CF .95	78 .39	509AX 1.49	957 3/$1		1N45 1.20
1LE3 1.08	3D6/1299 .48	6B5 .99	6V4 .99	14E6 1.20	79 .39	S10AX 2.69	958A 2/$1	WE BUY! & SELL! & TRADE AS WELL! TOP DOLLAR	1N46 .40
1LG5 1.09	3D21A 2.94	6B6 .89	6V6 1.39	14EF 1.19	80 .59	S11X 3.20	959 1.25		1N52 .85
1LH4 1.19	3D23 4.84	6B7 1.29	6V6GT .90	14F7 1.00	EM81 2.39	512AX 1.95	991 5/$1		1N54 .55
1LN5 .78	3DT6 .68	6B8 1.35	6W4 .79	14F8 1.29	EZ80 .81	518AX 1.95	1005 3/$1		1N63 1.40
1N5 .89	3E29 8.44	6BA5 .99	6W6 .89	14HF .99	81 1.59	522X 1.95	1006 3.70		1N65 .85
1P5 .68	3J31 35.00	6BA6 .59	6W7 .99	14J7 1.29	ECC81 1.25	525AX 1.90	1007 .50		1N67 .45
1P21 29.99	3K23 159.99	6BA7 .99	6X4 .39	14NF 1.29	EZ81 1.05	526AX 1.90	1027 1.00		1N69 .40
1P24 1.39	3Q4 .68	6BA8 .99		14QF 1.00	FG81 3.20	527AX 1.95	1087 2.95		1N70 1.50
1P28 9.09	3Q5 .86	6BC4 1.49		14RF 1.29	QK81 Q	528AX 1.49	CK1089 2.40		1N81 1.18
1P30 1.29	3S4 .68	6BC5 .69	6X5 .49	14S7 1.19	82 .97	529AX 1.89	CK1090 2.69	5932 3.75	1N82 .60
1P32 1.09	3V4 .99	6BC7 1.10	6X8 1.19	14W7 1.19	ECC82 1.05	S31 3.79	R1100 12.95	5965 1.15	1N90 .75
1P37 8.59	3X2500A3 99.92	6BC8 1.19	6Y5 1.69	14X7 1.05	83 .95	531DX 1.95	R1130 10.95	5977 2.95	1N91 1.20
1Q5 .86	4A1 1.92	6BD4A 6.95	6Y6 .89	14Y4 .97	83V .89	532DX 1.95	R1148 4/$1	6005 1.75	1N92 2.70
1Q22 44.99	4AP10 7.42	6BD5 1.69	6Z4 .99	15 .35	ECC83 1.19	533AX 1.95	1201 .95	6012 5.25	1N93 3.45
1Q23 129.99	4A11 .99	6BD6 .69	6Z5 1.29	15E 1.19	84/6Z4 1.69	534AX 1.95	1203 .95	6035 9.00	1N119 .85
1R4/1294 .88	4B25 15.22	6BE6 .59	6Z7 1.39	15R .34	EL84 1.75	535AX 1.50	1231Z 5.50	6038 8.50	1N126 .75
1R5 .78	4B26 7.49	6BF5 1.08	6Z9S 1.39	C16J Q	85 1.89	536AX 1.49	1232 .95	6095 1.25	1N127 1.35
1S4 .78	4B27 4.72	6BF6 .69	7AK7 5.95	FG17 3.49	ECC85 1.39	537AX 1.95	1237 .95	6116 115.00	1N128 1.15
1S5 .68	4B28 2.99	6BF7 1.99	7A4 .79	17AX4 1.08	EF86 1.29	538DX 1.45	1294 .95	6135 2.29	1N198 2.25
1T4 .78	4B31 20.99	6BG6 1.49	7A5 .89	18 .35	89 .89	539DX 1.95	1608 2.95	6146 4.25	1N497 1.10
1T5 1.09	4B32 10.59	6BG7 1.99	7A6 .72	19 .35	EB91 .81	541DX 1.95	1609 4.95	6214 .90	1N498 1.30
1T6 1.29	4B35/349A 7.09	6BH6 .79	7A7 .79	19AU4 1.10	EC90 1.26	542DX 1.95	1612 1.20	6216 2.99	1N499 1.50
1U4 .68	4B38 6.89	6BH8 1.05	7A8 .72	19BG6G 2.15	EF94 .96	542DXS 2.25	1613 .89	6292 25.00	1N500 2.00
1U5 .89	4BCB 1.30	6BJ6 .72	7AD7 .99	19C8 1.15	EK90 .99	543DX 1.95	1614 2.00	6626 3.09	1N501 3.40
1V .68	4BN6 1.00	6BJ7 .89	7AF7 .90	19J6 1.00	EZ90 .79	544DX 1.45	1616 .65	6627 3.99	1N502 5.25
1V2 .62	4BQ7A 1.19	6BK5 1.11	7AG7 .99	19T8 1.16	ECC91 1.15	546DX 1.95	1619 4/$1	6792 6.39	2N156 7.99
1X2 .68	4BS8 1.19	6BK7 .99	7AH7 .92	19V8 1.12	VR92 5/$1	547DX 1.98	1620 2.00	7193 20/$1	2N158 7.99
1Y2 9.99	4BU8 .93	6BL6 57.29	7AU7 .89	19X8 1.20	FG95 18.00	548DX 1.95	1621 1.50	8000 9.00	2N180 5.74
1Z2 1.40	4BZ7 1.25	6BL7 1.95	7B4 .72	20 .49	FG97 Q	549DX 1.85		8002 17.50	2N181 7.19
2A3 1.26	4C21 8.99	6BN4 .69	7B5 .75	T20 Q	FG98 14.75	551AX 2.25	1622 1.65	8005 4.45	1N503 7.19
2A4 1.16	4C35 18.99	6BN6 1.08	7B6 .79	RK20 Q	100TH 6.39	555AX 2.25	1623 1.50	8008 1.65	1N504 14.00
2A5 1.19	4CB6 .74	6BN7 1.99	7B7 .79	A21 12.95	100TL 11.29	556AX 2.25	1624 1.25	8011 1.95	1N505 21.50
2A6 .74	4D21/4-125A $30.	6BQ5 1.99	7B8 .85	PJ21 5.90	102D 3.00	559 .39	1625 3/$1	8012 1.25	1N506 28.50
2A7 .74	4DT6 .68	6BQ6 1.19	7C4 .69	RV21 8.90	102F 2.90	563CX 1.15	1626 5/$1	8013A 3.85	1N507 43.00
2AC15 6.94	4E27 9.99	6BQ7 1.19	7C5 .79	22 .45	102G 2.00	570AX 2.25	1629 8/$1	8015 .90	1N508 61.00
2AS15 5.25	4E27/5-125 10.42	6BR8 .99	7C6 .82	246/3C24 1.95	FG104 28.90	571AX 1.49	1630 .65	8020 1.95	1N511 7.19
2B4 4.02	4J22 98.00	6BS8 1.15	7C7 .82	24A .39	FG105 10.90	573AX 1.95	1631 1.50	8025A 2.50	1N512 14.00
2AF4A 1.29	4J31 60.00	6BU8 .89	7C8 1.19	20 .49	FG95 18.00	574AX 1.95	1632 4/$1	9001 .80	1N513 21.50
2BN4 .80	4J50 98.60	6BV8 .99	7C29 69.00		F108 12.00	575A 13.35	1633 3/$1	9002 .65	1N514 28.50
2C22 .18	4J51 215.00	6BX7 1.11	7E5 .99	CE36C Q	111H		1634 2/$1	9003 1.35	1N515 43.00
2C26 .18	4J52 49.80	6BY5 1.19	7E6 .99	CE36D Q	114B 2.65	601B .39	1635 1.60	9004 .85	1N516 61.00
2C33 .98	4J53 100.00	6BY6 .75	7E7 1.15	25A6 1.19	HY115 5/$1	605CX 1.95	1636 .75	9005 1.85	1N519 7.00
2C34 .29	4-65A 16.99	6BZ6 .75	7F7 .95	25A7 2.19	117L7 2.39	606CX 1.95	1641 1.20	9006 5/$1	1N520 14.00
2C39 5.79	4-125A 31.99	6BZ7 1.25	7F8 1.20	25AV5 1.45	117N7 1.98	608CX 1.95	1642 3/$1	9376 Q	1N521 21.50
2C39A 10.92	4X150A 19.99	6BZ8 1.49	7G7 1.95	25AX4 1.07	117Z3 1.69	KU610 3.50	1643 .65	9903 Q	1N522 28.50
2C40 6.92	4-250A 35.99	6C4 .49	7G8 1.80	25BK5 1.08	117Z4 1.10	HY615 .90	1649 2.00	CR-TUBES	1N523 43.00
2C42 9.09	4X250B 41.99	EL6C 16.29	7H4 1.19	25BQ6 1.39	117Z6 1.10	WL616 42.50	1680 2.00	2AP1 3.95	1N524 61.00
2C43 7.84	4X500A 46.00	EL6CF 16.29	7H7 .79	25C5 .81	CK118 Q	619CX 1.95	1850A 36.00	2AP1A 5.00	WRITE!
2C44 .22	4X500F 44.00	6C5 .69	7J7 1.20	25CA5 .99	124A Q	KU618 Q	1851 1.95	3AP1A 6.50	
2C46 5.29	5AM8 1.05	6C6 1.08	7K7 1.10	25CD6 1.85	VXR130 1.39	624CX 1.95	2050 1.25	3AP5 9.00	WE STOCK CBS RCA GE AMPEREX EIMAC PENTA DUMONT MICRO TAYLOR
2C51 2.00	5AN8 1.09	6C8 1.08	7L7 .99	25CU6 1.45	CV147 4.95	KU627 6.95	2050W 3.45	3BP1 1.90	
2C52 2.64	5AQ5 .71	6C21 13.49	7N7 .89	25D8 1.89	CV148 4.95	WL629 Q	2051 .85	3BP1A 5.50	
2C53 9.89	5AS4 .64	6CA7 3.49	7Q7 .99	25DN6 1.99	152TL 12.75	631P1 4.95	R4330 18.35	3BP5 12.00	
2C57 1.98	5AS8 1.09	6CB5 2.29	7R7 1.25	25DQ6 1.69	FG166 15.25	WL670A Q	5514 5.95	5ABP1 21.00	
2D21 .68	5AT8 1.01	6CB6 .80	7S7 1.20	25L6 .72	FG167 15.00	KU676 29.50	5516 6.45	5ADP1 24.00	
2D29 3.00	5AV8 1.09	6CD6 1.49	7V7 1.20	25T Q	FG190 4.98	KU677 Q	5517 1.25	5ADP7 24.00	
2E5 .92	5AW4 1.10	6CF6 .85	7W7 1.20	25W4 .77	HF200 10.25	WL678 39.00	5528 5.00	5AP1 2.95	
2E22 1.92	5B/4B22 5.32	6CL6 1.10	7X6 .92	25W6 .90	201 .39	WL686 38.00	5545 34.55	5BP1 1.49	
2E24 2.49	5BE8 1.06	6CS6 .70	7X7 1.15	25Y5 1.08	203A 3.95	701A 3.95	5551 37.50	5BP1A 9.00	
2E25 6.99	5BK7A 1.06	6CD6 1.80	7Y4 .89	25Z5 .72	204A 23.00	702A 3.75	5552 35.00	5BP4 3.25	SYLVANIA TUNGSOL ELECTRONS MUTHE BOMAC
2E26 2.99	5BQ7A 1.21	6CE5 1.15	7Z4 .72	25Z6 .75	205B 4.95	703A 1.00	5553 90.00	5BP7A 25.00	
2E27 .69	5BR8 .96	6CG7 .80	8AU8 1.19	25Z6W 2.25	211 .49	704A .50	5554 145.00	5CP1 1.95	
2E29 Q	5C22 26.62	6CG8 1.12	8CG7 .75	26 .39	RX215 5.75	705 .50	5555 140.00	5CP1A 6.50	
2E30 1.92	5CG8S 1.01	6CM6 .79	8CN7 .85	26A7 3.69	215 10.00	707A 2.00	5557 3.49	5CP5 12.00	
					217C 1.85	707B 3.50			

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4X150A	18.50	421A	4.75
4X150D	20.00	423A	7.50
4X150G	28.50	429A	8.00
5D23/RK65	7.00	450TH	40.00
6C21	15.00	471A	4.00
15E	1.20	508	190.00
24G	2.00	575A	12.00
HK24	2.00	HK #654	15.00
53A	5.00	750TL	30.00
HY65	1.40	801A	.35
100TH	5.00	803	2.50
UT127	1.50	813	8.50
UT-127A	2.50	814	2.00
F-128A	7.25	828	8.00
VT-158	9.50	829	3.50
211	.40	829B	8.00
220B	55.00	830B	.45
250TH	21.00	832A	5.75
251A	40.00	838	.70
272A	14.00	838W	4.00
300B	5.00	843	.35
305A	2.75	845	3.00
310A	3.85	852	4.00
313C	2.70	858	140.00
316A	.40	864	.25
327A	3.50	880	200.00
331A	7.50	889R	170.00
348A	4.75	892A	200.00
349A	5.00	1611	1.00
359A	1.50	1613	.90
371A	1.00	1619	.30
374A	3.25	1620	3.50
403B	2.65	1625	.30
404A	14.00	5680	130.00
407A	2.75		

RECEIVING TUBES

RUGGEDIZED

5Y3WGT	$2.75	6J6WA	$1.50
6AC7W	1.40	6SK7W	1.10
6AK5W	1.20	6SN7WGT	.90
6AL5W	.70	6X4W	1.20
6BF7W	2.40	7F8W	1.35
6C4W	3.75	12AT7WA	3.75
6J4WA	2.25	2625W	3.00
6J6W	.90		4.50

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1D8GT	6D6	6SH7	12AT7
1C6	6F6	6SJ7	12C8
1G4GT/G	6F8G	6SK7	12J5GT
1U4	6G6G	6SK7GT	12K8
2A3	6H6	6SK7GTY	12SA7
6AB7	6H6GT	6SK7Y	12SG7
6AC5GT/G	6J4	6SL7GT	12SH7
6AC7	6J5	6SN7GT	12SJ7
6AG5	6J6	6SR7	12SL7G1
6AG7	6K8GT	6U6	14C5
6AH6	6L6	6U6GT	14J7
6AK5	6L6GA	6U6Y	37
6AK6	6L6G	6X4	41
6AQ5	6L6Y	6X5GT	50B5
6AT6	6N7	6Y6G	76
6BA6	6R7	7A8	77
6BA7	6S7	7C7	78
6C4	6SA7	7F8	
6C5	6SF5	7S7	
		12A6	

THYRATRONS

C1K	$7.50
1C	1.00
2D21	.70
2D21W	.90
3C45	5.75
4B25	7.50
C5B	.75
EL5B	5.00
5C22	25.00
66M/5528	7.00
FG-32	4.00
FG105	11.00
5G154	9.00
VT-158	9.00
FG172	15.00
FG-271	22.00
KU-627	7.00
677	30.00
715C	10.00
885	.75
VC1258	P.O.R.
2050	1.00
2050W	3.75
2051	.65
5559/FG57	9.00
5560/FG95	16.00
5948/1754	250.00
6130/3C45	5.75

MAGNETRONS

2J22	$4.50
2J26	4.50
2J27	4.50
2J34	13.00
2J55	45.00
2J56	45.00
2J61	12.00
2J62	5.50
4J21	100.00
4J42	25.00
4J26	45.00
4J34	35.00
4J50	90.00
4J51	100.00
4J58	90.00
4J61	145.00
4J64	45.00
5J26	150.00
QK60	19.50
QK62	19.50
QK284	95.00
706AY-GY	14.00
706CY	15.00
714A	9.50
714AY	50.00
725A	2.75
5586	105.00
5657	105.00
5780	175.00

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5588	75.00	5719	21.50	5977	3.00
5610	1.00	5719A	2.75	5977A	3.00
5633	5.75	5722	3.25	5993	9.00
5635	6.00	5725	2.00	5995	4.60
5636	2.85	5726	.70	6005	1.75
5637	3.75	5726/6097/ 6AL5W	3.00	6021	3.85
5639	5.75	5744	1.20	6045	2.95
5640	5.85	5749	1.20	6080	4.75
5641	5.85	5750	2.50	6080WA	6.00
5642	1.00	5751	2.00	6087	4.00
5643	4.95	5751WA	3.50	6096	1.30
5644	6.25	5763	1.10	6098CT	1.90
5645	5.50	5783	4.25	6099	1.40
5646	4.50	5784	4.75	6100	2.00
5647	4.50	5784WA	7.00	6101	1.50
5651	1.40	5787	4.50	6110	5.50
5651WA	3.25	5794	5.00	6111	4.75
5654	1.30			6112	4.75
5654/6AK5W/ 6096	2.95	5814	.75	6147	3.00
5656	4.50	5814A	1.50	6152	6.00
5663	1.20	5814WA	3.50	6159	3.00
5670	1.00	5829	1.00	6161	45.00
5670WA	4.25	5840	3.50	6201/ 12AT7WA	3.50
5672	1.25	5840A	4.75	6211	1.10
5677	5.00	5844	.75	6263	11.50
5678	1.00	5845	5.00	6279/SC22	27.00
5686	1.75	5851	3.50	6280/416B	35.00
5687	2.40	5854	1.30	6386	5.00
5687WA	5.35	5876	7.00	7193	.20
5691	4.50	5896	3.00	8012	1.00
5692	4.85	5898	7.50	8025A	1.75
5693	4.65	5899	4.00	9001	.75
5696	1.00	5899A	5.75	9002	.50
5702	1.50	5902	6.00	9003	1.00
5702WA	4.50	5931/5U4WG	4.75	9004	.75
5703WA	4.50	5932	3.50	9005	2.25
5704	1.35	5933	1.50	9006	.20
5718	1.75	5967	10.00		

RECTIFIERS & REGULATORS

OB2	$ .60	5R4WGY	$2.75	371A	$1.00
OB3	.75	5Y3WGT	1.50	371B	2.50
OC3	.60	5X3	2.20	515A RCA	13.50
OD3	.55	6-4	1.00	575A	12.50
SB	2.00	6-7	1.00	705A	.65
SC	1.95	6-11	1.00	816	1.40
1V	.90	7H4B	1.00	836	1.20
2X2	.25	15R	.30	888A	1.20
2X2A	1.00	RX21	5.00	869B	32.50
3B24	1.35	100R/8020	1.75	872A	1.15
3B24W	4.75	249B	3.00	876	.75
3B28	4.00	249C	3.00	878	.50
5R4GY	1.25	250R	7.50	5931/5U4WG	4.00
		314A	80.00	8013	2.00

SCOPE TUBES

2AP1	$2.75	3EP1	$1.25	5JP1	$3.75
2BP1	4.00	5BP1A	8.50	5JP1A	25.00
3AP1	2.75	5BP4	2.25	5NP1	2.00
3CP1	1.75	5CP1	1.75	7CP1	4.99
3DP1/S2	4.75	5CP1A	7.00	9LP7	10.00
3FP7	2.50	5CP11	7.00	12DP7	12.00
3GP1	2.00	5CP11A	8.50	51UCP11	25.00
3JP1	7.50	5FP7A	2.50	902P1	2.25
3W2P1	50.00				

KLYSTRONS

SRX16	$100.00	6BL6	$24.00	726B	$14.00
2K25	12.00	6BM6	29.50	726C	13.00
2K28	24.00	6BM6A	32.50	5611	40.00
2K45	32.50	V45	P.O.R.	5721	135.00
2K48	50.00	V50	80.00	5981/5650	60.00
2K54	14.00	V82	P.O.R.	6116	140.00
2K55	14.00	723A/B	7.00	6236	180.00
3K30	95.00	726A	4.75		

LIGHTHOUSE TUBES

2C39A	$10.00	3C22	$60.00	464A	$1.90
2C40	7.00	4C27	7.00	559	.40
2C42	8.75	446A	.50	8011	1.00
2C43	7.75	446B	1.24	8014A	60.00
2C46	5.00				

TR. AND ATR. TUBES

1B24	$5.50	1B47	$7.00	532A	$ .25
1B24A	12.50	1B63A	18.50	709A	.50
1B35	3.50	1B58	45.00	724B	.65
1B35A	8.00	1Q22	40.00	6232	20.00
1B40	2.00	GA4	4.00		

DIODES

1N21	$ .45	1N25	$2.15	1N38A	$.65
1N21C	2.00	1N32	8.75	1N44	.90
1N23B	.80	1N34A	.45	CK705	.60
1N23C	2.25	1N38	.50	6006	P.O.R.

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2G21	$2.00	6ANSWA	$4.75	5965	$1.20
6AN5	2.75	5964	1.00	6211	1.10

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.03 at 600 VDC . . . . . $7.50 per C

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56—MMFD ±1 5%	@	$38.00 per M
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#154B . . . . . @ $60.00 per C

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77M1P11	@	$54.00 per M
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3—13—CAPS	@	$47.00 per M
3—17—CAPS	@	$49.00 per M

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1 watt 3¢
2 watt 4¢ Minimum 100 of a ±, 20 diff. #'s

Insulated American carbon resistors, all tolerances

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2 watt	25.00	

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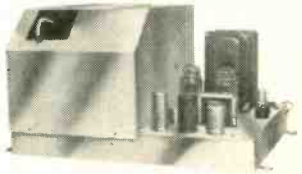

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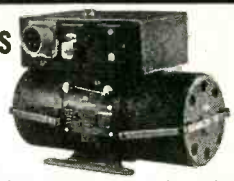

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Output: 115 VAC; 400 cyc; single phase; 45 amp. Input: 24 VDC, 5 amps. **$35.00**

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Output: 26 volts; 400 cycles, 6 volt amperes, 1 phase. Input: 24 VDC; 1 amp. **$15.00**

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Output: 115 V; 3 phase; 400 cycle; amps. .5 Input: 24 VDC; 12 amp. **$49.50**

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Output: 26 volts; 3 phase; 400 cycle; 10 VA; 6 PF. Input: 27.5 volts DC; 1.25 amps. **$24.50**

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Output: 125.5 VAC; 1.5 amps. 400 cycles single phase, 141 Va. Input: 20-30 VDC. 18-12 amps. Voltage and frequency regulated. **$49.50**

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Output 250 VA, 115 volts, 3 phase, 400 cycle, 1.25 amp., 0.8 pf. Input 27.5 volt DC, 20 amp. **$59.50**

12142-1-A Bendix
Output: 115 volts, 3 phase, 400 cycle, 250 VA. Input: 27.5 VDC, 22 amps. Voltage and frequency regulated **$99.50**

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Output: 115 VAC 400 cycles; single phase. Input: 24-30 VDC; 8 amps. **Price $39.50 each**

778 Bendix
Output: 115 volt 400 cycle; 190 VA; single phase and 26 volt, 400 cycle, 60 VA, single phase. Input: 24 VDC. **$37.50**

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Output: 115 volts AC; 750 VA, 3 phase, 400 cycle, .90 pf and 26 volts. 50 VA single phase, 400 cycle, .40 pf. Input: 27.5 VDC 60 amps. cont. duty, 6000 rpm. Voltage and frequency regulated. **$59.50**

10339 Leland
Output: 115 volts; 190 VA; single phase; 400 cycle, .90 pf and 26 volts; 60 VA; 400 cycle, .40 pf. Input: 27.5 volts DC, 18 amps. cont. duty, voltage and freq. regulated. **$49.50**

10486 Leland
Output: 115 VAC; 400 cycles; 3-phase; 175 VA; .80 pf. Input: 27.5 DC; 12.5 amps.; cont. duty. **$70.00**

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Output: 115 VAC; 400 cycle; 3-phase; 115 VA; 75 pf. Input: 28.5 VAC; 12 amps. **$35.00**

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Output: 115 VAC, 400 cyc.; single phase, 1.53 amp.; 8000 rpm. Input: 13.5 VDC; 29 amp. **$50.00**

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2J1F3 Gen. 115/57.5V 400 cy.	10.00
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50DG Diff. Gen. 90/90V 60 cy.	34.50
5F Syn. Mtr. 115/90VAC 60 cy.	34.50
5G Syn. Gen. 115/90VAC 60 cy.	34.50
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6DG Diff. Gen. 90/90V 60 cy.	25.00
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2900 Transicoil 115V 400 cy.	15.00
15CX4a Synchro Transmitter MK 22 MOD 1	15.00 ea.

SIMPLE DIFFERENTIAL

Size: 2-5/32" long x 1¼" dia.; bearing one end ½" O.D.; Shaft Size: 1" long, threads 8-32-¾" long, with bearing shaft ⅛" dia. x ¼" long. Gear on shaft end 1-7/16" dia., gear on bearing end 1¼" dia. Drive gear 25/32" dia.

Stock No. 101 **$3.95 ea.**

SIMPLE DIFFERENTIAL

1:1 reverse ratio, 60 teeth on large gear; ¼" shaft. Size: 3" long with 1-15/16" dia.

Stock No. 106 **$3.95 ea.**

DIFFERENTIAL

Size 2-11/16" long 1-11/16" dia. 1-1 reverse ratio. ¼" shaft on each end; one shaft 25/32" long, one shaft 15/32" long. Input and output gear 15/16" dia. 60 teeth.

Stock No. 148 **$3.30 ea.**

Dual Simple Differential

1:1 reverse ratio or both. Size: 3¼" long x 1-7/16" dia. Shaft size ⅛" and 5/32".

Stock No. 110 **$7.50 ea.**

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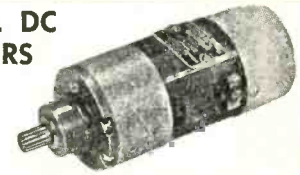

(approx. size overall 3¾" x 1¼" dia.:)

5067126 Delco PM, 27 VDC, 125 RPM, Governor Controlled	$15.00 ea.
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5068571 Delco PM 27.5 VDC 10,000 rpm (1x1x2")	5.00
5069625 Delco 27.5 VDC 120 rpm w/governor	15.00
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5BA10A118 GE 24 VDC 110 rpm	10.00
5BA10AJ37 GE 27 VDC 250 rpm reversible	10.00
5BA10AJ52 27 VDC 145 rpm reversible	12.50
5BA10AJ50, G.E., 12 VDC, 140 R.P.M.,	15.00
206-1001 PM Planetary Gear Reduced Motor with Magnetic Brake. Mfgd. by Air Equipment 26 volts 600 ma 145 rpm	17.50
5BA10FJ33, G.E., 12 VDC, 56 R.P.M., reversible	15.00
806069 Oster series reversible 1/50 h.p. 10,000 rpm 27.5 VDC 1⅝" x 3½"	5.00
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SS5

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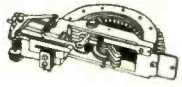
Volts DC	1 level Stk#	1 level Price*	2 level Stk#	2 level Price*	3 level Stk#	3 level Price*
6- 12	R960	9.50	R977	10.50	R642	11.50
24- 36	R975	10.50	R978	11.50	R600	12.50
48- 60	R976	11.50	R979	12.50	R645	13.50
100-125	R643	12.50	R644	13.50	R646	14.50

SS6

Mfd. by Western Electric Co.; 22 step; 5 levels; Bridging wipers; Contacts; Gold plated brass. Interrupter Switch: 1 Break-Make; Net Weight: 2 lb. 2 oz. "Homing" type; 180° Wipers; Step in One Direction.



		ea*			ea*
#R926;	6 to 12 VDC	13.75	#R981;	48 to 60 VDC	15.75
#R980;	24 to 36 VDC	14.75	#R615;	100 to 125 VDC	16.75

SS7

Mfd. by Western Electric Co.; 44 step; 2 levels Bridging Wipers; Contacts: Gold plated brass; Interrupter Switch: 1 Break-Make; Net Weight: 1 lb. 14 oz. "Homing" Type; 360° Wipers; Step in One Direction.

		ea*			ea*
#R927;	6 to 12 VDC	13.75	#R983;	48 to 60 VDC	15.75
#R982;	24 to 36 VDC	14.75	#R616;	100 to 125 VDC	16.75

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The vertical response is within 3 db from 20 cycles to 20 megacycles. The horizontal response within 3 db from 10 cycles to 100 kc and the "Z-axis" response within 3 db from 30 cycles to 3 megacycles. Deflection sensitivity .1 volt rms per inch deflection. The horizontal sensitivity .9 volts rms per inch deflection. The "Z-axis" sensitivity 15 volts peak signal is enough to bring the beam from just being extinguished to normal brilliance. The instrument operates from 105 to 125 volts, 50-60 cycle source and consumes 150 watts. Physically the instrument is 16" in overall height, 17" in overall depth and 10½" in overall width. Weight: 60 lbs. Available complete with instruction book.

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Measurements Corp. Mod. 62 V.T.V.M. 60.00
L&N Mod. 4282 Ohmeter..... 60.00
G. R. Mod. 726-A V.T.V.M..... 50.00
L&N Mod. 5300 Wheatstone Bridge.. 85.00
Freq. time counter, Potter Mod. 801.150.00
Measurements Corp. Mod. 78-B Sig. Gen. 50.00

Top seven items new; others in good cond.

ALGERADIO ELECTRONICS CO.
236 N. Franklin St., Hempstead, N. Y.

COMMUNICATIONS EQUIPMENT CO.

TIC SIGNAL GENERATOR

The type 1900 Multi-Frequency Generator is a 10 frequency, 400 cps modulated, crystal controlled oscillator intended for the preliminary alignment of stagger tuned IF amplifiers of television receivers. Crystals ranging from 17 to 40 mc can be provided to exact frequencies specified. Crystals are arranged in sequence. The frequency accuracy is better than .05% and the modulation is adjustable from zero to approximately 30% by an internal control. Frequency selection is instantly accomplished by means of a special coin silver contact rotary switch actuated by a heavy duty pulsing solenoid and front panel push button selector switch. The output signal is 0.5 volts across a 75 ohm terminated output cable 4 feet long. The output signal is capable of attenuation over a range of 1000 to 1. The power supply is electronically regulated to assure complete freedom from line voltage fluctuations from 105 to 125 volts.

The instrument is contained in a grey wrinkle finished cabinet 12½" wide, 9½" deep, and 8" high. Shielding is adequate to prevent excessive radiation. All units are supplied with a minimum of five crystals as follows: 41.25 mc/42.75/45.5/44.2, and 4.5 mc. Used, excellent..... **$32.50**

PULSE TRANSFORMERS

352-7150. Primary 50 ohms. Secondary 1000 ohms. 12,000v, 12.0 Amp. Pulse: 1 or 2 usec. at .001 duty ratio. Fitted with magnetron well and bifilar winding for filament supply $32.50

MAGNETRON PULSE TRANS. #964: Prim. imp. 30 ohms. 1600 v. pulse. Secondary imp. is 1250 ohms, 12 KV pulse. Turns ratio sec:pri. is 7.5:1. Duty ration is 0.001 at 1.2 usec. Bifilar winding 1.2A.....$8.50

RAYTHEON WX 4298E: Primary 4KV., 1.0 USEC. SEC. 16K-16 AMP DUTY RATIO: 001 400 CYCLE FIL. TRANS. "BUILT-IN".....$22.50

GE #K-2449-A Primary: 9.33 KV, 50 ohms Imp. Secondary: 28 KV, 350 ohms. Pulse length: 1.05/5 usec @635/120 PPS. PK Power Out: 1,740 KW, Bifilar: 1.5 amps.....$62.50

GE #K-2748-A, 0.5 usec @ 2000 Pps. Pk. Pwr. out is 32 KW impedance 40:100 ohm output. Pri. volts 2.3 KV Pk. Sec. volts 11.5 KV Pk Bifilar: rated at 1.3 Amp. Fitted with magnetron well.....$24.50

K-2745 Primary: 3,1/2,.8 KV, 50 ohms Z. Secondary: 14/12.6 KV 1025 ohms Z. Pulse length: 0.25/1.0 usec @ 600-600 PPS. Pk. Power 200/150 KW. Bifilar: 1.3 Amp. Has "built-in" magnetron well.....$32.50

9000 MC RF PACKAGE

A Set of four major components to form a 35 KW (peak) RF head operating in the range of 9345-9405 mc, consisting of the following:

(1). Pulse-forming network, 30 ohms imp, 2 usec (at 350 pps)/0.6 usec (at 2000 cps)

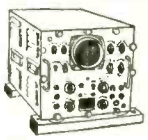
(2) Pulso transformer to match 30 ohms to 1250 ohms. Primary 1.6 KV, Secondary 12 KV. Bifilar Winding: 1.2 A.

(3). Magnetron, type 725A (Fits into magnetron well on Transformer)

(4.) Magnet for 725-A (4,850 Gauss)

Complete Package, with Schematic diagram **$35.00**

SYNCHROSCOPE/TS 28/UPM



This unit is an instrument originally designed for testing beacons and radar sets, but may be used for general laboratory work. The scope is equipped with a type 5CP1 CR tube and uses triggered sweeps ranging from 1 to 6 usec/inch. Free-running sawtooth rates are 20 to 3000 cps. Positive and negative output triggers having rep rates of 330/500/1,000/2000 and 4000 cps are supplied. Marker periods are 2/10, and 25 usec accurate to 1%. The 2-stage video amplifier has a bandwidth of 5 mc and a gain of 100. Used, in excellent condition..... **$175.**

DYNAMOTORS

TYPE	INPUT VOLTS	INPUT AMPS	OUTPUT VOLTS	OUTPUT AMPS	Price
BOAR83	14		375	.150	$6.50
POSX-15	14	2.8	220	.08	8.95
DM33A	28	7	540	.250	3.95
B-19	12	9.4	275	.110	6.95
			500	.050	
OA-3A*	28	10	300	.260	3.95
			150	.010	
			14.5	5.	
PE 73 CM	28	19	1000	.350	10.50
BD 60†	14	2.8	220	.08	8.95
DAG-33A	18	3.2	450	.06	2.50
BOAR 93	28	3.25	375	.150	6.95

† Less Filter * Replacement for PE 94.

PE 94-, Brand New 5.95

MICROWAVE COMPONENTS
10 CM.—RG48/U Waveguide

POWER SPLITTER for use with type 726 or any 10 CM Shepherd Klystron. Energy is fed from Klystron antenna through dual pick-up system to 2 type "N" connectors $12.50

LHTR. LIGHTHOUSE ASSEMBLY. Parts of RT39 APG 5 & APG 15, Receiver and Trans. Cavities w/ assoc. Tr. Cavity and Type N CPLG. To Recvr. Uses 2C40, 2C43, 1B27, Tunable APX 2400-2700 MCS. Silver Plated $15.00

BEACON LIGHTHOUSE cavity p/o UPN-2 Beacon 10 cm. Mfg. Bernard Rice, each.....$27.50

MAGNETRON TO WAVEGUIDE Coupler with 721-A Duplexer Cavity, gold plated.....$31.50

721A TR BOX complete with tube and tuning plungers $12.50

McNALLY KLYSTRON CAVITIES for 707B or 2K28, 2700-2900 MC $4.00

HOLMDELL-TO-TYPE "N" Male Adapters. W. E. #D167284 .....$2.75

BEACON ANTENNA AS31/APN-7 in Lucite Ball. Type "N" feed.....$22.50

ANTENNA, AT49A/APR; Broadband Conical, 300-3300 MC Type "N" Feed.....$12.50

"E" PLANE BENDS, 90 deg. less flanges.....$7.50

K-Band, X-Band Eqpt. Available.....Send for List

X BAND – 1" x ½" WAVEGUIDE

90 degree elbows. "E" or "H" Plane 2½" radius $8.50

AT-68/UP 3 Cm Horn with type N. feed for receiver measurements, etc. New $7.45

ROTARY JOINT (APS-6) Sperry PT #658275, 180 deg. rotation, choke to choke. Has "Built-in" Di-Coupler, 20 DB., with "N" Takeoff.....$22.50

PARABOLOID DISH, 18" diam. Spun Aluminum, 8" Focus. For AN/APS-6.....$4.95

3 CM. DIPOLE and Reed Assembly. (May be used with above dish.) 8 inches long.....$5.00

FLEXIBLE SECTION 9 in. long, Cover-to-Cover **$5.50**

ROTARY JOINT (APS-6) Sperry PT #658275, 180 deg. rotation, choke-to-choke. Has "Built-in" Di-Coupler, 20 DB., with "N" Takeoff.....$22.50

3 CM. DIPOLE FEED, 10½" Focus.....$14.50

3 CM. ANTENNA ASSEMBLY: Uses 17" paraboloid dish, operating from 24 vdc motor. Beam pattern: 5 deg. in both Azimuth and elevation.....$35.00

30" PARABOLIC DISH, aluminum focus 10½"...$4.85

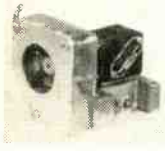
INVERTERS

PE-218H: Input: 25/38 vdc, 92 amp. Output 115V 300/500 cy. 1500 Volt-ampere. NEW.....$59

EICOR—ML 3011-5, Input: 13.75 V; 18.4A, Output: 115V/400~, 3φ, 0.95 PF. 100 VA. New.....$59

343 Canal St., New York 13, N.Y. Dept. E-3 Chas. Rosen Phone: CAnal 6-4882

MINIATURE BLOWERS:



MOTOR and BLOWER—DELCO 5068571 .27 VDC Reversible PM Motor, 6000 RPM, with Blower. Overall size, including Blower: 2⅝" x 2¼" x 3". Wt. 9 oz. As pictured to left. Price **$4.50**

DELCO 5069267 — 27 VDC. 6000 RPM, 1.5 oz. in torque. Reversible Shunt Motor. Flang Mounted. Size: 2¾" x 2⅝" L. Flange 2¼" D. Shaft: ¼" x 1". Blower Fan attached. No. 10D267 ..... **$2.95**

24 VOLT 10 CFM BLOWER—Housed in a cast aluminum case. Shunt Type Motor 24 VDC @ .6 A. 5000 RPM with motor noise Filter. Size: 3¼" D x 4½" L x 4½" L x 4" H. Wt. 1 lb. 10 oz. No. SS2345 ..... **$5.95**

115 VAC 400 CY. 10 CFM BLOWER—7200 RPM 1/100 HP. Bakelite blower Housing. Overall sizee: 3½" x 3½" x 4½". Wt. 1 lb. 7 oz. Eastern Air Devices No. J31A..... **$5.95**

10 CFM BLOWER—OSTER MOTOR C2BP-1A—27.5 VDC 1/100 HP. 7000 RPM. Bakelite blower Housing. Overall size: 3¼" x 3½" x 4½". Wt. 1 lb. 4 oz. Price..... **$5.95**

New List— *Just Out—Including many other Motors, Blowers, Dynamotors, etc. Free—Write for copy today!*

115 V. 60 CYCLE BLOWERS:

At Left: 115 VAC 60 Cycle **SINGLE TYPE** — 100 CFM — 2¼" intake; 2" outlet. Complete size: 5" x 6" — **$9.95**
No. 1C939 .....

115 VAC 60 Cycle DUAL TYPE —100 CFM—4" intake; 2" Dis. Each Side. Complete size: 8' x 6"
No. 1C880 ..... **$14.95**

115 VAC 60 cycle COMPACT TYPE—108 CFM; Motor built inside squirrel cage; 4½" intake: 3⅝" x 3" Dis. Complete size 4½" W x 8⅜" H x 8⅛" D—No. 2C067 ..... **$15.95**

115 VAC 60 cycle FLANGE TYPE—140 CFM; 3½" intake: 2½" Dis. Complete size: 7½" W x 7¼" H x 6¾" D—No. 1C807 ..... **$14.95**

115 VAC 60 cycle FLANGE TWIN—275 CFM; 4½" intake; 3½" x 3" Dis. Complete size: 11⅜" W x 2⅜" H x 8-1/16" D—
No. 2C069 ..... **$22.95**

DYNAMOTORS

INPUT VOLTS	OUTPUT VOLTS	OUTPUT MA	STOCK No.	PRICES USED	PRICES NEW
12 VDC	220	80	DM-34	$2.95	$4.95
12	625	225	DM-35	9.95	
12	230	90	PE-133	4.95	6.95
12 or 24	540	450	DA-12		14.95
12 or 24	230	100	DA-14		8.95
14	220	70	DM-24	4.95	7.95

FAIR RADIO SALES • 132 SOUTH MAIN ST. LIMA, OHIO

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Top quality communications and test equipment at low prices.

Here are a few leaders . . . . .

BC-375—Complete two cases, export, packed, unused ground transmitting equipment.

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TS-323/UR—Frequency meter.

334-E—Control box.

R-252/ARN-14	Receivers
R-122-A/ARN-12	Marker Beacon
TS-125/AP	Test Equipment
TS-186/UP	Test Equipment

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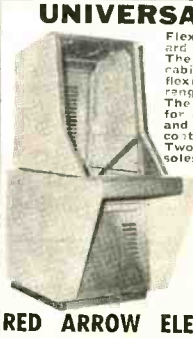
TWX: N. Y. 1–3731

UNIVERSAL CONSOLE



Flexible—accommodates any standard RMA 19" rack mounted unit. The same unit may be installed in cabinets or consoles permitting flexibility in expansion or rearrangement.

The universal console is designed for operator comfort, viewing ease and maximum accessibility to all controls and chassis. Two, three or more universal consoles may be ganged together. Thereby utilizing a minimum of space. Dimensions—Max. height: 57". Width: 19⅛" without end bells. 27⅛" with end bells. Distance floor to shelf: 27¾". Max. depth: 37½". Weight: 150 lbs. approx. with end bells and shelf.

COMPLETE UNIT $59.50 *while they last—*

RED ARROW ELECTRONIC SALES CO.
12 - 17 Summit Ave. Union City, N. J.

CONDENSERS

4 mfd.—600 V . . . . . $.95
Inverted cylindrical cap. single term. Mount through ¾" hole in chassis. Hardware included. Factory cartons. Qua. disc.

16 mfd.—600 V $1.89
Dual 8 mfd oil filled cond. hermetically sealed and packed. Tobe type PT-SC-11 measuring 3¾"x2⅝"x2⅝". Stud mntg. centers 2". Plugs into standard four prong socket.

10 mfd.—400 V . . . . . $.65

10 mfd.—600V $1.19
Pyranol. Brackets included

Mfd	Volts	Price
.001	50KV	24.95
.005	15KV	9.75
.005	25KV	20.95
.005	50KV	29.50
.01	1500	.65
.012	25KV	12.95
.015	16KV	14.50
.02	8000	4.75
.02	10KV	5.25
.02	20KV	10.95
.025	50KV	32.95
.03	7500	4.25
.03	16KV	6.95
.04	17KV	8.95
.05	7500	4.25
.05	25KV	16.50
.05-.05	12KV	9.95
.05-.05	50KV	60.00
.08	12.5KV	8.95
.1	1250	.29
.1	1500	.39
.1	2000	.58
.1	2500	.79
.1	3000	.69
.1	3000	1.19
.1	4000	1.39
.1	5000	3.25
.1	6000	2.25
.1	7500	.95
.1	7500	4.25
.1	12KV	6.95
.1	12.5KV	12.50
.1	15KV	15.95
.1	20KV	19.50
.1	25KV	24.50
.125	27.5KV	27.50
2x.1	2000	.89
2x.1	6000	2.29
.2	10KV	8.50
.2	13KV	10.50
.2	15KV	13.90
.2	50KV	69.50
.25	50KV	69.50
3x.2	4000	2.85
.25	1500	.88
.25	2000	.98
.25	3000	1.45
.25	4000	1.98
.25	6000	.89
.25	15KV	15.95
.25	20KV	19.95
.25	25KV	40.00
.3	2000	.49
2x.25	2000	.98
.4	10KV	10.90
.4	37.5KV	PUR
2x.4	7500	5.25
.5	600	.39
.5	1500	.59
.5	2000	1.19
.5	2500	1.29
.5	3000	2.39
.5	5000	3.05
.5	7500	5.75
.5	12.5KV	37.50
.5	25KV	39.95
.5	30KV	PUR
.5-.1	2000	.39
2x.5	600	.69
2x.5	9000	9.25
1	500	.35
1	600	.44
1	1000	.69
1	1500	.99
1	2000	1.85
1	2500	2.20
1	3000	2.95
1	4000	4.95
1	5000	6.25
1	6000	6.50
1	6000	8.95
1	7500	14.75
1	10KV	25.95
1	15KV	32.50
1	25KV	65.00
1	25KV	75.00
1	30KV	PUR
2x1.25	7500	20.00
1.25	330VAC	.49
1.5	15KV	49.50
2	600	.55
2	1000	.79
2	1000TLA	1.29
2	1500	1.15
2	2000	2.80
2	2500	3.45
2	4000	7.50
2	5000	12.50
2	7500	23.25
2	10KV	59.95
2	15KV	65.00
3	1000	.98
3	2000	2.50
3	4000	8.50
3	8000	29.50
4	600	.75
4	600TLA	.95
4	1000	1.10
4	1500	2.65
4	2000	3.75
4	3000	6.99
4	4000	17.50
4	5000	24.95
4	7500	59.50
4	10KV	74.50
4	15KV	PUR
4	220AC	1.19
5	330AC	1.39
5	1000	1.89
5	1500	2.45
5	5000	27.50
2x5	400	.89
2x5	600	1.19
6	600	1.69
6	330AC	1.69
6	1000	1.95
6	1500	2.95
6	2000	3.50
6	7500	63.50
7	110AC	.59
7	600	1.35
7	800	1.55
8	600	1.29
8	1000	2.15
8	1000	1.39
8	1500	3.65
8	2000	6.95
8	2500	9.50
2x8	600	1.89
4x8	600	3.85
9	10KV	PUR
2x2.5-5	600	1.75
10	400	.65
10	600	.75
10	600	1.50
10	1000	3.75
10	1500	4.25
10	2000	6.35
10	2500	10.95
10	4000	PUR
10	5000	PUR
12	1000	3.50
13.5	10KV	PUR
12	660AC	3.95
14	660AC	4.25
15	440AC	3.85
15	1000	4.10
15	1500	6.35
20	330AC	3.25
20	4000	PUR
24	500	1.98
28	1000	5.95
30	2500	13.50
32	600	3.85
42	600	4.75
50	330AC	6.50
80	4000	45.50
100	4000	PUR

TYPE "J" POTS $.65

Ohms	Ohms	Ohms
50 L †	10 000 L † *	250 000 L † *
100 L †	15 000 L †	500 000 L †
200 †	0 000 L †	600 000 †
500 † *	25 000 L † *	1 Meg L † *
1000 L † *	50 000 L † *	1.5 Meg †
1000 † Switch	75 000 † *	2 Meg L †
1500 †	100 000 L † *	2.2 Meg L †
2000 L †	150 000 † *	2.5 Meg †
2500 † *	200 000 L †	4 Meg †
5000 L † *		

L = Locking Shaft * = ⅛SD † = ¼" Shaft Plus

TYPE "JJ" POT $1.50

Ohms	Ohms	Ohms
1500 †	100 000 ‡	500 000 ‡
15 000 ‡	150 000 ‡	750-75 K †
50 000 ‡	250 000 ‡	1 Meg †
75-750 K ‡		4 Meg †

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Bathtub Channel & Mica Condensers.
Carbon & WW Pots. Pwr Resistors & Rheostats

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SPECIAL PURPOSE TUBES

OA2	.70	4C33	75.00	VX-33A	5.00	631-P1	5.00	5651WA	3.50
OA2WA	3.00	4C35	15.00	35T	2.85	WE-701A	1.50	5654	1.35
OA3/VR75	.90	4D32	19.50	35TG	2.85	707B	2.00	5656	6.00
OA5	4.00	4E27	7.00	VX-41	5.00	715C	10.00	5663	.95
OB2	.60	4J38	100.00	FP-54	25.00	717A	.35	5670	1.85
OB3/VR90	.75	4J39	100.00	HK-54	2.00	719A	15.00	5672	1.00
OC3/VR105	.60	4J46	25.00	VX-55	6.00	721A	.50	5675	6.85
OC3W	2.50	4J51	100.00	FG-57	9.00	721B	6.85	5676	1.00
OD3/VR-150	.60	4J52	50.00	RK65/5D23	6.50	723A/B	7.25	5678	.75
OD3W	2.50	4J61	150.00	FG-67	8.00	WE-725A	2.50	5685	12.00
EL-C1A	6.00	4X100A	10.00	HY-69	2.00	726A	4.50	5686	2.00
1AD4	.90	4X150A	18.50	RK-73	.75	726B	12.50	5687	2.75
1AE4	1.00	4X500F	50.00	FG-81A	3.50	802	3.00	5687WA	4.50
1AF4	2.50	5A6	2.00	FG-95	15.00	803	2.00	5691	4.50
1AG5	2.00	5AP1	5.00	100TH	5.00	804	7.50	5692	5.00
1B23	2.00	EL-5B	5.50	WE-121A	1.50	805	3.50	5693	4.50
1B24	6.00	5BP1A	7.50	WE-122A	1.50	807	1.15	5696	.85
1B27	12.50	5BP2A	5.00	WE-123A	2.50	807W	1.50	5702	1.50
1B35	3.50	5C22	22.50	WE-124A	3.50	807WA	5.00	5703	1.00
1B35A	7.50	5CP1	2.00	VT-127	1.50	809	2.00	5704	1.50
EL-1C	1.25	5CP1A	7.50	VXR-130	1.50	810	10.00	5719	1.50
1P21	30.00	5CP7A	8.00	FG-172	15.00	811	3.00	5720	15.00
1P22	5.00	5CP11A	9.50	FG-190	2.50	812	2.50	5725	2.50
1P28	7.25	5CP12	10.00	CE-203	5.00	813	10.00	5726	.75
1Z2	2.25	5FP14	5.00	203A	2.50	814	1.25	5727	1.25
2AP1	2.50	5HP1A	10.00	WE-211D	8.00	815	1.25	5728	8.00
2AP1A	6.00	5J29	4.00	CE-235A	5.00	826	.75	5734	9.00
2B22	2.00	5J30	4.00	FG-235A	55.00	828	8.00	5740	25.00
2C36	35.00	5JP1	8.50	WE-242C	10.00	829B	8.50	5749	1.25
2C39	5.00	5JP2	5.00	QK-243	40.00	832A	4.85	5750	2.50
2C39A	10.00	5JP2A	7.50	WE-244A	7.50	836	1.25	5751	2.50
2C39B	29.00	5JP4	3.50	WE-245A	6.00	837	1.25	5755	7.50
2C40	7.50	5JP5A	10.00	WE-249B	3.50	838W	3.50	5762	125.00
2C40A	26.00	5JP11A	7.50	WE-249C	2.50	845	2.75	5763	1.15
2C42	8.00	5LP1	9.50	250R	5.00	850	10.00	5771	275.00
2C43	8.50	5LP2A	10.00	WE-251A	50.00	851	6.50	5783WB	5.50
2C46	5.00	5R4GY	1.25	WE-252A	7.50	866A	1.35	5787WA	6.00
2C50	6.00	5R4WGY	2.50	WE-253A	2.00	866JR	1.25	5796	10.00
2C51	3.50	5RP1A	17.50	WE-254A	2.25	868/PJ-23	1.50	5798	10.00
2C52	2.75	5RP11A	75.00	WE-257A	3.00	869B	50.00	5800	7.50
2C53	10.00	5SP1	50.00	FG-258A	75.00	872A	1.00	5801	5.00
2D21	.70	5X3	2.00	WE-259A	15.00	874	.85	5803	6.00
2D21W	.85	5XP1	50.00	WE-262B	5.00	884	.95	5814	.75
2E22	2.50	5Z2P7	25.00	FP-265	18.50	885	.75	5814WA	3.25
2E24	2.25	5Z4P11	50.00	WE-267B	5.00	913	17.50	5827	5.00
2E26	3.35	EL-C6J	12.00	WE-268A	5.00	917	1.40	5828	7.50
2J51	175.00	EL-C6L	6.50	WE-271A	5.00	918	1.50	5829	.85
2J52	50.00	EL-6C	7.00	WE-272A	7.50	920	2.00	5830	85.00
2J54	25.00	6AC7W	.85	WE-274B	.75	922	1.50	5836	93.00
2J55	35.00	WE-6AK5	1.25	WE-275A	3.50	923	1.25	5840	3.25
2J56	50.00	6AK5W	1.00	WE-276A	7.50	931A	4.30	5842	15.00
2J59	50.00	6AL5W	.75	WE-282A	2.25	958A	.30	5847	15.00
2J61	12.50	6AN5	2.25	WE-282B	4.50	959	1.15	5854	1.00
2J62	5.00	6AQ5W	1.70	WE-283A	3.25	991/NE-16	.25	5876	6.75
2J64	100.00	6AR6	1.35	WE-285A	4.50	CK-1006	2.25	5881	3.00
2K25	10.00	6AR6WA	2.50	WE-286A	3.50	1611	1.00	5886	2.75
2K26	35.00	6AS6	1.25	WE-287A	3.00	1613	1.00	5902	4.50
2K28	30.00	6AS6W	2.50	GL-299	1.50	1614	1.75	5915	.50
2K29	25.00	6AS7G	2.50	WE-300B	7.50	1619	.50	5932	3.50
2K30	50.00	6AU6WA	2.50	304TH	12.50	1620	3.25	5933	1.50
2K33A	60.00	6BA6W	1.25	304TL	12.50	1622	1.50	5933WA	5.00
2K34	100.00	6BE6W	2.50	WE-310A	3.85	1624	1.50	5948/1754	200.00
2K35	100.00	6BL6	30.00	WE-311A	4.00	1625	.50	5962	5.00
2K39	100.00	6BM6	30.00	WE-313CD	4.00	1845	50.00	5963	1.25
2K41	85.00	6C4W	4.00	WE-316A	.50	1945	50.00	5964	1.00
2K45	30.00	6C21	15.00	WE-323A	8.50	2050	.95	5977	2.75
2K47	100.00	6F4	2.25	WE-323B	5.00	2050W	3.50	5979	10.00
2K48	50.00	6J4	1.25	WE-328A	3.50	5528	6.50	5980	8.50
2X2A	.85	6J4WA	2.00	WE-336A	4.50	5550	25.00	5981	60.00
3ABP1	75.00	6J6W	1.00	WE-338A	4.00	5551	40.00	5998	4.75
3AP1	2.00	6K4	2.00	WE-339A	10.00	5552	55.00	6005	1.70
3AP11A	5.00	6K4A	2.75	WE-347A	2.50	5553	75.00	6021A	4.50
3B24	.85	6L4	3.50	WE-348A	5.00	5556	6.75	6028	2.00
3B24W	4.50	6L6WGA	3.75	WE-350A	2.50	5557	3.50	6037	50.00
3B24WA	8.00	6L6WGB	3.50	WE-350B	2.00	5558	4.00	6038	7.50
3B25	3.50	6Q5G	2.50	WE-352A	15.00	5559	9.00	6073	2.00
3B26	2.75	6SJ7WGT	2.00	WE-354A	8.50	5560	15.00	6087	4.25
3B28	4.50	6SK7W	.85	WE-355A	8.50	5584	3.00	6098	2.50
3B29	5.50	6SK7WA	2.00	WE-388A	1.25	5591	2.75	6100	2.25
EL-3C	4.50	6SL7WGT	1.25	WE-393A	3.50	5610	1.00	6130	5.00
EL-C3J	8.50	6SN7WGT	1.25	394A	2.50	5632	8.50	6134	4.50
EL-C3JA	10.50	6SU7GTY	2.25	WE-396A	3.50	5633	6.00	6136	2.50
3C23	3.50	6X4WA	2.00	WE-403A	1.35	5634	6.00	6137	2.00
3C24	3.00	6X5WGT	1.25	WE-403B	2.75	5635	6.00	6189	2.50
3C33	6.00	7F8W	1.50	WE-404A	15.00	5636	2.75	6201	3.00
3C45	5.00	12A6	.60	WE-407A	3.75	5636A	3.25	6236	185.00
3D22	9.50	12AP7	50.00	WE-408A	2.00	5637	3.75	6263	12.50
3DP1A	5.00	12AT7WA	3.00	WE-409A	1.25	5638	6.50	6264	10.00
3E22	4.85	12AU7WA	3.00	WE-416B	35.00	5639	6.00	6280	35.00
3E29	8.50	12DP7	15.00	WE-417A	15.00	5639A	6.50	6322	12.50
3GP1	2.00	12GP7	15.00	WE-418A	15.00	5640	6.00	6328	6.50
3J21	50.00	FG-17	3.50	WE-420A	7.50	5641	5.00	6463	1.95
3J31	40.00	HK-24	2.00	WE-421A	4.75	5642	1.00	8005	4.50
3JP1	7.50	HK-24G	3.00	WE-429A	10.00	5643	8.50	8012A	3.50
3JP12	10.00	26E6WG	2.00	446A	.50	5644	6.00	8013A	4.50
3K27	150.00	26Z5W	3.00	446B	1.25	5645	5.50	8020	1.00
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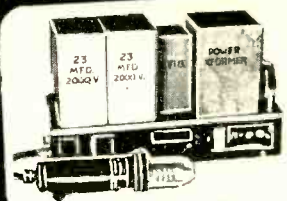

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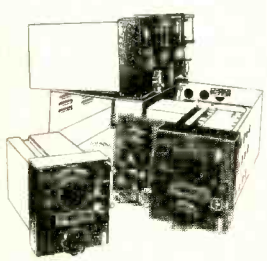

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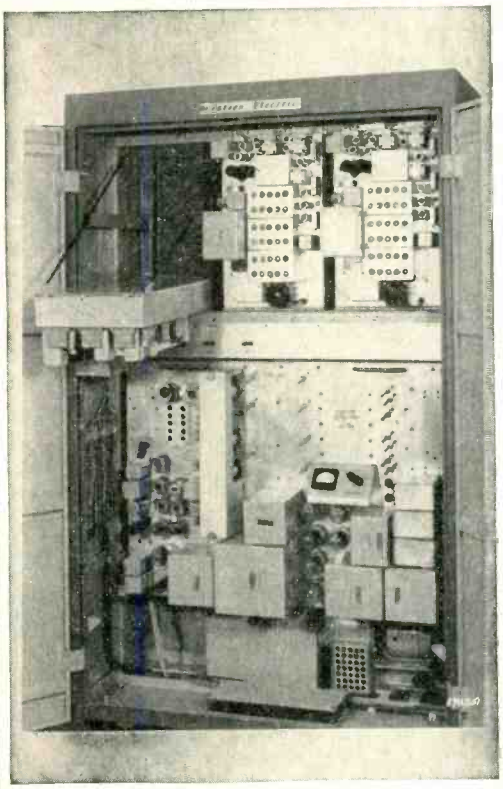

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Barry, 512 Broadway, New York 12, N. Y.

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Send special offers with net price and types to:

W-1882, Electronics
Class. Adv. Div., P.O. Box 12, N.Y. 36, N.Y.

SAVE UP TO 70% OF WHOLESALE COST

TYPE "J" POTENTIOMETERS
2 Watt Carbon
Full Range of Values Available From Stock for Immediate Delivery
Single Type J Units..... $ .95 Ea.
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In Stock For Immediate Delivery
VARIOUS COLORS and SIZES
Inquire For Complete Listing At Money Saving Prices

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PRECISION POTENTIOMETERS
50K 10 Turns 0.5% Linearity—Van Dyke Instr. Miniature Type 3/4" dia. x 2-1/4" lg..... $7.95 Ea.
20K 10 Turns 0.1% Linearity—Gibbs Micropot..... $6.95 Ea.
10K 25 Turns 0.1% Linearity—Helipot..... $19.50 Ea.
10K 10 Turns 0.5% Linearity—Helipot..... $6.95 Ea.
10K 10 Turns 0.1% Linearity—Helipot..... $7.50 Ea.
2K 10 Turns 0.1% Linearity—Helipot..... $6.95 Ea.
Helipot Duo Dials available for above.

HI CURRENT FILAMENT TRANSFORMERS
AMERTRAN type W-PRI-105-125v 60cy 1 ph-SEC.5V, 190amp. 35KV Ins Ea. 529.50
KENYON - S - 14940 - PRI - 105-125V 60cy 1 ph-SEC. 5V 115 amp..... Ea. $19.50
MIL-T-27 Type-PRI-115/230V 50/60 cy.-SEC. 5V 10 AMP 10 KV Ins... Ea. $6.25

ALL COMPONENTS 1ST QUALITY AND 100% GUARANTEED

TUBES
NEW—COMPLETELY GUARANTEED

750TL $19.95 Ea.	807W $1.75 Ea.
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FULL LINE OF RECEIVING TUBES, POWER TUBES, MAGNETRONS, KLYSTRONS, CRYSTAL DIODES AVAILABLE AT SIMILARLY LOW PRICES.

IMMEDIATE DELIVERY

KOLLSMAN SERVO MOTORS WITH TACH GENERATOR
TYPE 890-0160640-MOTOR-115V-60Cy. 2 Ph. 3350 RPM-5 Watts Output. GEN. 6.5V/1000 RPM..... $59.50 Ea.
TYPE 1623B-0410120 Motor-26V-400 Cy-2 Ph.-6500 RPM .045 Watts Output. GEN. 0.34V/1000 RPM..... $42.50 Ea.

SOUND POWERED PHONES
Head and Chest Set
U. S. NAVY TYPE "M"
Heavy Duty Includes Headset, Chest Mike and 20 Ft. Cord. $14.88 Ea.
T.S. 10 Type S.P. Handset. $9.48 Ea.

Terms: 20% cash with order, bal. C.O.D unless rated. All prices net F.O.B. our warehouse Phila., Pa. subject to change without notice.
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1CT	$37.50	5N	$22.50
1DG	37.50	5SDG	12.50
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1G	37.50	6G	34.50
3D	62.50	6GD	27.50
3HCT	62.50	6HG	42.50
5B	22.50	7G	42.50
5CT	34.50	7DG	47.50
5HCT	42.50	23CX6	45.00
5F	34.50	2J1F1	4.95
5G	34.50	2J1G1	3.95

MANY OTHER TYPES IN STOCK QUOTATIONS ON REQUEST

PULSE TRANSFORMERS
OVER 50 TYPES LOW AND HIGH POWER TYPES IN STOCK FOR IMMEDIATE DELIVERY
MFD. BY UTAH, G.E., RAYTHEON, PHILCO, WESTINGHOUSE, WESTERN ELECTRIC, ETC.

132AW2F	7P1	$6.95
134BW2F	7P4	6.95
176AW2F	7P10	7.50
139DW2F	7P13	5.95
148DW2F	7P15	7.60
Utah X124T2-9262		12.50
Utah X139T1-9278		3.75
G.E. 68G828		14.50
G.E. 68G627		16.50

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POLYSTYRENE CAPACITORS
1% Tolerance
Hermetically Sealed-200VDCW-500VDCT
0.5 MFD..... $7.50 Ea.
1 MFD..... $12.10 Ea.
Mdf. by Western Electric..... Brand New

FROM ONE OF THE LARGEST INVENTORIES IN THE U.S.A.

TEST EQUIPMENT
HEWLETT-PACKARD AUDIO OSCILATOR
Model LAJ 20-20,000 cy..... *$85.00

BC-221 FREQUENCY METER 125 KC to 20,000KC—Accur. .05%..... *$115.00

TS-33/AP FREQUENCY METER 8700-9500MC—Accur. .03%..... *$145.00

TS-34/AP OSCILLOSCOPE 30cps to 1MC—Portable..... *$195.00

LAE-1 Signal Gen. (510-1300MC) . $225.00
LAF Signal Gen. (90-600MC)..... *$325.00
LAG Signal Gen. (1200-4000MC). *$375.00
LP-5 Signal Gen. (9.5KC-50MC). *$425.00
Measurements 79B Pulse Generator $165.00
Waterman 3" Rakscope S-12-B..... $325.00
Hewlett Packard 325-B—Distortion Analyzer..... *$220.00
Dumont 208 Oscilloscope..... *$80.00

GENERAL RADIO
GR 572B 1KC Hummer..... 7.50
GR 700P1 Volt. Divider..... 27.50
GR 713B Beat Freq. Osc..... *$225.00
GR 715 AE DC Amplifier..... 225.00
GR 720A Het. Freq. Meter..... 275.00
GR 723C VT Fork 1KC..... 89.50
GR 726A VTVM..... *$85.00
GR 727A VTVM (Battery Oper.).. *$105.00
All items new except where noted *Excellent Used—Guaranteed).

2.4KVA POWERSTAT
Superior $649
Input—115/230V 60 cy. 1 ph.
Output—0-270V 9 Amps.
Brand New.
Special Price **$37.50 Ea.**

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715-19 Arch St., Phila. 6, Pa. • MArket 7-6771-2-3
Cable Address: LECTRONIC, Philadelphia

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KOILED KORDS 3 wires $1.26
22 inches long stretches to 9 ft.

GONIOMETER
TYPE CFT-47372 — 250 to 1500 K.C.

nitelighter —Automatic light switch. Darkness throws the switch — turns lights on at dusk . . . off at dawn. Fools burglars who watch for signs of an empty house. Same as your city buys for $45 on top of lamp posts. $15.95

TELECHRON Motors

2 RPM ...	$2.90	1 RPM ...	3.95
3 RPM ...	3.90	3 R.P. Hr..	2.85
4 RPM ...	2.90	1 R.P. 2Hr.	2.80
3. 6 RPM.	3.15	1 R.P.12Hr.	3.25
		60 RPM ...	4.85

1 RPM—50 Cycles, $1.85
Laboratory Special 1 of Each Motor $25

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General Radio **VARIACS** in stock. Special Sale on a few **200-B** (1 amp.) removed from equip't..... $8.95

HAND WOUND 10 Sec. to 24 Min. TIMER SWITCH $1.35

6 Watt Most POWERFUL TELECHRON MOTOR
110V 60 Cy
6 RPM reversible $10.00
1 RPM $6.50

HAYDON TIMING MOTORS
110v 60 cycle 30 RPM.. $2.60
110v 60 cycle 1 RPM... 2.60
230v 60 cycl 1 RPM..... 1.00
HANSEN Synchron 4 rpm $4.24
CRAMER 4 rpm $4.65

DIEHL-DELCO
P. M. motors. Made for 24 volts. Will work at lower speed at 12v. or 6v. Battery or Rectifier. Size 1"x1"x2" $3.75

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received by March 4th will appear in the April 1st issue subject to space limitations.
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Cadmium or olive drab finish.

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RMA GUARANTEE—From 10% to 95% Below Manufacturers Price—Look and Compare

Special Prices to Quantity Buyers. Most of Our Tubes are Jan.—95% are Original boxed — Brands such as R.C.A., G.E., Ken-Rad., Sylvania, Tung-Sol and Raytheon.

Type	Price
AB/150	$1.99
C3J	6.35
C5B	.49
C6J	7.99
CK-551AX/2E41	1.79
CRP RK-72	.49
EC1	1.99
EF-50	.80
E1148	.29
EM-3GA	39.50
F123A	5.99
FG17	4.50
FG-105	14.99
FG-154	14.99
FG172	24.95
HF-100	7.49
HK-24	3.69
HK-54	3.99
HY-65	1.20
HY-114B	.69
KU-610	3.49

Type	Price
VR-150	.79
OA2	.74
OB2	.89
1B22	1.69
1B24	5.99
1B29	9.95
1P30	1.99
2A4/G	1.10
2AP1	3.99
2AP1A	6.44
3B22	1.89
2BP11	7.99
2C21	.49
2C22	.39
2C26	.39
2C26A	.49
2C33	.89
2C39	4.99
2C39A	11.50
2C40	10.99
2C42	9.75
2C43	10.99
2C44	1.35
2C46	7.49

Type	Price
2K22	14.50
2K23	16.50
2K25	18.99
2K28	29.50
2K33A	59.95
2K41	72.50
2K45	32.50
2K54	8.95
2K55	9.50
2V3/G	1.39
2X2	.34
2X2A	.89
3A5	.69
3AP1	5.95
3AP11A	4.95
3B22	1.49
3B23	3.25
2B24	2.99
3B24W	4.99
3B25	3.99
3B27	3.49
3B28	4.69
3BP1	2.99
3BP1A	6.35

Type	Price
5BP1	2.49
5BP1A	8.99
5BP4	2.99
5C22	25.00
5CP1	3.99
5CP1A	12.49
5CP7	9.99
5CP11A	14.99
5D21	6.99
5FP7	3.99
5HP4	2.49
5JP1	16.99
5JP4	14.99
5J32	65.00
5J33	7.99
5LP1	13.99
5NP1	6.99
5R4WGY	3.19
6C21	19.95
6AC7	.64

Type	Price
12AU7	.76
12GP7	12.95
15E	1.25
15R	.39
26AT/GT	2.99
26C6	1.19
28D7	.89
7BP7	6.25
9LP7	5.00
10Y	.39
12X3	1.59
24R	1.89
35T	4.99
35TG	7.25
53A	2.29
QK-62	24.50
RK65/5D23	14.95

Type	Price
271A	12.99
274A	5.95
274B	1.79
276A	7.25
282A	6.49
282	7.25
286A	7.50
304TH	7.95
304TL	13.95
307A	1.85
310A	3.99
316A	.69
329A	4.69
347A	3.88
350B	2.99
354C	14.95
388A	1.49
394A	2.99

Type	Price
706A	6.75
706B	14.50
706C	17.50
706DY	35.00
707A	3.55
707B	3.95
708A	2.99
709A	1.69
713A	.96
714AY	24.95
715A	2.65
715B	6.45
715C	14.50
717A	.49
718AY/CY/EY/DY	29.75
719A	14.65
720CY/DY/EY	29.75
721A	1.49
721B	3.99
722	1.99
723A/B	8.99
724A	1.15
724B	1.45

Type	Price
815	1.99
816	1.05
826	.75
829B	9.95
830B	2.99
832A	7.49
833A	31.50
836	1.99
837	1.99
838	3.50
841	.59
843	.49
845	6.49
851	16.50
860	3.49
861	19.00
864	.69
865	.49
866A	1.19
866JR/2B26	1.40
869B	30.00
GL-872A	2.49
872A	1.29

Type	Price
1616	.59
1619	.92
1625	.29
1626	.29
1629	.29
1630	.79
1632	.59
1641	1.88
1642	.39
1644	.48
1806P1	4.99
2050	.95
2050W	2.40
5651	.76
5651	1.39
5654	1.40
5656	3.25
5670	2.20
5686	1.79
5687	2.69
5702	1.49
5702WA	3.10
5703	1.19
5725	1.99
5726	1.00
5744	∞

CRYSTAL DIODES					
	1N21	.19	1N23B	1.10
	1N21A	.55	1N26	3.55
	1N21B	.99	1N27	.69
	1N22	.49	1N34	.41
	1N23A	.49	1N34A	.64

Manufacturers, exporters, and large quantity users—Inquire on your letterhead for our inventory listing of receiving tubes, special purpose tubes, resistors, condensers, and other radio and television parts.

Type	Price
HY-65	1.70
REL-21	1.00
RK-34	.39
RK-59	1.88
RK-60	1.99
RK-61	3.50
RK-65/5D23	14.99
RK-73	.69
RX-233A	.69
VT25/10	.49
VT25A/10Y	.39
VT67/30 Spec	.26
VT-158	17.50
VU-111	.19
XB32/532A	.99
QK-59	29.50
QK-61	32.00
QK-185	99.00
VR-78	.89
VR-90	.89
VR-105	.79

Type	Price
2C51	2.75
2C53	9.90
2E24	2.49
2E27	.95
2D21	.79
2D21W	1.39
2G22	2.29
2J21	2.99
2J21A	4.95
2J22	4.99
2J26	2.50
2J27	5.99
2J30	14.50
2J31	14.50
2J32	13.50
2J33	13.50
2J34	13.50
2J38	14.00
2J39	11.00
2J49	39.50
2J61	16.40
2J62	9.60

Type	Price
3C21	1.29
3C22	64.95
3C23	5.99
3C24	1.50
3C28	5.95
3C33	8.99
3C45	6.25
3CP1	2.25
3D23	4.99
3DP1	1.88
3E29	10.25
3EP1	1.88
3FP7	2.95
3GP1	3.95
3HP7	2.95
3J21	49.94
4A-11	.49
4B36	4.69
4C27	8.95
4C28	35.50
4E27	9.95
5AP1	3.95

Type	Price
6AC7W	1.50
6AG7	.79
6AJ5	1.19
6AK5	.64
6AK5W	1.35
6AN5	2.12
6AR6	1.49
6AS6	1.19
6AS7/G	2.49
6BM6	39.50
6C4	.49
6D4	2.99
6F4	2.99
6J4	2.50
6J4W	3.75
6J6W	1.29
6K4	3.99
6K4W	2.49
7BP1	9.95
12A6	.39
12AT7	.85
12DP7A	18.95

Type	Price
89Y	.15
100TH	6.95
203A	5.99
205B	1.99
205D	3.99
207	49.50
211	.72
215A	3.25
217A	2.99
217C	4.99
221A	3.99
233A	1.19
242C	8.00
249B	2.99
249C	3.99
250TH	24.95
250TL	13.95
250R	4.99
253A	3.39
259A	5.99
264C	3.90
269A	13.50

Type	Price
WL-417A	2.74
GL-434A	6.66
446A	1.49
446B	1.79
WL-460	8.99
WL-464A	4.25
471A	1.25
CK-508AX	1.10
CK-521AX	1.10
527	14.50
WL-530	19.50
WL-531	6.25
532A	.99
700A/B/C/D/E	10.99
701A	4.99
702A	2.25
703A	1.90
704A	1.59
705A	1.25

Type	Price
725A	3.99
726A	9.50
726B	25.00
726C	24.50
728AY/BY/CY/DY/FY/GY	35.00
730A	7.95
800	1.29
801A	.42
802	2.89
803	2.69
804	9.99
805	4.90
807	1.25
807W	3.25
808	1.79
809	3.15
810	12.95
811	3.19
813	11.49
814	2.49

Type	Price
874	1.25
876	.99
878	.90
884	1.00
885	1.10
9-1	.69
902P1	2.99
918	1.99
927	1.45
931A	2.99
954	.19
955	.29
956	.25
957	.35
958A	.39
959	1.40
991	.39
CK1005	.46
CK1006	1.97
1500T	94.50
1608	2.99
1613	.95
1614	1.49

Type	Price
5751	2.15
5760	2.95
5763	1.29
5814	1.35
5851	3.20
5879	3.15
5933	2.99
5963	1.19
5964	.74
5977	3.89
6080	2.99
6080W	3.90
8002R	18.50
8005	4.50
8012	1.85
8013	2.50
8013A	3.49
8020	2.99
8025	1.99
9001	.79
9002	.69
9004	.19
9006	.19

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All boxed and fully guaranteed. Special quantity discount—10% on 100 or more of same type. Minimum order $10.00. Thousands of other types in stock . . . Send us your requirements. F.O.B. New York 25% deposit with order or if paid in advance save C.O.D. charges. Rated firms net 10 days. Prices subject to change without notice. For fast service ask for Sy.

COAX CONNECTORS

SO239	M359A
24¢	15¢
831R	831AD

FOR SALE

Ecco Induction Heater

Mfd. by Ecco High Frequency Corp. Type TO-5-1, 220V, 60 Cy., 1 Ph., 2B Amp. AC Supply, 6 KVA output, portable on wheels. Electronic tube type; utilizes 851 tubes; complete with instrumentation. Installation & operating instruction book available. Like new. $495.00 f.o.b. Boston

ELECTRO SALES CO., INC.

50-58 Eastern Avenue, Boston 9, Mass.

INFRARED SNOOPERSCOPE TUBE

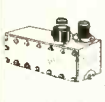
TYPE 6032—Infrared Image Converter Tube. Electrostatic focusing. Size 2x4½". List $150.00. Requires 20,000 volt, 0.05 milliamp supply. This tube is in current use in all U. S. military infrared equipment & is 2 to 3 times superior to the old 1P25 in definition and performance. Diagram for simple power-supply included. A $120.00 saving—NEW SURPLUS. Guaranteed. ONLY $29.95 postpaid.

INFRARED LIGHT SOURCE

Snooperscope Part #1364A.—Input 6 volts, 5 amps. Has special 5⅝" dia. #A-1529 glass filter & goldplated reflector. Projects a powerful beam of invisible infrared radiation (free of all visible light) that illuminates objects for infrared viewing up to 400 feet. For any infrared system. Complete with bulb.

STK #L-5459.—NEW, ONLY.....$7.95 Ppd.

IMAGE TUBE POWER SUPPLY



Part #1450A.—Power-pack for 1P25 Tube (will also supply CV-147 Tube) input 6 V.D.C., output 4,250 V.D.C. and additional focusing voltages. Checked-out, complete & operating with 1654 tube. Gov't cost $68.00. Used. NEW CONDITION $7.95 Ppd.

McNEAL ELECTRIC & EQUIPMENT CO.

4736 Olive St. Dept. E3, St. Louis 8, Mo.

Terms: Prices Include Postage, Cash With Orders. Well Rated Concerns (D & B) Net 10 Days Cash.

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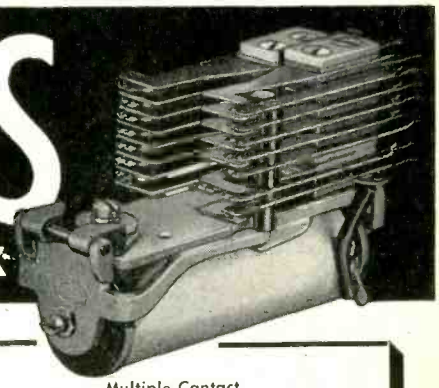
world's largest stock



★ Immediate Delivery
★ Hundreds of Types
★ All Standard Makes
★ New-Inspected-Guaranteed

See our ad on page 85

Multiple Contact

Standard Telephone Type Relay

CODE 4 TWIN CONTACTS

11-Form A 1-Form B 1-Form C 1-Form D

Heavy duty armature bearing. Available in all standard coil resistances from 12 ohms to 12,000 ohms. Single or quantity prices on request. In stock.

24 HOUR DELIVERY OF THESE TYPES

- Standard Telephone Relays
- Short Telephone Relays
- Midget Relays
- Timers
- Aircraft Contactors
- Rotary Relays
- Western Electric Type "E" Relays
- Keyed Relays
- Hermetically Sealed Relays
- Voltage Regulators and Cutouts
- Differential and Polarized Relays
- Special Relays
- BK Series
- Antenna and Ceramic Relays
- Motor and Control Relays
- Relay Assemblies
- Latching and Interlocking Relays
- Mechanical Action Relays
- Ratchet and Stepping Relays
- Time Delay Relays

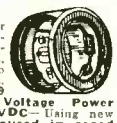
Write for New Relay Sales Catalog, C-7

Relay Sales

P. O. Box 186-AA, West Chicago, Ill. Phone West Chicago 1100

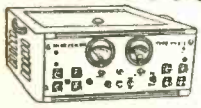
"TAB" THAT'S A BUY

INFRARED SNOOPERSCOPE
SEE IN DARK TUBE



Selected, GTD & Tested for resolution. 1st class image converter viewing tube. Hi-Sensitivity simplified design 2" dia. Willemite screen. Resolution up to 350 lin in. Tube & Data **"TAB" SPECIAL $4.75; 2/$9**

New Snooperscope HI Voltage Power Supply Model PS2002, 4500VDC— Using new improved triplet circuits. **Housed in caged Chassis. Ready to work. "TAB" @ $31.95**



TEST EQUIPMENT

G.E. YYZ-1 Decade Scaling Unit for high speed

COUNTING OR NUCLIONICS, contains two Decade scaling dkts count rate 5x106/R.T./0.1 Mu Sec, 115V/60cy operation..... **$150**

G.E. MICROWAVE Sic Generator 9 to 11cm/3333 to 2724 mes op/115v/60cy, CW or Pulsed, direct reading..... **$200**

WESTON Model 45 Range 0-150VDC/Lab. Std. **$45**
LAVOIE 105 FREQ. MTR. 300-600 mes..... **$45**
WILCOX CW3 AIRWAYS, POLICE fixed Freqs. RCVR operates 1.9 to 16.5 mes NEW less coils. **$50**
F3 or CW3 Coils per Set (3)..... **$10**
Measurements Model 84 Standard Signal Generator Range 300 to 1000 mes 400, 1000 & 2500 cys CW Modulation & Pulse Regularly $1950; SPECIAL **$349**
TS34AP W.E. osc. & SYNCHRO-SCOPE. $125
TS47APR Freq-Meter & Oscillator 40 to 115 & 115 to 500 mes operates Bats or AC..... **$225**
SPERRY R.F. WATTMETER Low Level... **$75**
DuMont Scope OBL3-245/115 & 230v..... **$60**
DuMont Scope 224A Lab Hi Sensitivity..... **$75**
VIBROTEST #218 MEGGER 0-500 volts... **$50**
EICO #470/7" OSCILLOSCOPE..... **$110**
PRECISE #300/7" OSCILLOSCOPE..... **$100**
Sig. Gen. 1-126/15 to 26 & 180 to 235 mes. **$139**

G.E. Time Interval Meter measures elapsed time From 1/1000 to 5 secs/made in 8 ranges .001, .003, .01, .03, 0.1, 1 & 3 secds..... **$175**
G.R. Type 561D Vacuum Tube Bridge..... **$295**
Lavoie LA-61 (500 to 2000 mc's) Freq. Meter. Accy 0.001%. Sens. 500 mv. Std freq. 2.5 mc's, accy 0.0001%. Input Imp. 50 ohms, output V.50mv. Opr. 115-230 v., 50-1000 cy. New, late model..... **$500**
MIT Model III Calibrater Pulse Testing... **$49**

!SPECIALS! LATE ARRIVALS

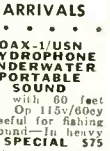
OAX-1/USN HYDROPHONE UNDERWATER PORTABLE SOUND

Testing Equipment complete with 60 feet underwater cable & hydrophone. Op 115v/60cy used for underwater sound. Useful for fishing & detection visual (meter) & sound—In heavy duty metal case **$1200 cost. SPECIAL $75**

RALS/USN RADIO RECEIVER 0.4 to 23 mes. NEW with Power Pack..... **SPECIAL $185**
RALS/Used less power supply..... **$100**
SLRF/USN 80 to 550ke & 1.9 to 24 mes Rec **$125**
MICROWAVE ANTENNA AT49A/APR4... **$10**
MICROWAVE ANTENNA AS-125/APR... **$10**
SCANNER APG13 & Motor & Parabolic used **$5**
Carter DC-AC Converter 115..... **$14**
AN-PRS15/USN Detector Geological Survey. **$50**
ANCRW3/UHF Radio Transmitter..... **$3**
Mitter/Citizens Band 100 to 250 mes..... **$5**
30mcs IF STRIP less tubes Higain..... **$5**
EE65 Telephone Test Set..... **$10**
RM29A & Case NEW Telephone Remote & ringer generator..... **$5 @ 2 for $9**

W.E. Model 2A Terminating Network..... **$25**
PQ1/USN Pulse Counting Recorder..... **$125**
0-2500VDC Insulation tester & factory megger variac controlled. Shock & foolproof includes Weston 2500V mtr & V'Regulator & cutout.. **$50**
G.E. Magnetic Counter 3HP/3 Pole/dilbreak **115VAC/60cy** in metal box..... **$10 @ , 2 for $18**
ADVANCE Relay 12VDC/4PDT 52 @ , **6 for $10**
MICO #501 S-6 to 20 Cm Wavemeter..... **$45**
MICO #433 L-20 to 75 Cm Wavemeter..... **$45**
AN/PDR/T1B GEIGER COUNTER..... **$65**
TS174U F.M. 20 to 250 mes AC operated..... **$265**
I-222 Signal Generator..... **$50**

230 TO 115 V AUTOFORMERS



For 220v/60cy Input. To 110-120V or Step up. † With Cord Plug & Receptacle.

TPA050/50W †	52.55
TPA075/75W †	3.95
TPA100/100W †	4.00
TPA200/200W †	5.75
TPA250/250W †	6.75
TPA500/500W †	8.25
TPA750/750W †	11.79
Model TPA 1000 Watts: 1 kw †	16.95
TPA1500/1500W *. $22.50; TPA2000/2KW *.	$34

***Less Cord, Plug & Receptacle.**

Isolation & Control Transformers

Indoor Power	Circuit Type
Primary 230/460 —	Secondary 115/230 1ø 60cys
TPP050/50W $10;	TPP075/75W $12
TPP100/100W $13;	TPP150/150W $14
TPP250/250W $17;	TPP500/500W $25
TPP750/750W $32;	TPP1000/1KW $39
TPP2000/2KW $59;	TPP3000/3KW $81

Also 1-Phase & 3-Phase Booster Transformers Discounts to Quantity Users

TRANSFORMERS
Mil-T-27 Specs
HERMETIC SEALED

Input 115v/60cy/1ø/2KVT eat Electrostatic shld to gnd.
Chittran FH610/6.3VCT/10A @ 55
Freed 24096/6.3v/12A..... @ $2.50
BD24/6.3VCT/9A & 6.3v/1.2A & 6.3V/1.2A @ $5
#579/6.3V/4.2A & 5v/3A..... @ $4
T53294/2.5v/6A & 2.5v/6A/3 Kv..... @ $4
T52897/5v/3A & 5v/3A & 5v/2A & 5v/2A.. @ $6
TRIAD HB231/5VCT/3A & 6.3VCT/5A.... @ $6
Choke C50159/1000 hys/5ma/12 Kv..... @ $5
Input 115v/400cys/1ø G.E. Mfr.
#80G669/5x6.3v/0.8A & 2x12.6v/0.3A & 12.6VCT/3.3A $3@, 4/$10, 12/$25
#80G763/2x600v/.005A $3@, 4/$10, 12/$25
#80G683G1/2x300v@.0005A, 6.3v/0.9A, 6.3v/1.2A 12v/.001A $2@, 5/$10, 12/$20

New Fly Way Binding Posts

Similar to Superior DF30*, takes plugs, tips, lugs, wire, 1/16" to ¼" panel, Red & Black.
BP30*, 30 Amp, 29c @ 12/$3, 50/$11, 100/$19
BP10*, 10 Amp, 18c @, 12/$2, 50/$6, 100/$11
BP60*, 60 Amp, 75c @..... 50/$30
BP100, 100 Amp, $1 @..... 24/$18
Mfrs. write quantity prices

FINEST HI-FI RECORDING TAPE

1200 Ft.—7" Reel **$1.45** *Lots of 12*
Money Back Gtd.

Ins. Spade Lug/Banana Recep/R&B 5/$1, 50/$7, 100/$12
Ins. Spade Lug/Solderless/R&B 6/$1, 50/$6, 100/$10
Ins. Tip Jacks (R&B) 8/$1, 45/$5, 90/$9
Ins. Solderless Phonetip Plugs B&R 7/$1, 50/$6, 100/$10
Alligator Clip Screw Type 18/$1, 60/$3, 100/$4
Alligator Clip Insulated B&R 11/$1, 50/$4, 100/$7
Ins. Banana Plugs Solderless (all colors) 6/$1, 50/$6, 100/$10
7" REEL, 1200 FOOT Highest Quality Precision Coated & slit, **FERRO-SHEEN** processed, constant output. Noise Free. Splice Free. **Free. 7½ IPS 40-15 KC Oxide Wnd In. "TAB" SPECIAL @ $1.59 EA; 3 @ $1.50 EA**
New 1st Quality "MYLAR" 2400 ft.—7" Reel Ferro-Sheen processed Recording Tape @ $4.49
"TAB" Special @..... 3/$12; 12/$45

NEW G.E. PHONO CARTRIDGES
Original Boxed, Money Back Gtd.

RPX050A .001 & .003 (SS)..... $6.75
RPX052A Golden Treasure (DS) $19.25
RPX053A Golden Treasure (DD) $28.00

Replacement Needles "TETRAD" Diamond T

RPJ013A Dual (DS) .001 & .003 "TETRAD"...
RPJ01D or **RPJ03D** Single (D) "TETRAD" $8.98
RPJ01S or **RPJ03S** Single (S)..... $1.65
RPJ003 or **RPJ004** Single (D) "TETRAD"... $8.98
MG or **78** Single (D) "TETRAD"†..... $8.98

NEW IMPROVED "TAB" HI-FI
With Inbuilt Network Ticonal Alnico 5 Plus Magnet, 4 to 8 Ohms V.C.

15" TRIAX, 25 Watt/20-20,000 Cycles. MODEL F15H3X..... $37.50
12" TRIAX, 20 Watt/40-20,000 Cycles. MODEL F12H3X..... $28.50
12" COAX, 20 Watt/35-18,000 Cycles. MODEL F12H2X..... $22

HI-MEG HI-VOLT NEW RESISTORS

.2 Meg/10w/10KV	.90 @ ; 12/ $9
.75 Meg/10w/15KV MVP	.90 @ ; 12/ $9
.8 Meg/10w/10KV	.90 @ ; 12/ $9
2 Meg/4w/5KV "MVG"	$1 @ ; 12/$10
2.5 Meg 5w/7.5KV MVT	$1 @ ; 12/$10
2.5 Meg/20w/25 KV MVA	$1.50 @ ; 12/$16
5 Meg/10w/15KV "MVP"	$1.50 @ ; 12/$16
6 Meg/10w/15KV "MVP"	$1.50 @ ; 12/$16
7 Meg/10w/15KV "MVP"	$1.50 @ ; 12/$16
10 Meg/4w/5KV "MVG"	$1.50 @ ; 12/$16
10 Meg/10w/15KV "MVP"	$2 @ ; 12/$20
12 Meg/10w/10KV	$1.50 @ ; 12/$16
20 Meg/30w/50KV "MVO"	$2 @ ; 12/$20
50 Meg/25w/40KV "MVE"	$2.50 @ ; 12/$25
100 Meg/10w/15KV MVP	$3.50 @ ; 12/$36

Deduct 20% Disc Qtys—100 May Be Asst'd

NEW MICA CONDENSERS GTD.

MFD	WVDC	Price
.03	600	45c; 100/$35
.01	1200	35c; 100/$25
.001	1200	20c; 100/$15
.002	1200	35c; 100/$30
.015	2500	75c; 100/$50
.002	2500	45c; 100/$35

Deduct 20% Disc. Qtys 100—May be asst'd.

"TABTRAN" Rectifier Xfmrs

Sec'd Volts (DUAL † 0-9-15-18 & 0-9-15-18 Series Sec'ds 0-3-6-9-12-15-18-21-24-27-30-33-36 Volts

TR5007 1 Amp†	$5.70
TR5001 2 Amp†	7.20
TR5001 5 Amp†	9.45
TR5002 12 Amp†	18.60
TR5003 24 Amp†*	39.00
TR5004 50 Amp†*	66.00
TR5005 100 Amp†*	117.00

18 Volt 2 Amp..... $1.98; 2 for $3.50
Wndgs in Series at Ratings shown; Parallel 2X Current; Voltage 0-9-15-18.
***Dual Pri 115 & 220V 60 cy**

"TABTRAN" Rectifier Chokes

CR6001/ 1 Amp/0.1 HY/1.4 Ohm	$3.60
CR6002/ 2 Amp/0.1 HY/.67 Ohm	6.45
CR6003/ 5 Amp/.07 HY/.6 Ohm	9.45
CR6004/ 12 Amp/.01 HY/.1 Ohm	18.00
CR6005/ 24 Amp/.001 HY/.025 Ohm	33.00
CR6006/ 50 Amp/.001 HY/.001 Ohm	60.00

FILTER CAPACITORS

CE156M 6000MFD 15V	...52@; 2/53; 10/$12
CE502M 2000MFD 50V	...54 ea. 10 for $30
BRACKET for CE156M or CE502M 25c@, 5/$1	
CE 2005M 500mfd@200V	56@, 4/$22, 10/$45
Brackets for.....	

PRECISION POTENTIOMETERS
HELIPOT, G.R., MULTIPOT, MICROPOT, FAIRCHILD, BOURNS, DEJUR.

MULTIPOT 25, 100, 300, 2000, 5000, 10000, 20000 Ohms/0.5%/ 10 Turns Equiv. **HELIPOT HELIPOT** Also 20K Each $5.98
Heli & Multipot 10, 70, 5K, 10K ohms/0.5% 3 turn..... Each $5.98
SERVOPOT "G"/100 ohms/0.5%..... @ $3.95
G.R., DeJur, Muter LAB potentiometers
GR#301/10,000 ohm/4W833..... .95@
GR#314/50,000 ohm/8Watt..... 2.45@
GR#214/20 ohm/10Watt..... 1.35@
Muter 0214/500 ohm/10Watt..... 1.50@
DeJur 20,000 ohm/12Watt..... 3.00@
TRIMPOT Miniature 2,000 ohms C W..1.50@
Fairchild #746/2.5Watt/ ±.5%, 5K, 9.5K, 10K, 20K, 40K..... DUAL $4@, TRIPLE 56@

PRECISION RESISTORS
1% ACCURACY GTD

Shallcross, Mepco & Others, W.E., Wilkor, IRC, Carbofilm & W.W. types. Many & sizes. No Mfrs Choice — We ship types in stock

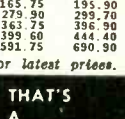
Ohms	Ohms	Ohms	Ohms	Ohms	Ohms
0.116	500	2463	13550	66K	450K
0.200	510	2485	13500	66600	458K
0.420	527	2500	14K	67500	470K
0.425	550	2700	14250	68K	475K
1.005	560	2750	14500	68500	500K
2.50	580	2860	14550	69K	510K
4.0	588	2900	14600	70K	520K
5.13	600	3000	15K	75K	521K
5.18	620	3100	16800	80K	525K
7.9	625	3163	17K	82K	550K
13.52	640	3259	17500	84K	560K
15	641	3270	17950	85K	573K
16.37	649	3290	17977	85750	600K
19.5	650	3300	18K	88K	620K
20.	655	3384	18380	90K	650K
25.	657	3500	18500	91K	654K
26.	673	3600	18800	93330	658K
31.5	675	3700	19K	97K	660K
50.	680	3760	19500	100K	680K
51.78	689	3900	20K	110K	690K
55	697	4000	20441	115K	750K
63	700	4200	21K	116667	761300
74	711	4280	21500	120K	800K
75	743	4300	22K	125K	820K
81.4	750	4314	22500	130K	850K
88	800	4444	22780	135K	878300
100	806	4500	22990	140K	900K
105	820	4700	23K	145K	910K
107	854	4850	24K	147K	950K
120	899	4900	24600	150K	970K
125	900	5000	25K	155K	1M
148	910	5100	25200	166750	1.1M
150	917	5210	25400	175K	1.2M
165	946	5235	25833	180K	1.25M
175	1000	5500	26K	180600	1.3M
179	1030	5600	26400	185K	1.35M
180	1036	5730	26500	190K	1.39M
182	1067	6000	27K	198K	1.4M
200	1100	6100	27500	200K	1.5M
220	1155	6140	28500	205K	1.579M
225	1162	6190	28700	210K	1.65M
230	1200	6495	29K	215K	1.8M
240	1225	6500	29500	220K	2M
245.4	1250	6800	30K	225K	2.2M
250	1260	6900	31K	229K	2.25M
260	1280	7000	32K	230K	2.3M
270	1300	7320	33K	235500	2.7M
271	1355	7500	33600	238K	2.75M
275	1400	7675	34200	240K	2.855M
280	1495	7700	34350	245K	3M
289	1500	7920	35K	250K	3.3M
299	1518	7930	36K	260K	3.5M
300	1550	7950	37K	270K	3.6M
310	1578	8000	38500	275K	3.673M
311.5	1600	8004	39K	294K	3.75M
320	1646	8200	39500	300K	3.9M
325	1670	8500	40K	307500	4M
330	1740	8700	43K	313K	4.23M
350	1770	9000	45K	314K	4.5M
360	1800	9100	47K	325K	4.7M
375	1818	9445	47500	330K	5M
380	1830	9500	48660	333K	5.5M
389	1900	9800	49K	333500	5.6M
390	1925	9900	50K	346K	6M
400	1960	9902	51K	350K	6.58M
414.3	1980	10K	51700	353500	6.8M
425	2000	10450	52300	360K	7M
426.9	2045	10936	53K	375K	7.5M
427	2080	11K	56K	380K	8M
430	2095	11400	56200	390K	8.2M
440	2142	11500	57065	399K	8.5M
450	2145	11690	58240	400K	9.05M
452	2150	12K	58333	402K	10M
470	2195	12578	60K	422K	11.55M
475	2200	12600	62K	425K	12.5M
478	2400	13K	64K	430K	15M
480	2450	13100	64900	433K	18M

K = *thousands* M = *megohms*

SPECIAL ALL VALUES each **18c**
TEN OF ONE VALUE each **15c**
100 OF ONE VALUE **$10**
Shallcross-MEPCO-IRC 1Meg/1Watt/W.W.
$1.25@,10/$10
GREAT SAVINGS TO QUANTITY USERS!
SPRS WRITE & LIST YOUR NEEDS.

NEW "DIODES"
Boxed & Lead Jacketed
SYLVANIA, M.A., CLEVITE, KEMTRON
1N21C each $5@, 2 for $8
1N23B each 89c@, Ten for $5
1N21@20c, 1N22@$1, 1N21B@$2
1N25@$4, 1N26@$5.5, 1N32@$12
MA408 Spcl $3@, Two for $5

NEW "TABTRON" SELENIUM RECTIFIERS*
ENGINEERED FOR AUTOMATION & INDUSTRY



"Technical Apparatus Builders" mfgrs. Power Rectifiers to your specs. From one amp up to and above 1000 amps.

*** FULL WAVE BRIDGE ● DATED & ONE YEAR GTD**

Max Amp	18VAC* 14VDC	36VAC* 28VDC	54VAC* 42VDC	72VAC* 56VDC	130VAC* 100VDC	266VAC 217VDC	3-phase 120VAC 150VDC	3-phase 208 VAC 256VDC	3-phase 240VAC 300VDC
1	51.95	53.00	53.40	55.30	58.40	527.90	$21.45	539.75	$45.90
2	2.40	3.75	5.70	6.45	10.50	33.60	24.95	47.90	58.80
3	3.45	4.80	6.30	9.60	14.70	42.90	27.60	63.30	73.95
4	3.90	7.50	11.70	16.15	27.75	49.80	31.15	69.75	84.15
6	4.50	8.85	12.90	19.30	32.85	63.90	48.45	81.90	99.90
10	6.60	12.60	21.90	27.90	42.50	89.70	63.60	117.75	139.50
12	8.10	15.90	24.00	32.75	45.90	111.45	69.75	137.90	159.60
20	13.20	25.50	39.90	52.50	87.75	177.90	124.15	165.75	195.90
24	16.15	32.40	48.45	63.60	96.15	210.60	149.70	279.90	299.70
30	19.80	37.80	61.95	78.75	120.75	256.35	189.60	363.75	396.90
36	24.90	48.45	72.45	95.70	147.60	326.70	225.75	399.60	444.40
50	33.45	63.75	121.50	135.75	192.75	445.90	297.90	591.75	690.90

WRITE FOR DC POWER CATALOG *Q—Write for latest prices.*

New Variable Voltage X-fmrs

SUPERIOR-GR-STACO

0-132v-1.25A	$7.23
0-135/3A	10.63
Cased 0-135V/7.5A	19.55
Uncased/0-135V/7.5A	15.30
Cased/0-270V/3A	22.10
Uncased/0-270V/3A	17.00
Cased/0-135V/15A	39.10
Cased/0-270/9A	39.10
Uncased 0-27V/7.5A	51.64
Cased 0-270V/9A	81.60
Cased 0-270V/12A	107.10
Cased 0-270V/15A	124.95
Cased 0-270V130A	154.70
100BU3-3ø@240/out 0-240/520W/1.2A	$36
300BU3-3ø@230/out 0-230/1.2KVA/3A	$50
500BU3-3ø@230/out 0-270/3.5KVA/7.5A	$57
1500B3-3ø@230/out 0-270/7KVA/15A	$132
3000B3-3ø@230/out 0-270/14KVA/30A	$164
3000B6-3ø@230/out 0-270/28KVA/60A	$354
also 3ø460/outputs 0-540 Inquire!	

ELECTRONIC FLASH! LUCKY PURCHASE $59 SHAWLITE 40011 SPECIAL $20

Assembled & ready to work! Not a Kit. Latest features SUPER CIRCUIT—Low cost flash less than ½c. inbuilt AC & Batteries* all in one case, powerful, compact. Guide No. Color 60 +. B&W 200 +. Recycles 2 secds. Limited Qty Special $20.
*Batteries not included. Two (2)/240V $10.
Photoflash Cond. 525MFD/450V/53W SEC. NEW LOW leakage. Famous mfgr. $6 @, 2/$11, 6/$30, 25/$100

NEW "TAB" BUILT POWER SUPPLIES

1100VDC @ 200ma. Brute Force filter, oil capacitors. Bleeder. Bridge 866A Rectifiers & FH 6.3V@ 4A±125VDC Bias $48. Kit with chassis $39. Built Same Only 550VDC @ 200ma $36. Kit $28 Built 2200VDC@200ma DC Supply $66.

KITS! KITS!

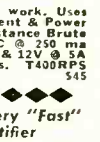
All Kits Contain Most Popular Values & Sizes

EXTRA: 11 Kits for $10

25 Precision Resistors	25 Power Resistors
10 Switches	65 Mica Cond's
25 Knobs	5 Ceroy Diodes
75 Carbon Resistors*	250 ft. Hookup Wire
36 Panel Lamps	100 Fuses
10 Electrolytic Cond's	35 Ceramic Cond
15 Volume Controls	10 Rotary Switches
25 Tube Sockets	6 Crystals
50 Tubular Cond's	60 Inductors & Coils
500 Lugs & Eyelets*	5 Microswitches
10 Bathtub Oil Cond's	10 Wheat Lamps
5 lbs. Surprise Kit	40 Insulators
10 Xmit Mica Cond's	*In Plastic Box

1 EACH KIT ONLY..... 99c

AMOUNT GYRO ORDINANCE

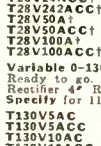


AMOUNT GYRO ORDINANCE
W.E./GA51045/8008976 Now Late Design. Cased hermetic sealed, easily opened. Contains: Gyro Motor Assemblies & sensing pot. Erection motor. Relay. Limit switches. Senses the attitude of the device about its pitch and roll axis. Wgt 6 lbs. hgt 3" dia. 4". Cost $1200. SPECIAL $20 @ 3/$50, 6/$90.

"TAB" REGULATED POWER SUPPLY

LAB & HIFI, Built & ready to work. Uses "SOLA" constant voltage Filament & Power Xfmr w/rectifier tube. Low Resistance Brute Force Filter. Furnishes 400VDC @ 250 ma from filter system 3% regulated & 12V @ 5A filtered DC for filaments. 45 lbs. T400RPS $45

Heavy Duty Battery "Fast" Charger Rectifier



13-0-13V (CT) 100 Amp Fan Cooled or 34 Amp Air Cooled. Rep'mt 6V Booster Charger.
Model CR5..... **$13**
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Stock NUMBER	Continuous Rating	With Meters
T28V5A*	0-28WVDC at 5 Amp	$57
T28V5ACC	5 Amp (1% Ripple)	$95
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T28V12A	0-28 VDC at 12 Amp	$138
T28V12ACC	12 Amp (1% Ripple)	$175
T28V12A2CC	12 Amp 0.01% Ripple	$250
T28V24A†	0-28 VDC AT 24 Amp	$175
T28V24ACC†	24 Amp (1% Ripple)	$250
T28V242ACC†	24 Amp 0.01% Ripple	$345
T28V50A†	0-28VDC at 50 Amp	$325
T28V50ACC†	50 Amp (1% Ripple)	$450
T28V100A†	0-28VDC at 100 Amp	$550
T28V100ACC†	100 Amp (1% Ripple)	$750

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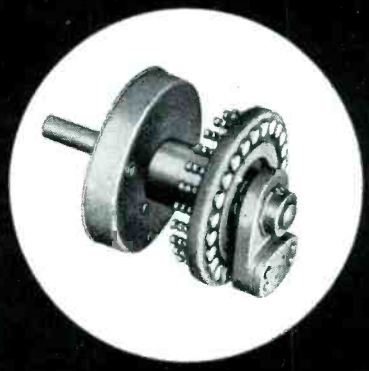

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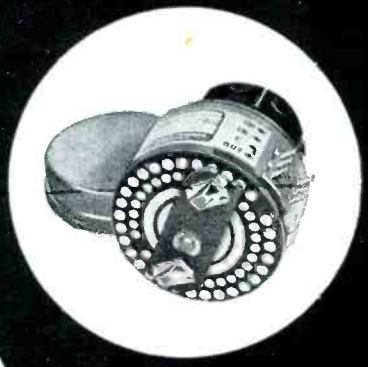

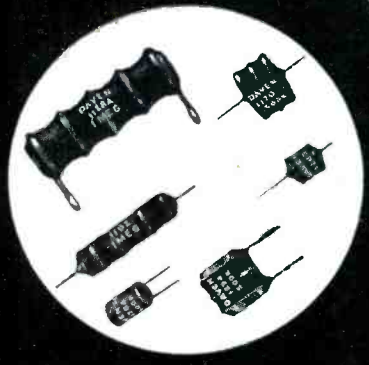

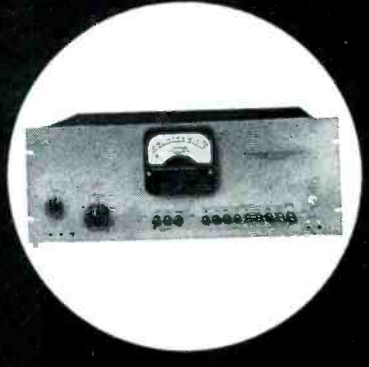

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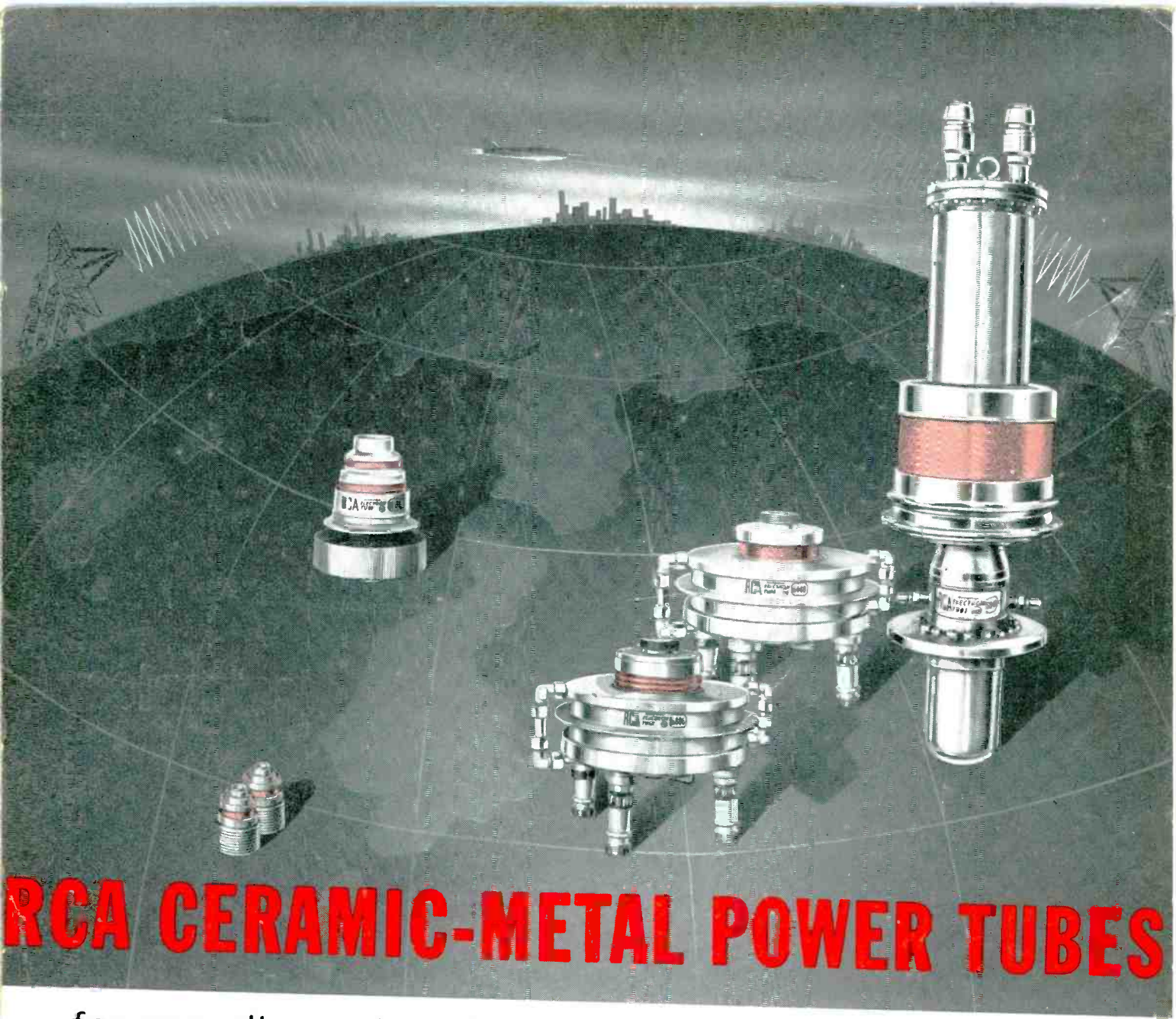

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